Updated Technical Report on the Meliadine Gold Project, Nunavut, Canada

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PREPARED FOR

Agnico Eagle Mines Limited

145 King Street East, Suite 400

Toronto, Ontario, Canada

M5C 2Y7

Telephone: / 416.947.1212

Facsimile: / 416.367.4681

BY

Julie Larouche, P.Geo.

Denis Caron, ing.

Larry Connell, P.Eng.

Dany Laflamme, ing.

François Robichaud, ing.

François Petrucci, ing. P.Eng.

Alexandre Proulx, ing.

February 11, 2015

Date and Signature Page

The effective date of this Technical Report is February 11, 2015. The undersigned are all qualified persons and were responsible for preparing or supervising the preparation of parts of this Technical Report, as described in Item 2.

By *(signed) Julie Larouche* Date March 12, 2015

Julie Larouche, P.Geo. (sealed)

By *(signed) Denis Caron* Date March 12, 2015

Denis Caron, ing. (sealed)

By *(signed) Larry Connell* Date March 12, 2015

Larry Connell, P.Eng. (sealed)

By *(signed) Dany Laflamme* Date March 12, 2015

Dany Laflamme, ing. (sealed)

By *(signed) François Robichaud* Date March 12, 2015

François Robichaud, ing. (sealed)

By *(signed) François Petrucci* Date March 12, 2015

François Petrucci, ing., P.Eng. (sealed)

By *(signed) Alexandre Proulx* Date March 12, 2015

Alexandre Proulx, ing. (sealed)

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Item 1. Summary

The Meliadine gold project located near Rankin Inlet, Nunavut Territory, Canada, is an advanced exploration and development project 100% controlled by Agnico Eagle Mines Limited ("Agnico Eagle" or the "company") as a result of its July 6, 2010, acquisition of Comaplex Minerals Corp. Agnico Eagle is a public company based in Toronto, Ontario, Canada, whose shares are listed on the Toronto Stock Exchange and the New York Stock Exchange, and is a "Producing Issuer" according to the rules and definitions provided by the Canadian Securities Administrators.

Agnico Eagle published a National Instrument 43-101 – *Standards of Disclosure for Mineral Projects* ("43-101") report on the Meliadine project dated February 16, 2011 (Agnico-Eagle, 2011), which outlined an initial probable reserve, but recommended further study to expand the mineral reserves, increase the understanding of the mineralization, and improve the economics.

Subsequent exploration, engineering and metallurgical test work have led to an updated technical study and economic analysis as of January 2015 (Petrucci *et al*., 2015), supporting a new statement of mineral reserves, disclosed in a news release dated February 11, 2015 (Agnico Eagle, 2015).

This technical report summarizes the scientific and technical information from the updated technical study used to support those mineral reserves. It has been prepared by Agnico Eagle's staff and Qualified Persons (as such term is defined in 43-101) based at the Meliadine Project as well as in the regional office at Preissac, Quebec, and the Toronto head office.

1.1 Property Description and Location

The Meliadine gold project is located in the Kivalliq District of Nunavut in northern Canada, approximately 25 km northwest of Rankin Inlet on the west coast of Hudson Bay. The larger property consists of 111,757 ha, which includes 25,507 ha as claims, 51,286 ha as leases, and 34,964 ha of subsurface Nunavut Tunngavik Incorporated ("NTI") concessions.

A private all-weather access road constructed by Agnico Eagle connects Rankin Inlet to the Meliadine project. The current Meliadine exploration camp is located on the shore of Meliadine Lake, approximately 2.3 km east of the Tiriganiaq deposit. The camp can accommodate 196 personnel.

1.2 Environmental and Social Impact and Agreements

The Meliadine gold project has undergone a comprehensive environmental and socio-economic impact assessment in accordance with the Nunavut Land Claims Agreement ("NLCA") under the direction of the Nunavut Impact Review Board ("NIRB"). This process took four years and involved regulatory agencies from the Government of Canada and Government of Nunavut, the Kivalliq Inuit Association ("KIA") and the general public. NIRB recommended to the Government of Canada that the project be allowed to proceed, concluding that the project should not cause any significant adverse environmental or socio-economic impacts, and would be

beneficial to the economic wellbeing of the region. The Government of Canada accepted this recommendation, with the NIRB issuing a Project Certificate to Agnico Eagle in February 2015. Consequently Agnico Eagle is confident that the Meliadine project can proceed, with the belief that all environmental and social issues can be addressed.

An Inuit Impact Benefit Agreement ("IIBA") is required for the Meliadine project under the NLCA because the property is on Inuit Owned Lands ("IOL"). The IIBA is currently under negotiation with the KIA, and will focus on jobs, training, local hiring programs, contracting, and community liaison. Negotiations are well advanced.

1.3 Geological setting and deposit type

The Meliadine gold project is located in the Archean Rankin Inlet Greenstone Belt, in the Churchill Structural Province of the northern Canadian Shield. This belt consists of mafic volcanic rocks, felsic pyroclastic rocks, sedimentary rocks and gabbro sills of about 2.7 billion years old that have been polydeformed and metamorphosed. The Meliadine trend is defined by northwest-trending rock units as well as a major fault zone known as the Pyke Fault: a high-strain zone characterized by multiple foliations and regionally important shear zones.

Seven gold deposits have been identified at the Meliadine project, of which Tiriganiaq is the most significant. The other deposits are the Discovery, F zone, Wesmeg, Normeg, Wolf and Pump. The Normeg deposit, discovered in 2012, is a southern expansion of the Tiriganiaq deposit, and extends as far as the Wesmeg deposit. Gold mineralization in these seven deposits is mostly mesothermal quartz-vein-dominated gold systems in strongly sheared and complexly folded host rocks of Archean turbidites, iron formation and volcanic rocks. Within each deposit are many gold-bearing lodes of quartz vein stockwork, laminated veins and sulphidized iron formation with strike lengths of up to 3 km. The stratigraphic units generally strike northwest-southeast, dip steeply to the north and are overturned, with the oldest units to the north. All seven deposits remain open at depth.

1.4 Exploration

Detailed surface mapping of the deposits is not possible due to the general sparse occurrence of rock outcrop in the property area and the almost complete lack of outcrop in the immediate vicinity of the deposits. The geology of the property and deposits has therefore been interpreted from a combination of drill information, airborne and ground magnetic surveys, outcrop mapping and channel sampling.

Since acquiring the property in July 2010, Agnico Eagle has completed approximately 389,000 metres of diamond drilling, mainly from 2011 through 2013. The main focus of the project in 2014 has been the extension of the underground exploration ramp.

In November and December 2013, Agnico Eagle rehabilitated the portal of the underground development that had been used to take bulk samples from the Tiriganiaq deposit in 2008 and 2011, in order to start an exploration ramp. This ramp, located in the Tiriganiaq footwall, will

provide geological information on the Normeg zone mineralization and will allow more efficient and cost-saving underground conversion and exploration drilling.

During 2014, the company developed 1,363 m of ramp.

1.5 Mining Methods

The current plan is to mine the Tiriganiaq deposit, including the Wesmeg 650, lode from two open pits and an underground mine. It is estimated that approximately 3.4 million tonnes of ore is extractable from surface mining and 9.1 million tonnes by underground mining over a nine-year mine life. An additional 1.4 million tonnes of lower grade material from underground development and open pit mining (marginal ore) will be stockpiled for processing at the end of the mine life.

The mining plan shows that production from the underground operation will deliver 3,000 tonnes per day ("tpd") of ore to the process plant over approximately nine years. Underground access will be by decline, with long-hole mining recommended. Every stope will be backfilled, with cemented pastefill used in primary stopes, and dry rockfill for the secondary stopes.

Starting at the end of Year 2, the open pits will be developed, adding 2,000 tpd of ore to the mill feed starting in Year 4. A conventional truck/shovel operation is recommended for both open pits.

1.6 Recovery Methods

To the end of 2014, more than 39 metallurgical test programs have been conducted on the Meliadine deposits. Based on the results of these programs, a conventional gold circuit is recommended comprising crushing, grinding, gravity separation and cyanide leaching with a carbon-in-leach circuit (CIL), followed by cyanide destruction and filtration of the tails for dry stacking.

Global gold recovery for all Meliadine deposits is estimated at 94.7% based on mineral resources plus mineral reserves (as of December 31, 2014). The economic analysis, in this report, was made on the proven and probable mineral reserves only. The mineral reserves are all contained in the Tiriganiaq and Wesmeg deposits, so their respective recovery models were used. The assumed gold recovery for the reserves therefore averages 96.0% at a 7.44-g/t gold average mill feed grade.

The process flowsheet is based on an ore processing rate of 1.1 million dry tonnes per year (3,000 dry tonnes per day) for the first three years, and 1.98 million dry tonnes per year (5,000 dry tonnes per day) for the remaining years at 92% process plant availability.

1.7 Mineral resource and reserve estimates

The database used for the current Meliadine resources estimate comprises historical drill-holes (1990 to 2010) in addition to the 2011 to 2014 data for all deposits through November 5, 2014.

Agnico Eagle conducted a resource estimate for all seven deposits using Datamine software (Version 3.22). All high-grade domains have been updated with the new drilling information. The estimation parameters such as the block size, the composite length, the extreme values treatment, the variography, the search ellipsoids, the estimation method and others were established by domains (low-grade or high-grade) and by deposits, and are appropriate for the mineralization style at Meliadine. Open pit mineral resources correspond to the blocks showing a gold grade above the cut-off grade and are included in pit shells designed using a Lerchs-Grossmann 3D algorithm. Underground mineral resources are all the blocks located outside the open pit shells and showing a gold grade above the underground cut-off value.

The categorized resource block models were used for the mineral reserves conversion process. The mineral reserves are the portion of the Tiriganiaq and Normeg/Wesmeg indicated resources that are economically recoverable by mining. Because of the very close proximity of the Tiriganiaq-Normeg-Wesmeg deposits and their equivalent genetic model, the resource block models for these three deposits have been merged together for the mineral reserve conversion.

The design parameters include mining dilution of 42% for open pit and 30% for underground mining. A 95% mining recovery factor has been applied to both the open pit and underground mineral reserves mined by open pit blasthole mining or underground blasthole stoping. A 100% mining recovery factor has been used for mineral reserves resulting from underground development.

The economic assumptions used to establish the reserve cut-off grades include a gold price of US$1,150/oz, and a C$/US$ exchange rate of 1.08. A gold refining cost of C$2.50/oz has been used. The operating costs of C$81.97/tonne for open pit mineral reserves and C$176.44/tonne for underground mineral reserves are derived from the current updated technical study. These parameters and assumptions were used to determine an economic diluted cut-off gold grade of 2.28 g/t (open pit) and 4.80 g/t (underground), and a marginal cut-off gold grade of 1.81 g/t (open pit) and 1.79 g/t (underground).

Based on the results of the current economic analysis, the Meliadine project has estimated proven and probable mineral reserves of 13.9 million tonnes grading 7.44 g/t gold, containing 3.3 million ounces of gold as of December 31, 2014 (Table 1.1). Agnico Eagle reports mineral resources exclusive of mineral reserves. The new mineral reserves and updated mineral resources at the Meliadine project include the Tiriganiaq, Wesmeg, Normeg, Discovery, F zone, Pump and Wolf deposits. Tonnes and grade are reported above cut-off grades and by expected mining method (open pit or underground), and transport distances to the proposed mill site as defined in the updated economic study.

Table 1.1 - Meliadine gold project mineral reserves (as at December 31, 2014)

Classification	Deposit	Category[(1)]	Tonnes (000)	Gold grade (g/t)	Contained gold (000 oz)
Proven Reserves	Tiriganiaq	Stockpile	34	7.31	8
	Subtotal		***34***	***7.31***	***8***
Probable Reserves	Tiriganiaq	Open pit	3,862	5.13	638

		Underground	9,787	8.39	2,640
	Wesmeg	Underground	261	5.84	49
	Subtotal		***13,910***	***7.44***	***3,327***
	Total		***13,944***	***7.44***	***3,335***

(1) Open pit mineral reserves are classified inside the operational pit design and open pit mineral resources are classified inside the ultimate pit shells

After the conversion of measured and indicated mineral resources to reserves, the remaining mineral resources as of December 31, 2014, consist of indicated mineral resources estimated at 20.2 million tonnes grading 5.06 g/t gold, containing 3.3 million ounces of gold, and inferred mineral resources estimated at 14.1 million tonnes grading 7.65 g/t gold, containing 3.5 million ounces of gold. The mineral resources exclusive of mineral reserves are shown in Table 1.2.

Table 1.2 - Meliadine gold project mineral resources exclusive of mineral reserves as of December 31, 2014

Classification	Deposit	Category[(1)]	Tonnes (000)	Gold grade (g/t)	Contained gold (000 Oz)
Indicated Resources	Tiriganiaq	Open pit	1,208	3.79	147
		Underground	6,756	5.66	1,230
	F zone	Open pit	1,254	4.46	180
		Underground	1,275	5.16	212
	Wesmeg	Open pit	2,241	4.12	297
		Underground	1,522	5.23	256
	Normeg	Open pit	1,250	3.99	160
		Underground	346	5.06	56
	Discovery	Open pit	945	5.00	152
		Underground	1,572	6.35	321
	Pump	Open pit	671	5.32	115
		Underground	707	4.54	103
	Wolf	Open pit	115	3.63	13
		Underground	383	4.12	51
	Total		***20,246***	***5.06***	***3,293***
Inferred Resources	Tiriganiaq	Open pit	-	-	-
		Underground	2,402	9.59	740
	F zone	Open pit	46	6.26	9
		Underground	1,427	6.82	313
	Wesmeg	Open pit	181	5.92	35
		Underground	2,175	7.59	531
	Normeg	Open pit	237	4.24	32
		Underground	2,351	8.51	643
	Discovery	Open pit	-	-	-
		Underground	529	7.55	128
	Pump	Open pit	304	6.78	66
		Underground	2,022	7.75	504
	Wolf	Open pit	262	4.43	37
		Underground	2,145	6.17	425
	Total		***14,083***	***7.65***	***3,464***

(1) Open pit mineral reserves are classified inside the operational pit design and open pit mineral resources are classified inside the ultimate pit shells

1.8 Infrastructure requirements

The project infrastructure is designed to accommodate the personnel, equipment and fuel demands for nine years of mine life. Power will be generated on site.

Because of its location, the Meliadine infrastructure will require special cold climate and permafrost design considerations. The arctic design of the buildings will be reflected notably in insulation and special foundation requirements, use of heated utilidors (insulated, enclosed utilities corridors) to connect the buildings, and space-heating requirements.

Infrastructure will also be required at Rankin Inlet to accommodate the annual sea lift of goods via Hudson Bay and to store fuel.

1.9 Conclusions

The Meliadine project hosts a proven and probable reserve comprising 3.3 million ounces of gold contained in 13.9 million tonnes grading 7.44 g/t gold. Current studies are based on exploiting the Tiriganiaq deposit as well as part of the Wesmeg deposit only. Low-grade marginal ore stockpiles will be processed at the end of the mine life.

Gold recovery is estimated at 96.0% based on proven and probable reserves.

The key results below are based on four years of construction followed by a nine-year mine life, assumptions including a gold price of US$1,300/oz, an exchange rate of C$1.15/US$1.00, and the capital and operating costs detailed in this report:

- Average annual production of 365,000 ounces of gold
- US$267 million (C$307 million) after-tax net present value at 5% discount rate
- 10.3% after-tax internal rate of return
- Average total cash cost of US$531 (C$610) per ounce of gold produced
- Initial capital cost of US$911 million (C$1,048 million)
- Life of Mine capital cost of US$1,309 (C$1,505 million) total (including initial and sustaining capital)
- Life of Mine operating cost of C$1,877 million

1.10 Recommendations

The main recommendation for this project is to convert as much of the inferred resources (14 million tonnes averaging 7.65 g/t gold as of December 31, 2014) as possible into mineable reserves. This will significantly improve the project's economic viability, especially if the additional mill feed requires minimal or no additional infrastructure other than what is described in this document. Specific additional recommendations include:

- Validate the groundwater inflow rate (dewatering volume) with a more detailed hydrogeological study.
- Acquire additional supporting data to improve confidence in the metallurgical recovery estimates for the Wesmeg, Normeg, Pump, F zone and Discovery deposits, and to better assess the robustness of the processing for these deposits.
- Improve the 3D geological modelling for all deposits to increase the reserve and resources accuracy and confidence.

Item 2. Introduction

The Meliadine property is 100% owned by Agnico Eagle Mines Limited (Agnico Eagle). Agnico Eagle is a public company based in Toronto, Ontario, Canada, whose shares are listed on the Toronto Stock Exchange and the New York Stock Exchange, and is a "producing issuer" according to the rules and definitions provided by the Canadian Securities Administrators.

2.1 Terms of reference and sources of information

Agnico Eagle published a 43-101 report on the Meliadine project dated February 16, 2011 (Agnico-Eagle, 2011), which outlined an initial probable mineral reserve on the property of 9.4 million tonnes of ore grading 8.54 g/t gold (containing 2.6 million ounces of gold), and concluding from an initial feasibility study that a 3,000 tpd mining and processing operation was feasible; the report recommended further study at a higher production rate.

Extensive exploration as well as an underground bulk sample and test work from 2010 to 2014 has led to a better defined geological model and metallurgical character of the deposits at Meliadine. Different mine plan scenarios were evaluated, in light of the decreasing gold price and changing Canadian/US currency exchange rate over this period. The studies have resulted in an updated technical study in February 2015 (Petrucci *et al.*, 2015). The study included an economic analysis of the mine plan with anticipated costs, showing a positive after-tax net present value and internal rate of return. A new estimate of mineral reserves and mineral resources as of December 31, 2014 was announced in a news release on February 11, 2015 (Agnico Eagle, 2015).

This report summarizes the technical information that supports the new mine plan and the new mineral reserves and mineral resources as of December 31, 2014. This report also presents, among other information, the operating and capital cost estimates and an economic analysis demonstrating the economic viability of the current mine plan. It includes an update of the permitting for the project, and the ongoing negotiation of an IIBA with the KIA, which would be required before a commercial production lease can be issued.

2.2 Qualified Persons

The compilation of this technical report represents a collaborative effort by Agnico Eagle staff and independent consultants under the supervision of Qualified Persons as defined by NI 43-101, in conformity with generally accepted CIM "Exploration Best Practices" and "Estimation of Mineral Resources and Mineral Reserves Best Practices" guidelines (CIM, 2003). The Qualified Persons are all Agnico Eagle employees at the Company's regional office in Preissac, Quebec, or the head office in Toronto, Ontario. Each Qualified Person retains the responsibility for their contribution as indicated in Table 2.1. Their qualifications and site visits are summarized in the paragraphs below.

Table 2.1 - Responsibilities of each qualified person.

Qualified Person	Period Worked at Meliadine Project	Responsible for items in the report
Julie Larouche	February 2012 (one week) March 2012 (two weeks), May 2012 (two weeks), November 2013 (3 days) and July 2014 (3 days)	Sections 1 to 4 (part), 6,7,8,9,10,11,12,14,15, 23, 24 to 27 (part)
François Robichaud	May 6th to 9th 2013 (site visit with BBA)	Sections 1 to 3 (part), 13, 17, 24 to 27 (part)
Denis Caron	One visit in Feb 2014 (3 days)	Sections 1 to 3 (part), 16, 24 to 27 (part)
Larry Connell	One site visit in summer 2014 (1 day); negotiations with Inuit Stakeholders and regulatory agencies (continuously throughout 2014 and into 2015)	Sections 1 to 4 (part), 5, 20, 24 to 27 (part)
Dany Laflamme	May 2013 (2 days)	Sections 1 to 3 (part), 18, 24 to 27 (part)
François Petrucci	Last visit Feb 9-11 2015 (3 days)	Sections 1 to 3 (part), 19 , 21, 22, 24 to 27 (part)
Alexandre Proulx	May – Dec 2014 (25 days) Jan – Feb 2015 (6 days)	Sections 1 to 3 (part), 24 to 27 (part)

Ms. Julie Larouche, P.Geo. (Ordre des géologues du Quebec #881, Northwest Territories and Nunavut Association of Professional Engineers and Geoscientists #L2837**)** is a Qualified Person and has been employed by Agnico Eagle since October 2006. She is currently Superintendent Geology at Technical Services. She has worked for nine years in the fields of exploration and resource geology. She supervised the preparation of all the geological sections of this report including Appendix 4.1, 10.1, 14.1 through 14.4. Since February 2012, she has visited and inspected the Meliadine camp site five times for an average of seven days per visit, offering technical assistance to the geology team, inspecting logging procedures, visiting underground development and supervising the mineral resources and mineral reserves estimation process.

Mr. François Robichaud, ing. (Ordre des Ingénieurs du Quebec #122668) is a Qualified Person and has been employed by Agnico Eagle since May 2002. He is currently Metallurgy Superintendent at Agnico Eagle Technical Services. He is a mining engineer with specialty in mineral processing with 16 years of experience in process plant operations and project development. He supervised the preparation of metallurgy-related infrastructure, capital, operating cost and gold recovery data for the economic analysis sections of this report including the appendices for items 13. Since February 2012, he has visited the Meliadine project site once with the engineering firm responsible for the feasibility study of the process plant and surface infrastructure.

Mr. Denis Caron, Ing. (Ordre des Ingenieurs du Quebec #39176) is a Qualified Person who has been employed by Agnico Eagle since November 2011. He is currently acting as Senior Advisor (Mining) in the Technical Services group. He is a professional mining engineer who graduated in 1983 from Laval University, Quebec City, QC with over 30 years of experience in open pit and underground mine operations. During his career Mr. Caron has occupied different technical and managerial positions at different phases (construction / development, operation, closure) at other mining projects. Mr. Caron supervised the preparation of all the aspects related to the open pit and underground mine design, mine planning, production schedule and operating and capital costs related to the mine development and operation. He visited the Meliadine site February 9-11, 2015 (3 days) to review surface and underground conditions existing and the underground mine development plan expected during the pre-production period.

Mr. Larry Connell, P.Eng. (British Colombia #23696, Ontario #9099508, NWT/NU #L1720), is a Qualified Person and has been employed by Agnico Eagle since October 2007. He is currently the Corporate Director of Regulatory Affairs. He is a mining engineer with 40 years of experience in the fields of mineral processing, environmental management, sustainable development and regulatory affairs, all in the mining industry. He supervised and co-authored sections of this report that deal with the property description, accessibility, environmental permitting and community social impacts. Mr. Connell last visited the Meliadine project site in August of 2014 as Corporate Director of Regulatory Affairs. As well, he has been involved in negotiations with the Inuit stakeholders and various regulatory agencies continuously throughout 2014 and into 2015. He visited the neighbouring community of Rankin Inlet in each of 2011, 2012, 2013 and 2014 in his roles of coordinating the the ongoing permitting process and ongoing negotiations with the KIA and NTI.

Mr. Dany Laflamme, Ing. (Ordre des Ingenieurs du Quebec #132266) is a Qualified Person who has been employed by Agnico Eagle since August 2008. He is currently acting as Mechanical Engineer in the Technical Services. He is a professional mechanical engineer who graduated in 2003 from Abitibi-Temiscamingue University, Rouyn-Noranda, Quebec, with over 10 years of experience in project infrastructure. During his career Mr. Laflamme has been involved with many infrastructure projects at different phases (scoping, pre-feasibility, feasibility study and construction stages). He wrote and supervised the preparation of the infrastructure requirements considered for Meliadine deposit. He visited the Meliadine site in May 2013 (2 days) to offer assistance regarding the infrastructure for the project. He has been working on the Meliadine project since 2011, working on and supervising the infrastructure engineering for the project at pre-feasibility, feasibility and updated technical study stage.

Mr. François Petrucci, Ing, P.Eng. (Ordre des Ingenieurs du Quebec # 45322 and Professionnal Engineers of Ontario # 900525676) is a Qualified Person who has been employed by Agnico Eagle since December 2005. He is currently acting as Meliadine Study Manager in the Technical Services group located at the Company's regional office in Preissac, Quebec, Canada. He is a professional mining engineer who graduated in 1987 from Ecole Polytechnique in Montreal, Quebec, with 28 years of experience in open pit and underground mine operations. During his career he has occupied different technical and managerial positions at Agnico Eagle and other major mining companies. Mr. Petrucci wrote and supervised the preparation the economic aspects of this technical report. He also co-authored part of items 1, 25, 26, 27 and reviewed item 18. He last visited the Meliadine site on February 9-11, 2015 (3 days) to review the surface and underground conditions and the underground mine development plan expected during the pre-production period. Mr. Petrucci has been involved in Meliadine project since 2011. He has participated in all previous Meliadine internal studies.

Mr. Alexandre Proulx, ing. (Quebec #117423) is a Qualified Person who has been employed by Agnico Eagle Mines Limited since October 2009. He is a mining engineer with 20 years of experience working in the mining industry and has been employed by Agnico Eagle since October 2009. He has been the Program Manager for the Meliadine Project since May 2014. He has visited the project nine times since May 2014 with an average duration of 3 to 5 days per visit. Field inspections were mainly conducted during these visits. He co-authored and supervised the preparation of items 1 to 3 (part) and 24 to 27 (part) in this report.

2.3 Units of measurement and Abbreviations

Unless otherwise stated, all units of measurement in this report are metric and all costs are expressed in Canadian dollars (C$). The payable metal, gold (Au), is priced in United States dollars (US$) per Troy ounce.

The standard unit of mass is the metric tonne (t). Other units used include kilometre (km), metre (m), millimetre (mm), micrometre (μm), cubic metre (m^3), square metre (m^2), hectare (ha), gram (g), kilogram (kg) and degrees centigrade (°C). Gold metal production is in Troy ounces (oz). Metal concentrations are in grams per tonne (g/t), parts per million (ppm) and percent (%). Other acronyms and abbreviations used in this report are noted in Table 2.2.

Table 2.2 - Acronyms and abbreviations

acid-base accounting	ABA	atomic absorption	AA
acid rock drainage	ARD	banded iron formation	BIF
abrasion index	Ai	Bond Ball mill Work index	BWi
Aboriginal Affairs and Northern Development Canada	AANDC	Bond Crusher Work index	CWi
Agnico Eagle Mines Limited	Agnico Eagle or the Company	Bond Rod mill Work index	RWi
All-weather Access Road	AWAR	calcium chloride	$CaCl_2$
arctic grade light fuel oil	LFO	Canadian dollar	C$
arsenopyrite	Aspy	Canadian Institute of Mining	CIM
carbon-in-leach	CIL	net smelter royalty	NSR
carbon-in-leach simulation	SIMCIL	Nunavut Impact Review Board	NIRB
carbon-in-pulp	CIP	Nunavut Land Claims Agreement	NLCA
closure and reclamation plan	CRP	Nunavut Tunngavik Inc.	NTI
coefficient of variation	CV	Nunavut Water Board	NWB
Community Lands and Resources Committee	CLARC	open pit	OP
continuous gravity amenability test	GAT	Orway Mineral Consulting	OMC
Contract Support Services	CSS	oxygen uptake rate	OUR
cubic feet per minute	CFM	percent solids by weight	%w/w
diamond drill-hole	ddh or drill-hole	potential of hydrogen	pH
Draft Environmental Impact Statement	DEIS	product 80% passing	P80
Dry tailings storage facility (generally called “dry stack”)	DTSF	pyrite	Py
Emergency Response Team	ERT	pyrrhotite	Po
Engineering, procurement and construction management	EPCM	quality assurance/quality control	QA/QC
Environmental Impact Study/Statement	EIS	Regional Study Area	RSA
Extended Gravity Recoverable Gold	E-GRG	Resource Development Inc	RDi
feed 80% passing	F80	Rock Quality Designation	RQD
Final Environmental Impact Statement	FEIS	SAG mill comminution	SMC
Geological Survey of Canada	GSC	search volume	SVol
Gravity recoverable gold	GRG	semi-autogenous grinding	SAG
Half Absolute Relative Difference	HARD	square kilometre	km^2
high-density polyethylene	HDPE	standard deviation	SD
High Pressure Grinding Rolls	HPGR	tonne per cubic metre	t/m^3
humidity cell test	HCT	total cyanide	CN_{TOT}
Hydrocarbon-contaminated soils	HCS	total suspended solids	TSS
Inco cyanide destruction technology with SO_2/air	SO_2/air	transfert size 80% passing	T80
Indian and Northern Affairs Canada	INAC	underground	UG
Intensive Leach Reactor	ILR	United States dollar	$
internal rate of return	IRR	waste rock storage facility	WRSF
Inuit Impact Benefit Agreement	IIBA	water treatment plant	WTP
Inuit Owned Land	IOL	weak acid dissociable cyanide	CN_{WAD}
Inverse distance squared	ID^2	WMC International Limited (Western Mining Corporation)	WMC
JK Drop-weight Test	DWT	weight	wt
Kivalliq Inuit Association	KIA		
Local Study Area	LSA		

Life of Mine (Plan)	LOM
lime	CaO
Meliadine	MEL
Metal Mine Effluent Regulation	MMER
metres above sea level	masl
Metso Vertimill grinding mill	VTM
miligram per litre	mg/L
millilitre	ml
Mine Closure and Reclamation Plan	CRP
National Instrument 43-101 – Standards of Disclosure for Mineral Projects	NI 43-101
net acid generation test	NAG
net present value	NPV

Item 3. Reliance on other Experts

This report was compiled through the efforts of Agnico Eagle staff under the supervision of Qualified Persons, as described in Item 2. There has been no reliance on experts who are not Qualified Persons or who have not been supervised by a Qualified Person in the preparation of this report.

Golder Associates Ltd. (Golder) provided support for the geomechanical data collection in 2013 and provided the mine design analyses and recommendations for the Tiriganiaq open pit slope design.

Knight Piésold Ltd. (KP) and Mine Design Engineering Inc. (MDEng) were retained by Agnico Eagle in 2014 to provide geomechanical support for the Tiriganiaq underground mine design. This work was intended to build upon the recommendations provided in AGNICO EAGLE's internal (Phase 1) Technical study Report. KP also provided support for the collection, treatment and analysis of geomechanical data during the second geological drilling and laboratory testing campaign during the summer 2014. The scope of work for KP/MDEng included rock mass domain definition and characterization. Mine design input was provided based on defined rock mass parameters and boundary conditions using a mine-wide 3D numerical stress model, detailed 3D and 2D stope scale numerical modeling, and empirical and limit-equilibrium analyses. Mine design recommendations were provided on the suitability of stope and pillar dimensions, aniticipated dilution, mining sequence, inter-lode pillar stability and ground support. Additional mine design input was provided on key infrastructure location and vertical development, crown pillar stability, backfill strength requirements and investigations required for portal design.

BBA was retained by Agnico Eagle to provide engineering support for the main infrastructure design in 2013 and 2014. This infrastructure includes the process plant and process equipment, crusher, paste plant, maintenance shop, camp complex, warehouse, power plant and site distribution network, fuel tank farm on-site and off-site, and foundations for buildings. BBA also participated in the cost estimate for this infrastructure and equipment.

EBA (Tetratech) was retained by Agnico Eagle to provide engineering support for the design in 2013 and 2014 of the tailing facility, the landfarm, the landfill and all water management infrastructure. EBA also completed the water balance assessment and the water quality model.

Stantec was retained by Agnico Eagle to provide engineering support for the design of underground infrastructure in 2013 and 2014. Stantec was involved in the underground ventilation design.

Item 4. Property Description and Location

4.1 Location

The Meliadine project is located in the Kivalliq District of Nunavut in northern Canada, near the western shore of Hudson Bay (Figure 4.1). Tiriganiaq, which is currently the most significant of the gold deposits on the property, is located at 63°01'30"N, 92°12'30"W (National Topographic Survey sheets 55/J, N and O).

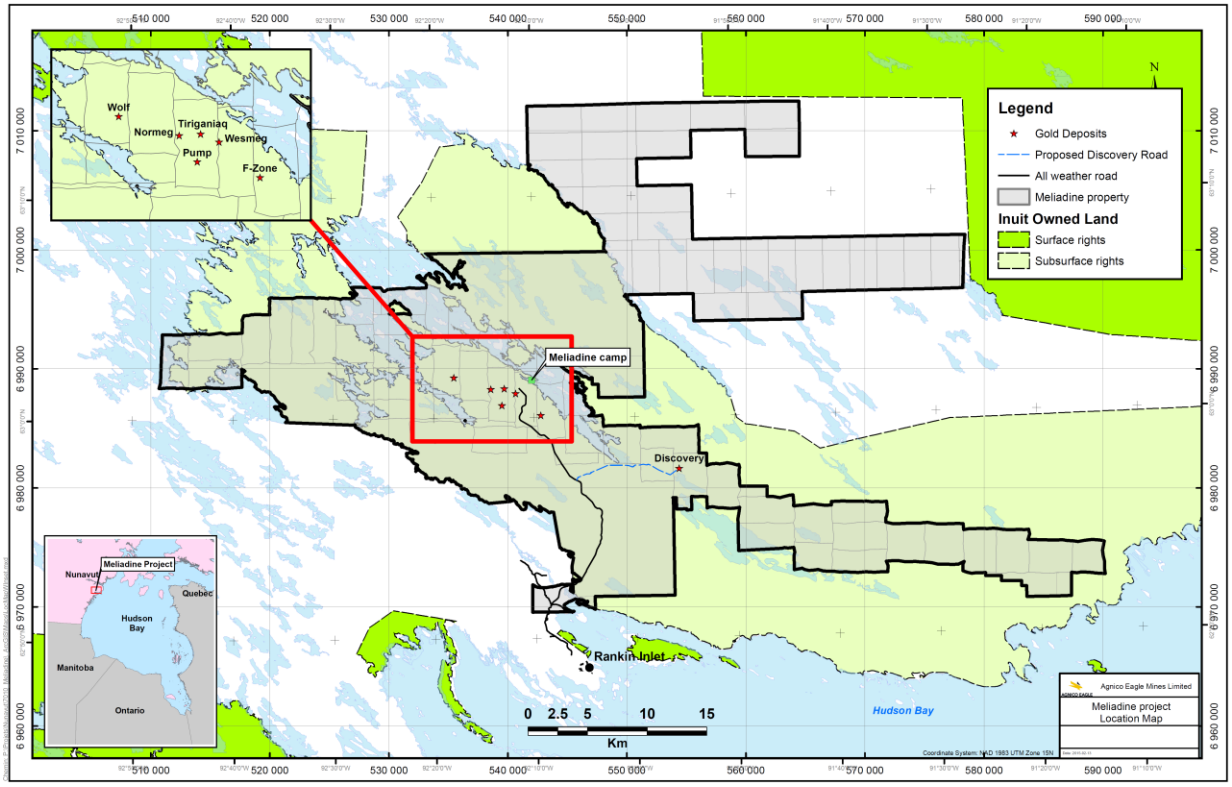


Figure 4.1 - Meliadine project location and mineral land position

4.2 Area of the Property and Land Tenure Status

The Meliadine property is 100% owned by Agnico Eagle following the acquisition of Comaplex Minerals Corporation ("Comaplex") on July 6, 2010. At that time, Agnico Eagle assumed responsibility for the Comaplex-held claims, ensuring that all annual land use fees, work commitments and reporting requirements to KIA, Aboriginal Affairs and Northern Development Canada ("AANDC") and NTI continue to be met. As of December 2014, all of these obligations have been met, to the best of the Company's knowledge, with nothing significant outstanding. Agnico Eagle has received no notifications from KIA, AANDC or NTI advising it of any outstanding fees or requirements.

4.2.1 Sub-surface rights

The Meliadine project consists of three different types of mineral rights, as shown in Figure 4.2. Details of the claims and leases are available in Appendix 4.1.

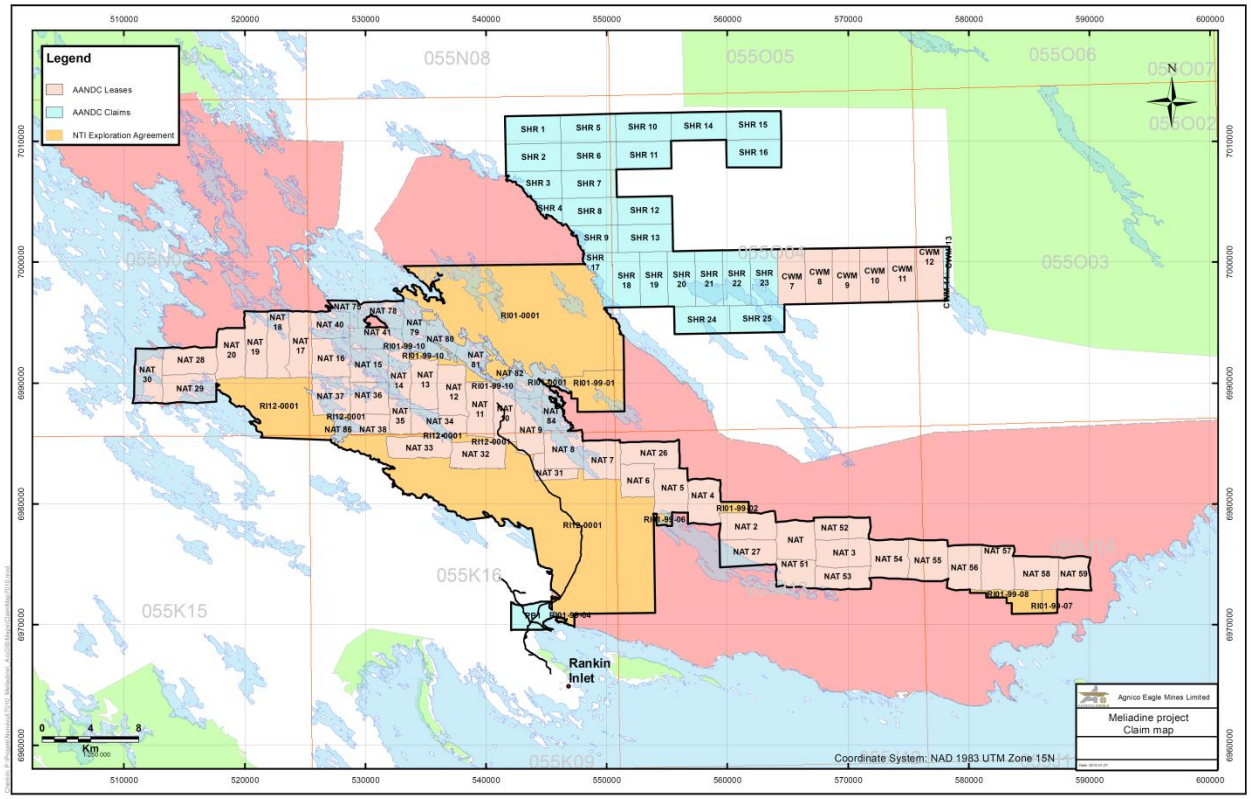


Figure 4.2 - Meliadine project claims, leases and concessions as of December 31, 2014

General details and background about the mineral tenure systems governing the property and area are available in Strathcona (2005).

The main gold deposits of the Meliadine project are situated on Inuit Owned Land ("IOL") where the surface rights are administered by the KIA on behalf of Inuit Beneficiaries of the Kivalliq District of Nunavut under the terms of the Nunavut Land Claims Agreement ("NLCA"), and the sub-surface mineral rights are administered by NTI. The mineral claims underlying the main deposits at the Meliadine project were staked and then recorded with the Government of Canada prior to the signing of the NLCA in 1999, and have been held continuously by the mining rights holder (initially Comaplex, and now Agnico Eagle). Consequently, they are considered to be grandfathered under the NLCA, meaning that the mineral production royalties payable to the land and mineral rights owner are administered by the Government of Canada under the Territorial Lands Act (specifically the Nunavut Mining Regulation under the Territorial Lands Act). Under this legislation any royalties collected by the Government of Canada for production from these claims would be transferred to NTI as the new sub-surface mineral rights owner.

The terms equate to a 12% royalty on gold ounces produced, with allowable deductions for capital and operating costs incurred to produce the gold.

The larger Meliadine property consists of 111,757 ha. This includes 25,507 ha as claims and 51,286 ha as leases. The 51,286 ha of leases are held under the Territorial Lands Act, a Federal Act administered by AANDC, and referred to as Crown Land. Appendix 4.1 shows the AANDC mineral claims and the Crown mining leases for the Meliadine project.

As well, Agnico Eagle holds 34,964 ha of sub-surface NTI concessions where the sub-surface mineral rights are administered directly by NTI. Appendix 4.1 gives details of the NTI concessions; the annual fees and work commitments required for these concessions are shown in Appendix 4.1 as well as Table 4.1 and Table 4.2.

Table 4.1 - Annual fees for NTI concessions

	NTI annual fee (C$/ha)	
	ANT 1, ANT 3, TAN 1, FAY 1B, FAY 2, FAY 3, FELSIC 1	RAPTOR
Year 1	1.00	1.00
Year 2 to 5	2.00	2.00
Year 6 to 10	2.50	3.00
Year 11 to 15	4.00	4.00
Year 16 to 20	4.00	5.00

Table 4.2 - Annual work commitments for NTI concessions

	NTI annual work commitment (C$/ha)	
	ANT 1, ANT 3, TAN 1, FAY 1B, FAY 2, FAY 3, FELSIC 1	RAPTOR
Year 1 to 2	4.00	5.00
Year 3 to 5	10.00	10.00
Year 6 to 10	18.00	20.00
Year 11 to 15	30.00	30.00
Year 16 to 20	40.00	40.00

4.2.2 Surface rights

For the main components of the Meliadine project that lie on IOL, the surface rights are administered by the KIA. Agnico Eagle has a series of land use leases from the KIA allowing it to explore and develop the minerals found under this property. The main land use leases are as follows:

- KVCL102J168 – Commercial Lease for exploration and underground development activity;
- KVL308C07 – Mel E Exploration Land Use Lease covering exploration and drilling on the Meliadine East IOL; and
- KVL302C268 – Allowing drilling activity on RI-01 and RI–12 IOL.

Agnico Eagle holds a number of right-of-way leases covering an all-weather access road linking the Meliadine camp with the hamlet of Rankin Inlet, and esker quarrying on IOL. The Company also holds leases from AANDC covering exploration, drilling and quarrying on adjacent federally owned land (crown lands).

4.3 Agreements and Encumbrances

Aside from the royalty arrangements with the Government of Canada (and, by default, with NTI) discussed in Item 4.2, there are no other royalty agreements or encumbrances against future production on the Meliadine property.

Agnico Eagle is required to negotiate and implement an IIBA with the KIA for the Meliadine project before the project can commence construction. Details of the agreement and the status of the ongoing negotiation are given in Item 20 of this report. Similarly, the Company is required to negotiate and implement a Water Rights Compensation Agreement in accordance with Article 20 of the NLCA and a Commercial Production Lease with the KIA. Both the Water Rights Compensation Agreement and the Commercial Production Lease are required before construction can start. Agnico Eagle initiated discussions with the KIA on both of these agreements in 2014, with the associated financial terms being negotiated as part of the ongoing IIBA negotiating process. These negotiations are well advanced; Agnico Eagle expects that the IIBA, Water Rights Compensation Agreement and Commercial Production Lease will all be successfully concluded in 2015.

The Company has numerous land use authorizations allowing it to conduct mineral exploration, to have overland access to the property and to quarry esker material (Table 4.3). The duration of these land use permits, leases, right-of-way permits and quarry permits is variable, but they are typically extendable on a yearly basis if compliance from the previous year is shown. Agnico Eagle, working with the KIA, has a multi-year history of successfully renewing these land access and land use authorizations for the following exploration season. Permit renewal, work plan submission, *etc*., is an ongoing process. The various licences, permits and authorizations that will be required to construct, operate and ultimately decommission the Meliadine mine project can be found in Item 20 of this report.

Table 4.3 - Current licences and permits for the Meliadine project

Licence Number	Details	Issued By	Expiry
KVL302C268	NTI Parcel Drilling including Tiriganiaq	KIA	01-Jul-16
KVCL102J168	Commercial Lease	KIA	30-Jun-15
KVRW98F149	Meliadine Right-of-way	KIA	30-Apr-15
KVCA07Q08	Tiriganiaq Quarry Permit	KIA	15-Sep-15
KVCA11Q01	Permanent Road Quarries	KIA	19-Apr-16
KVRW11F02	Permanent Road Right-of-way	KIA	19-Apr-15
KVL308C07	Mel E Exploration RI01	KIA	13-Jun-15
N2014C0007	PB1, Drilling Permit	AANDC	16-Sep-16
2BB-MEL0914	Bulk Sampling - Water Licence	NWB	21-Jul-24
2BE-MEP0813	Exploration - Water Licence	NWB	31-Oct-18
2BW-MEL1215	Road - Water Licence	NWB	31-May-15
N2013-C002	Exploration, drilling, claims CWM	AANDC	23-May-15
Nunavut GOV	Land Lease, laydown Itivia Street Rankin Inlet	NU GOV	1-Jul-21

4.4 Environmental liabilities

The Final Environmental Impact Statement ("FEIS") concluded that all significant residual environmental impacts associated with the construction, operation and decommissioning of the

Meliadine mine project could be mitigated. This FEIS was submitted to NIRB in May 2014. Following extensive technical review and public hearings, NIRB recommended that the Meliadine project be allowed to proceed.

In January 2015, the AANDC Minister accepted the NIRB Final Hearing Report for the project (including the recommended Project Certificate terms and conditions) and NIRB issued the Project Certificate in February 2015. This clears the way for Agnico Eagle to now obtain the required permits and authorizations to start construction and commence operation of the proposed mine.

4.5 Additional factors and risks

To the extent known there are no other significant factors and risks that may affect access, title, or the right or ability to perform work on the property.

Item 5. Accessibility, Climate, Local Resources, Infrastructure and Physiography

Information in this section has been updated from Agnico-Eagle Mines (2011, 2012b), Snowden (2010), Micon (2009) and Beca (2001).

5.1 Topography, elevation and vegetation

The physical features of the Meliadine region have largely been determined by glaciation. The terrain consists predominantly of broadly rolling uplands and lowlands with little topographical relief (very few hills). Rankin Inlet is located on the shore of Hudson Bay with a mean elevation of 28 m above sea level. Strung out across the landscape are long, sinuous eskers. This undulating landscape is studded with innumerable lakes, ponds, and wetlands. Cryosols are the dominant soils, and are underlain by continuous permafrost with active layers that are usually moist or wet throughout the summer.

5.2 Proximity to a population centre

The Meliadine gold project is located approximately 25 km north of the nearest community, the Hamlet of Rankin Inlet in Nunavut. Rankin Inlet is a predominantly Inuit community on the northwest coast of Hudson Bay between the communities of Chesterfield Inlet and Arviat. The closest major city is Winnipeg, Manitoba, about 1,500 km to the south.

The hamlet of Rankin Inlet was established as a mining community in the early to mid-1950s with the discovery and subsequent development of a nickel mine. It is now the regional centre and the largest community of the Kivalliq District. Rankin Inlet is the second-most populated community in Nunavut after the capital of Iqaluit, with a population of approximately 2,400 people, 80% Inuit and 20% non-Inuit. The community has developed strong entrepreneurship, and serves as a regional business centre.

5.3 Access to the property and transportation

The project is serviced via Rankin Inlet, which provides summer shipping access and year-round airport facilities. The project is designed as a "fly-in/fly-out" operation, with the Rankin Inlet airport being the main arrival destination. A 23.8-km-long private all-weather access road ("AWAR") constructed by Agnico Eagle connects Rankin Inlet to the Meliadine Project.

The current Meliadine exploration camp is located on the shore of Meliadine Lake, approximately 2.3 km east of the Tiriganiaq deposit. The camp can accommodate 196 personnel, following an expansion in 2012.

All construction and operating supplies for the project will be transported by ocean-going ship during the summer open water season to Rankin Inlet.

5.4 Climate and Length of Operating Season

The monthly mean air temperature is typically above 0°C for the months of June to September, and is below 0°C between October and May. July is typically the warmest month and January the coldest. Winters are typically long and cold, while summers are short and cool. Spring and autumn are short. The mean annual temperature for the period of record from 1981 to 2009 was -10.4°C.

Mean annual precipitation is estimated to be 411.7 mm. Half of the precipitation approximately occurs as rain, the other half as snow. The 24-hour extreme rainfall intensity with a 10-year return period is estimated to be 1.9 mm/h, for a total depth of 45.6 mm. Corresponding values for the 100-year return period are 2.6 mm/h or 62.4 mm total depth.

The region is known for high winds, which are due in part to the broad, flat, uninterrupted expanses offered to moving air masses. The wind blows from the north and north-northwest direction more than 30% of the time.

Late-winter ice thickness on freshwater lakes in the project area can range from 1 m to about 2.4 m. Ice covers usually develop by the end of October and are completely formed in early November. The spring ice melt typically begins in mid-June and is complete by early July.

Surface exploration work can be done from mid-May to mid-October, while drilling can take place throughout the year (but is avoided in January and February due to the cold and darkness). Open pit and underground mining operations are possible all year long.

5.5 Surface rights

The Meliadine project has sufficient surface lands available to allow for flexibility in the project design, should the need arise. The surface rights are currently held by Agnico Eagle under a surface lease obtained from KIA. The current lease is a Commercial Exploration Lease that will be converted into a Commercial Production Lease once the project has received the required authorizations, permits and leases from the various regulatory agencies. The granting of the Commercial Production Lease is predicated upon negotiating and implementing an IIBA.

5.6 Power Source

Power for the Meliadine gold mine will come from a new diesel-fuelled power generation plant to be constructed at Meliadine. Details of the power generation and fuel storage facilities are given in Item 18.

5.7 Fresh Water Source

Fresh water for the exploration camp is pumped from Meliadine Lake under the authority of Water Licence B obtained from the Nunavut Water Board ("NWB"). For the mine site, fresh water will be pumped from Meliadine Lake from a location to be determined under the terms of a Type A Water Licence to be obtained from the NWB. Process water will be reused as much as possible in order to minimize fresh water intake. Details of the water pumping infrastructure are given in Item 18.

5.8 Source of Mining Personnel

The main source of qualified mining personnel will be mostly from other parts of Canada, as has been Agnico Eagle's experience at Meadowbank mine. The project will draw its Inuit workforce from the whole Kivalliq region and the rest of Nunavut. The population of the Kivalliq region was 8,955 people in 2011 (Statistics Canada, 2012), of which 90% are Inuit. The population is quite young, with a median age of around 21 years. Table 5.1 below provides some indication labour force characteristics in Kivalliq between 2001 and 2006.

Table 5.1 - Kivalliq Employment, 2001 and 2006

	2001	2006
Labour Force	2775	3240
Participation Rate (%)	66.9	61.7
Unemployment Rate (%)	18.6	15.7

Source: *http://www.statcan.gc.ca/tables-tableaux/sum-som/l01/pro01/pro113-eng.htm*

5.9 Infrastructure Areas

Agnico Eagle believes that the Meliadine project has sufficient land under lease from the KIA to allow for flexibility in the surface infrastructure design including for potential tailings storage areas, potential waste disposal areas, and potential sites for required facilities such as a processing plant and a power plant.

An assessment of alternative tailings storage facilities (Golder Associates, 2009a) compared different location/type options for Meliadine tailings disposal. The dry stack option was chosen. Details of the tailings storage facilities are given in Item 18.

The proposed locations for storing rock material (waste rock, low-grade ore, and/or overburden) are given in Item 18.

A single process plant structure is proposed, which will reduce both capital and operating (heating) costs. A second building will host the paste plant. The main facilities are located about 2 km north of the Tiriganiaq open pit. This location is the most favourable site because of its relatively shallow overburden and positive geotechnical conditions. Details of the planned processing plant site can be found in Item 18 of this report.

Item 6. History

6.1 Previous work, ownership and resource estimations

Information in this section has been updated from Agnico-Eagle (2011) and Snowden (2010).

Lack of outcrop resulted in the use of ground and airborne magnetic surveying and prospecting glacial materials, followed by drilling, as the most common and successful exploration strategy on the property.

Exploration activities on the Meliadine project by previous owner-operators are summarized in Agnico-Eagle, 2011 (Item 8 – History). A number of resource estimates were prepared by Western Mines Corporation (WMC) on the various deposits. Many of these studies were for internal use only, were not reported according to NI 43-101 disclosure requirements, and were not released to the public. Details on the history and results of the various WMC resource estimates are outlined in Strathcona (2005) and are not repeated here. The location of claim groups on the property (referred to in this item) is shown in Figure 4.2.

Exploration drilling statistics for the Meliadine project to the end of 2010 are summarized in Table 6.1 specifically for the Tiriganiaq and Wesmeg deposits and in Table 6.2 for F-Zone, Pump and Wolf deposits.

Table 6.1 - Summary of exploration drilling at the Meliadine project as a whole, and in the Tiriganiaq and Wesmeg deposits, from pre-1995 through the end of 2010

	Meliadine Project total		Tiriganiaq deposit		Wesmeg deposit	
Year	No. Holes	Metres Drilled	No. Holes	Metres Drilled	No. Holes	Metres Drilled
Pre-1995	196	20,707	1	80	10	915
1995	73	13,042	12	2,553	4	1,049
1996	132	24,237	42	10,732	5	994
1997	146	35,473	54	16,467	3	983
1998	166	40,652	66	14,731	8	1,900
1999	143	23,021	123	20,124	0	0
2000	63	12,877	31	6,360	0	0
2001*	0	0	0	0	0	0
2002*	0	0	0	0	0	0
2003	22	5,421	22	5,421	0	0
2004	24	9,264	20	8,498	4	766
2005**	55	15,820	47	14,221	3	650
2006	77	18,033	64	16,120	0	0
2007**	104	21,799	104	21,799	0	0
2008**	105	28,439	61	22,269	0	0
2009**	138	27,250	52	17,845	0	0
2010**	209	34,112	130	22,745	7	1,401
Total	1,653	330,147	829	199,965	44	8,658

** No drilling*

*** includes geotechnical drill-holes*

Table 6.2 - Summary of historical drilling in the F zone, Pump and Wolf deposits from 1990 through 2010

		F zone deposit		Pump deposit		Wolf deposit	
Year	Operator	No.Holes	Metres drilled	No.Holes	Metres drilled	No.Holes	Metres drilled
1990	Asamera	0	0	0	0	0	0
1991	Asamera	1	200	2	184	0	0
1992	Asamera	0	0	7	926	4	321
1993	Comaplex	3	193	0	0	0	0
1994	Comaplex	37	3,026	19	1,557	3	205
1995	WMC	3	552	5	748	5	1,152
1996	WMC	15	3,060	3	634	7	1,688
1997	WMC	20	5,328	8	1,837	10	2,489
1998	WMC	25	5,847	15	4,278	29	9,016
1999	WMC	5	616	0	0	0	0
2000	WMC	0	0	0	0	5	1,044
2001	WMC	0	0	0	0	0	0
2002	WMC	0	0	0	0	0	0
2003	WMC	0	0	0	0	0	0
2004	Comaplex	0	0	0	0	0	0
2005	Comaplex	0	0	0	0	0	0
2006	Comaplex	0	0	0	0	0	0
2007	Comaplex	0	0	0	0	0	0
2008	Comaplex	19	2,024	0	0	0	0
2009*	Comaplex	46	3,383	0	0	5	840
2010	Comaplex/ Agnico Eagle	48	6,201	0	0	16	3,593
Total		222	30,430	59	10,164	84	20,348

** includes geotechnical drill-holes as well*

6.2 Comaplex Resources Estimates, 2005 to 2010

In 2005, Strathcona (2005) prepared the first mineral resource estimates in compliance with CIM Definition Standards (Canadian Institute of Mining, Metallurgy and Petroleum, 2005) for the Tiriganiaq deposit (Table 6.3). Then, Snowden (2006, 2007) prepared a new mineral resource estimate for the Tiriganiaq deposit for year 2006 and 2007 (Table 6.4 and Table 6.5). In July 2008, Agnico Eagle obtained an 11% interest in the Meliadine project by purchasing an equity interest in Comaplex from Troy Resources. Also in 2008, Resource Capital Fund completed 21 drill-holes for 3,832 m in the area of the Discovery deposit and prepared a mineral resource estimate for the Discovery deposit (Pincock, Allen & Holt, 2008) (Table 6.6), and Snowden (2008) prepared a mineral resource estimate for the Tiriganiaq deposit (Table 6.7). Snowden (2009) prepared a new mineral resource estimate for Tiriganiaq (Table 6.8). Micon also prepared a mineral resource estimate for F zone (Micon, 2009) (Table 6.9). Early in 2010, Snowden (2010) prepared a mineral resource estimate for Meliadine that included the Tiriganiaq, Discovery, F zone, Pump and Wolf deposits (Table 6.10).

Table 6.3 - Mineral resource statement, Tiriganiaq deposit, Meliadine project as of January 2005 (Strathcona, 2005)

Resource Category	Tonnage (000)	Gold grade (g/t)	Contained gold (000 oz)
Indicated mineral resource			
Tiriganiaq Main zone	2,467	10.8	853
Inferred mineral resource			
Tiriganiaq Main zone	421	12.9	175
Tiriganiaq West zone	725	13.4	311

Table 6.4 - Mineral resource statement, Tiriganiaq deposit, Meliadine project as of January 2006 (Snowden, 2006)

Resource Category*	Tonnage (000)	Gold grade (g/t)	Contained gold (000 oz)
Indicated mineral resource			
Tiriganiaq from surface to 150 m depth	4,200	7.5	1,009
Tiriganiaq below 150 m depth	507	11.3	184
Inferred mineral resource			
Tiriganiaq from surface to 150 m depth	3,244	4.1	432
Tiriganiaq below 150 m depth	3,188	10.9	1,120

**Gold cut-off grade of 2.5 g/t from surface to 150 m depth; gold cut-off grade of 6.5 g/t below 150 m depth.*

Table 6.5 - Mineral resources statement, Tiriganiaq deposit, Meliadine project as of April 2007 (Snowden, 2007)

Resource Category*	Tonnage (000)	Gold grade (g/t)	Contained gold (000 oz)
Indicated mineral resource			
Tiriganiaq from surface to 150 m depth	5,180	6.7	1,112
Tiriganiaq below 150 m depth	1,146	10.6	391
Inferred mineral resource			
Tiriganiaq from surface to 150 m depth	1,910	4.1	249
Tiriganiaq below 150 m depth	2,884	11.4	1,057

**Gold cut-off grade of 2.5 g/t from surface to 150 m depth; gold cut-off grade of 6.5 g/t below 150 m depth.*

Table 6.6 - Mineral resource statement, Discovery deposit, Meliadine project as of January 2008 (Pincock, Allen & Holt, 2008)

Resource Category*	Tonnage (000)	Gold grade (g/t)	Contained gold (000 oz)
Indicated mineral resource			
Discovery above 120 m depth	636	7.4	151
Discovery below 120 m depth	296	10.2	97
Inferred mineral resource			
Discovery above 120 m depth	309	7.2	71
Discovery below 120 m depth	258	8.4	70

**Gold cut-off grade of 2.5 g/t from surface to 120 m depth; gold cut-off grade of 5.5 g/t below 120 m depth.*

Table 6.7 - Mineral resource statement, Tiriganiaq deposit, Meliadine project as of January 2008 (Snowden, 2008)

Resource Category*	Tonnage (000)	Gold grade (g/t)	Contained gold (000 oz)
Indicated mineral resource			
Tiriganiaq from surface to 150 m depth	6,136	6.4	1,258
Tiriganiaq below 150 m depth	1,510	10.9	530
Inferred mineral resource			
Tiriganiaq from surface to 150 m depth	1,622	4.1	216
Tiriganiaq below 150 m depth	3,261	11.2	1,169

**Gold cut-off grade of 2.5 g/t from surface to 150 m depth; gold cut-off grade of 6.5 g/t below 150 m depth.*

Table 6.8 - Mineral resource statement, Tiriganiaq deposit, Meliadine project as of July 2009 (Snowden, 2009)

Resource Category*	Tonnage (000)	Gold grade (g/t)	Contained gold (000 oz)
Measured and Indicated mineral resource			
Tiriganiaq from surface to 70 m depth	2,231	6.2	448
Tiriganiaq below 70 m depth	4,767	10.4	1,589
Inferred mineral resource			
Tiriganiaq from surface to 70 m depth	582	3.7	69
Tiriganiaq below 70 m depth	3,225	7.9	824

**Gold cut-off grade of 2.5 g/t from surface to 70 m depth; gold cut-off grade of 5.5 g/t below 70 m depth.*

Table 6.9 - Mineral resource statement, F zone deposit, Meliadine project as of February 2009 (Micon, 2009)

Resource Category*	Tonnage (000)	Gold grade (g/t)	Contained gold (000 oz)
Indicated mineral resource			
F zone from surface to 100 m depth	693	4.66	104
F zone below 100 m depth	27	8.31	7
Inferred mineral resource			
F zone from surface to 100 m depth	775	3.88	97
F zone below 100 m depth	65	8.06	17

**Gold cut-off grade of 2.5 g/t from surface to 100 m depth; gold cut-off grade of 6.5 g/t below 100 m depth.*

Table 6.10 - Mineral resource statement, Tiriganiaq, Discovery, F zone, Pump and Wolf deposits, Meliadine project as of January 2010 (Snowden, 2010)

Resource Category*	Tonnage (000)	Gold grade (g/t)	Contained gold (000 oz)
Total measured mineral resource	295	10.6	101
Total indicated mineral resource	12,652	7.9	3,191
Measured + indicated mineral resource	12,947	7.9	3,292
Total inferred resource	8,388	6.4	1,731

**Gold cut-off grade of 2.5 g/t for the shallower portions of Tiriganiaq, F zone, Pump and Wolf; 3.0 g/t for Discovery. Gold cut-off grade of 5.5 g/t for the deeper portions of Tiriganiaq, F zone, Pump and Wolf; 6.0 g/t for Discovery.*

The elevation that separates shallow and deeper resources was different for each deposit in the Snowden (2010) estimate (Table 6.11).

Table 6.11 - Depth below surface separating the shallow and deeper resources for the gold deposits at the Meliadine project, used in the Snowden (2010) mineral resource estimate

Deposit	Base of shallow resources (metres below surface)
Tiriganiaq	90
Discovery	120
F-Zone	120
Pump	75
Wolf	110

6.3 Agnico Eagle Resource Estimates, 2010 to 2013

In July 2010, Agnico Eagle acquired 100% interest in the Meliadine property from Comaplex. Since the acquisition Agnico Eagle has conducted intensive drilling campaigns (described in Item

10 of this report) and has updated Meliadine's mineral reserves and resources annually incorporating the new drilling results.

In February 2011, Agnico Eagle published a 43-101 technical report (Agnico-Eagle, 2011) showing initial mineral reserves at the project for (in the Tiriganiaq and F zone deposits) as well as mineral resources for Tiriganiaq, F zone, Wesmeg, Discovery, Pump and Wolf deposits. This report was based on a feasibility study (Matte *et al*., 2011). Agnico Eagle used the same fixed elevations as Snowden (2010) had used to separate shallow and deeper resources, and used 120 m depth for the Wesmeg deposit, which was reporting resources for the first time. The 2011 mineral reserves and resources are shown in Table 6.12.

Table 6.12 - Mineral resource and reserve statement, Tiriganiaq, Discovery, F zone, Pump, Wesmeg and Wolf Deposits, Meliadine project as of December 31, 2010 (Agnico-Eagle, 2011)

Resource Category*	Tonnage (000)	Gold grade (g/t)	Contained gold (000 oz)
Total probable mineral reserve	9,467	8.54	2,600
Total indicated mineral resource	8,807	5.21	1,476
Total inferred mineral resource	11,834	6.94	2,642

** Gold cut-off grade of 2.5 g/t for the shallower portions of Tiriganiaq, F zone, Pump, Wesmeg and Wolf; 3.0 g/t for Discovery. Gold cut-off grade of 5.5 g/t for the deeper portions of Tiriganiaq, F zone, Pump, Wesmeg and Wolf; 6.0 g/t for Discovery.*

In December 2011, an updated mineral reserve and resource was estimated (Agnico-Eagle, 2012), and is shown in Table 6.13.

Table 6.13 - Mineral resource and reserve statement, Tiriganiaq, Discovery, F zone, Pump, Wesmeg and Wolf Deposits, Meliadine project as of December 31, 2011 (Agnico-Eagle, 2012 Agnico Eagle Press Release, February 2012)

Resource Category*	Tonnage (000)	Gold grade (g/t)	Contained gold (000 oz)
Total probable mineral reserve	12,468	7.18	2,877
Total indicated mineral resource	12,621	4.09	1,658
Total inferred mineral resource	12,687	5.98	2,438

** Average gold cut-off grade of 3.05 g/t for the shallower portions of all deposits. Average gold cut-off grade of 5.3 g/t for the deeper portions of all deposits.*

In December 2012, an updated mineral reserve and mineral resource was estimated (Agnico-Eagle, 2013), and is shown in Table 6.14. This update incorporated new drilling results.

Table 6.14 - Mineral resource and reserve statement, Tiriganiaq, Discovery, F zone, Pump, Wesmeg, Normeg and Wolf Deposits, Meliadine project as of December 31, 2012 (Agnico-Eagle, 2013)

Resource Category*	Tonnage (000)	Gold grade (g/t)	Contained gold (000 oz)
Total probable mineral reserve	13.300	6.98	2,987
Total indicated mineral resource	17,233	3.94	2,186
Total inferred mineral resource	14,816	6.15	2,932

** Average gold cut-off grade of 2.9 g/t for the shallower portions of all deposits. Average gold cut-off grade of 5 g/t for the deeper portions of all deposits.*

The last update of the mineral reserves and resources estimate before the one reported in this technical report was made as of December 2013 (Agnico Eagle, 2014), and is shown in Table 6.15. This update incorporated new 2013 drilling results.

Table 6.15 - Mineral resource and reserve statement, Tiriganiaq, Discovery, F zone, Pump, Wesmeg, Normeg and Wolf Deposits, Meliadine project as of December 31' 2013 (Agnico Eagle, 2014)

Resource Category*	Tonnage (000)	Gold grade (g/t)	Contained gold (000 oz)
Total probable mineral reserve	11,977	7.38	2,841
Total indicated mineral resource	18,986	5.05	3,082
Total inferred mineral resource	11,710	7.20	2,711

** Average gold cut-off grade of 2.6 g/t for the shallower portions of all deposits. Average gold cut-off grade of 6.00 g/t for the deeper portions of all deposits.*

6.4 Production from the property

There has been no commercial gold production from the property.

Item 7. Geological Setting and Mineralization

Information in this section has been sourced and condensed from Agnico-Eagle (2011) and updated from Agnico Eagle's field work in 2012 and 2013.

7.1 Regional Geology

The Meliadine gold project is located in the northern portion of the Archean Rankin Inlet Greenstone Belt, which is located in the Northwest Hearne Sub-domain of the Churchill Structural Province that forms part of the northern Canadian Shield (Figure 7.1) (Tella *et al.*, 1996). Supracrustal rocks of this belt consist of mafic volcanic rocks, felsic pyroclastic rocks, sedimentary rocks and gabbro sills of about 2.7 billion years old that have been polydeformed and metamorphosed (Bannatyne, 1958; Laporte, 1983; Tella *et al.*, 1986; Tella, 1994). These rocks were deformed in both the Archean and Proterozoic eras.

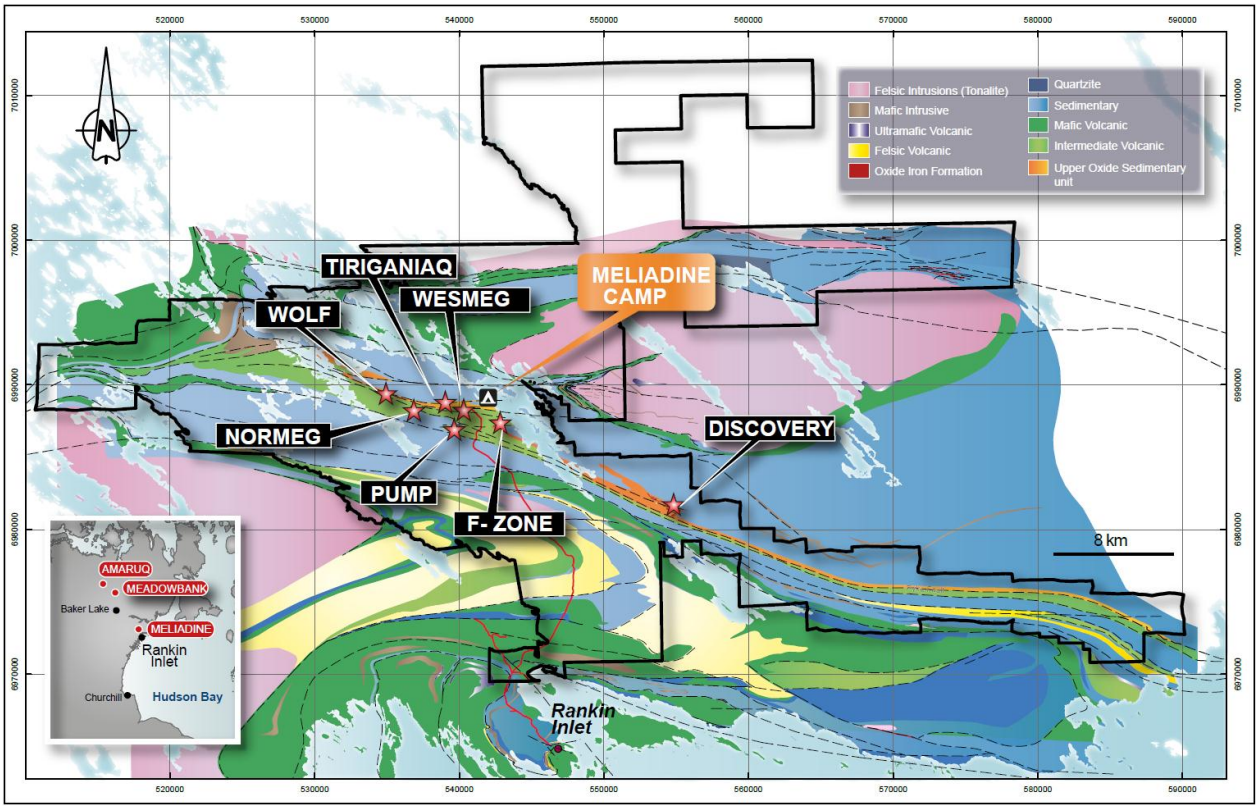


Figure 7.1 - Meliadine area regional geology

The Meliadine trend is defined by northwest-trending rock units as well as a major fault zone known as the Pyke Fault. The Pyke Fault is a several-kilometres-wide high-strain zone characterized by multiple foliations and regionally important shear zones (Carpenter *et al.*, 2005).

7.2 Local Geology

Interpretation of the bedrock geology and faults in the vicinity of the Tiriganiaq, Normeg, Wesmeg, F zone, Pump, and Wolf deposits is presented in Figure 7.2 and for the Discovery deposit in Figure 7.3.

Structural deformation in the project area originated with the development of an east-southeast-dipping fold and extensive thrust faults. The Archean rock layers in the Rankin Inlet area were refolded due to northeast-southwest crustal shortening in the early to mid-second deformation event. This resulted in a regionally pervasive, penetrative shear foliation striking east-southeast and dipping 53° northeast as well as tight southeast-trending second generation folds.

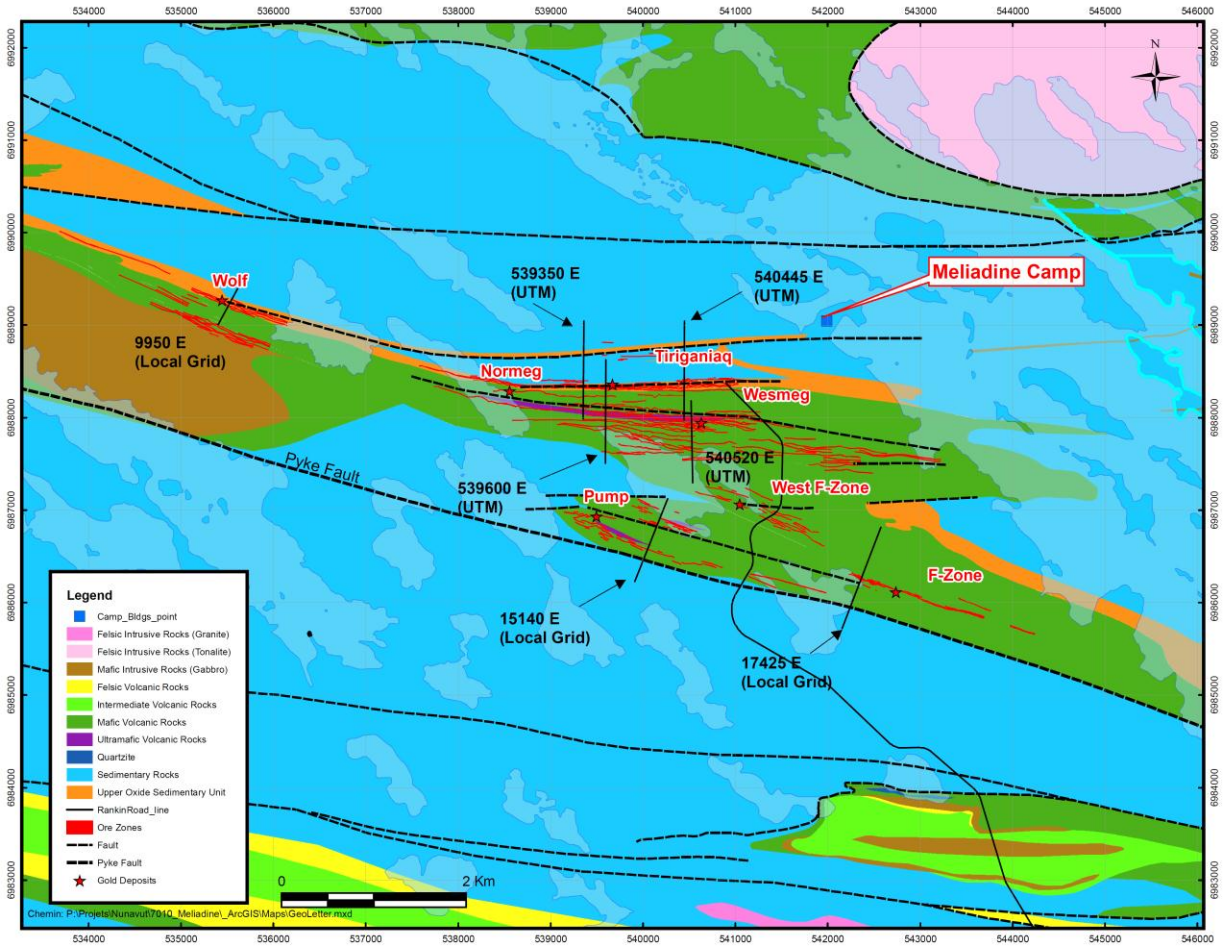


Figure 7.2 - Local geology map showing the Tiriganiaq, Normeg, Wesmeg, F-Zone, Pump and Wolf deposits. The black lines indicate cross sections.

The Pyke Fault was generated by the mid-second generation deformation event, at a slightly oblique angle to the regional stratigraphy and well-developed Z-shape folds across the entire length of the property. Individual folds range from centimetre to kilometre scale and are well developed north of the Pyke Fault.

Subsequent north-south shortening during a third deformation event resulted in shears trending roughly east-west as splays off the main southeast shear trend. Gold mineralization is interpreted to have been introduced during this event, and is postulated to be Proterozoic in age (Miller *et al.*, 1995; Carpenter *et al.*, 2005).

The weaker mica-bearing and argillite units show late-stage crenulation of the penetrative shear fabric locally. The crenulation is thought to post-date the gold mineralization.

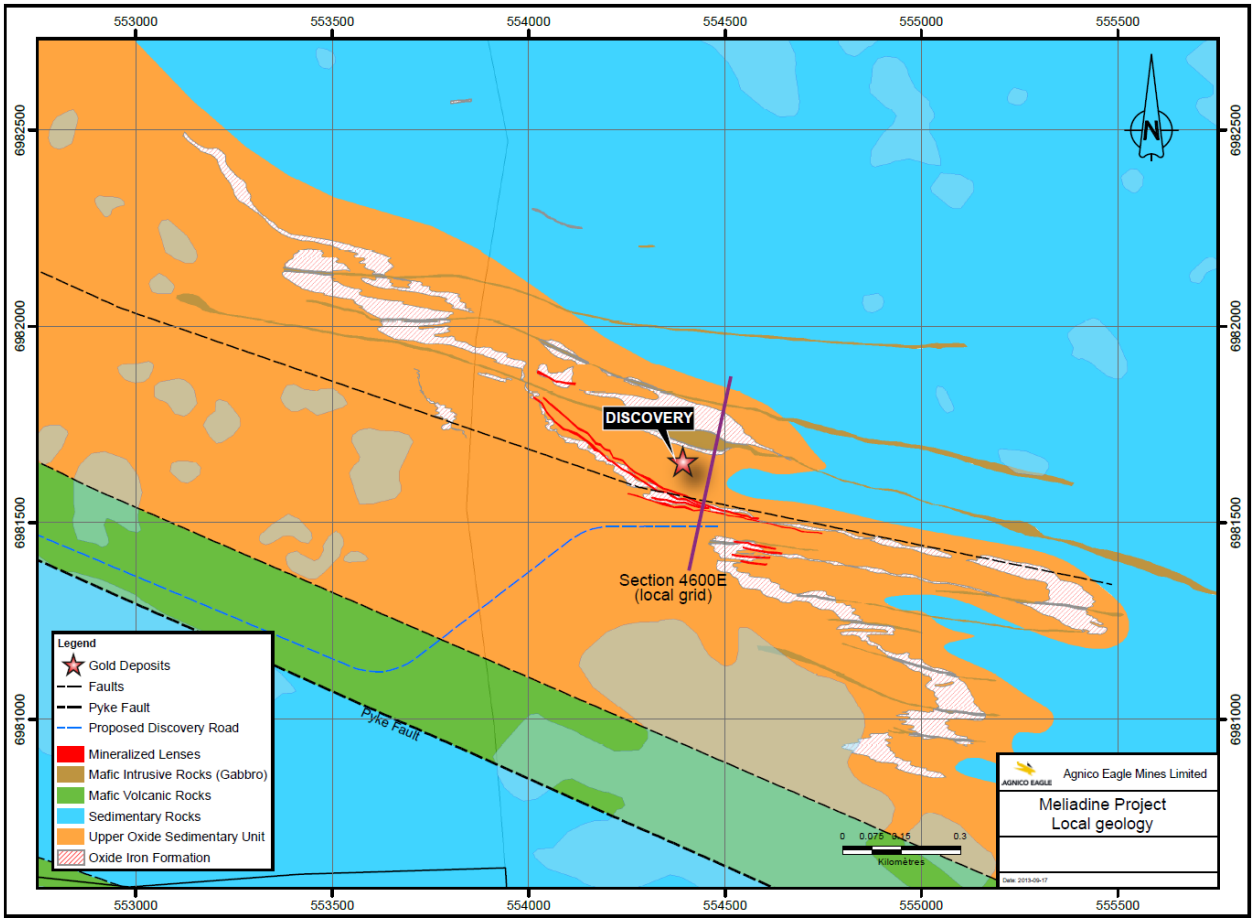


Figure 7.3 - Local geology map showing the Discovery deposit area. The purple line indicates a cross section.

7.3 Property Geology

Seven mineral deposits have been defined at the Meliadine property. The Tiriganiaq, Discovery, F zone, Wesmeg, Wolf and Pump deposits have been described before in detail (Agnico-Eagle, 2011) and are summarized here. The Normeg deposit is a new discovery in close proximity to the Tiriganiaq and Wesmeg deposits and is described for the first time in this report.

Detailed surface mapping of the deposits is not possible due to the general sparse occurrence of rock outcrop in the property area and the complete or almost complete lack of outcrop in the immediate vicinity of the deposits. The geology of the property and deposits has therefore been

interpreted from a combination of drill information, ground and airborne magnetic surveys, and local outcrop mapping.

The facing direction evidence suggests that the rock layers have been overturned at each deposit, with the older rocks to the north lying structurally on top of the younger ones to the south.

Gabbro dykes and sills of several ages are recognized on the property. The oldest gabbro bodies are contained within the Wesmeg Formation and are interpreted as feeders to the overlying basalt pile. The youngest gabbro intrusions commonly cross-cut the second generation folds in the Sam Formation and postdate the deformation associated with the gold deposits.

Minor narrow, undeformed lamprophyre dykes are intersected locally and cross-cut all older rock units, including mineralized veins.

All the rocks in the deposit areas are metamorphosed from lower to middle greenschist grade.

7.4 Mineralization

Zones of gold mineralization at Meliadine have been grouped into lode models, where a lode is defined as a mineral deposit consisting of a zone of veins, veinlets, disseminations or planar breccias (American Geological Institute, 1987). The lode models are defined by the presence of shearing, elevated levels of quartz veining, rock-type and/or structural contacts, coarse arsenopyrite, gold grade and continuity. Known structural trends, dominantly shearing, have been used to define the lode orientations. The term lodes can be used interchangeably with the term zones of mineralization. The lodes are numbered and grouped into the known deposits.

7.4.1 Tiriganiaq deposit

7.4.1.1 Stratigraphic Sequence

The stratigraphic sequence in the Tiriganiaq deposit area strikes east-west and dips to the north at an average of 60º. The east-west orientation of the Tiriganiaq gold deposit is aligned for more than 3 km along what is interpreted as the mineralized shear direction.

Figure 7.4 and Figure 7.5 show typical cross section views of the rock layers, mineralized zones faults and dykes of the Tiriganiaq deposit.

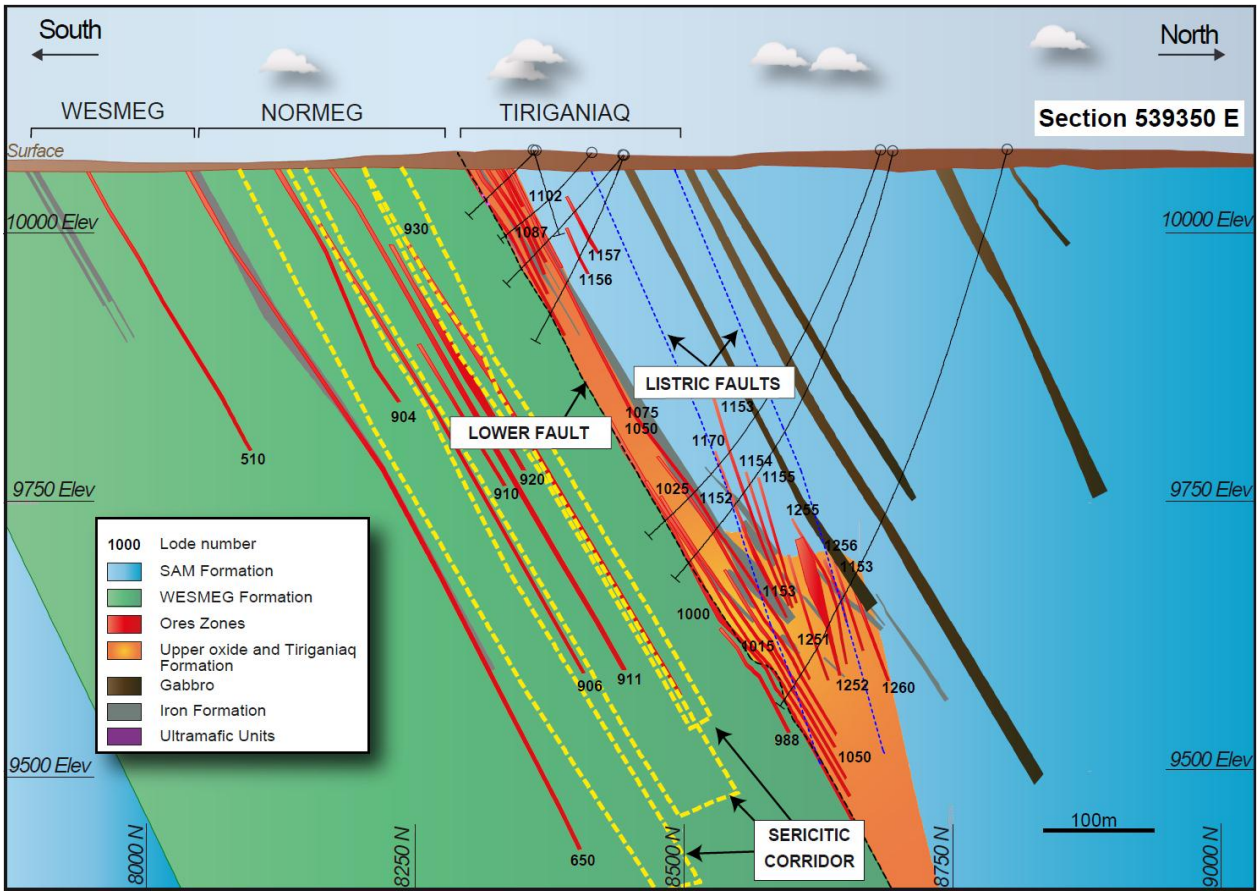


Figure 7.4 - Tiriganiaq vertical cross section at 539350E showing geology and lode wireframes (indicated by red ore zones)

Clastic turbidites of the Sam Formation are the oldest (northernmost) rocks. Beneath the Sam Formation is the Upper Oxide Formation, a diverse package of iron-rich rocks that includes beds of magnetite, chert, chloritic mudstone and greywacke. The upper contact with the Sam Formation is marked by the distinct, laterally consistent "Upper Oxide Iron Formation," which is easily recognized and traceable across the property due to its high magnetic susceptibility. Further south is the Tiriganiaq Formation of laminated siltstones.

At the base of the Tiriganiaq Formation there is sporadic black and graphitic argillite that commonly underlies the 1000 lode mineralization. The Lower Fault likely formed along this obvious stratigraphic weakness. This fault defines the contact between the Tiriganiaq Formation and the underlying Wesmeg Formation of chlorite-rich massive basalts with rare gabbro dykes and interflow sediments. The Lower Fault is the locus of intense late shearing that decreases away from the contact surface, but is more developed in the structural hanging wall. Associated faults emanating from the Lower Fault have resulted in repetition of the stratigraphy in the Tiriganiaq gold deposit.

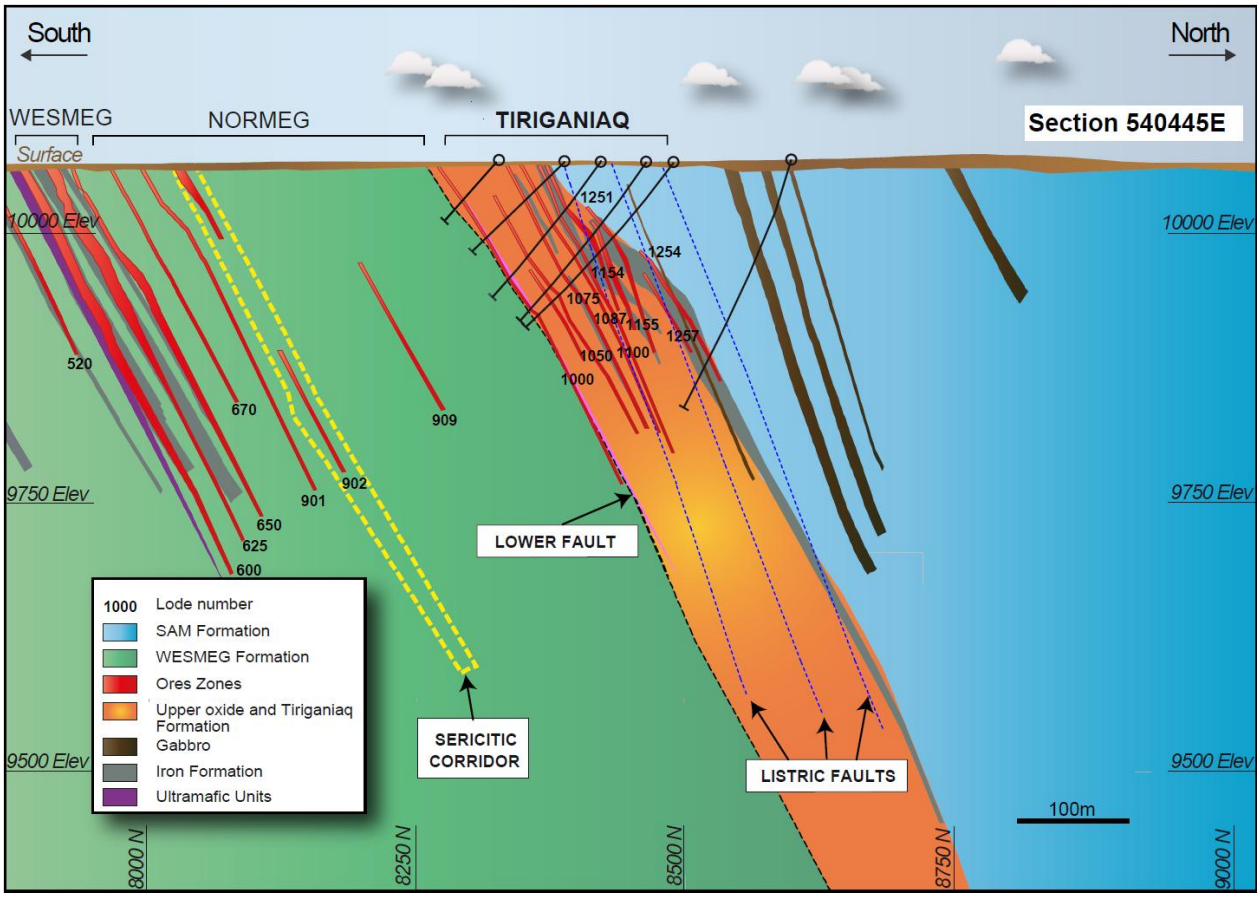


Figure 7.5 - Tiriganiaq vertical cross section at 540445E showing geology and lode wireframes (indicated by red ore zones)

7.4.1.2 Mineralization

Mineralization in the Tiriganiaq gold deposit is strongly associated with shearing and quartz veining, which likely developed during the Proterozoic third deformation event. The most intense and consistent gold mineralization is present within both the Upper Oxide Iron Formation and proximal to the Lower Fault in the siltstones of the Tiriganiaq Formation, but minor amounts of mineralization have been reported in all rock types. Areas of intense shearing are 'healed' by quartz veining and there is generally little to no brittle deformation.

The Tiriganiaq gold deposit has been subdivided into the Main and Western Deeps zones, the latter discovered in 2000, five years after the discovery of the Main zone. Drilling in and between the zones from 2005 to 2008 indicated the Western Deeps is the western down-plunge continuation of several of the Tiriganiaq gold deposit Main zone lodes. The current interpretation is that the Western Deeps zone and Main zone lodes are all part of the same deposit.

7.4.1.2.1 Quartz veining

Gold mineralization is directly associated with syn- to post-deformational quartz veining. Vein appearance is highly variable from a several-metres-thick laminated vein along portions of the Lower Fault to wispy, apparently erratic quartz stringers and stockwork in the Tiriganiaq

Formation. With some exceptions, quartz-only and quartz-ankerite veins tend to be mineralized with gold, while quartz-calcite veins are commonly barren in all lodes. This observation implies to multiple veining events.

Oriented drill core measurements taken in 2005 and in 2014 indicated the most prevalent vein sets measured are sub-parallel to the dominant second generation foliation across the deposit, which is predominantly sub-parallel to bedding. This style of veining is localized and best developed in areas of high strain and associated gold mineralization (*e.g.*, the 1000 lode). Although less prevalent, a second late vein set is recognized that crosscuts the prevalent veining and dips flatly to moderately northwards. The quartz-ankerite veins in this latter set are typically narrow and infrequent, but contain visible gold. Similar to the prevalent veining, the crosscutting set is most often associated with mineralized zones of high strain, formed perhaps as ladder-style extensional veins.

7.4.1.2.2 Sulphides

Sulphide minerals in the Tiriganiaq gold deposit are of two distinct generations: primary and late sulphides.

Primary sulphides consist of wispy, discontinuous, bedding-parallel laminations of pyrrhotite, pyrite and chalcopyrite in oxide iron formations and black argillite. Fine-grained, web-textured sulphides in oxide iron formations close to quartz veins may represent remobilization of primary sulphides, but may alternatively signify sulphur introduced during mineralization. Gold values are generally low to absent in this sulphide assemblage, in the absence of quartz veining.

Sulphidation of the iron formation is incomplete and variable in the Tiriganiaq gold deposit, even in well-mineralized gold-bearing lodes, and is clearly not a prerequisite to significant gold values.

Late sulphides consist of coarse-grained (sub-centimetre-size) clots of arsenopyrite crystals and pyrrhotite associated with highly gold-bearing zones located in and close to quartz veining. The coarse arsenopyrite crystals rarely show signs of strain, having suffered little post-depositional deformation. Arsenopyrite of this type, in association with quartz veining, is a good visual indicator of elevated gold values.

Both primary and late sulphide assemblages host minor, local concentrations of galena and less abundant sphalerite. These minerals appear to be more prevalent in gold-rich areas in the Tiriganiaq Formation, specifically in the 1025, 1050, 1075 and 1087 lodes (see description of lodes below).

Visible gold is common in all lodes in the deposit and is present in quartz veins, pyrrhotite, and along the margins and late fractures of arsenopyrite crystals.

7.4.1.2.3 Alteration

Zones of significant gold mineralization that occur near the Lower Fault are associated with moderate to strong sericite hydrothermal alteration that may be tens of metres thick. This is especially apparent in Tiriganiaq Formation siltstones and Wesmeg Formation volcanics, where the intensity of alteration and deformation makes it difficult to differentiate the two units.

Sericite is present, but less well developed, in mineralized lodes in the iron formations. Chlorite and disseminated magnetite are common in the Upper Oxide Iron Formation but are interpreted to be part of the mineralogy of the silicate bands in the iron formations rather than a distinct hydrothermal alteration product.

Potassium replacement is present locally as biotite-bearing selvages in sedimentary rocks hosting mineralized quartz veins and/or iron formations.

7.4.1.2.4 Lodes

Gold mineralization in the Tiriganiaq gold deposit is hosted in the Upper Oxide Iron Formation as well as in clastic sedimentary and mafic volcanic rocks. It is associated with pyrrhotite- and arsenopyrite-bearing iron formation, and quartz veins with an alteration assemblage of ankerite, sericite, chlorite, and quartz.

Five dominant lodes host the gold mineralization in the Tiriganiaq deposit. These five lodes have been subdivided into a total of 35 domains for wireframe modelling and resource estimation purposes. Lode geometries, in general, fall into two basic categories: layer-parallel lodes, and plunging or non-layer-parallel lodes.

The dominant geologic control for layer-parallel lodes is a late penetrative, bedding-parallel shear system (*e.g.*, 1000, 1015, 1025, 1050, 1075, 1087 and 1100 lodes). Two of the lodes (1000 and 1100) host significant high-grade gold concentrations over substantial widths. Geology, gold grade, alteration, mineralization and strength of structure of these two lodes are moderately consistent and predictable within the Main zone of the Tiriganiaq deposit. The overall orientation of mineralization in these two lodes suggests a moderate plunge to the east, but mineralization of economic interest is restricted to shoots of smaller size that appear to have a slight west plunge within the overall body of lower grade mineralization. The 1015, 1025, 1050, 1075 and 1087 lodes may also follow this pattern.

The main control for plunging and non-layer-parallel lodes is that they host gold in multiple sub-parallel, west-plunging shear structures such as the 1153 and 1252 lodes. These interpreted fold structures may be related to reactivated faulting and/or fold repetition of the Upper Oxide Iron Formation (the iron formation at the lower end of the 1100 lode). Many mineralized shears cut through the fold nose and the overall package plunges 10º to 20º to the west. Gold grades appear to be higher and more continuous where the shears cut the thicker iron formation in the nose of these folds.

A description of lodes, from south to north, follows. Relative lode positions are presented in schematic form in Figure 7.6.

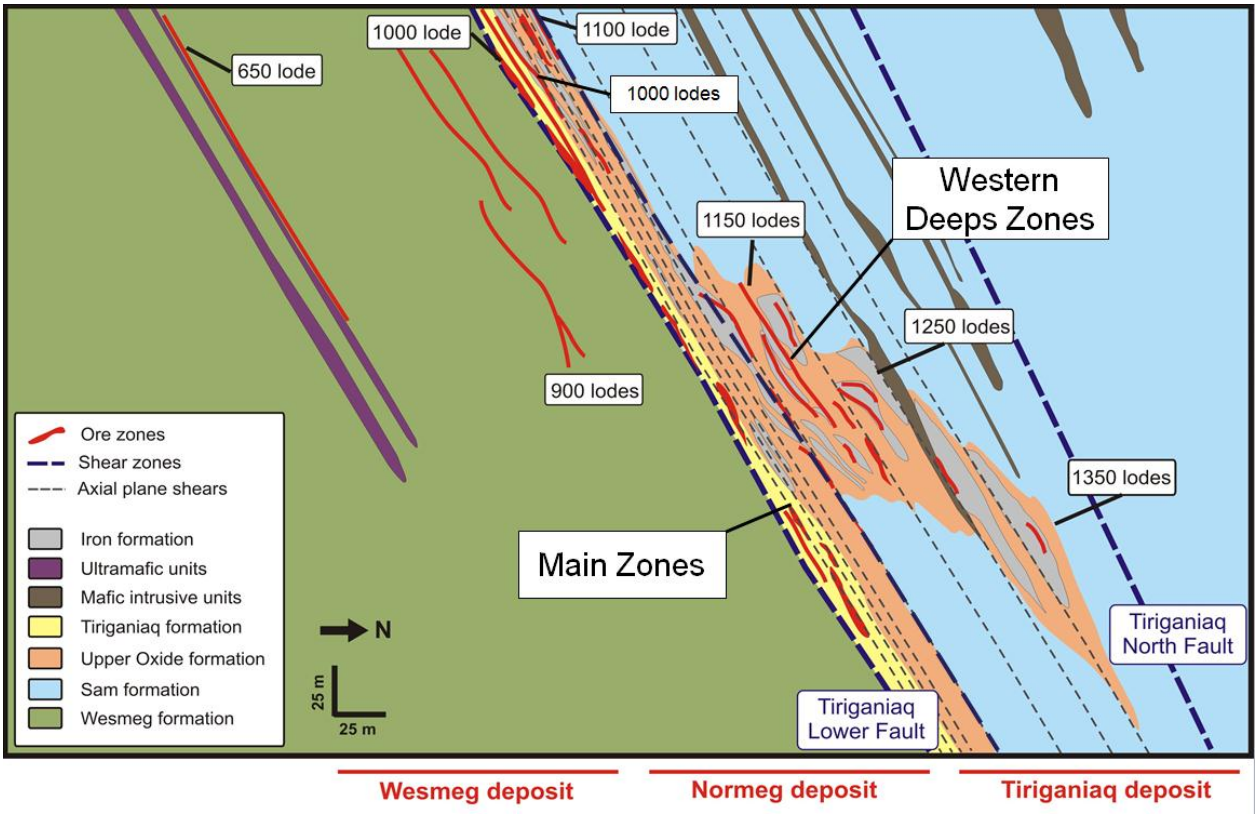


Figure 7.6 - Composite geological cross section, Wesmeg-Normeg-Tiriganiaq, showing the relative position of the lodes

1000 Lode

The 1000 lode is narrow, shear-hosted and controlled by the nearby Lower Fault. The lode is centred on a semi-continuous laminated to networking quartz-vein system that varies from centimetres to several metres in thickness and is hosted in strongly sericitized greywackes and siltstones.

The 1000 lode is tabular, averages less than 2 m in true thickness and dips 60° to the north. Slight bends in the dip of the lode surface and the associated thickening appear to be an important control on the internal distribution of mineralization. It is interpreted that localized dilation zones were created slightly above the flexures, forming favourable pathways for mineralized fluid flow and gold deposition.

As elsewhere in the Tiriganiaq gold deposit, the more gold-rich sections within the lode have strongly developed coarse arsenopyrite concentrations and visible gold. There is no consistent correlation between gold grade and the presence of quartz. The zones of best mineralization, particularly in the upper portions of the lode, tend to coincide with continuous laminated quartz veining. This observation has allowed for the interpretation of a well-defined high grade subdomain within the 1000 lode that comprises predominantly laminated quartz veining and immediately nearby high intensity, but more irregular, quartz veining.

1000 Lode Series

Located between the 1000 and 1100 lodes, as shown in Figure 7.6, the 1000 lode series are generally moderately narrow, sub-parallel, discontinuous zones of shear-controlled gold mineralization hosted in both sericitized clastic sediments and thin discontinuous iron formations oriented parallel to the 1000 and 1100 lodes.

All available geological data were used to constrain these lodes during the modelling process, including the presence and intensity of quartz veining, arsenopyrite, pyrrhotite, sericite alteration and shear intensity. Quantitative and semi-quantitative structural information collected from drill core with respect to shearing was used to define the orientation of these lodes. This orientation was largely consistent with the dominant second generation foliation across the deposit.

The most consistent geological information used to define the lodes was anomalous gold grades respecting, where possible, cut-off grades for open pit or underground mining and minimum mining widths. These gold-bearing zones are commonly spatially related, though not necessarily coincident with the above constraints. As a result, gold grades within one lode can vary significantly from one drill intercept to another. The 1000 lode was observed and thoroughly sampled by underground exposure on the 9950 Level but the controls on the localization of gold is uncertain for the other lodes. This can only be resolved by underground exposure and detailed sampling, including detailed infill drilling in all of the lodes in the 1000 series.

1100 Lode

Defined as the first significant oxide iron formation to be encountered when drilling from north to south, the 1100 lode consists of several thick, banded chert-magnetite units with variable silicate layers interbedded with several narrow siltstone and greywacke beds. The lode varies from 4 m to 12 m in true thickness, generally becoming thinner down dip. Much of the thickening is attributed to structural repetition of the iron formation through local tight folding and/or faulting.

Potentially economic concentrations of gold can encompass the entire lode, but they are commonly restricted to arsenopyrite-rich concentrations in narrow shears at the hanging-wall and footwall contacts of the Upper Oxide Iron Formation.

A poor understanding of the controls on the shearing (possibly a combination of crosscutting and bedding-parallel shearing) within the larger iron formation unit, and therefore on gold distribution, has made the selective definition of discrete higher grade portions of the 1100 lode difficult. The 1100 lode was observed over 164 m of strike length and thoroughly sampled by underground exposure on the 10,000 Level and it proved to be continuous.

1150 Lode Series

This lode series comprises nine lodes occurring between the hanging wall of the 1100 lode and the footwall of the 1250 lode in up-thrust sections of folded and sheared Upper Oxide Iron Formation. The thrusts are not clearly understood, but could be interpreted from diamond drill core interpretation to be reactivated faults emanating from the Lower Fault. The entire package of folded and fault-repeated iron formation and sediment has a shallow (±13º) plunge to the west.

The gold mineralization occurs in narrow, dominantly non-layer-parallel, and lesser layer-parallel, quartz-filled shears. These shears are broadly sub-parallel to the orientation of the folded system. Concentrations of arsenopyrite, pyrrhotite and local visible gold are common in the mineralized shears. The more continuous and wider parts of the economic zones are concentrated in the nose position in complexly folded and sheared iron formation. Mineralized shears have been divided in the resource model into subdomains labelled (from south to north): 1150, 1151, 1152, 1153, 1154, 1155, 1156, 1157, 1160 and 1170. Some appear layer-parallel while others appear to migrate from the structural footwall to the hanging wall, moving from east to west across the zone.

1250 Lode Series

The 1250 lode series is a northerly repetition of the 1150 lodes. The overall lode shape has a westerly plunge. The higher-grade gold mineralization in the lode appears to be controlled by a similar series of narrow but continuous shear zones. The shears have been subdivided in the resource model and labelled as follows (from south to north): 1250, 1251, 1252, 1253, 1254, 1255, 1256, 1257, 1258, 1259, 1260, 1261, 1262, 1263 and 1264. These subdomains contain most of the gold in the Western Deeps zone of the Tiriganiaq gold deposit.

1350 Lode

The 1350 lode is a northerly repetition of the 1250 lode, interpreted as a third reactivated fault. The overall lode shape appears to have a westerly plunge, but drilling in this zone is as yet limited. The higher-grade gold mineralization in the lode appears to be controlled by a similar series of narrow but continuous shear zones with five spatially restricted domains: 1265, 1270, 1275, 1350 and 1360.

7.4.2 Wesmeg deposit

The Wesmeg deposit was the target of a dedicated drill program for the first time in 2010. The host Wesmeg Formation consists of chlorite-rich massive basalts, interlayered mafic volcaniclastics with rare gabbro dykes, and some interflow sediments comprising siltstone, mudstone (some graphitic) and minor iron formation. Occasional metre-scale ultramafic units are present in the sequence. The chert-rich and iron-poor rocks of the Lower Lean Iron Formation consist of metre-scale cherty iron formation units interbedded with centimetre-scale volcanic and sedimentary units. The iron formation units hosting the gold mineralization at Wesmeg vary in thickness from metres to tens of metres.

There appear to be two parts to the Wesmeg deposit: a northern and southern part. The northern part corresponds to the uppermost iron formation (650 lode). The stratigraphic sequence here strikes east-west and dips 65º to the north. This is similar to the east-west orientation of the Tiriganiaq gold deposit (about 400 m to the north of Wesmeg) where it is interpreted as the mineralized shear direction. The same orientation has been demonstrated by a high-resolution magnetic survey over the northern part of the Wesmeg area. Figure 7.4 and Figure 7.5 show typical cross sections of the rock units and gold mineralization of the northern Wesmeg area. The stratigraphic sequence in the southern part of the Wesmeg deposit strikes northwest-southeast and dips 50º to the north. This part has been named West-F zone and is not included in the current Mineral Resources (Figure 7.2).

Mineralization in Wesmeg is strongly associated with shearing and quartz veining within the Lower Lean Iron Formation, with thicker, higher-gold-grade sections. For modelling purposes the Wesmeg deposit is composed of 36 lodes classified as the Tiriganiaq 200 to 700 series (225 to 740).

Free gold occurs as discrete to coarse blebs, locally disseminated, associated with very coarse to finely disseminated arsenopyrite.

Alteration envelopes occur adjacent to quartz-calcite veining and are characterized by ankerite-, silica-, chlorite- and biotite-bearing assemblages that overprint the pre-existing regional greenschist metamorphic facies.

7.4.3 Normeg deposit

The Normeg deposit was defined in 2012. It is located between the Tiriganiaq and the Wesmeg deposits, more precisely between the Lower Fault (the contact of the Tiriganiaq Formation sediments and the underlying Wesmeg Formation mafic volcaniclastics) and the uppermost iron formation or the uppermost ultramafic unit of the Wesmeg Formation.

Normeg is within a stratigraphic sequence that strikes approximately east-west and dips approximately 60° to the north. The sequence is within the northern part of the Wesmeg Formation and is hosted by chlorite-rich massive basalts and interlayered mafic volcaniclastics with rare gabbro dykes.

Mineralization in Normeg is strongly associated with sheared quartz veins with strong sericitic alteration haloes in the mafic volcanic rocks. Those veins, cross-cutting or sub-parallel to the foliation, locally contain chlorite, calcite and tourmaline. The Normeg zones are identified as the 900 series lodes, though the deposit is mainly characterized by the 911 and 920 lodes.

Free gold occurs disseminated in the sheared/fractured quartz veins. The gold is commonly associated with fine- to coarse-grained arsenopyrite and pyrite, and fracture-filled galena, pyrrhotite and pyrite.

Alteration envelopes occur adjacent to quartz-ankerite veining and are characterized by sericite, silica and fuchsite assemblages that overprint the pre-existing regional greenschist metamorphic facies.

7.4.4 Discovery deposit

The stratigraphic sequence in the Discovery deposit area strikes northwest-southeast and dips from 45º to 60º to the north. Figure 7.7 shows a typical cross section of the rock units and gold mineralization in the Discovery deposit.

Clastic turbidites of the Sam Formation are the oldest (northernmost) rocks. As at Tiriganiaq, these overlie the Upper Oxide Formation and its uppermost portion, the “Upper Oxide Iron Formation”. Chlorite-rich massive basalts of the Wesmeg Formation form the structural footwall to the sequence but occur at least 600 m south of the Discovery deposit. The Lower Fault forms the contact between the Wesmeg and Upper Oxide formations and is interpreted as a basal detachment surface, but in the area of the Discovery deposit it is not exposed and has not been

encountered by drilling yet. The Lower Fault therefore represents a potential target for Tiriganiaq-style lode gold vein zones similar to the 1000 lode.

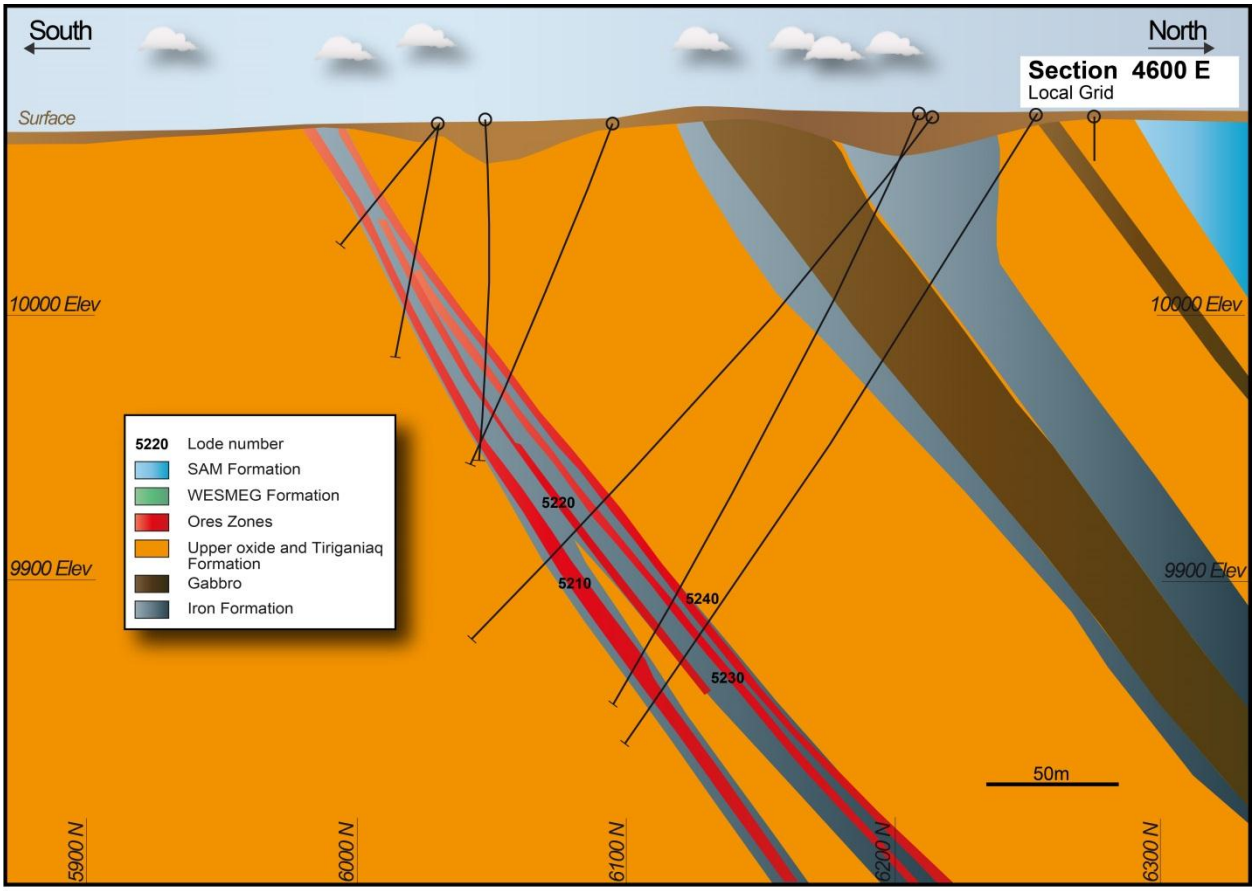


Figure 7.7 - Discovery vertical cross section at 4600E (local grid) showing geology and lode wireframes (indicated by red ore zones)

Mineralization in the Discovery gold deposit is strongly associated with shearing and quartz veining within the Upper Oxide Iron Formation, which is strongly folded. The thicker, higher-gold-grade sections are controlled by Z-shaped folds that trend east-northeast and plunge 47º.

Free gold occurs as coatings and fracture fillings in large recrystallized arsenopyrite and pyrrhotite grains, and as disseminations in quartz veins and chlorite layers. Trace amounts of sphalerite and chalcopyrite are found locally.

Alteration envelopes occur adjacent to quartz-calcite veining and are characterized by hornblende/grunerite-, biotite- and calcite-bearing assemblages that overprinted the pre-existing regional greenschist metamorphic facies.

For the purposes of the current resource estimate, ten domains were developed and are referred to as lodes 5110, 5120, 5130, 5140, 5150, 5210, 5220, 5230, 5240, and 5310. All of these lodes represent the same Upper Oxide Iron Formation unit, but have been subdivided to facilitate modelling of the fold nose. Lodes 5210, 5220, 5230 and 5240 represent the area of the Upper

Oxide Iron Formation within the resource area that outcrops and was channel-sampled. To eliminate the influence of these higher grade channel samples, they were excluded for variography and resource estimation, since the QA/QC and sampling protocol for the channel-sampling had not been documented.

7.4.5 F zone deposit

The stratigraphic sequence in the F zone deposit area strikes northwest-southeast and dips from 45º to 50º to the north.

Figure 7.8 shows a typical cross section of the rock units and gold mineralization at the F zone. The host rocks for F zone are chlorite-rich massive basalts of the Wesmeg Formation, which are cut by gabbro dykes, narrow lamprophyre dykes and interflow sediments. Within the Wesmeg Formation are chert-rich and iron-poor rocks of the Lower Lean Iron Formation that consist of metre-scale cherty iron formation units interbedded with centimetre-scale volcanic units.

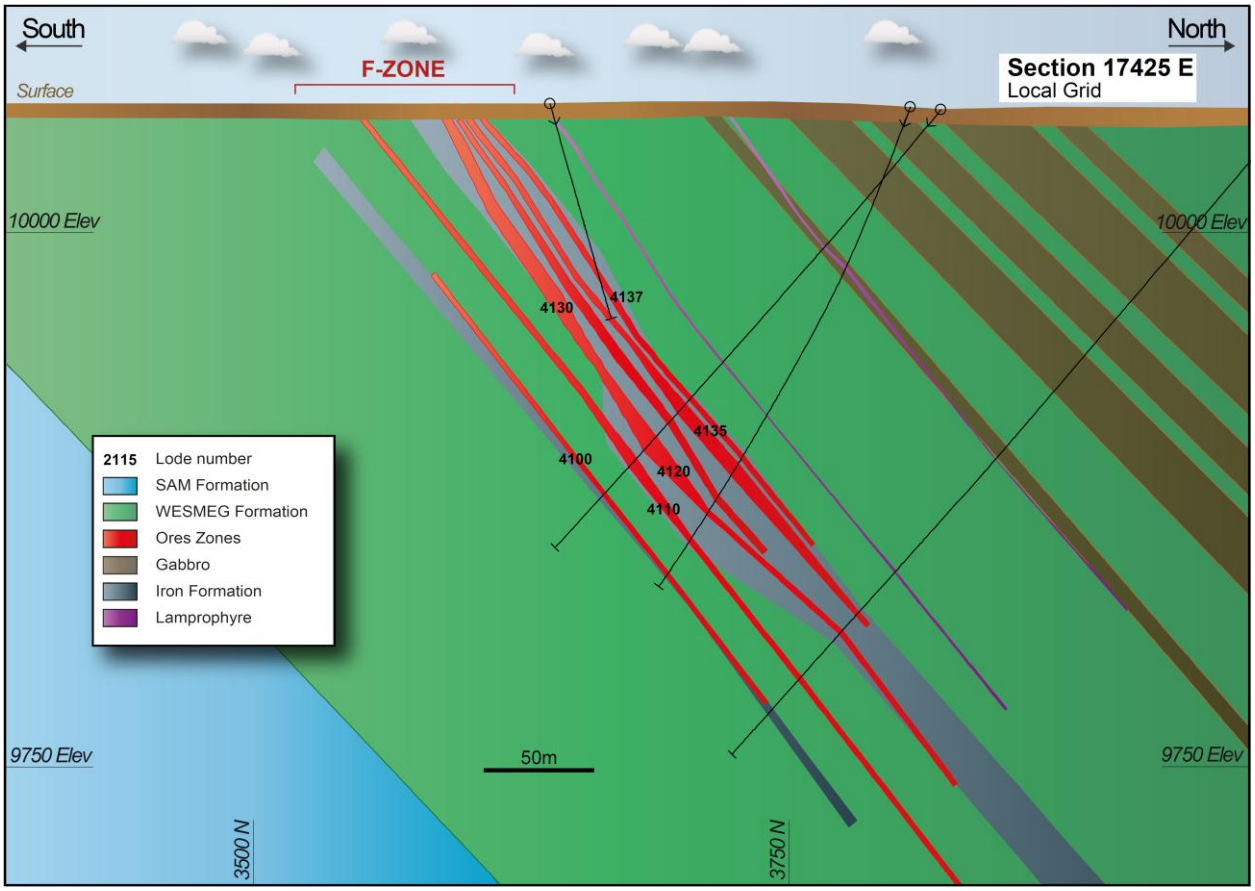


Figure 7.8 - F zone vertical cross section at 17425E (local grid) showing geology and lode wireframes (indicated by red ore zones)

Mineralization in the F zone gold deposit is strongly associated with shearing and quartz veining within the Lower Lean Iron Formation. The iron formation that hosts the gold mineralization varies in thickness from metres to tens of metres. Thicker sections with higher gold grades are controlled by the intersection of the east-southeast-trending iron formation with a dominant east-west-oriented structure and a second southeast-trending structure. Plunges of this thickening vary from steeply northeast to steeply northwest depending on local changes in strike.

Free gold occurs as discrete blebs in pyrrhotite and quartz shears, and to a lesser extent along fractures and grain boundaries in large recrystallized arsenopyrite.

Alteration envelopes occur adjacent to quartz-calcite veining and are characterized by hornblende/grunerite-, biotite- and calcite-bearing assemblages that overprint the pre-existing regional greenschist metamorphic facies.

For the purposes of the current resource estimate, thirteen domains were developed and are referred to as lodes 4100, 4105, 4110, 4115, 4120, 4130, 4135, 4137, 4140, 4150, 4160, 4170 and 4180. They were defined by tracing areas of mineralization along the Lower Lean Iron Formation from section to section.

7.4.6 Pump deposit

The stratigraphic sequence in the Pump deposit area strikes northwest-southeast and dips 50º to the north. Figure 7.9 shows a typical cross section of the rock units and mineralization at the Pump deposit. As at the F zone, the host rocks for the Pump deposit are chlorite-rich massive basalts of the Wesmeg Formation, which are cut by rare gabbro dykes and interflow sediments. At Pump, there are three types of chert-rich iron formation in the Lower Lean Iron Formation: chert-magnetite-chlorite iron formation, grunerite-cummingtonite-rich iron formation, and sulphide-rich beds in chert-dominated iron formation. Occasional metre-scale ultramafic units are noted in the sequence. The main structural feature is a kilometre-long Z-shaped fold formed by the intersection of east-west-oriented shear structures and the Lower Lean Iron Formation. The Z-shaped fold is divided in three fold hinges as shown in Figure 7.10.

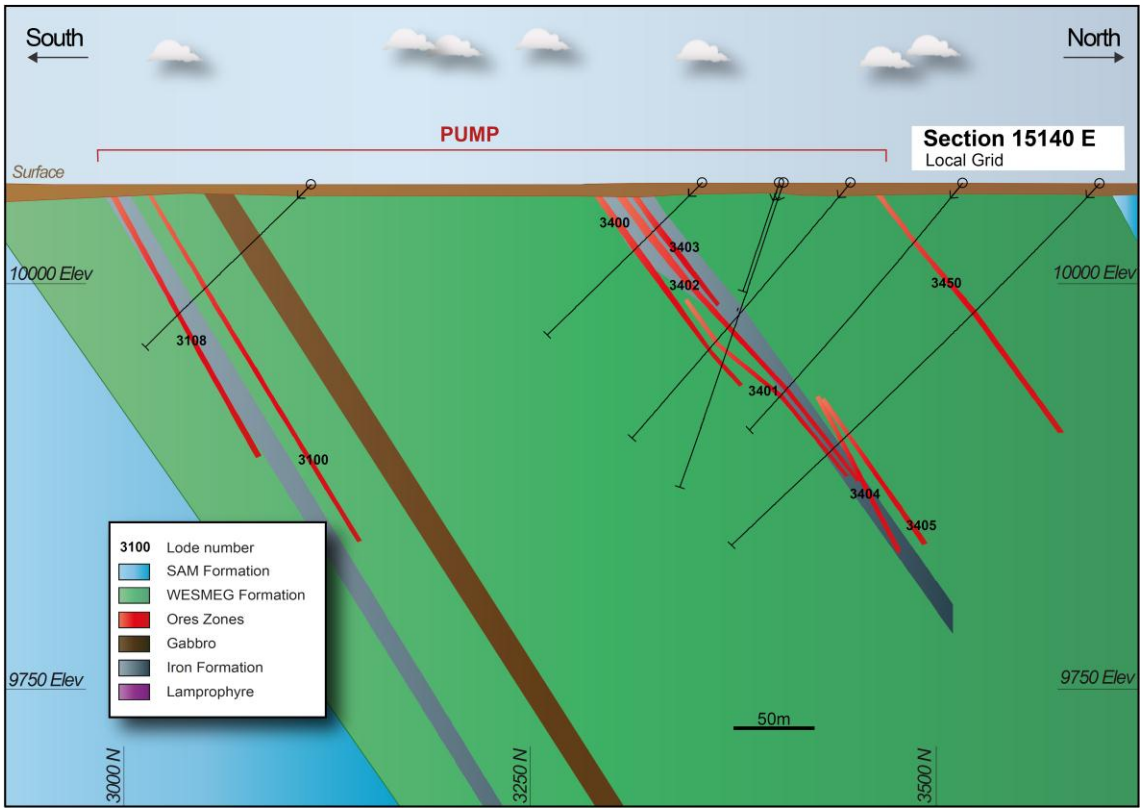


Figure 7.9 - Pump vertical cross section at 15140E (local grid) showing geology and lode wireframes (indicated by red ore zones)

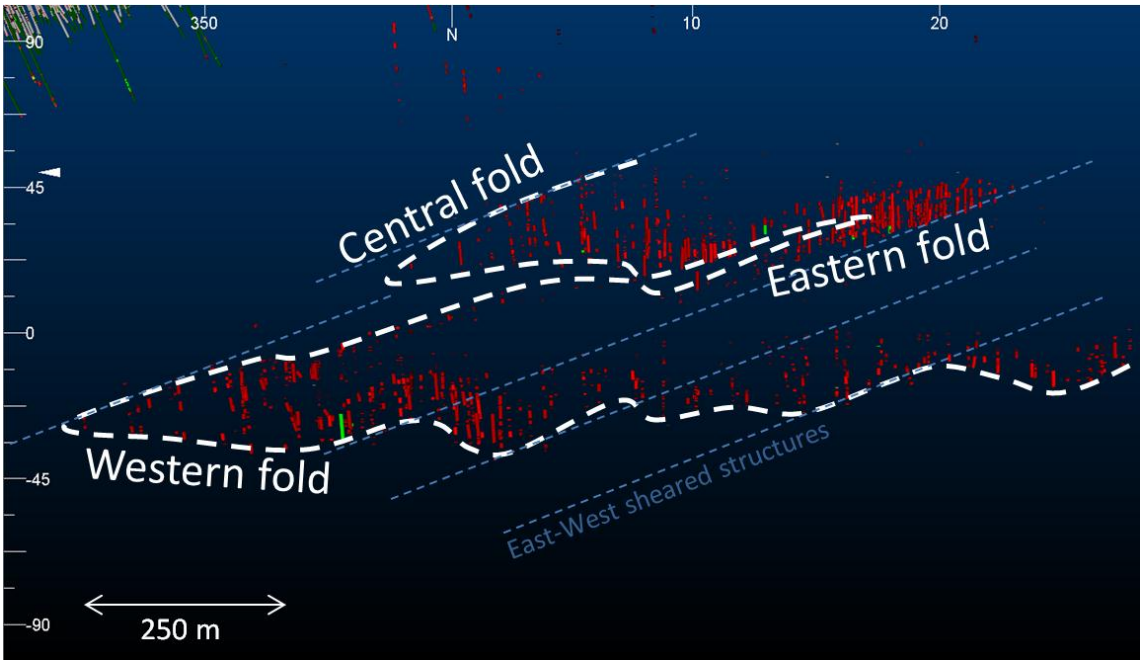


Figure 7.10 - Isometric view looking north-east (with an approximate plunge of -50°) showing the main structural feature at the Pump deposit is a Z-shaped fold; red lines are the drill-hole iron formation band intersections

Mineralization in the Pump gold deposit is also strongly associated with shearing and quartz veining within the Lower Lean Iron Formation, with thicker, higher-gold-grade sections associated with east-west shearing. As at F zone, the plunges of this thickening vary from steeply northeast to steeply northwest depending on local changes in strike.

Free gold occurs as discrete blebs in pyrrhotite and quartz shears, and to a lesser extent along fractures and grain boundaries in large recrystallized arsenopyrite.

Alteration envelopes occur adjacent to quartz-calcite veining and are characterized by ankerite-, silica-, chlorite- and biotite-bearing assemblages that overprint the pre-existing regional greenschist metamorphic facies.

For the purposes of the current resource estimate, 25 different zones were developed and were regrouped into five spatial domains described in Item 14 of this report, consistent with the Z-shaped folding. They were defined by tracing areas of mineralization along the Lower Lean Iron Formation from section to section.

7.4.7 Wolf deposit

The stratigraphic sequence in the Wolf deposit area strikes northwest-southeast and dips 70º to the north. The Wolf deposit is divided into two areas: the northern Wolf North is hosted in stratigraphy similar to the Tiriganiaq deposit, while the southern Wolf Main is hosted in stratigraphy similar to the Wesmeg deposit.

Figure 7.11 shows a typical cross section of the rock units and gold mineralization at the Wolf deposit. Clastic turbidites of the Sam Formation are the oldest (northernmost) rocks. These overlie the Upper Oxide Formation and its uppermost portion, the "Upper Oxide Iron Formation", which hosts the Wolf North mineralized zones.

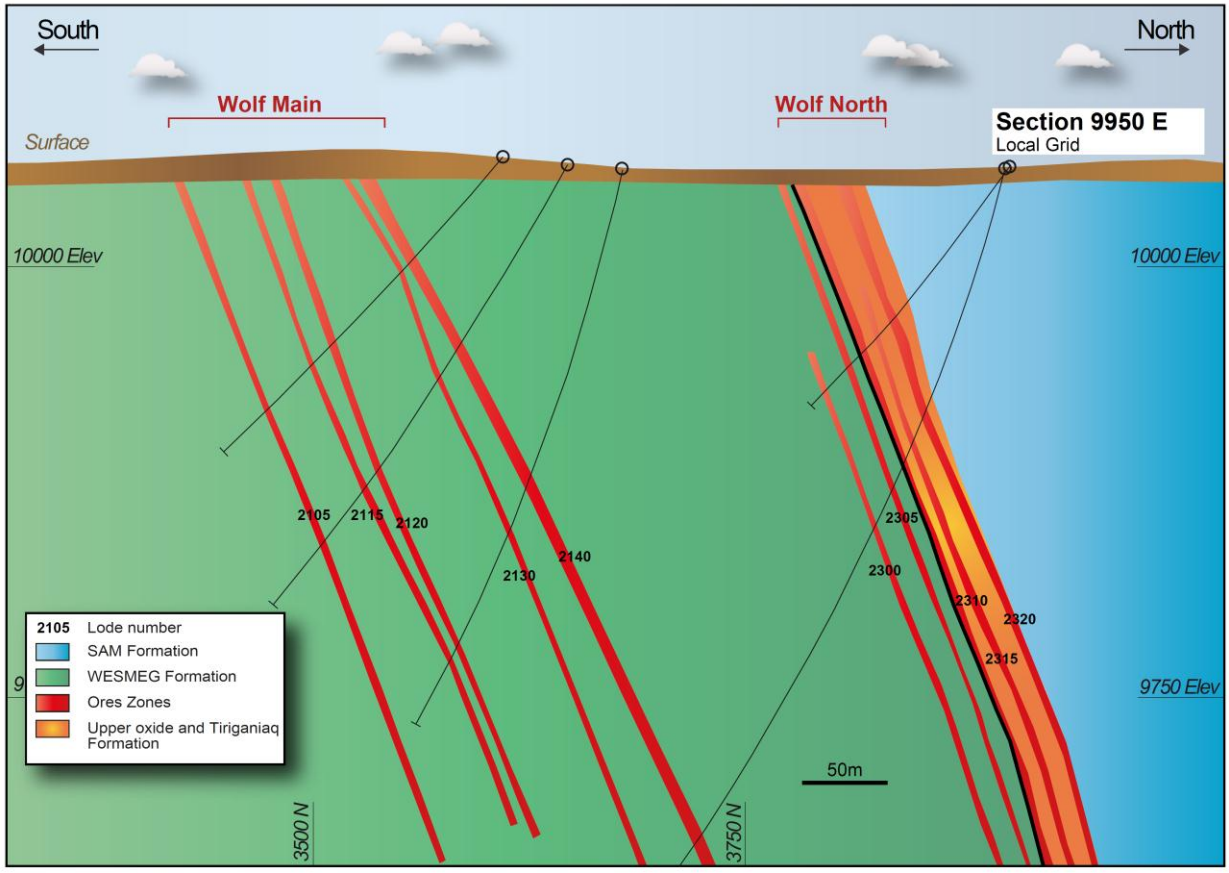


Figure 7.11 - Wolf vertical cross section at 9950E (local grid) showing geology and lode wireframes (indicated by red ore zones)

Chlorite-rich massive basalts of the Wesmeg Formation form the structural footwall to the sequence. Within the Wesmeg Formation are chert-magnetite-chlorite iron formations of the Lower Lean Iron Formation that host the Wolf Main mineralization.

East-west structures intersecting the dominant east-southeast stratigraphic trend may control the gold mineralization at Wolf North and Wolf Main.

Mineralization at the Wolf deposit is divided into the 2300 series (resembling Tiriganiaq) and the 2100 series (similar to Wesmeg, Pump and F zone).

The 2300 series lode mineralization is strongly associated with shearing and quartz veining within the Upper Oxide Iron Formation and thus is analogous with the 1000 lode series and the 1100 lode at Tiriganiaq in setting and character. Gold mineralization occurs as disseminated and coarse blebs of gold within sheared, silica-replaced iron formation and within coarse arsenopyrite and pyrrhotite concentrations in veins. The 2310 lode is analogous with the 1000 lode at Tiriganiaq. Gold mineralization occurs as free gold in laminated and non-laminated quartz veins with lesser concentrations of arsenopyrite and pyrrhotite.

As at Wesmeg, Pump and F zone, the 2100 series lodes were defined by tracing areas of mineralization along the Lower Lean Iron Formation. Free gold occurs as discrete blebs in

pyrrhotite and quartz shears and to a lesser extent along fractures and grain boundaries in large recrystallized arsenopyrite.

Alteration envelopes occur adjacent to quartz-calcite veining and are characterized by ankerite-, silica-, chlorite- and biotite-bearing assemblages that overprint the pre-existing regional greenschist metamorphic facies.

Item 8. Deposit Types

The Meliadine gold district comprises a combination of orogenic greenstone- and banded iron formation ("BIF") hosted gold mineralization. Gold in the district is associated with hydrothermally altered and sulphidized BIF (Lawley, *et al.*, 2013).

The seven gold deposits defined on the property are vein- and shear-dominated occurrences hosted predominantly in iron formation, fine-grained sediments and volcanics, either on a splay off the regional Pyke Fault (such as the Tiriganiaq, Wesmeg and Normeg deposits) or else on structures parallel to the Pyke Fault (such as the Discovery, Pump, F zone and Wolf deposits). While these gold deposits are similar to other recognized iron formation-hosted gold deposits, such as Lupin in Canada's Northwest Territories (*e.g.*, Bullis *et al*., 1994) and Homestake in South Dakota, U.S.A. (*e.g.*, Rye and Rye, 1974), the strong association of quartz veins with gold mineralization in sediments at Meliadine is distinct from these other deposits.

Tectonic interleaving of the Archean supracrustal rocks, together with local and regional textural and mineralogical evidence, suggest that a combination of early Archean structural preparation and later Proterozoic re-activation was responsible for the Lower Fault splay and subsequent dextral movement along it. Evidence to date suggests that the main gold mineralizing event at the Meliadine property was Proterozoic in age (Miller *et al*., 1995). This age is supported by a $^{207}Pb/^{206}Pb$ age of 1,854±6 million years determined on hydrothermal monazite from gold-bearing quartz veins at the Tiriganiaq deposit (Carpenter *et al*., 2005).

Gold mineralization in the deposits is strongly correlated with shearing and quartz veining. Mineralized lodes are hosted in quartz-vein stockwork, laminated veins and variably sulphidized iron formations, in complexly folded and sheared iron formation, sedimentary and volcanic rocks in or near the volcanic-sedimentary contact. The most important exploration targets of exploration in the project are mainly located along regional shear zones, especially where they intersect BIF. The exploration drilling therefore includes holes angled perpendicular to the regional foliation in the area of these intersections, following the mineralized shoots. Because of the scarcity of outcropping bedrock, geophysical surveys have been used to locate new targets, followed up by prospecting and limited diamond drilling.

Item 9. Exploration

Gold mineralization was first noted on the Meliadine property in 1972, but extensive exploration did not begin until 1987 when Asamera and Comaplex followed up on the original gold find. Their work consisted of various ground and airborne geophysics, geochemistry surveys, mapping, sampling and eventually extensive drilling.

By the time Agnico Eagle took over the project in July 2010, the main activity was drilling the known deposits. Surface exploration was limited due to the scarcity of outcrop and the priority of developing the deposits.

9.1 Prospecting

A regional prospecting program carried out by Agnico Eagle in 2010 collected 209 rock grab samples from several historical gold occurrences on the ANT 1, ANT 3, TAN 1, Felsic 1 and FAY 2 claims, plus 34 channel samples totalling 33.6 m (Table 9.1). Eight 10-kg till samples and 149 250-g soil samples were also collected from the TAN 1 claims. The surface rock samples and the soil samples were assayed only for gold. The 10-kg till samples were processed for gold grain extraction.

Table 9.1 - Summary of the 2010 regional prospecting results

Category/Claim	ANT 1	ANT 3	TAN 1	Felsic 1	FAY 2
Rock samples					
Channels				3	
Channel length (m)				33.6	
Channel intercept (g/t gold over length)				3.0 g/t over 6.2 m	
Channel samples*				34	
Surface rock samples	51	1	28	113	16
Highest assay (g/t gold)	27.90	0.57	4.34	24.00	5.47
Soil and till samples					
250 g soil samples			149		
Highest assay (g/t gold)			0.117		
10 kg till samples			8		
Highest gold grain count			6		
**No duplicates, blanks or standards were submitted with the samples*					

Prospecting results obtained within the ANT 1 claim led to follow-up drilling in 2011 in the area of the Noel showing. The Felsic 1 and FAY 2 claims are located at the eastern end of the Meliadine property and follow-up field work is still recommended.

Field work between July and September 2011 consisted of collecting grab and till samples from the Felsic 1 and FAY 2 claims (Table 9.2).

The surface rock samples were assayed only for gold. The 10-kg till samples were assayed for gold and arsenic.

Table 9.2 - Summary of the 2011 regional prospecting results

Category/Claim	Felsic 1	FAY 2
Rock samples		
Surface rock samples	55	32
Highest assay (g/t gold)	6.47	6.81

Till samples		
Till samples	65	32
Highest assay (g/t gold)	4.47	0.68
Highest assay (ppm arsenic)	2,680	943

With these encouraging results obtained at surface in 2010-2011 within both claims follow-up drilling was recommended.

In 2012, 380 samples were collected from boulders on the SHR and CWM claims during a prospecting program. No significant assay results were returned. The highest assay value was 2.4 g/t gold from an iron formation boulder.

Considering that large areas of high magnetism on the SHR claims are entirely covered by glacial overburden, the next exploration step for this area would be to complete a till and boulder sampling campaign using a north-south grid to cover the entire SHR claims area..

In 2013, 675 of rock samples were collected during the prospecting of 17 areas of the Meliadine property (Figure 9.1 and Table 9.3). The areas tested were located well away from the known deposits. The campaign consisted of prospecting traverses over areas of anomalous geophysics, which are often associated with poorly-defined historical gold occurrences. Selective rock sampling was completed and geological information was compiled in an effort to better define the geological context of the areas with the aim to validate drill testing on promising regional targets. Detailed channel sampling for a total of 80 samples was done on key outcrops in the Aklak area. Follow-up exploration work is recommended for Peter Lake, Wolf, Southeast Discovery, Snowgoose and Tonic areas.

Table 9.3 - Summary of the 2013 regional prospecting results

2013 prospecting campaign		
Area name	**Rock samples**	**Highest gold assay (g/t)**
Airaq	67	1.64
Aklak	35	31.20
Carriere R-14	6	0.03
Discovery	4	2.11
Naluit Narrows	5	0.03
Peter Lake	108	53.10
Savanah	23	3.03
Snow Goose	35	14.75
South Discovery	19	0.39
South F-Zone	7	0.03
Southeast Discovery	33	17.95
Tonic	42	31.30
Ukpik	74	34.20
Ukpirniq	160	65.60
Upper 55	1	0.03
West Orion	27	8.61
Wolf	29	14.35
Total samples	675	

Table 9.4 - Summary of 2013 channel sampling at Aklak area

AKLAK area – 2013 channel sampling			
Channel name	**length (m)**	**Rock samples**	**Highest gold assay (g/t)**
CH13-001	1.0	1	0.03
CH13-002	1.0	1	0.03
CH13-003	6.0	6	0.28
CH13-004	1.0	1	0.03
CH13-005	1.0	1	0.03
CH13-006	1.0	1	0.73
CH13-007	5.0	5	0.51
CH13-008	1.0	1	1.56
CH13-009	1.0	1	0.89
CH13-010	1.0	1	0.03
CH13-011	1.0	1	0.03
CH13-012	2.0	2	0.03
CH13-013	3.6	4	2.78
CH13-014	0.5	1	2.74
CH13-015	6.2	8	6.36
CH13-016	5.4	7	10.35
CH13-017	5.5	6	4.41
CH13-018	5.2	5	0.68
CH13-019	3.6	5	0.91
CH13-020	4.2	5	2.17
CH13-021	2.6	4	0.47
CH13-022	2.4	3	0.03
CH13-023	2.8	4	0.67
CH13-024	4.6	6	0.84

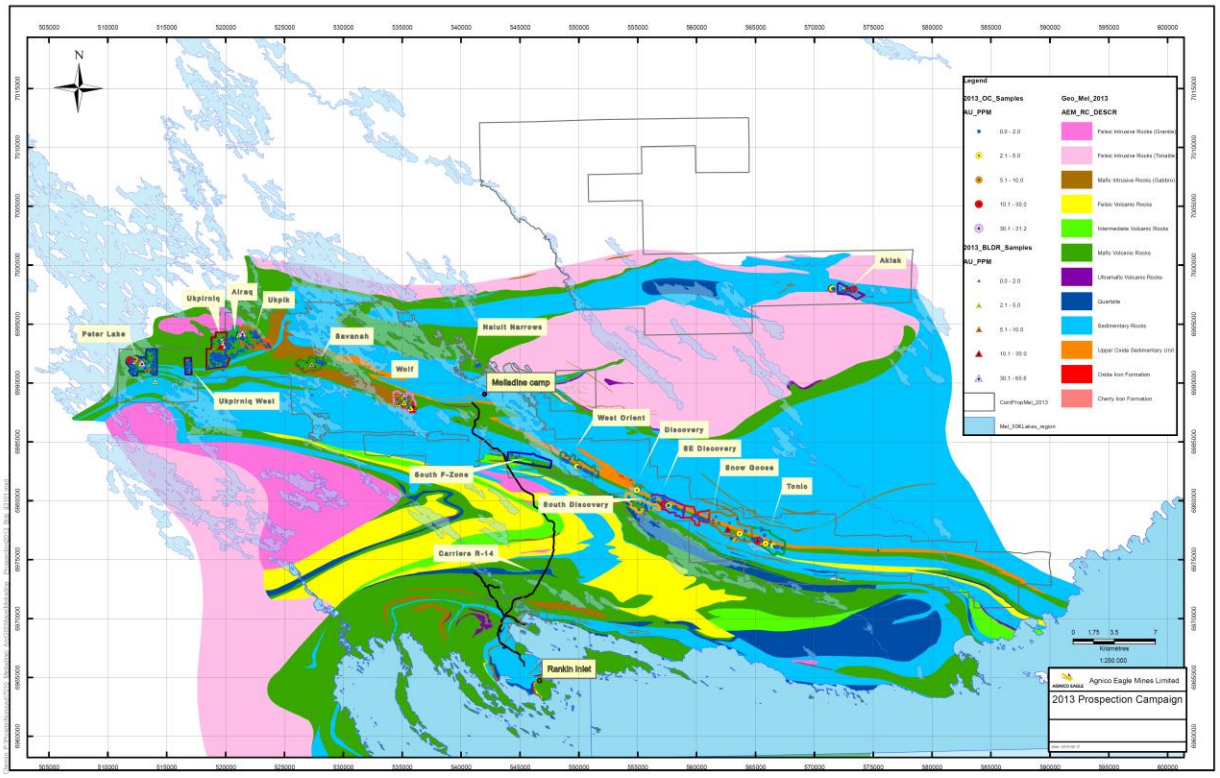


Figure 9.1 - Meliadine property showing location of known showings as of year-end 2013

In early 2014, the property area was increased substantially with the signing of NTI exploration agreements RI-01-0001 (Raptor area) and RI-12-0001 (Mustang and Road areas). During 2014, 248 surface rock samples were collected during prospecting within and around these new parts of the Property (Table 9.5, Figure 9.2). The campaign consisted of boulder sampling and geological characterization focused on geophysical anomalies revealed in the 2014 VTEM airborne survey, in order to determine future diamond drill targets. Follow-up diamond drilling was completed during the summer period in the Raptor and Mustang areas.

Table 9.5 - Summary of the 2014 regional prospecting results

Category/Claim	AANDC lease	Mustang	Raptor	Road
Surface rock samples	58	30	62	98
Highest assay (g/t gold)	14.40	0.24	0.77	10.80

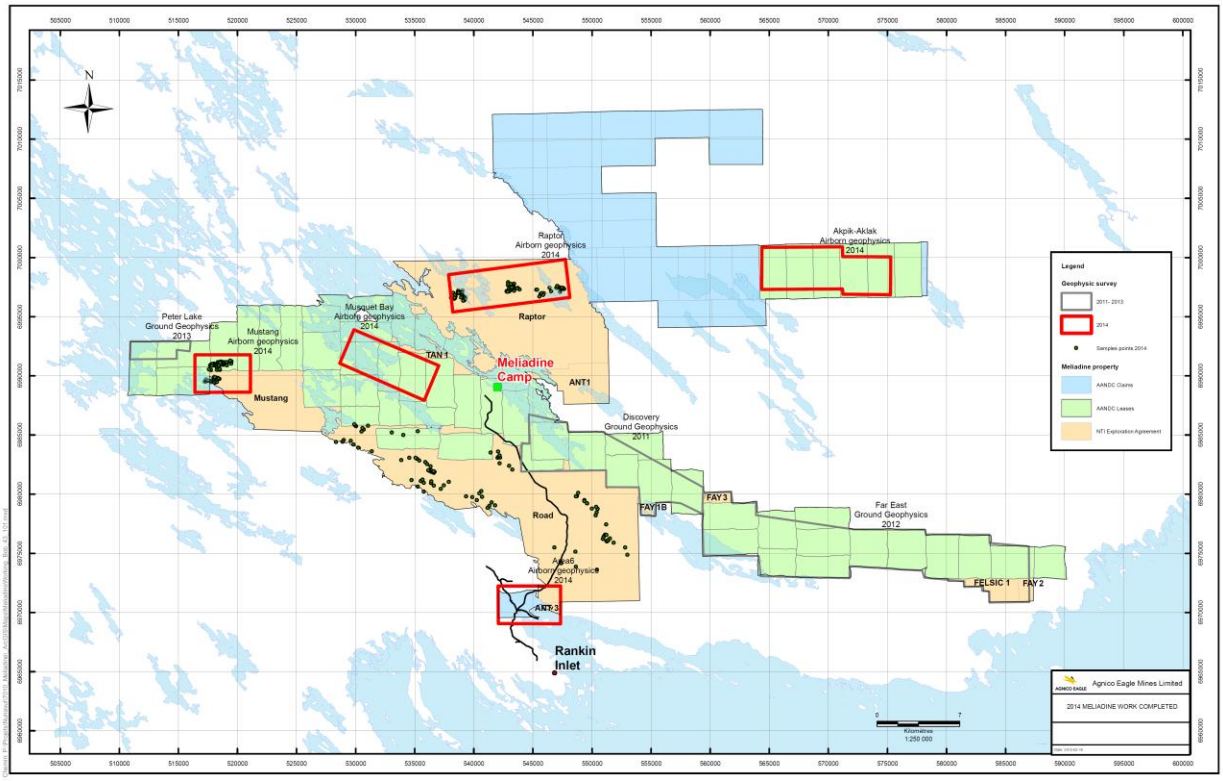


Figure 9.2 - Exploration work completed in 2014 including surface rock samples and geophysical surveys

9.2 Ramp

In November and December 2013, Agnico Eagle rehabilited the portal of the underground development that had been used to take bulk samples from the Tiriganiaq deposit in 2008 and 2011, in order to start an exploration ramp (Figure 9.3). This ramp, located in the Tiriganiaq footwall, will provide geological information on the Tiriganiaq 900 (Normeg zone) mineralization and will allow more efficient and cost saving underground conversion and exploration drilling.

During 2014, the company developed 1,363 m of ramp in mafic volcanic rock of the Wesmeg Formation, which hosts the Normeg deposit (Figure 9.3). Mapping and sampling is done regularly as the ramp progresses, and the ore 3-D model is adjusted.

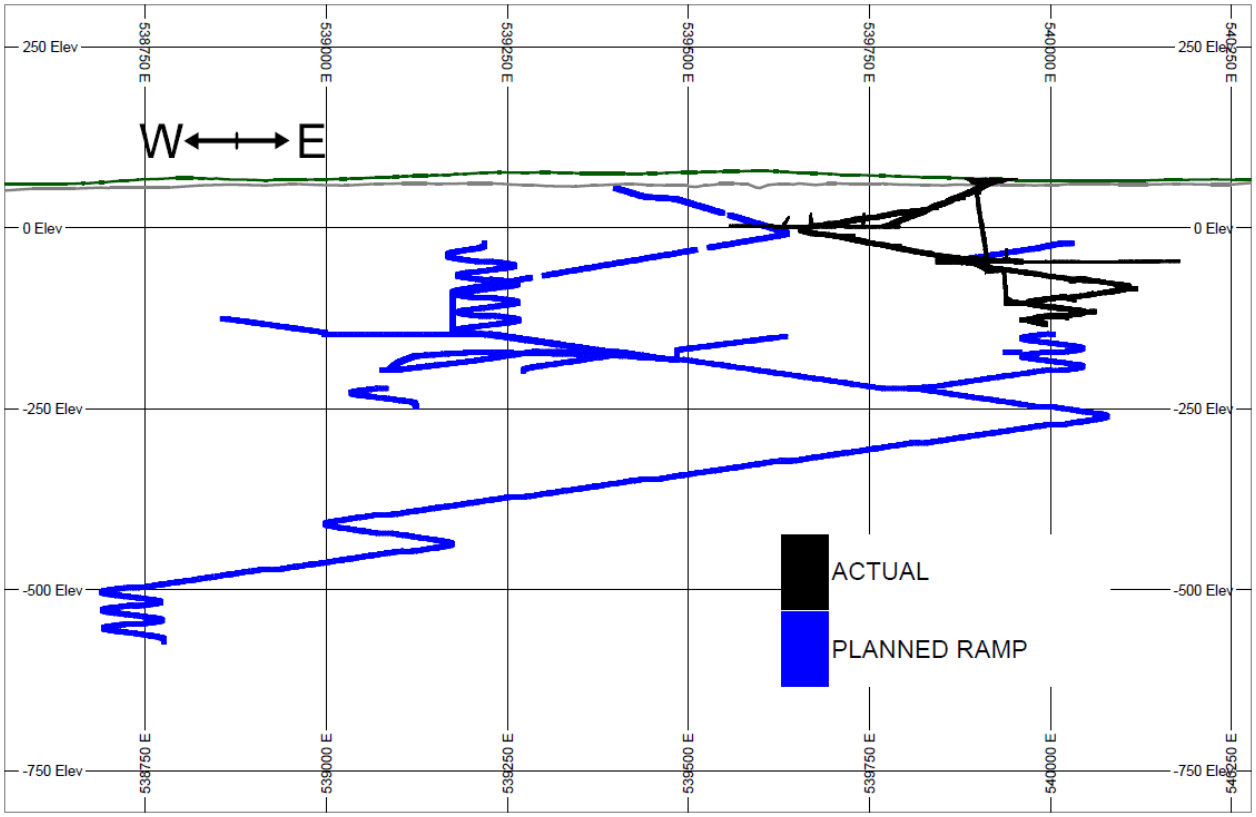


Figure 9.3 - Long section view looking to the north, showing the actual exploration ramp development to the end of 2014, and the future plans for the ramp. The elevations are in metres above sea level.

9.3 Geophysical surveys

In March 2011, a 919.8 line-kilometre ground magnetometer survey was completed along a 20-km east-southeast-trending area that ranged from 2 km to 5.5 km wide. This survey was designed to extend the high-resolution magnetic coverage to the south-east from the existing (historical) data to beyond the Discovery occurrence (Figure 9.2). The survey was successful in obtaining high resolution data to follow up previously generated airborne magnetic data.

During April and May 2012, 1,407 line-kilometres of ground magnetometer surveying was completed along a 28-km east-southeast trending area that ranges from 3.5 km to 5.5 km wide. This survey was designed to extend the high-resolution magnetic coverage east of the 2011 survey to almost the eastern extremity of the Meliadine property (Figure 9.2). The purpose for this surveying was to provide better resolution of anomalous features detected in airborne magnetics to aid with the ongoing regional exploration program.

During May 2013, 78.8 line-kilometres of ground geophysics consisting of Total-field MAG and Horizontal Loop Electromagnetic (MaxMin I, HLEM) surveys was completed in the Peter Lake

area (Figure 9.2). Results indicate a series of narrow linear magnetic anomalies oriented mostly east-west. As well, at least seven conductive trends were mapped.

During June 2014, 1,352.6 line-kilometres of helicopter-borne geophysics consisting of horizontal gradiometer MAG and versatile time domain electromagnetic (VTEM) surveys was completed in five areas throughout the Meliadine property, as indicated in Figure 9.2. The results from this survey were the focus of the limited prospecting completed during the summer of 2014; three exploration drill-holes were completed in 2014 on anomalous features detected by this survey.

Item 10. Drilling

Drill core and two underground bulk sample campaigns make up the sole sources of data for the current mineral resource estimate. Information in this section has been updated from Agnico-Eagle (2011).

10.1 Type and extent of drilling

In July 2010, Agnico Eagle acquired 100% interest in the Meliadine property from Comaplex. During the year, 209 holes (34,112 m) were drilled on the Meliadine property of which 15,447 m was drilled by Comaplex before July 7 and the rest drilled by Agnico Eagle after this date. Of the total, Tiriganiaq received 63% of the drilling, F zone 19%, Wolf 11% and Wesmeg 4%. The other 3% of drilling was geotechnical and twinned holes.

The diamond drilling at the Meliadine project from 2011 through 2014 is summarized in Table 10.1.

Table 10.1 - Summary of diamond drilling at Meliadine from 2011 through 2014

	2011		2012		2013		2014	
Meliadine DDH	**metres**	**# holes**	**metres**	**# holes**	**metres**	**# holes**	**metres**	**# holes**
Geotechnical	2,313	28	826	68	1,749	40	448	35
Tiriganiaq*	40,091	130	48,777	114	15,124	45	7,922	25
Condemnation	15,353	74	-	-	-	-	5,115	25
Wesmeg/Normeg	32,400	127	51,372	196	18,845	92	6,750	32
Pump	-	-	21,067	103	19,833	96	9,094	30
F zone	-	-	17,507	99	11,244	34	-	-
Discovery	-	-	5,157	11	9,506	41	1,364	3
Wolf	9,974	35	-	-	-	-	4,954	17
Regional exploration	4,405	18	1,904	12	5,414	35	2,032	15
Annual Total	**104,536**	**412**	**146,610**	**603**	**81,715**	**383**	**37,679**	**182**

** In 2014 the Tiriganiaq drilling includes 15 underground drill-holes (3,317 m)*

10.2 Drill-hole locations

A plan of drill-hole locations for all deposits in West Meliadine is shown in Figure 10.1 and for the Discovery deposit in Figure 10.2. Representative drill cross sections for Tiriganiaq-Normeg-Wesmeg, Discovery, F zone, Pump and Wolf deposits respectively are shown in Item 7 (Figure 7.4 and Figure 7.5, Figure 7.7, Figure 7.8 Figure 7.9 and Figure 7.11).

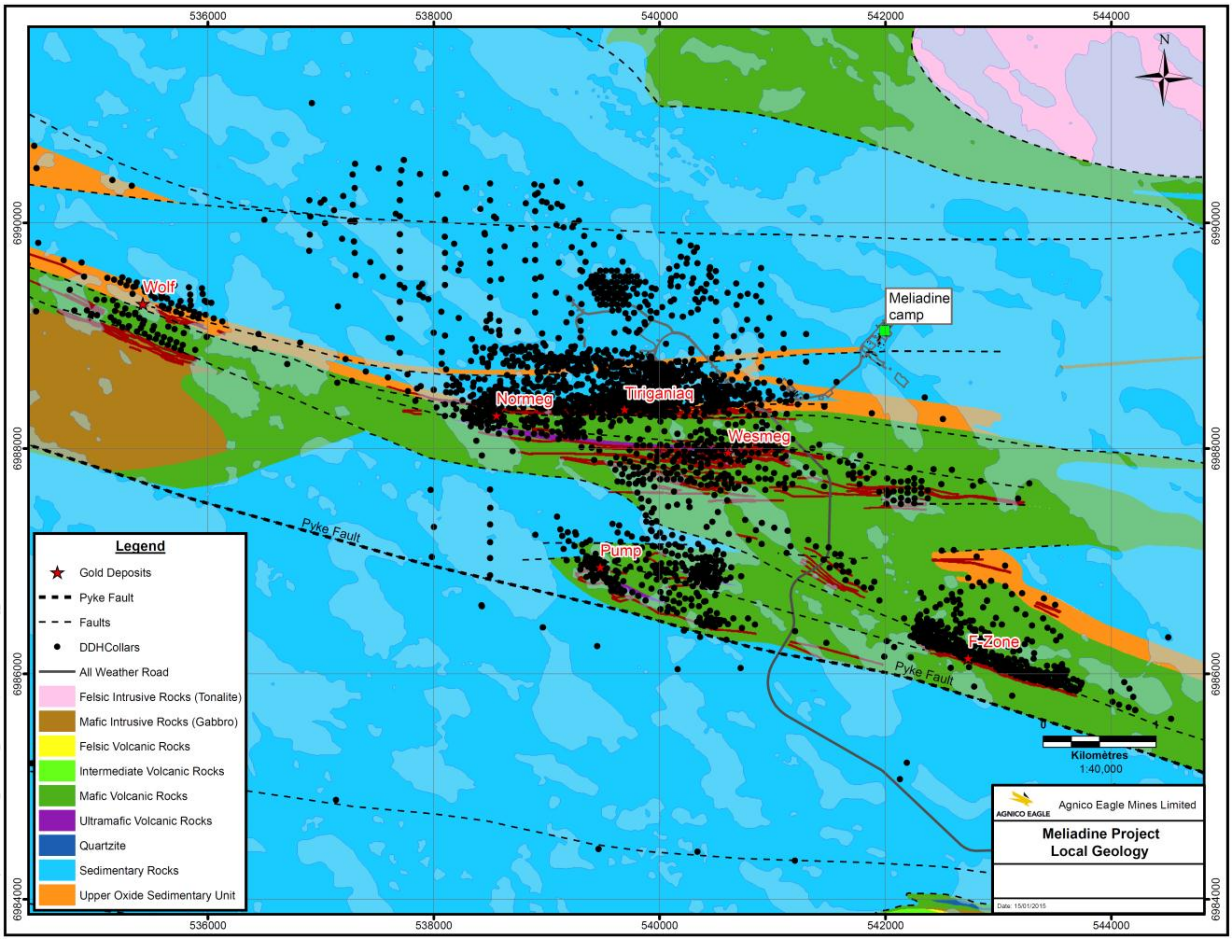


Figure 10.1 - Location of drill-hole collars in the West Meliadine area.

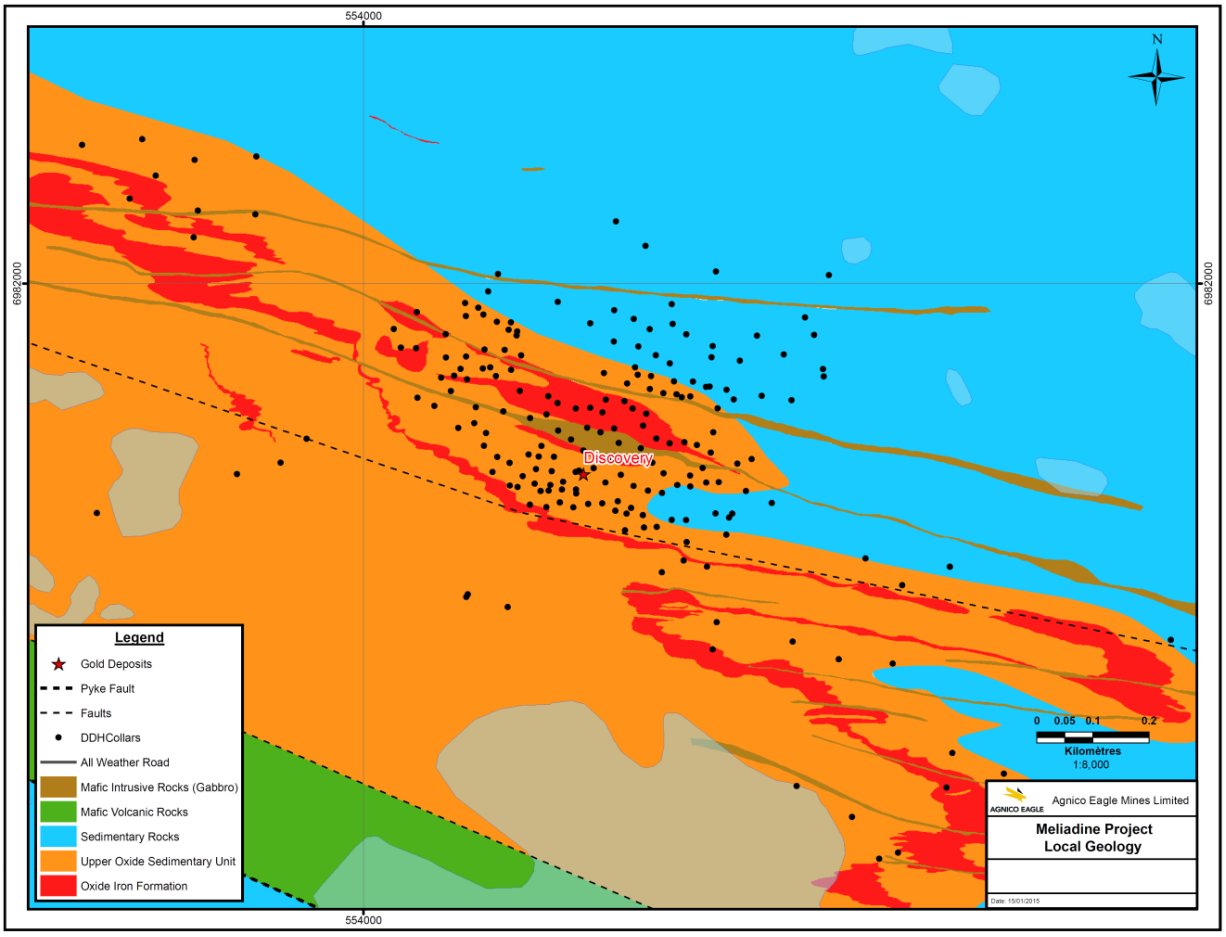


Figure 10.2 - Location of drill-hole collars at the Discovery deposit

The collar coordinates for each hole drilled between 2011 and 2014 are given in Appendix 10.1. The collar locations for previous drilling are given in Appendix A of Snowden (2010) and Appendix C of Agnico-Eagle (2011).

A list of all drill intercepts from 2011 to 2014 that were used in calculating mineral resources and reserves is given in Appendix 10.1.

10.3 Drilling procedures

10.3.1 Core size and drill-hole spacing

Almost all of the drilling completed on the Meliadine gold project has been diamond drilling of NQ size (47.6 mm core diameter).

Average drill-hole spacing for each deposit is given in Table 10.2. For all deposits, drill-hole spacing increases with depth and at the peripheries of the deposits.

Table 10.2 - Drill-hole spacing at the Meliadine project

Deposit	Strike Spacing (m)	Dip Spacing (m)
Tiriganiaq	25 - 40	15 - 40
Discovery	30	30 - 40
F zone	15 - 25	20 - 40
Pump	30 - 60	30 - 60
Wolf	50	60 - 80
Wesmeg/Normeg	30 - 60	15 - 70

10.3.2 Drill-hole collar surveys

Conventional survey techniques were used to locate drill collars at the Discovery, F zone, Pump and Wolf deposits prior to 1997. Since then, differential GPS systems have been used at all deposits.

Collar locations for all holes drilled in 2009 and 2010 were surveyed by Comaplex personnel (and later Agnico Eagle personnel) using a Trimble R8 GNSS Differential GPS system, except at Discovery where collar surveys in 2009 were done by Meliadine Resources (a private subsidiary of Comaplex). Collar locations for all holes drilled in 2011, 2012, 2013 and 2014 were surveyed by Corriveau Jean Luc Arpenteur Géomètre personnel using a Viva Leica GS 15. Once a hole was cased and drilling had commenced, three points on the drill rod were surveyed using a Nikon DTM-362 Total Station before 2011, and using a TS-15 Total Station starting in 2011. Accurate collar azimuth, dip, and collar location were thus calculated. Underground collar locations drilled in 2014 were surveyed by CMAC surveyor.

10.3.3 Downhole surveys

Not all drill-holes on the project have had complete downhole surveys. In some cases with historical drill-holes, only planned or projected bearings and dips were entered into the database. In 2004, Comaplex applied an azimuth correction factor to any unsurveyed drill-holes as well as Tiriganiaq drill-holes for which only dip information was available. Although this gave only an approximation of the true location of the hole, it was considered a more realistic approach than ‘straight lining’ the drill-hole path based on the collar azimuth information alone. Downhole surveys and collar locations were shifted for a small number of other drill-holes which were believed, based on intersections of well-known marker horizons, to be incorrectly surveyed.

Drill-holes have been surveyed using one of four instruments.

The Reflex Maxibor II instrument collects highly accurate readings relatively closely spaced (usually between 1.5 m and 6.0 m) by calculating the spatial coordinates along the drillhole path based on optical measurements of direction changes and gravimetric measurements of dip changes. The non-magnetic measuring principle allows for use in magnetically disturbed rock or inside drill rods.

The Reflex GYRO is the most technologically advanced survey tool used on the project so far. It provides accurate directional data (azimuth and dip) at any interval and in multi-shot mode. An accurate collar survey with azimuth orientation is preferable when using this instrument for enhanced accuracy down the hole. The instrument’s readings are not affected by magnetic interference, and it is used inside all types of drill rods and/or in magnetically disturbed ground.

The Light Log uses a completely different borehole surveying technique based on a light source in one end of a long rigid tube, with the light beam focused on a target in the other end of the tube. Bending of the tube as it moves in the borehole causes deflections of the light on the target, and this information is converted into borehole orientation survey data. The technique is not affected by magnetic fields and can be used inside metal pipes or drill rods. The light log was not used frequently.

The Reflex EZ-Shot is used frequently and collects a single shot at a depth determined by the operator. The instrument is lowered into the rod string (using the wire line), and goes through the bit to allow an azimuth reading as well as a dip reading. The azimuth reading can be affected by magnetically disturbed ground in some cases.

Table 10.3 gives the approximate percentage of holes that were surveyed at each deposit from 1990 through 2010 using the various borehole surveying devices. Forty-seven percent of the holes in the database were surveyed using the multi-shot downhole survey method which is unaffected by magnetic fields. The instruments used for this were the Reflex Maxibor II, the Reflex Gyro or a Light Log. The results obtained from these instruments should provide accurate three-dimensional plots of the drill-hole path.

Table 10.3 - Summary of downhole surveys at the Meliadine project with approximate percents for the period 1990 through 2010

Deposit	Number of Holes Drilled*	Approximate % Holes With Downhole Tests (All types)	Approximate % Holes With Downhole Surveys (Multi-shot)
Tiriganiaq	740	95%	60%
Discovery	196	89%	24%
F zone	210	96%	34%
Pump	59	98%	14%
Wolf	87	98%	45%
Wesmeg	44	98%	17%
Total	**1,336**	**95%**	**47%**

**Excluding holes from the Regional exploration project*

In 2011, 73% of holes longer than 250 m and 29% of holes shorter than 250 m were surveyed using the Reflex GYRO or Reflex Maxibor II. In 2012, 90% of holes longer than 250 m and 36% of holes shorter than 250 m were surveyed using the Reflex GYRO (Table 10.4).

Table 10.4 - Summary of downhole surveys at the Meliadine project with approximate percents for the period 2011 through 2014

Deposit name	Number of Holes Drilled*	Approximate % Holes with Downhole Tests (All types)	Approximate % Holes With Downhole Surveys (Multi-Shot)
Tiriganiaq	-314	100%	84%
Discovery	-55	100%	68%
F zone	-133	100%	59%
Pump	-229	100%	53%
Wolf	52	100%	83%
Wesmeg/Normeg	447	100%	65%
Total	**1 230**	**100%**	**68%**

**Excluding holes from the Regional exploration project*

From 2011 through 2014, the protocol has been to have a multi-shot downhole survey in holes longer than 200 m when field logistics allowed.

In 2013, 94% of holes longer than 250 m and 20% of holes shorter than 250 m were surveyed using the Reflex GYRO (the geotechnical holes for overburden study are not included). In 2014, 92% of holes longer than 250 m and 10% of holes shorter than 250 m were surveyed using the Reflex GYRO (the geotechnical holes for overburden study and the underground drill-holes are not included).

Fifty-six percent of the gold ounces contained in proven or probable reserves or indicated resources in the current estimate are within 200 m of the surface, where drill-hole deviations are considered minimal (Absalov, 2000). Downhole surveys have been done on the majority of the Tiriganiaq holes below the pit bottom; therefore the drill-hole deviation is considered to only have a moderate impact on the classification of the reserve and resource estimate at the probable and pndicated levels of confidence. Continuation of the downhole surveying of all future drill-holes is recommended in order to refine the drill-hole deviation database, to gain confidence in the position of mineral reserves and resources, and to enable improved targeting of mineralized zones at depth.

10.3.4 Core logging

The core is logged in detail using standardized codes for lithology, alteration, veins and mineralization. The information is stored in DHLogger developed by Century Systems. Criteria for sampling intervals of interest are based on visual interpretations related to the presence and quantity of silica/quartz veins, sulphides (arsenopyrite, pyrrhotite, sphalerite, chalcopyrite and galena), sericite alteration and visible gold, as well as rock types considered as being favourable mineralization hosts, such as iron formation or massive quartz veins, and 3D modelling. Continuous core samples are taken in visually mineralized or altered zones in sample lengths varying from 0.5 m to 1.5 m, with most samples being 1.0 m in length. Care is taken to restrict individual samples to a single major rock type and not across rock-type boundaries.

Core recovery is excellent at approximately 99.5%. Most core loss occurs near the bedrock-overburden interface, which does not affect the resource calculation. Rock quality designation (RQD) has been recorded since 2004.

10.3.5 Core storage

All remaining drill core from the F zone, Pump, Wolf, Wesmeg, Normeg and Tiriganiaq deposits is stored on site at or near the Meliadine camp; drill core from the Discovery deposit drilled before 2010 and reconnaissance on the former Meliadine East property is stored at the former Discovery camp site. More recent drill core (2012-2014) from the Discovery deposit is also stored on site at or near the Meliadine camp.

10.3.6 Relationship between core length and true thickness

Most drill-holes are inclined at angles of between 45º and 85º to the south. A former owner of the property, WMC, completed several drill-holes parallel to the strike of the zones (to the west) to test geological interpretations. Generally, however, drill-hole azimuth angles have been approximately perpendicular (±20º) to the east-west strike of the lodes. Lode intersection

thickness in the drill-holes is considered to approximate the true lode thickness for the majority of the drilling. This is due to the shallow dip of the near-surface drill-holes and the flattening of the steeper drill-holes at depth, becoming closer to perpendicular to the steep dip of the lodes.

10.4 Underground bulk sample campaigns

In 2011 Agnico Eagle undertook an additional bulk sample to gain greater confidence in the predictability of the Tiriganiaq mineralization (Duquette and Thalenhorst, 2012). Agnico Eagle's 2011 bulk sample program commenced in July and was completed in November. The sampling data and results are given in Table 10.5 and Table 10.6, respectively.

Table 10.5 - Underground development and bulk sampling completed in 2011

Opening	Nominal Size	Length	Bulk Sampling		Underground Sampling		
	Width x Height (m)	(m)	Tonnes	Number of Rounds	Muck Samples	Chip-Panel Samples	Channel Samples
Development on 10,000 Level							
1050 Lode Drift	5 x 2.8	23	1,040	14	88	63	26
1100 X-Cut	4 x 2.8	15	672	8	62	30	14
1100 Lode Drift	5 x 2.8	57	2,741	31	172	212	99
Development on 9,950 Level							
1000 Lode Drift	4 x 2.8	100	3,111	46	277	203	100
1000 N X-Cut	4 x 2.8	21	585	9	56	40	20
Clean-Ups			11		33		
Total Both Levels		**216**	**8,161**	**108**	**688**	**548**	**259**

Table 10.6 - Comparison of block model and 2011 bulk sample results

Lode and (Level)	Block Model				Bulk Sample		
	Drill-holes	Tonnes	Grade (g/t gold)	Ounces (gold)	Tonnes	Grade (g/t gold)	Ounces (gold)
1000 (9,950 L)	23	5,984	17.4	3,348	4,890	18.5	2,906
1100 (10,000 L)	27	6,652	9.7	2,083	6,396	9.6	1,981
1000 (10,000 L)	19	605	9.0	175	649	2.7	56
Low-grade (both levels)	58	6,917	0.9	206	6,816	1.3	274
Subtotal 2008	127	20,158	9.0	5,811	18,751	8.7	5,217
1000 (9,950 L)	20	2,391	9.4	720	2,158	10.0	691
1100 (10,000 L)	13	2,555	14.0	1,149	2,415	16.7	1,298
Low-grade (both levels)	77	2,207	5.0	352	2,169	2.3	161
Subtotal 2011	110	7,153	9.7	2,221	6,743	9.9	2,150
Total	**237**	**27,311**	**9.1**	**8,032**	**25,527**	**9.0**	**7,367**

In preparation for the 2011 bulk sample program, the areas were sampled by diamond drilling on 15-metre spacings. Each development round was also sampled individually through the on-site sampling tower, and the samples were shipped to an independent laboratory for assaying. The results of the program were compared with the December 31, 2011 reserve and resource estimate.

Agnico Eagle stockpiled the 2011 bulk sample mineralized material and named it as "proven mineral reserve".

10.5 Density Determinations

Minimal density determinations have been made during the different exploration programs at Meliadine. Comparisons between the drillhole density determinations and the bulk sample data (Strathcona, 2009; Duquette, and Thalenhorst, 2012) were in close agreement, validating the densities used in the resource estimate. Following the recommendations of the Snowden (2010) report, Agnico Eagle increased the number of spatially and geologically representative density determinations during the 2012 drilling campaign for F zone, Pump and Wesmeg deposits, and during the 2013 drilling campaign for Discovery deposit. Approximately 7,095 samples had been measured following appropriate QA/QC protocols (Table 10.7). The density measures were all done on pulps by pycnometer.

Table 10.7 - Number of measures for specific gravity ("SG") assignments

Deposit	Lithological unit	Agnico Eagle samples	Comaplex samples	Total SG samples
Tiriganiaq	aUa	-	3	3
	K	-	662	662
	L	-	12	12
	M	-	134	134
	N	-	161	161
	Q	-	21	21
Discovery	Ks-wa	1	-	1
	Kwa	1	-	1
	Kwa-s	11	-	11
	Mg	2	-	2
	N_N	1	65	66
	N_Nlj	1	-	1
	N_Nlm	3	-	3
	Nlj	7	-	7
	Nlm	2	-	2
F-Zone	aUa	2	-	2
	L_Llj	65	43	108
	Ll	40	-	40
	Llj	28	-	28
	Llm	18	-	18
	M	4	9	13
	Mb	4	-	4
	MV	777	-	777
	Q	-	10	10
	QQ	-	10	10
	Uv	5	-	5
Pump	lb	19	-	19
	Mb	149	-	149
	MV	630	-	630
	Mg	14	-	14
	Ub	4	-	4
	Q_Qak	5	-	5
	L	57	17	74
	Llj	82	-	82
	Llm	33	-	33
	L_Ll	48	-	48
	L_Llj	52	-	52
	L_Lmj	32	-	32
	L_Lml	5	-	5
Wesmeg	K_Kmg	2	-	2
	Kmg	2	-	2
	Ks	20	-	20
	Kwa-s	67	-	67
	L_ljm	7	-	7
	L_Ll	216	-	216
	L_Llj	19	-	19

	L_Llm	98	-	98
	Ll	122	-	122
	Llj	57	-	57
	Llm	356	-	356
	M_M	3	-	3
	M_Mv	190	-	190
	M	9	-	9
	Mb	551	-	551
	MV	2,910	-	2,910
	Mg	64	-	64
	U	27	-	27
	Ub	15	-	15
	Uv	217	-	217
	N_Nlj	33	-	33
	Nlj	33	-	33
	Q_Q	4	-	4
Wolf	L	-	92	92
TOTAL		**7,095**	**1,239**	**8,334**

10.6 Results and interpretation

The 2011 bulk sample program confirmed, within expected precision, the resource estimation model that had been developed for the two principal lodes (lodes 1000 and 1100). The sampling results indicated approximately 8% less gold than was predicted by the block model for these areas. Densities used in the previous resources exercise were validated and supported by the 2011 bulk sample program

The program also confirmed the previous assessment of the Company's block model in terms of grade continuity, consistency and distribution, and the evaluation of related mining properties through geological mapping, underground chip-, channel- and muck-sampling, and geotechnical observations (Agnico-Eagle, 2012a).

By 2012, more than two-thirds of the Tiriganiaq drilling was targeted below 350 m to test the continuity of ore shoots at depth. Work in 2013 focussed on improving the geological model of the largest deposits, and converting inferred resources into indicated resources. 2014 was a milestone year, because the rehabilitation and extension of the exploration ramp allowed the completion of the first underground drill-holes.

The main objective of the 2012 drilling campaign at the Discovery deposit was to become familiar with the geological setting and expand the mineral resource envelope. Drilling in 2013 succeeded in better defining the deposit.

Intensive conversion and exploration drilling was carried out at the F zone in 2012 and 2013, with a large portion of the drilling also targeting the extensions at depth of the inferred resources.

Pump was another site of intensive conversion and exploration drilling in 2012 to confirm the resources and explore for near-surface gold mineralization. Almost 25% of the entire 2014 drilling program was allocated to exploration close to surface and at depth on the Pump deposit. Highlights of this campaign include intercepts of 25.3 g/t gold (uncapped) over 5.7 m and 9.5 g/t gold over 4.1 m core length.

Agnico Eagle’s interpretation of the detailed magnetic features of the Wesmeg area, south of the main Tiriganiaq deposit, led to a large drilling campaign in 2011 totalling 32,400 m. Follow-up drilling in 2012 was mainly to convert the inferred pit resource to an indicated resource. The

2013 drilling targeted deep interesting resources, and converting the shallower part of the 650 lode.

The "Normeg mineralization style" (Tiriganiaq south extension) was discovered in 2011 when drill-hole M11-1314 was intentionally extended approximately 230 m into the Wesmeg Formation south of the main Tiriganiaq lodes. During the 2012 winter program, the same style of mineralization/veining was discovered close to surface while drilling the western area of the same mafic volcanic sequence. This discovery led to additional drilling and expansion of the deposit. Conversion drilling was the main objective in 2013 and 2014. Deeper extensions of this type of mineralization were also verified.

A campaign executed in 2011 explored the Wolf area and extended the existing resource envelope. A drill program in 2014 returned with a best result 9.1 g/t gold (uncapped) over 13.0 m core length.

In the opinion of the Qualified Persons, the quantity and quality of drilling data collected by Agnico Eagle in the exploration, conversion and condemnation programs in 2011 to 2014 are sufficient to support the current mineral resource and mineral reserve estimates. Core logging, collar surveys, downhole surveys, geotechnical logging and sampling have been performed using industry-standard instrumentation. Drilling patterns and orientation are appropriate for the mineralization style. There are no significant factors that could affect the accuracy and reliability of the drill results.

The conversion and exploration success demonstrate that the lode geometries and distribution are well controlled.

Regional exploration drilling away from the main deposits has represented only 2-5% of the total metres drilled any year since 2011. The program has tested the Aquarius, Snow Goose, Orion, Noel, Aqpik-Aklak, J2, 55-Upper, Tonic, Peter Lake, Mustang and Raptor showings.

Most of the condemnation drilling has been located north of the Tiriganiaq deposit to determine if infrastructure such as buildings, mill, tailings pond, waste pads, *etc.*, could be built within this area.

Item 11. Sampling Preparation, Analyses and Security

Agnico Eagle acquired the Meliadine gold project when it acquired Comaplex on July 6, 2010, and continued the sampling protocols that had been used by Comaplex. All sampling and logging activities at the Meliadine project have been directed by Agnico Eagle since that date. The assaying protocols used by Agnico Eagle have been modified since the beginning of 2014.

11.1 Sample Preparation and security

Drill core is placed in wooden core boxes that are labelled by hole number and box number at the drill. When a core box is full it is then covered with another core box and the box and lid are secured by rubber bands made from tire inner tubes. Approximately once a day the accumulated core boxes are transported by ground transport in the winter and by helicopter during the rest of the year to the core receiving area adjacent to the core shack. The boxes are opened and the core is measured; the metreage is checked against the metre markers in the core boxes. The core is then stored until it is logged by a geologist.

After the core is logged and marked for sampling, the core samples are split longitudinally using a diamond cutting saw, in such a way that the samples shipped for assay are representative of the entire core segment. One half of the core is put back into the original boxes, which are stored on pallets at the Meliadine camp, where they are appropriately labelled and accessible for re-logging or re-sampling as required. The remaining half of the core is prepared for shipment. Individual samples are placed in heavy-duty plastic sample bags, assigned a unique sample number along with an appropriately numbered sample tag, and sealed with plastic tie wraps. The sealed individual samples are then placed in rice bags along with sample dispatch sheets. These bags are then sealed with sturdy plastic ties and individually labelled security tags for transport to the laboratory. The sealed bags are driven by road in the winter and flown by helicopter the rest of the year to M & T Trucking in Rankin Inlet.

In 2011, M & T Trucking received the sealed samples in Rankin Inlet and took them to the First Air hangar and shipped samples by air to ALS Chemex's sample preparation facility in Yellowknife, NT. Canadian North service was also used (to a lesser extent) and samples were shipped by air to Thompson, Manitoba and then transported by truck to ALS Chemex's sample preparation facility in Sudbury or Thunder Bay, Ontario.

Starting in January 2012, the First Air charter flights were used from Rankin Inlet to Val-d'Or, Quebec. Since September 2013 the Nolinor 737 charter flights (shared with the Meadowbank mine) have been used to ship samples to Val-d'Or.

All samples are received by ALS Chemex and distributed to their preparation laboratories by truck.

11.2 Laboratory protocols

Since August 26, 2010 Agnico Eagle has used ALS Chemex as the primary laboratory for all exploration samples from the Meliadine project. ALS Chemex completes the core sample

preparation at its preparation facilities in Yellowknife, Thunder Bay, Sudbury and Val-d'Or followed by gold assay analysis at its laboratory in Val-d'Or or Vancouver, BC. Check assay samples are sent to TSL Laboratories Inc. (TSL Laboratories), a secondary laboratory in Saskatoon, Saskatchewan. ALS Chemex has a quality management system and is an accredited laboratory that conforms to the requirements of CAN−P−1579, CAN−P−4E (ISO/IEC 17025:2005).

TSL Laboratories has a quality management system that has been accredited by the Standards Council of Canada as conforming to the requirements of ISO/IEC 17025. Both ALS Chemex and TSL are independent laboratories and are not associated with Agnico Eagle other than in business relationships.

11.2.1 Sample Preparation

At the ALS Chemex laboratory sample preparation facility, the sealed rice bags are inspected for tampering, and individual sample numbers are checked against the enclosed manifests. Samples are dried overnight in an oven at 110°C and then weighed. Each sample is then crushed in a standard laboratory jaw crusher, usually to a minimum of 90% passing 10 mesh (1.7 mm). A 1,000-g sample is split from the crushed material using a Jones riffle splitter. This sample is then ground to a pulp in a ring-and-puck pulverizer to 95% passing 150 mesh (106 μm). Sieve analysis checks are run on both the crushed and the pulverized samples for one sample from every furnace run. Blank cleaning media are inserted randomly between samples and after samples containing visible gold (as identified by the core logging geologist) in the pulverizing stage; the blank cleaning media are later discarded.

11.2.2 Sample Analyses

At ALS Chemex, representative aliquots of 50 g are split from the pulp and assayed using standard fire assay techniques with an atomic absorption an atomic absorption ("AA") finish. All samples with initial results of 3 g/t gold and above are re-run with a fire assay method and gravimetric finish. For each furnace run (which consists of 78 pots), 62 core samples are run with the following sixteen control samples:

- 3 external standard of 150 g (field standard);
- 3 external core blank (field blank);
- 3 external core repeat (field duplicate);
- 3 external coarse duplictaes (coarse duplicate);
- 1 internal standard of 50 g (laboratory standard);
- 1 internal pulverized blank (laboratory blank);
- 1 internal pulp duplicate (laboratory pulp duplicate);1 internal coarse reject duplicate (laboratory coarse reject duplicate).

11.3 Quality Control Measures

Agnico Eagle has followed the same sample protocol as was established by Comaplex at Meliadine. It has conducted a rigorous quality assurance/quality control ("QA/QC") program on samples collected from the 2011 through 2014 exploration and resource definition drilling

programs at the Meliadine project. The majority of samples in the digital database are from drill-holes completed at the Pump (exploration and conversion), Normeg (exploration and conversion) Tiriganiaq, and Wolf deposits, with lesser amounts from the Orion and Discovery areas of the Meliadine project.

A total of 205,103 samples from this program were assayed including 8,022 custom gold standards.

Agnico Eagle continuously monitors the results of its QA/QC sample submissions including field duplicates, coarse and pulp reject duplicates, field standards and blanks. The quality of data uploaded in the database used for resource estimation is monitored daily and reported every quarter (Saraci, 2014a,b). The following sections are an analysis of results for samples submitted from the 2011 through 2014 drill programs for the Meliadine project, in the context of precision, accuracy and contamination.

During the exploration program, 8,040 blanks, 7,440 core duplicates and 7,966 coarse duplicates were incorporated in the sample stream to monitor the precision and accuracy of sampling and assaying, and to check for human error issues such as sample mislabelling and contamination. A summary of the 2011-2014 Meliadine duplicate sample analysis is given in Table 11.1.

Table 11.1 - Summary of 2011-2014 Meliadine duplicates

Field Duplicates								
Grade Range Au g/t	No. of Samples	Mean Au g/t Original	SD Original	CV Original	Mean Au g/t Duplicate	SD Duplicate	CV Duplicate	Relative Difference %
Total (0.003– 273)	7,440	1.046	6.161	5.893	1.041	6.936	6.665	-0.46
Coarse Duplicates								
Total (0.003– 495)	7,966	1.486	8.455	5.690	1.525	9.700	6.362	2.61
Pulp Duplicates (from ALS Chemex)								
Total (0.003– 467)	23,610	1.431	7.692	5.377	1.447	7.960	5.503	1.11

11.3.1 Certified Standard Samples

During 2011-2014, Agnico Eagle submitted 8,022 field standard samples from certified standards along with Meliadine samples. The certified grades of the standards are between 2.04 g/t and 11.21 g/t gold, which are similar to the expected economic cut-off grades and the average grade of the deposit. All the independently certified standards (MLAE-2, MLAE-4, MLAE-8A MLAE-11A, MLAE12-2, MLAE12-4, and MLAE12-9) have been prepared from material sourced from the 1100 lode at Tiriganiaq. Standards MLAE-2, MLAE-4, MLAE-8A and MLAE-11A were when until 2012 until the inventory was consumed. Custom standards MLAE12-2, MLAE12-4, and MLAE12-9 have been used since then. Agnico Eagle's QA/QC program considers an assay result for a standard to have failed if it is outside a ±2 standard deviation ("SD") range of the certified value of the standard. Batches in which standard failures occurred were selected for check assaying and the entire batch or selected samples associated with the standard failures were re-analyzed at a secondary laboratory. The repeat sample results were QA/QC checked, and only acceptable assay results were used in the database. Summary data of all standards used during 2011 to 2014 exploration program are shown in Table 11.2.

Table 11.2 - Summary of QA/QC elements used in 2011- 2014.

	Calculated Values				No. of Samples	Reference Sample Data		
Standard ID	Mean Au g/t	Std Dev	CV	Mean Bias		Expected Au g/t[1]	-2SD	+2SD
MLAE-2	2.064	0.179	0.087	-0.003	638	2.07	1.81	2.33
MLAE-4	4.585	0.367	0.080	-0.025	617	4.7	4.25	5.15
MLAE-8A	8.181	0.597	0.073	-0.005	616	8.22	7.71	8.73
MLAE-11A	11.149	0.673	0.060	-0.005	631	11.21	10.34	12.08
MLAE12-2	2.022	0.252	0.125	-0.009	1,835	2.04	1.88	2.2
MLAE12-4	4.549	0.344	0.076	0.000	1,841	4.55	4.31	4.79
MLAE12-9	8.796	0.594	0.067	-0.010	1,843	8.88	8.59	9.17

[1] Certified values for the MLAE12 series of standards are based on fire assay with gravimetric finish method. The MLAE12-2 standards were assayed only by fire assay with AA finish method during 2014.

11.3.2 Blank Samples

There were 8,040 field blank control samples inserted as part of Agnico Eagle's QA/QC protocol and assayed by ALS Chemex. The exploration program at Meliadine has used field blanks that were initially gabbro material from Tiriganiaq's project site (labelled as Blank_ML) replaced later by gabbro material from the Discovery area of the project (labelled as Blank_DI) with intermittent use of a 19 mm screened material from a Val-d'Or gravel pit prepared by Fournier & Fils (labelled as STD_F).

Agnico Eagle's QA/QC program considers an assay result for a field blank to have failed if it is outside the 3x detection limit range of the method used for gold assaying, Batches in which blank failures occurred were selected for check assaying and the entire batch or selected samples associated with the blank failures were re-analyzed at a secondary laboratory. Results for check assays of the batches with anomalous blanks indicate the possibility that blank samples may contain trace amounts of gold mineralization. These results indicate that there is no significant cross-contamination or sample switching in the sampling and sample preparation process. The repeat sample results were QA/QC checked, and only acceptable assay results were used in the database. Summary data of all blanks used during the exploration program are shown in Table 11.3.

Table 11.3 - Summary data of blanks used in 2011-2014

Standard ID	Mean Au g/t	Std Dev	CV	No. of Samples
Blank_ML	0.037	0.094	2.526	6,051
STD_F	0.028	0.057	2.042	1,454
Blank_DI	0.006	0.015	2.378	533
Blank - Total	**0.034**	**0.086**	**2.554**	**8,038**

11.3.3 Duplicate Drill Core Samples (Field Duplicates)

Field duplicates are submitted to assess the precision of the entire sampling, sample preparation and analysis process. Field duplicates also provide a measure of the inherent variability of the mineralization (the "nugget effect"). At the Meliadine gold project, 7,440 field duplicates were taken by submitting the second half of split diamond drill-hole core for analysis during 2011-2014 (Table 11.1).

In order to eliminate a selection bias, the sampling procedure implemented at the Meliadine project requires that the selection of the half core duplicate is made without any bias, *i.e.* the right-hand side of the split core is selected all the time as the field duplicate.

A scatterplot was used to compare gold values from the original (first half of core) and the field duplicate (second half core) samples submitted with samples from all zones of the Meliadine project (Figure 11.1) There is no evidence from the scatterplot of any systematic bias. However, there is evidence of the nugget gold effect particularly in the highest grade range (above approximately 50 g/t gold), with large variance between original and field duplicate results and a correlation factor "r" of 0.7745.

The precision, as measured by Half Absolute Relative Difference ("HARD") value plotted against the mean of the original and field duplicate samples, for the data (above 0.1 g/t gold) collected during 2011-2014 shows that 40% of the field duplicate sample data had a precision better than ±20% or a grade relative difference of -0.46% as shown in Figure 11.2. These results indicate that sub-sampling of field duplicate samples is well controlled, with no bias and a precision level in line with the "nugget gold" type of mineralization of the deposit. The author does not consider this to affect the current resource estimate.

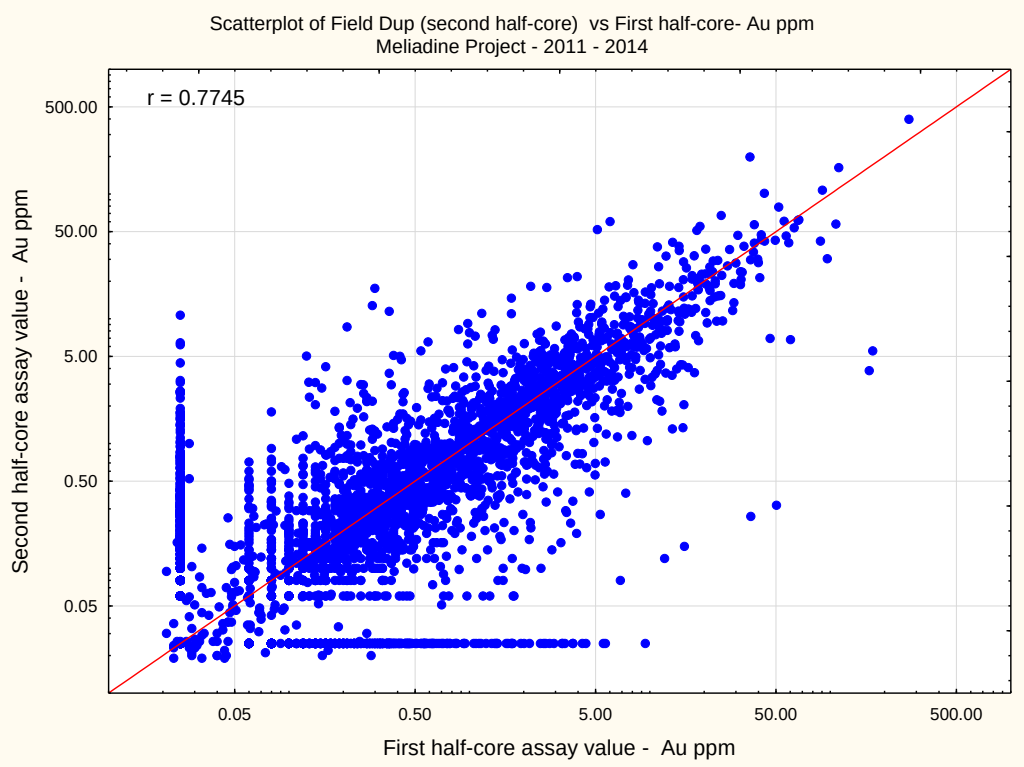


Figure 11.1 - Scatterplot of field duplicates, 2011-2014.

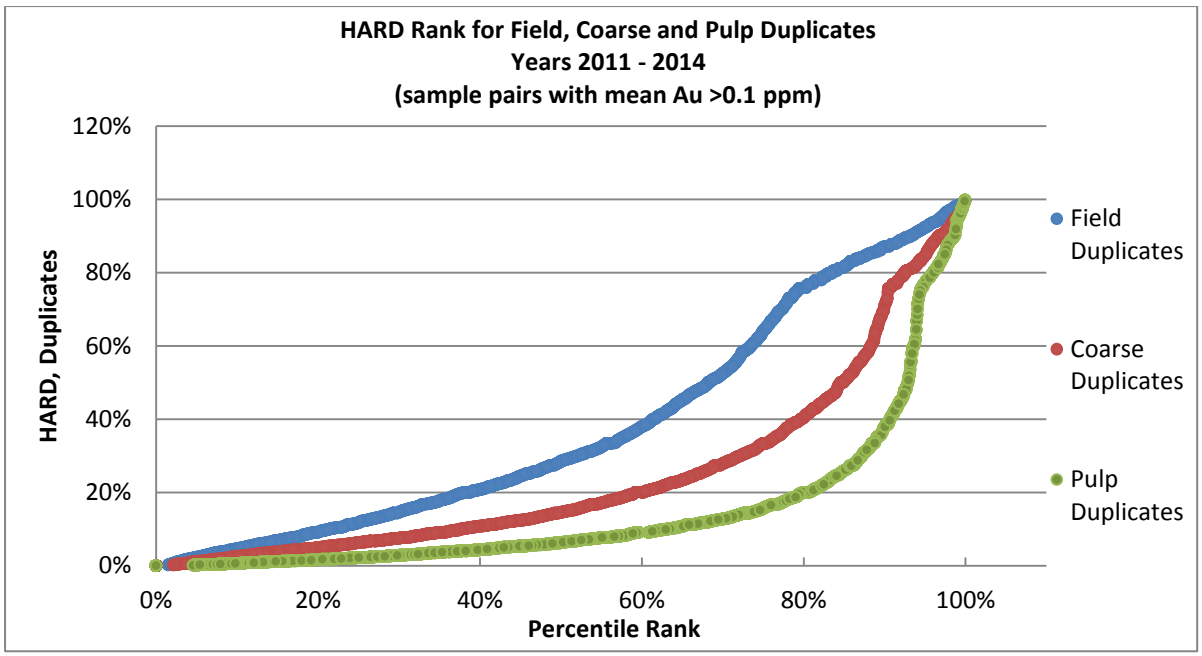


Figure 11.2 - HARD rank for field, coarse and pulp duplicates, 2011 - 2014 Meliadine project.

11.3.4 Duplicate Coarse Rejects

A total of 7,966 coarse reject duplicates were completed with Meliadine project samples at ALS Chemex as part of Agnico Eagle's QA/QC program during 2011 – 2014 (Table 11.1).

Duplicate coarse rejects are submitted to assess the precision of the crushing, grinding and the analytical process. At the laboratory, core samples from the Meliadine gold project are crushed (to a maximum size of 1.7 mm) in a jaw crusher prior to pulverizing. This crushed sample is split to produce a smaller sample for pulverizing. Analysis of a sample from the rejected portion of the coarse crushed sample (a coarse reject duplicate) provides a means for measuring the precision and effectiveness of this particular step in the sample preparation process.

Statistical analysis of the coarse reject duplicate results indicates that there is no bias between the original and duplicate data and that there is a high degree of correlation (with correlation coefficient "r" of 0.9546).

The precision, as measured by the HARD value plotted against the mean of the original and coarse duplicate samples, for the data (above 0.1 g/t gold) collected during 2011-2014 shows that 61% of the data had a precision better than ±20% or a grade relative difference of 2.61% as shown in Figure 11.2. These results indicate that sub-sampling of coarse duplicates samples is well controlled, with no bias and an acceptable level of precision in line with the "nugget gold" type of mineralization of the deposit.

A scatterplots was also used to compare the gold value from the original (first 1,000-g sample) and coarse duplicates (another 1,000-g split from the crushed sample) submitted with Meliadine project samples (Figure 11.3). These results indicate that sub-sampling of coarse crushed samples is well controlled with no bias observed between the two different populations.

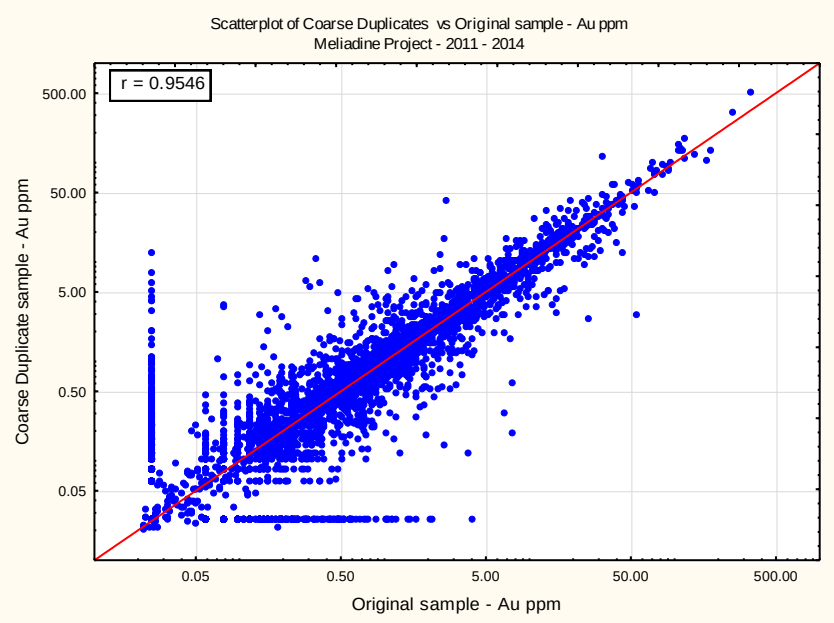


Figure 11.3 - Scatterplot of coarse duplicates, 2011-2014 Meliadine project.

11.3.5 Duplicate Pulps

Pulp duplicates are used to assess the precision of the grinding and analytical process, and comprise a second sub-sample split from the pulverized sample. The results of pulp duplicate sample grades also indicate the effectiveness of the pulverizing stage and sub-sampling of the pulverized material. ALS Chemex has assayed a total of 23,610 pulp duplicates during the period 2011–2014 with Meliadine samples.

A scatterplot was used to compare the gold values from the original (first 50-g pulp after pulverizing) and pulp duplicate samples (second 50-g pulp from the same material) from ALS Chemex (Figure 11.4). These results indicate that sub-sampling of pulp duplicate samples is well controlled with no bias observed between the two different populations.

Statistical analysis of pulp duplicate data indicates that there is no bias between the original and pulp duplicate samples and that there is a high degree of correlation (with correlation coefficient "r" of 0.9939). The precision, as measured by the HARD value versus pair mean, shows that 66% of pulp duplicates (Figure 11.2) had a precision better than ±10% or a grade relative difference of 1.11% as shown in Figure 11.4 and Table 11.1. These results indicate that sub-sampling of pulverized samples is well-controlled with no bias and acceptable precision.

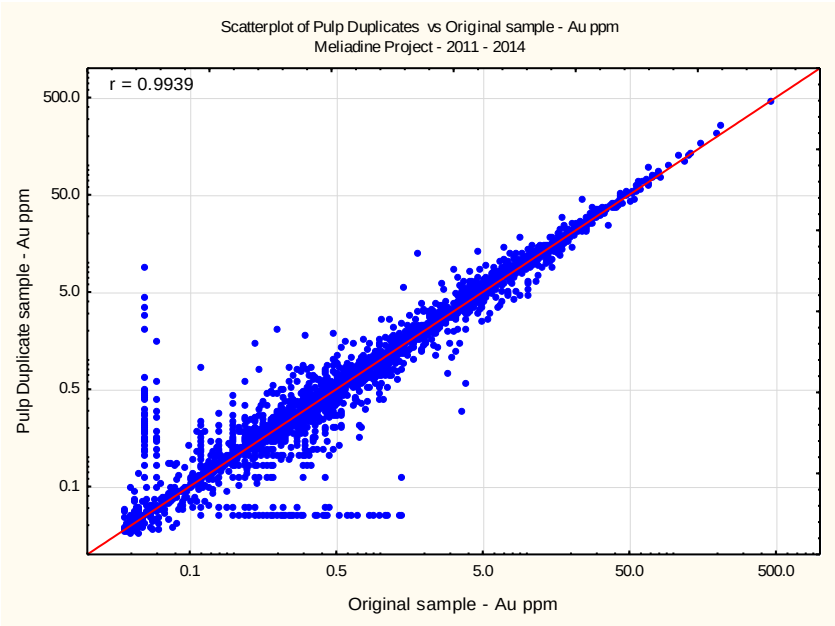


Figure 11.4 - Scatterplot of pulp duplicates, 2011-2014 Meliadine project.

The review of TSL Laboratory performed on behalf of Agnico Eagle by Analytical Solutions Ltd. in May 2010 (Analytical Solutions, 2010) concluded that the sample preparation procedures that were used by TSL Laboratory for the Meliadine samples are more rigorous than for most other Canadian projects. This may partially explain why the precision for the coarse duplicates is comparable to that for pulps.

11.4 Statement of Agnico Eagle Quality Control Samples

The quality of all samples and their representativeness correspond to Agnico Eagle standards. Since July 2010 when Comaplex and Agnico Eagle merged, Agnico Eagle geologists and technicians have continued using the procedures that had been used by Comaplex at Meliadine. These procedures were validated by Snowden Mining Industry Consultants (2009, 2010) and were verified by Agnico Eagle in 2010 (Agnico-Eagle, 2011) and 2011 (Agnico-Eagle, 2012b). There have been no independent reviews on sample preparation, analyses, and security since 2010.

During the exploration campaigns from 2011 to 2014, all results of the quality control sample blanks, standards and duplicates have been monitored and reported each quarter by Agnico Eagle personnel. Each quarter, approximately 10% of the original samples were sent for check-assaying at a secondary laboratory (TSL Laboratory) for replicate analysis with a total of 13,892 samples assayed. Correlation of all the original gold values and the check assay gold values for 2011-2014 was very good (r=0.9797) as shown in Figure 11.5.

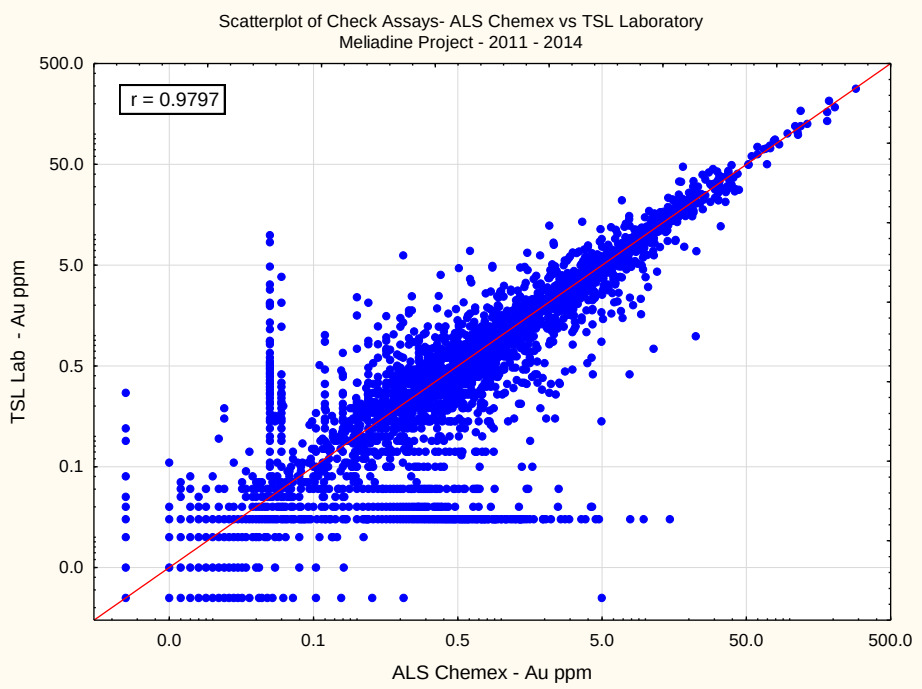


Figure 11.5 - Scatterplot and QQ scatterplot of ALS Chemex original assays *vs.* TSL Laboratory check assays, 2011-2014 Meliadine project.

Analysis of standards, blanks, field, coarse and pulp duplicates for the Meliadine project indicates that the sample preparation and analytical processes employed by ALS Chemex are appropriate, taking into account the highly variable nature of gold mineralization. The level of precision reported for each step is indicative of the highly variable nature of gold mineralization inherent to this type of deposit. This inherent variability, or nugget effect, must continue to be considered in the design of sampling protocols and in the estimation process.

Based on the QA/QC results, the author considers that the data from Meliadine gold project are reliable for use in resource estimation.

Item 12. Data Verification

12.1 Drill-hole Database

From 1993 to the end of 2010 all appropriate methods of mineral exploration were applied. A review of the historical exploration work by Western Mines Corporation (WMC) indicated all of the exploration programs appear to have been carried out by professionals to the industry standards of that time (Strathcona, 2005). Numerous reputable consultants were contracted to complete the various geophysical survey programs over the years. WMC staff reviewed this data as it was received for integration into, and interpretation of, the expanding database. Since the acquisition in 2010, rigorous verification is continually done on the Meliadine drill-hole database. Agnico Eagle verified and imported the historical drill-hole database into Fusion (a real time data management system) following the acquisition of the project. During that process, 100% of the major units and the assay data from historical drill-holes were verified and compared to the original logs. Then, 10% of the minor units, mineralization, veins and structure intercepts were verified; no major discrepancies were noted.

Since 2011, Agnico Eagle has used the Fusion CAE Mining system to manage the drill-hole data. All drill-holes at Meliadine, are logged in DHLogger, the logging software of Century System Technologies. This software alerts the user if any anomalies or discrepancies are detected such as overlaps of major rock units and/or assay sample intervals. The same alert is given for overlaps of minor rock units or in anomalies in the logged mineralization, textures, structures and veins. When deviations of drill-hole azimuths or dips exceed 10° from one reading to the next, the text automatically appears in red to alert the user, allowing the user to continue with the data entry or not. The system also disallows the overlap of assay sample intervals. Once the drill-hole is logged, the log has to be 'checked in' to a central database. The check-in process is automatically aborted if the system detects a duplicate assay sample number in the central database. This action prevents the same sample number being assigned to two different samples.

When assay certificate data are being imported into the database, an alert appears if a blank or a standard has failed. If a value in an assay certificate differs from that expected in the template, the importing process will fail. If assays are missing in the certificate, the user must choose to import or not import a partial certificate. Agnico Eagle policy prohibits the modification of any assay certificates. Assay modifications cannot be done by the user once the assay value has been imported into the database.

Prior to signing off from a log, the geologist must verify all the data entered into the log including collar coordinates, downhole survey data, major and minor units, assays, *etc*. All geologists signing off from a log must be official members of a recognized professional association.

A module of CAE Mining called "Audit Log" allows the tracking of all drill log modifications. This module is designed to ensure adherence to best practices and guidelines established for mineral resource evaluation by national and international regulatory bodies such as Sarbanes Oxley, National Instruments 43-101, JORC, SAMREC and others.

Once the database is closed for the estimation process, a report of errors describing missing deviation data, duplicates, gaps and overlaps is generated during the importation of the database into Datamine. Additionally, a visual comparison with previous drill-hole database imports is

done in Datamine software. This step rapidly highlights anomalous collar locations and drill-hole deviation traces.

12.2 Author's Opinion

The author, a Qualified Person (under NI 43-101) supervised the verification of the drill-hole database for collar surveys, down-hole orientations, lithological, sample information and assay result information found in the mineral resource model database against the original drill logs, survey records and assay certificates.

The author considers that the drill-hole database from Meliadine gold project is adequacy and reliable for use in resource estimation.

Item 13. Mineral Processing and Metallurgical Testing

To the end of 2014, more than 39 metallurgical test programs have been conducted on the Meliadine deposits to determine their physical characteristics and potential for gold recovery using various parameters. Based on the test results, a conventional gold circuit was selected comprising crushing, grinding, gravity separation and cyanide leaching with a carbon-in-leach circuit (CIL) followed by cyanide destruction and filtration of the tails.

Preliminary metallurgical testing of the Meliadine West property was performed by WMC, an earlier partner in the project. Separate test campaigns were conducted for WMC by Lakefield Research in 1997, 1998 and 2001. Composite samples came from the Tiriganiaq, F zone, Pump and Wolf deposits. Comaplex commissioned further testing in 2006 and 2007 that was performed by SGS Lakefield on composites from Tiriganiaq. In order to obtain additional metallurgical data to enable process flowsheet definition, test work was performed by Comaplex in 2009 on composites from the Tiriganiaq, F zone and Discovery deposits. The test work was interrupted in 2010 during the acquisition of the Meliadine project by Agnico Eagle, but the original program was modified and completed in 2011.

Since its acquisition of Meliadine in 2010, Agnico Eagle has managed additional metallurgical testing programs, extending knowledge of all deposits excluding Normeg which has not been tested. In 2013-2014, variability testing programs focused on the Tiriganiaq deposit as it will be the dominant source of feed for the process plant during the early years of production.

Metallurgical test work has included standard comminution tests such as the JK Drop-weight test ("DWT"), SAG mill comminution ("SMC") tests, Starkey SAG design tests, and all the Bond test series. Pilot-testing was carried out on the Vertimill technology, and high pressure grinding rolls ("HPGR") batch and locked cycle tests were also performed. Gold recovery of the Meliadine deposits was established performing different metallurgical testing programs covering all the processing steps including cyanide leaching, an Extended Gravity Recoverable Gold ("E-GRG") test and a continuous gravity amenability test ("GAT"), gravity concentrate intensive leaching, chemical reagents dosage, thickening and filtration, cyanide destruction, flotation, magnetic susceptibility and mineralogy. All sample preparation, assaying and metallurgical studies have been performed utilizing accepted industry standard practices.

Results from external metallurgical test work have been properly described and issued by: Lakefield Research (1997, 1998 and 2001); SGS Canada (2006, 2007, 2011, 2012, 2013a, 2013b, 2013c, 2014a, 2014b and 2015); Starkey Associates Inc. (2009, 2012 and 2014); Resource Development Inc. (RDi) (2009); Outotec (2011 and 2013); Golder Associates (2011); Knelson (2011 and 2013); Process Mineralogical Consulting (PMC) (2011); FLSmidth (2012); Eriez Magnetics (2012); EMSL Canada Inc. (2013a and 2013b); Air Liquide Canada (2013); Metso (2013); AMTEL (2013) and Pocock Industrial Inc. (2014). A chronological description of the test work is summarized in Appendix 13.1. A few external firms were asked to produce metallurgical studies: Strathcona Mineral Services Ltd. (2009); Wardrop (2011); Contract Support Services (CSS) (2012); BBA (2013a and 2013b) and Orway Mineral Consulting (OMC) (2013).

13.1 Sample Representativeness

Material used for the test work was obtained from different sources such as drill core samples, assay lab sample rejects, and two bulk sampling campaigns, described in Strathcona Mineral Services Ltd. (2009) and Duquette and Thalenhurst (2012). The samples were selected and subsequently blended to represent different zones and ore grades. Samples selected for testing represented the important mineralized domains, and are representative.

Metallurgical sample selection protocols were prepared for two types of composites:

- A grinding test work composite is mainly made of drill core of the same lode in order to characterize the deposit variability. This protocol favours the composite approach that uses several drill core and needs to assume the representativeness of the ore throughout the lodes. The composite sample gold grade and dilution were sometimes different than average LOM as the sample selection focused on selecting the entire interval of mineralization rather than respecting the mining plan dilution. Some grinding test composites were used for gold recovery testing.
- Gold recovery and remaining test work composites were made of samples from the same lode or different lodes. The gold grade and dilution ratio were in accordance with the mine plan.

Tested samples are defined, by deposit, to judge their representativeness.

The **Tiriganiaq** deposit represents 50% of contained gold in indicated and inferred resources as reported in the Item 14. It is the main deposit of the Meliadine project and was studied in almost all metallurgical programs. The Tiriganiaq samples show the most valuable information and a high level of confidence compared to other deposits of Meliadine. Samples are usually located in the mineralization and identified by its lode number, which is important for the metallurgical interpretation. Since 2013, almost every sample used to perform metallurgical testing was located in the mine plan, which increases the representativeness of the test work.

The **Wesmeg** and **Normeg** deposits are much more limited in terms of metallurgical test work and samples. As these deposits are close to Tiriganiaq, it is assumed that the metallurgical performance will be similar. However, the tested Wesmeg samples represent a limited proportion of the deposit, which is not representative of the whole deposit. Normeg has not been studied yet. Further metallurgical evaluations will need to be performed on both Wesmeg and Normeg deposits.

The **F zone** samples are well located through the deposit which makes it representative. Indicated resources are particularly well represented.

The **Discovery** samples are essentially localized in the mineralization and represent the entire deposit. However, the composites are limited in terms of number of samples selected, restricted to three to five locations in the deposit. While the composites are representative, it is recommended to increase sample variability.

The **Pump** samples are limited to three composites only. However, those samples are located in the deposit and it comes from economic ore zone, which is representative. Pump samples are

considered reliable. It is recommended to perform more test work on the Pump deposit in order to confirm previous test results.

The **Wolf** samples mainly represent resources from the open pit, with depth ranging from surface to level 9700. The metallurgical performance is assumed to be the same for both mining zones (open pit and underground), based on the continuity of the lithological domains with depth. Further evaluations will be required to confirm this assumptions as the underground ore represent 90% of the Wolf deposit's contained gold in mineral resources.

13.2 Test Work Program

13.2.1 Comminution

Samples were recovered for comminution testing to provide material for each deposit. The key comminution data generated by the SMC and the Bond ball mill grindability test are summarized in Figure 13.1 and Figure 13.2, respectively. Comparison of the measured Bond ball mill work index (BWi) and the Axb from SMC test, calibrated with the SGS Lakefield database, shows that the hardness of the mineralization is considered in the "hard" range in terms of Axb and "medium" range of hardness in terms of BWi. Axb results were also obtained from seven DWT that were performed on larger and coarser sample fractions. Result corroborates the Axb distribution from SMC test results.

Tiriganiaq ore hardness measurements were used for grinding circuit simulations. The selected grinding circuit final product is 75 µm, as it was not found economical to grind finer during metallurgical test work. The HPGR technology was discarded following a trade-off study.

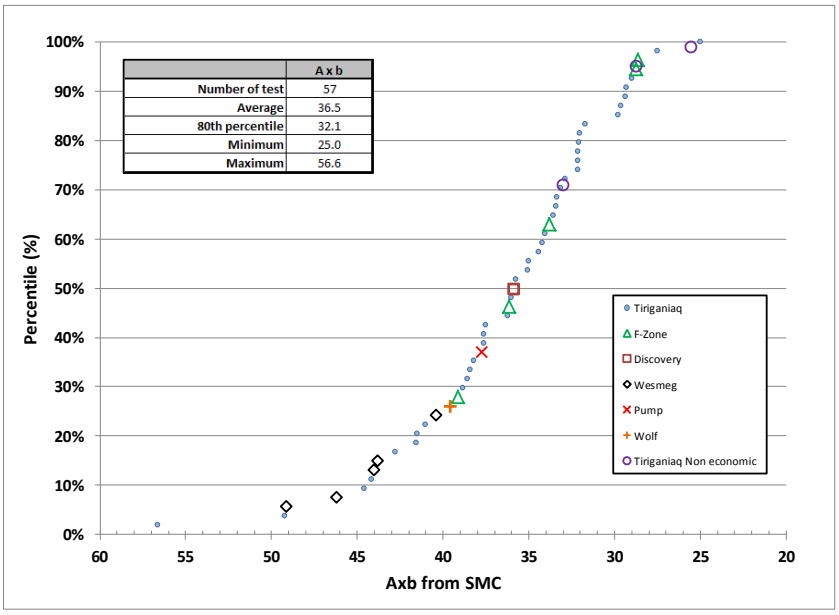


Figure 13.1 - Axb distribution from SMC test.

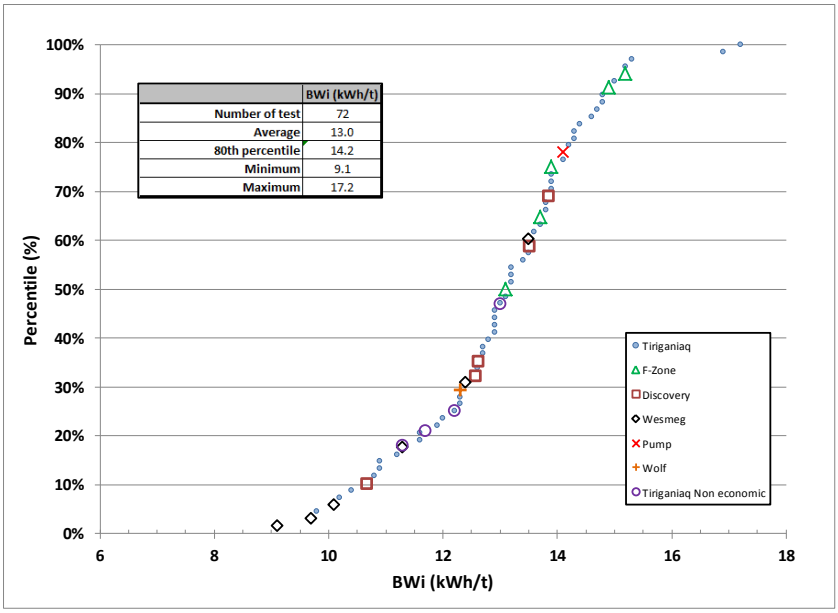


Figure 13.2 - BWi distribution from the Bond ball mill grindability test

13.2.2 Gravity Recovery

Mineralogy analysis and gravity test work results have justified the inclusion of a gravity recovery circuit in the flowsheet design. Studies have indicated the presence of coarse gold in the Tiriganiaq deposit, which generally favours gravity circuit recovery. Gravity gold recovery testing was performed in laboratory, using a Knelson MD-3 centrifugal concentrator, and the concentrate was upgraded on a Mozley C-800 mineral separator. The final concentrate was assayed to extinction and a mass balance was subsequently performed. The results of this test work demonstrated the suitability of the samples for gravity concentration.

Since 2012, four test work programs were performed to investigate the gravity recovery potential of the Meliadine deposits. Gravity recovery varied from 22% to 76% depending on the sample and target grind size, with an average recovery of 45%, which is higher than actual design criteria of 40%.

A sample of the master composite from the 2009-2011 test programs was sent to the Knelson Research and Technology Centre to perform a standard E-GRG test. This composite is a blend of representative Tiriganiaq deposit (55%), Discovery (4.7%), F zone (12%), Wesmeg (17.1%) and others (11.3%). Knelson's reports (2011 and 2013) confirm that the Meliadine ore responds well to gravity recovery techniques. The semi-quantitative classification scale for gold grain size, developed by AMIRA's P420B/C project, places the Meliadine master composite grain size between coarse and very coarse, which is positive for gold gravity circuit inclusion.

The four different testing programs were compared to confirm inclusion of the gravity circuit in the Meliadine design. Twenty composite samples were tested by direct cyanidation *versus* gravity recovery ahead of cyanidation. Direct ore cyanidation results resulted in lower recovery which demonstrated sufficient economic justification for the inclusion of gravity recovery at Meliadine.

Since 2012, continuous gravity recovery technology has been investigated. In 2013 and 2014, test work confirmed 1.5% increase in the global gold recovery for the Tiriganiaq ore. This technology consists of performing a second step of gravity recovery, which generates a higher gravity concentrate mass pull. This technology uses a continuous gravity system to allow higher concentrate mass pull, compared to a conventional batch gravity system. The gravity concentrate contains dense minerals such as arsenopyrite and magnetite that would be reground to 80% passing 38 µm prior to being pre-aerated and leached.

13.2.3 Pre-Aeration and Cyanidation

Tailings from the batch gravity recovery tests were used as feed for pre-aeration and cyanidation testing. The effect of pre-aeration on cyanidation was investigated in metallurgical test programs. The average residue assays indicated that pre-aeration had neither a positive nor a negative impact on gold recoveries; however, pre-aeration had the gratifying result of lowering cyanide consumption. In test work, more lime was added during pre-aeration to maintain the targeted pH. Lime consumption was, on average, higher for the pre-aeration tests than for the tests without any form of pre-aeration. The results were not sensitive to the use of air versus oxygen. Oxygen may offer slightly lower cyanide consumption than compressed air, but the differences fall within the range of experimental error and therefore no conclusions can be drawn. The increase of lime consumption due to pre-aeration, was largely compensated by the cyanide consumption reduction, which favours inclusion of pre-aeration in the process flowsheet.

For every cyanidation test, the density was adjusted to 40% solids and the pH was adjusted to 10.5-11 using lime. The cyanide concentration was maintained at 500 mg/L throughout the tests, and the total residence time was 48 hours with sub-sampling to determine the leach kinetics.

The combined gravity plus cyanidation recovery of gold ranged from 80.5% to 98.4% for all the deposits which agreed with the previous test work.

Early metallurgical testing program shows some carbonaceous minerals which are responsible for some preg-robbing (reducing gold recovery). This was observed only in the Tiriganiaq (lode 1000) and Pump deposits. Preg-robbing occurred in very specific location in these deposits. These areas clearly exhibit dark minerals like coal which are carbonaceous. Specific testing program was conducted by Agnico Eagle to mitigate the preg-robbing effect of the Tiriganiaq lode 1000 ore. Addition of activated carbon, as in a CIL circuit, completely mitigated the preg-robbing effect.

The following additional observations can be made:

- The majority of gold is dissolved after 24 hours of cyanidation.
- Arsenopyrite is not refractory to conventional gold processing; it may reduce leaching kinetic for ore zones with higher arsenopyrite content.
- Gold recoveries for the F zone and Pump deposits are lower than for the Tiriganiaq, Discovery and Wolf deposits. Therefore, further testing should be performed on the F zone and Pump deposits in order to validate the recovery differences.

13.2.4 CIP/CIL Modeling

Cyanidation and carbon adsorption simulations were performed to ascertain the number of CIL stages required. SGS had done some test work (SGS, 2012 and 2013) where most of the

simulations were run on carbon-in-pulp ("CIP") processing. As preg-robbing was observed in some composite from lode 1000 of the Tiriganiaq deposit, the CIP circuit was replaced by a CIL circuit, which was found to mitigate preg-robbing.

In 2013, the consulting firm BBA suggested CIL circuit simulation using a retention time of 48 hours and a carbon concentration of 15 g/L. The head grade of the gravity circuit was adjusted to about 70% of the feed grade to represent the gravity circuit gold recovery. Results indicated that a retention time of 48 hours combined with at least five leaching stages would yield the optimal gold solution concentration.

13.2.5 Recoverability

A model for gold recovery for the Meliadine deposits was developed based on recent and historical gravity recovery / leach tests. The data for each ore deposit were filtered to include only the most significant results corresponding to:

- Tests including gravity and cyanidation (CIL, CIP or direct leaching)
- P80 ranging from 54 to 110 µm
- Sample head grades from 1 to 14 g/t.

Logarithmic regression analysis was used to determine a model predicting gold recovery as a function of ore head grade up to a maximum expected recovery. The models are represented graphically in Figure 13.3. The gold recovery for the Tiriganiaq model includes a recovery increase of 1.5%, which comes from the addition of the continuous gravity circuit. However, the recovery model is capped at 96.5% to avoid over estimation of the gold recovery. The recovery curve of the Tiriganiaq deposit is used to represent the Wesmeg and Normeg gold recovery. This assumption is possible considering all the similarities between those deposits. Further test will be required to define the gold recovery of the Wesmeg and Normeg deposits which represent 20% of contained gold from indicated and inferred resources reported in the Item 14. Most of the gold recovery tests performed on the Wolf deposit were limited to head grades ranging from 1.5 to 4.0 g/t gold. The model regression extrapolates the recovery to up to head grade of 14 g/t gold.

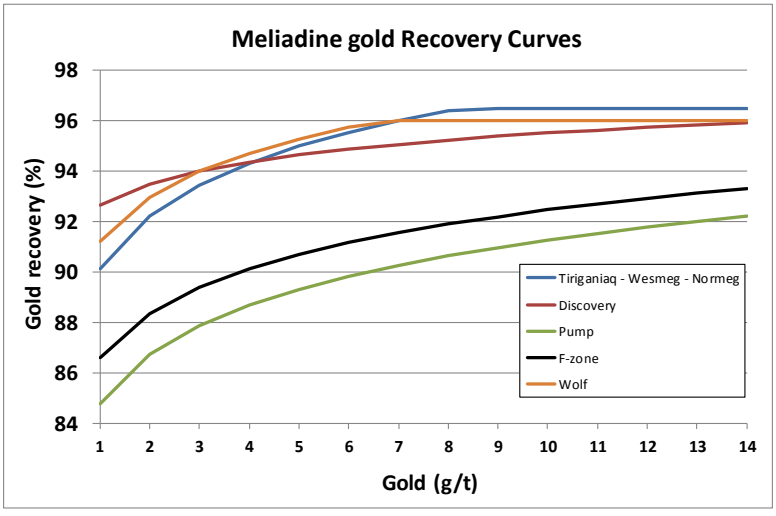


Figure 13.3 - Meliadine metallurgical models for gold recovery

Based on mineral resources and mineral reserves (as of December 31, 2014) for all Meliadine deposits, an average head grade of 6.5 g/t gold would give a global gold recovery estimated at 94.7%, which would include a 1.5% gain applied to the Tiriganiaq deposit only.

The economic analysis in Item 22 of this report is made on only proven and probable reserves. The mineral reserves are all contained in the Tiriganiaq and Wesmeg deposits, so their respective recovery models were used. The assumed gold recovery therefore averages 96.0% at a 7.44 g/t gold average mill feed grade.

13.2.6 Cyanide Detoxification

Laboratory test work on cyanide detoxification was performed by SGS in 2012 and 2013. The latter report is more useful because it involved test work on different composite samples from deposits. It was possible to achieve a weak acid dissociable cyanide (CN_{WAD}) destruction target level (<1 mg/L) using a conventional SO_2/air circuit. Tests also indicate the possibility of achieving a total cyanide (CN_{TOT}) of 15 mg/L by precipitating ferrocyanide with excess copper in a non-aerated vessel. However, as the CN_{WAD} destruction target is set at 10 mg/L, the ferrocyanide will not be precipitated and may build up in process water recirculation.

The test assumed a cyanide charge in the cyanide destruction circuit feed of 100 mg/L CN_{WAD}, which is similar to Agnico Eagle's Lapa mine process plant. The feed grade and feed composition of the Meliadine CIL process would be similar to that at the Lapa process plant, and it can be safely assumed that the cyanide detoxification circuit feed would be similar as well.

13.2.7 Dewatering (Thickening and Filtration)

Pocock Industrial (2014) conducted solid-liquid separation tests on the bulk sample sub-sample produced by Metso during the Vertimill pilot plant test. The overall objective of the test program was to develop a general set of data for the design of filtration equipment to dewater the tails material prior to final disposal. Prior to conducting formal equipment sizing procedures, flocculant screening tests were performed on each sample. These tests aided in the selection of flocculants that could provide the best overall performance with respect to overflow clarity, decantation rates, and underflow viscosity characteristics for each material. Static and dynamic thickening tests were then performed for each material to develop a general data set for conventional, high-rate, high-density, and paste thickener design. Accordingly, overflow suspended solids concentration measurements taken during dynamic testing provided a means to predict overflow clarities for each thickening technology.

The simulated tails material was generated from the grind material by following specifications provided by Agnico Eagle. As per the company's recommendations, the grind discharge sample was leached with 500 mg/L NaCN for 12 hours, followed by a cyanide detoxification simulation using 200 mg/L copper sulphate ($CuSO_4$) and 1,500 mg/L sodium metabisulphite. The remaining solids and liquor from this procedure was used for the simulated tails filtration test work. Viscosity tests performed on samples of underflow generated from the thickening tests evaluated the rheological properties of each material for rake mechanism and underflow pipeline design. These tests also served to establish the maximum recommended design underflow density for each thickener. Finally, vacuum and pressure filtration tests performed on specified samples of thickened underflow established a general set of data for horizontal belt vacuum filter design and membrane-type recessed plate pressure filter design.

Item 14. Mineral Resource Estimates

The December 31, 2014 mineral resource and reserve estimate for the Meliadine project, which forms the basis of this technical report, is the latest in a series of NI 43-101-compliant mineral resources estimates for this project. The previous estimates are summarized in Item 6 of this report.

The Meliadine drill-hole databases, summarized in Item 10 of this report, comprise collar coordinates, downhole survey data and assay results managed by Agnico Eagle's Technical Services group in Preissac, Quebec. Drilling data are collected, validated by QA/QC protocols, compiled and verified by Agnico Eagle staff with review by external auditors.

The current mineral resource model for the Meliadine project was prepared by Agnico Eagle's Technical Services group using diamond drill data exclusively, according to industry best practices as described in CIM (2014). The mineral resources estimate incorporates the latest surface and underground drilling results through 2014. This item of the report summarizes the methodology used by Agnico Eagle to estimate the current mineral resources at the project.

Agnico Eagle reports mineral resource and reserve estimates in accordance with the Canadian Institute of Mining, Metallurgy and Petroleum (CIM) guidelines for the estimation, classification and reporting of mineral resources and reserves that was adopted by CIM Council in May 2014 (CIM, 2014). Agnico Eagle reports mineral resources exclusive of mineral reserves. Mineral resources that are not mineral reserves do not have demonstrated economic viability.

Agnico Eagle prepared a detailed internal updated technical study (Petrucci et al., 2015) which forms the basis for the cut-off grades and shells for open pit and underground mining used for reporting the current mineral reserves at Tiriganiaq and Wesmeg deposits and the current mineral resources at Tiriganiaq, Wesmeg, Normeg, F-Zone, Discovery, Pump and Wolf deposits in this document.

There are no known environmental, permitting, legal, title, taxation, socio-economic, marketing, political or other relevant factors that could materially affect the Meliadine mineral resources estimate as of December 31, 2014, as discussed in Item 4 of this report.

14.1 Database

14.1.1 Supplied Data

The database used for the current Meliadine resources estimate comprises historical drill-holes (1990 to 2010) in addition to the 2011 to 2014 data for all deposits provided by Agnico Eagle's Exploration group through November 5, 2014, when the database was closed for this estimate.

Agnico Eagle compiled the historical drill logs and hole details (structure, alteration, mineralization, textures, minor rock units, RQD) into the DHLogger software system. From 2011 to 2014, the Agnico Eagle Exploration group provided the Technical Services group with valid and complete raw drill-hole data including collar locations and orientations, surveys, assays, major and minor lithologies, structures and RQD in DHLogger and Fusion Central software systems. Surface topography and base of till data from Comaplex in AutoCAD DXF format was

updated with the new 2014 drilling. Assay QA/QC reports were also provided each quarter, attesting to the validity of the assay results that have been added to the resource database since 2011.

These files were validated and compiled in the Meliadine Century Systems database managed by Agnico Eagle staff. Figure 14.1 shows the collar locations of all available drill-holes for the December 2014 mineral resource estimate. The coordinates for the collar locations are given in Appendix 10.1.

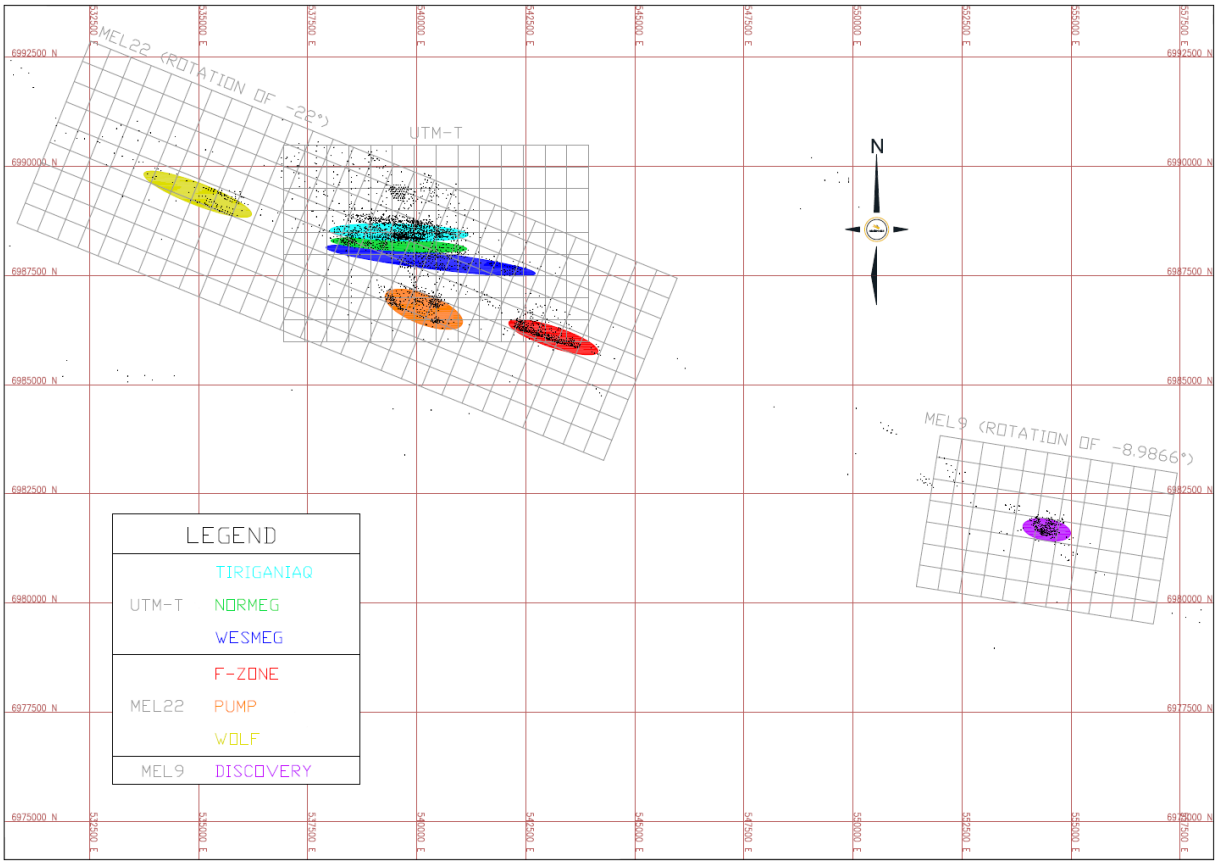


Figure 14.1 - Location of collars of all drill-holes available for the December 2014 mineral resource estimate, showing the local grids in the deposit areas

14.1.2 Grid and Data Transformation

Drill-hole data for the Tiriganiaq, Wesmeg and Normeg deposits are referenced to a local grid referred to as the "Tiriganiaq grid". The Tiriganiaq grid is the UTM grid NAD 83 Zone 15 transformed according to the formula in Table 14.1. Drill-hole data for the Wolf, Pump and F zone deposits reference a rotated local grid referred to as the "MEL 22 grid", which is transformed with a baseline azimuth of 112° according to the formula in Table 14.1. Drill-hole data for the Discovery deposit reference a local grid referred to as the" Discovery grid", which is transformed with a baseline azimuth of 98.9866° (Table 14.1). Figure 14.1 shows the three local grids on the property.

Table 14.1 - Transformation from UTM grid to Tiriganiaq, Mel 22 and Mel 9 local grid coordinates

		UTM NAD 83 Zone 15 Origin Coordinates			Local Grid Origin Coordinates			
Deposit	**Local Grid**	**Easting (X)**	**Northing (Y)**	**Elevation (Z)**	**Easting (X)**	**Northing (Y)**	**Elevation (Z)**	**Rotation**
Tiriganiaq, Wesmeg and Normeg	Tiriganiaq	0	0	0	-530 000	-6 980 000	10 000	None
F zone, Wolf and Pump	MEL 22	538 198.4059	6 990 518.1640	0	12 000	6 000	10 000	+22º
Discovery	MEL 9	553 856.4881	6 981 657.2100	0	4 000	6 000	10 000	+8.9866º

Agnico Eagle and Comaplex applied a correction to any magnetic azimuth values recorded in downhole surveys taken by Reflex EZ-Shot methods, to convert from magnetic to the appropriate grid. Agnico Eagle, Comaplex and partners also applied corrections to azimuth values as described in Item 10, and provided the Technical Services group with the final corrected azimuth data. Agnico Eagle converted the downhole dip to conform to Datamine convention (*i.e.*, downward direction holes are indicated with a positive dip sign).

14.1.3 Lost core treatment, unsampled intersections and drill-hole displacement

Agnico Eagle assigned a default value of 0 g/t gold to unsampled drill-hole intervals, to prevent smearing of sampled grades into unsampled intervals. However, for the specific unsampled intersections, "absent value" or removing the intersection has been applied. These specific intersections are:

- Six holes drilled for the grade control during the bulk sample that were sampled only for the developed lodes (1000 or 1100), even if they intersected the intervening lodes. These non-sampled intersections have been removed from the estimation process to avoid underestimates.
- Lost core intersections are rare at Meliadine but when one is included in a mineralized domain, it is studied and a decision is made depending on the neighbouring samples:
    - a lost core intersection is considered as absent or deleted when it is located in a mineralized intersection;
    - a lost core intersection is considered as 0 g/t when it is located in a low-grade intersection.

For the Tiriganiaq deposit, 12 intersections were manually moved for the 1000 and the 1100 lodes. During the bulk sample, these holes were seen and surveyed. Only the intersections have been moved, not the entire holes.

Appendix 14.1 shows all drill-hole intercepts that have been submitted to specific treatment.

No other transformations or rotations have been performed on the data or the models.

14.2 Geological Interpretation, Modelling and Domaining

The 2011 to 2014 drill information has been used to update previous geological interpretations for the Tiriganiaq, Wesmeg, Normeg, Pump, Wolf, Discovery and F zone deposits respecting the minimum modelling cut-off grade and the minimum mining width (Table 14.2).

The geological interpretation also takes into account the presence and continuity of the following mineralization controls: quartz-ankerite vein networks, iron formation, sulphide content (arsenopyrite and pyrrhotite) and visible gold. Also, Agnico Eagle adjusted the ore model to the lithological and structural 3D models built partially by InnovExplo Consultants for all deposits other than Wolf.

The seven deposits contain a total of 168 zones, each of which was calculated separately.

Table 14.2 - Modelling parameters for all deposits

Deposit	Minimum horizontal width (m)	Modelling cut-off grade (g/t gold)
Tiriganiaq	2.5	4
F zone	3	4
Discovery	3	4
Normeg	3	4
Wesmeg	3	1
Pump	3	1
Wolf	3	1

14.2.1 Geological Interpretation and Modelling

For all deposits, 3D solids representing the limits of the mineralized high-grade domains are built using Datamine software on sections and then adjusted in plan view. The interpretation is based on structural and lithological 3D solids and logging descriptions (sulphides, quartz veins and alteration). For the Tiriganiaq and Normeg deposits, the underground mapping and sampling has been incorporated in the digitized interpretation.

The 168 zones at Meliadine have been named using nomenclature shown in Table 14.3 to avoid confusion.

Table 14.3 - Mineralized zone name nomenclature

Deposit	Lodes	Number of zones
Wesmeg	0 to 899	36
Normeg	900 to 999	19
Tiriganiaq	1000 to 1999	35
Wolf	2000 to 2999	14
Pump	3000 to 3999	25
F zone	4000 to 4999	13
Discovery	5000 to 5999	10

14.2.1.1 Tiriganiaq deposit

The original wireframe solids of the various mineralized lodes in the Tiriganiaq deposit that were primarily built by Snowden (2010) have been refined by Agnico Eagle using the results of the 2011 to 2014 drill program and now total 35 wireframe solids corresponding to high-grade domains. For the current estimation, nine zones have been deleted and most of the wireframes have been shrunk to ensure greater recognition of unmineralized internal waste horizons, and to focus on economic areas and optimized geostatistical parameters.

Specific characteristics distinguish each lode series, and geological markers help in the interpretation of the stratigraphic contact zones, the structural trends, the faults and shear zones and the elevated levels of quartz veining, sulphides (arsenopyrite and pyrrhotite) and visible gold.

The 35 wireframes are subdivided in six domains (structural groups) as discussed in Item 7 (Figure 14.2). These groups are from north to south: 1000, 1000 series, 1100, 1150 series, 1250 series and 1350 series. All series strike between 270° and 290°. Groups 1000 to 1100 are located in a strongly sheared corridor associated with the Lower Fault deformation event called the Main zone. Their geometry is parallel to the shear system (-60° to -70°), which is the dominant control. The Main zones plunge dominantly to the east at 30° to 45°.

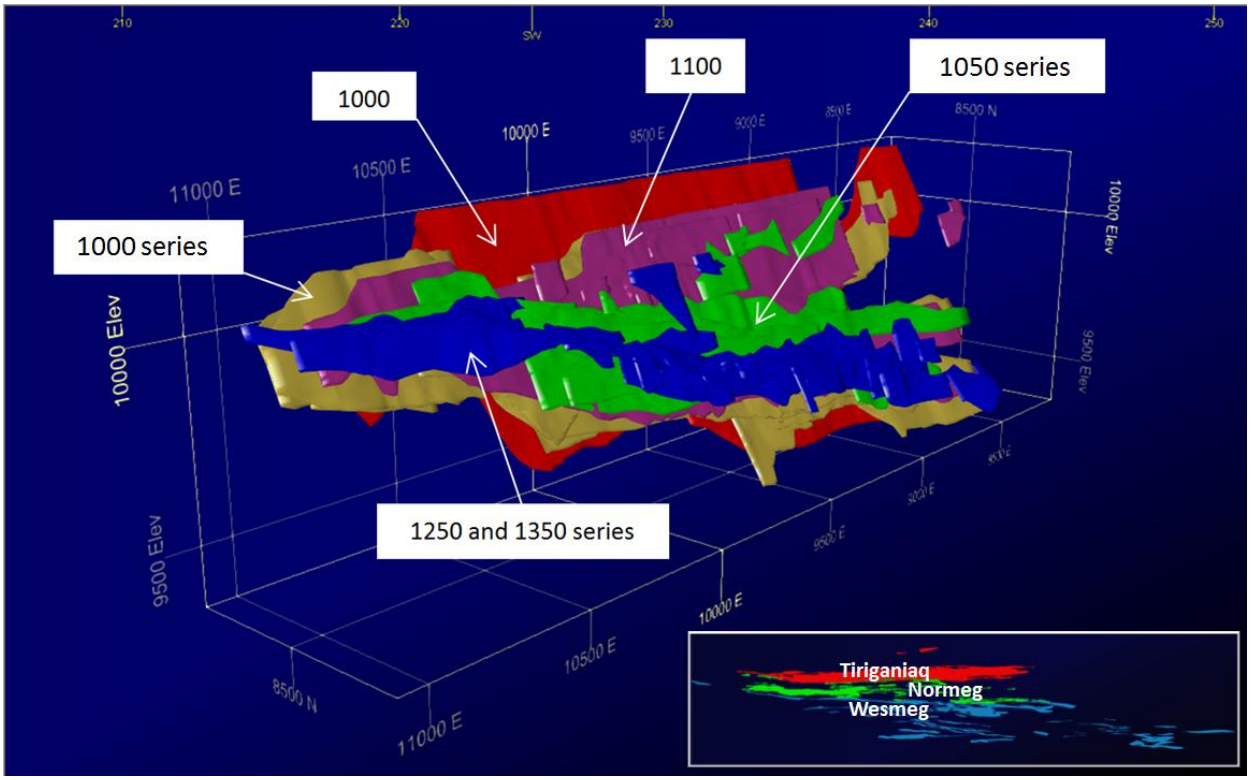


Figure 14.2 - Isometric view of the Tiriganiaq 3D high-grade zones looking to the southwest (Tiriganiaq grid)

The northward groups, numbered 1150 and higher, are located in an apparently less deformed but tightly folded area where each series is separated by subsidiary mineralized shear zones dipping at 60° to 70°. This group corresponds to the Western Deeps zones. The steeper zones show a dip of approximately 70° and are located in shear zones while the flatter zones (45° to 55°) are located in iron formation fold hinges. The Western Deeps zones plunge to the west at 10° to 20°.

The overall package extends almost 3 km along strike and shows an average true width of 40 m in the pit area and 140 m in the underground area. The deepest wireframe reaches 720 m below surface.

Using the high-grade domains as a base, a wider envelope corresponding to the Upper Oxide Formation was generated to create the low-grade domain. This domain is designed to provide dilution grade in the milling process and is considered in the stope design. Figure 14.3 shows the upper oxide low-grade domain, which has been divided in two domains, north and south. The south domain is associated with the Lower Fault sheared corridor (1000 to 1100 lode), and the north domain is located in the tight folded area (1150 to 1350 series).

Appendix 14.2 gives a statistical analysis of the intercepts from all six domains within the Tiriganiaq deposit.

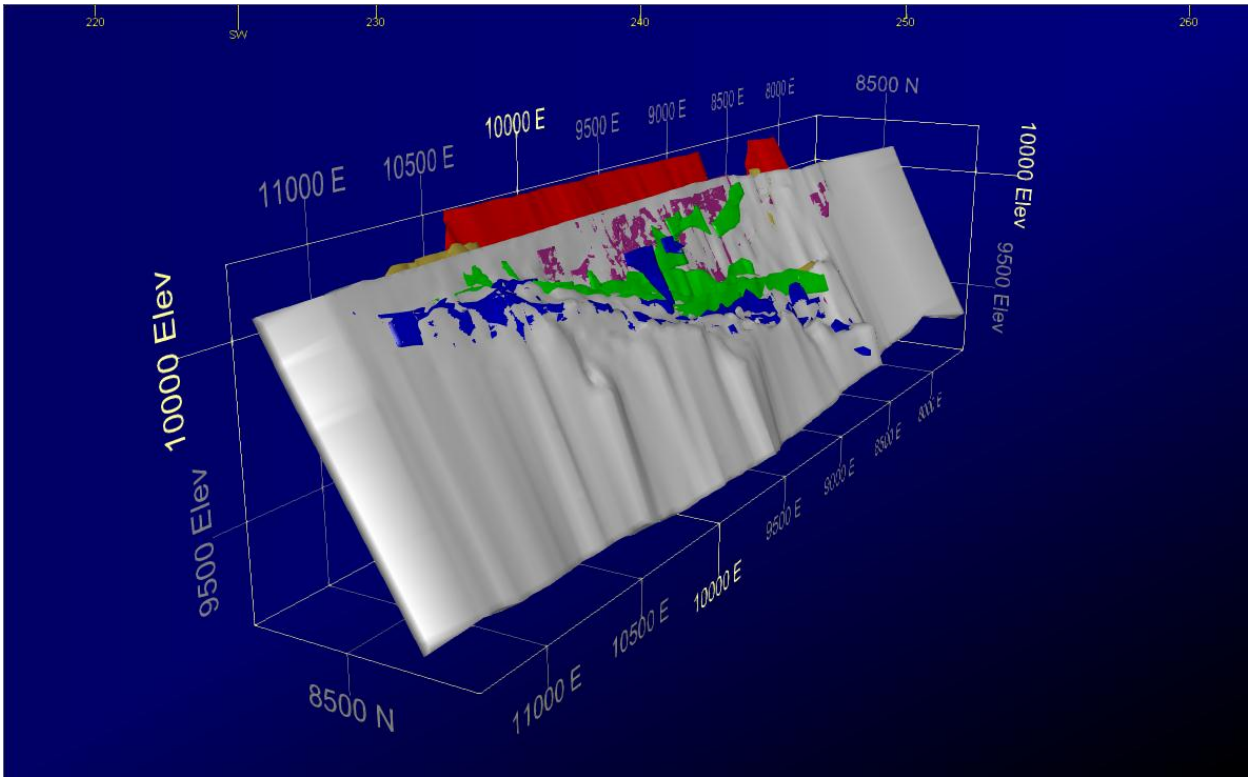


Figure 14.3 - Isometric view of the Tiriganiaq low-grade domain (Upper Oxide Formation 3D solids) in grey, looking to the southwest (Tiriganiaq grid)

14.2.1.2 Wesmeg deposit

Located approximately 400 m south of the Tiriganiaq deposit, the Wesmeg deposit consists of 36 zones grouped into five domains according to their structural distribution:

- "200-300" correspond to the southeast zones
- "400 Low" is the most southerly group of the deposit and represents mineralization parallel to the shear zones
- "400 High" is a central group showing a northwest trend
- "650" is the most important zone of Wesmeg and is included in the uppermost iron formation in the Wesmeg Formation
- "600-700" is a northern package showing the same trend as "400 High"

The zones associated with shearing ("400 Low" and most of "200-300") strike approximately east-west (270°) and dip 55° to 60° to the north. The zones located in major fold hinges strike west-northwest (275° to 285°) and are slightly steeper-dipping at 60° to 63° to the north. A statistical analysis of the intercepts from all the domains is given in Appendix 14.2 and their location is illustrated in Figure 14.4.

The domains are interpretated to follow deformed iron formation bands. Gold mineralization is mainly concentrated on the hanging wall and footwall of iron formation bands. The overall package trends at east-southeast (280°) and extends more than 5 km long. The domains are

separated by 5- to 50-m-wide waste horizons and reach generally 370 to 620 m below surface except the zone 650, which sretches continuously to more than 800 m depth.

The iron formation bands at Wesmeg are modelled and are used as a low-grade domain (Figure 14.5). As with the Upper Oxide Formation at Tiriganiaq, the iron formation domain at Wesmeg is designed to provide dilution grade in the milling process and is considered in the stope design.

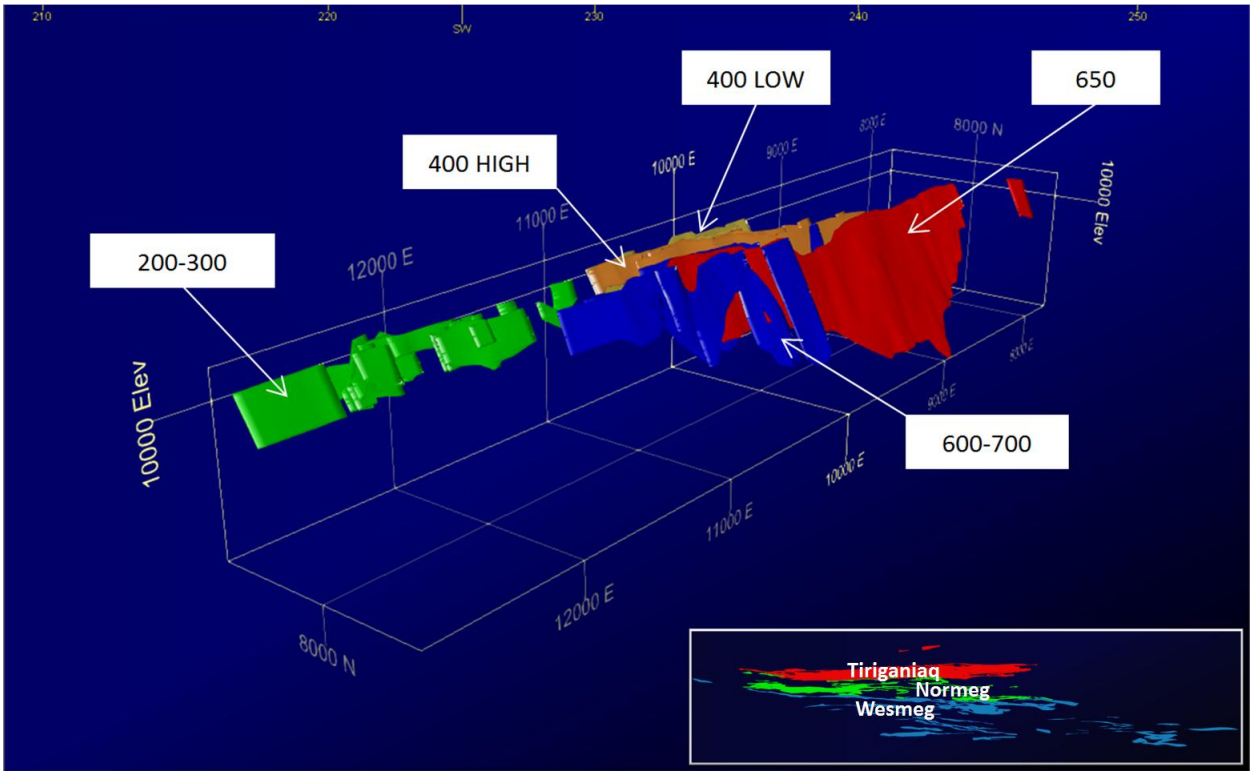


Figure 14.4 - Isometric view of the Wesmeg 3D high-grade zones looking to the southwest (Tiriganiaq grid)

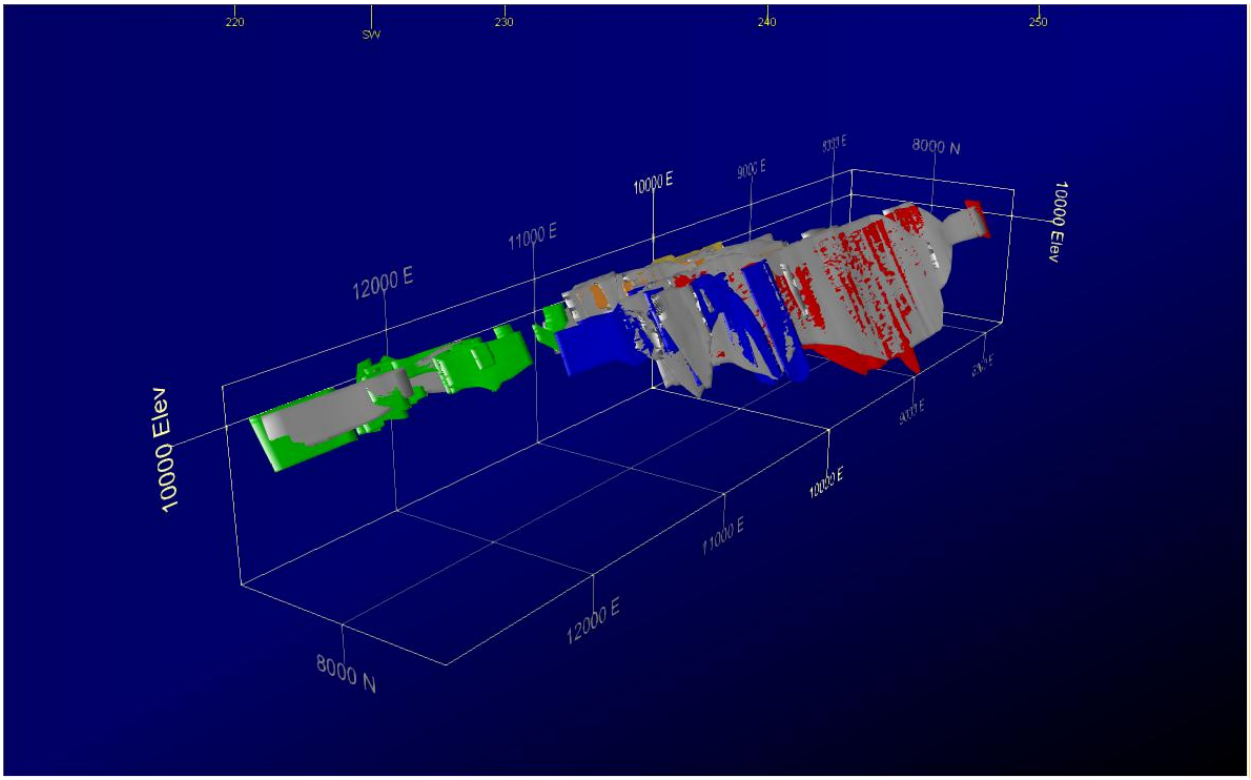


Figure 14.5 - Isometric view of the Wesmeg low-grade domain (iron formation bands) in grey, looking to the southwest (Tiriganiaq grid)

14.2.1.3 Normeg deposit

The Normeg deposit is composed of 19 zones that were constructed using a minimum horizontal width of 3 m. The zones are located between the Tiriganiaq Formation and the uppermost iron formation in the Wesmeg Formation and show a strike length of more than 2 km. The wireframes have been interpreted as deep as 650 m below surface.

The absence of iron formations is a characteristic of the Normeg zones. Quartz veining, sericitic and fuchsite alteration intensities are the most important guides used in recognizing the Normeg deposit. The zones strike generally east-west (272°) and dip approximately 61° north (Figure 14.6).

The northernmost zones (987 to 999) are located near the Tiriganiaq 1000 lode footwall. Zones 910 to 930 are the most important and are located in the central portion of Normeg. Most of these lodes have been encountered by the exploration ramp (910, 911, 920 and 930), and the wireframes have been adjusted using underground mapping from the ramp. The southern zones (900 to 909) are located to the north of the Wesmeg deposit. The zones are located on Figure 14.6. Characteristics and statistics of all the zones are shown in Appendix 14.2.

A low-grade domain characterized by sericitic volcanic rocks is modelled and estimated at Normeg but is strictly used for the pit shell generation (Figure 14.7).

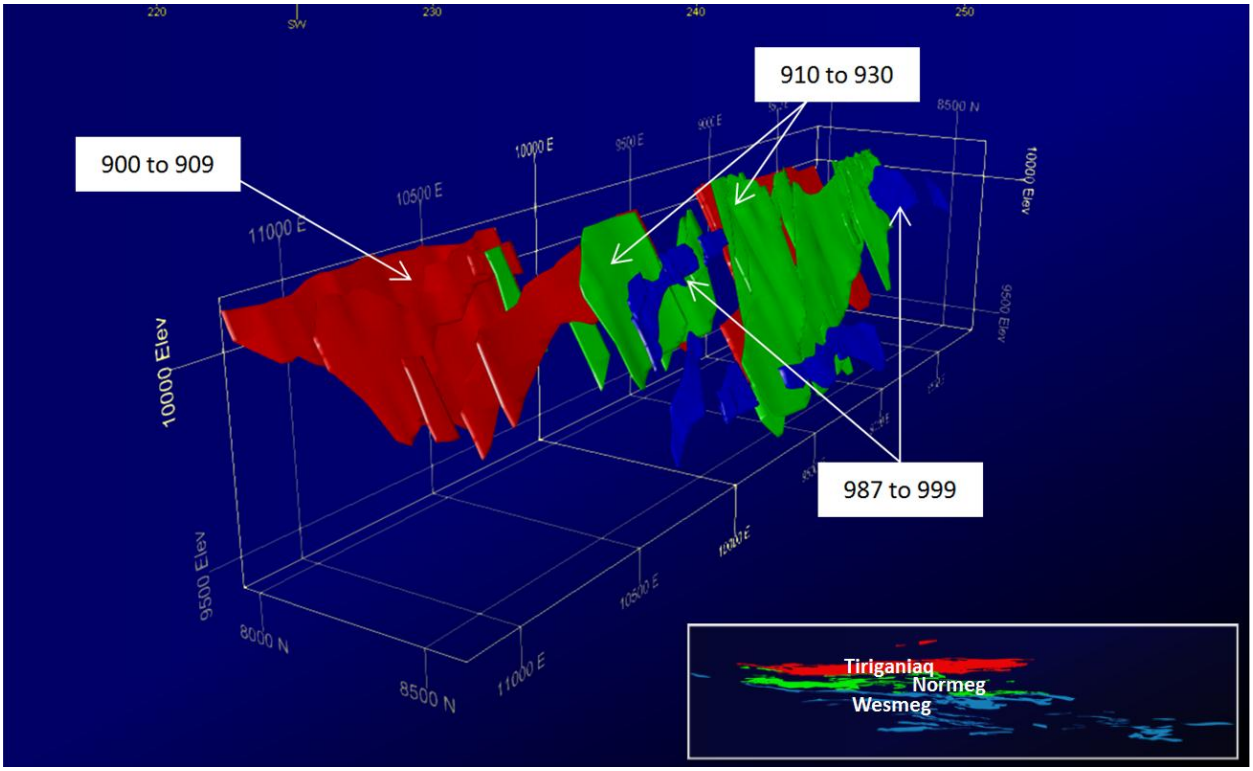


Figure 14.6 - Isometric view of the Normeg 3D high-grade zones looking to the southwest (Tiriganiaq grid)

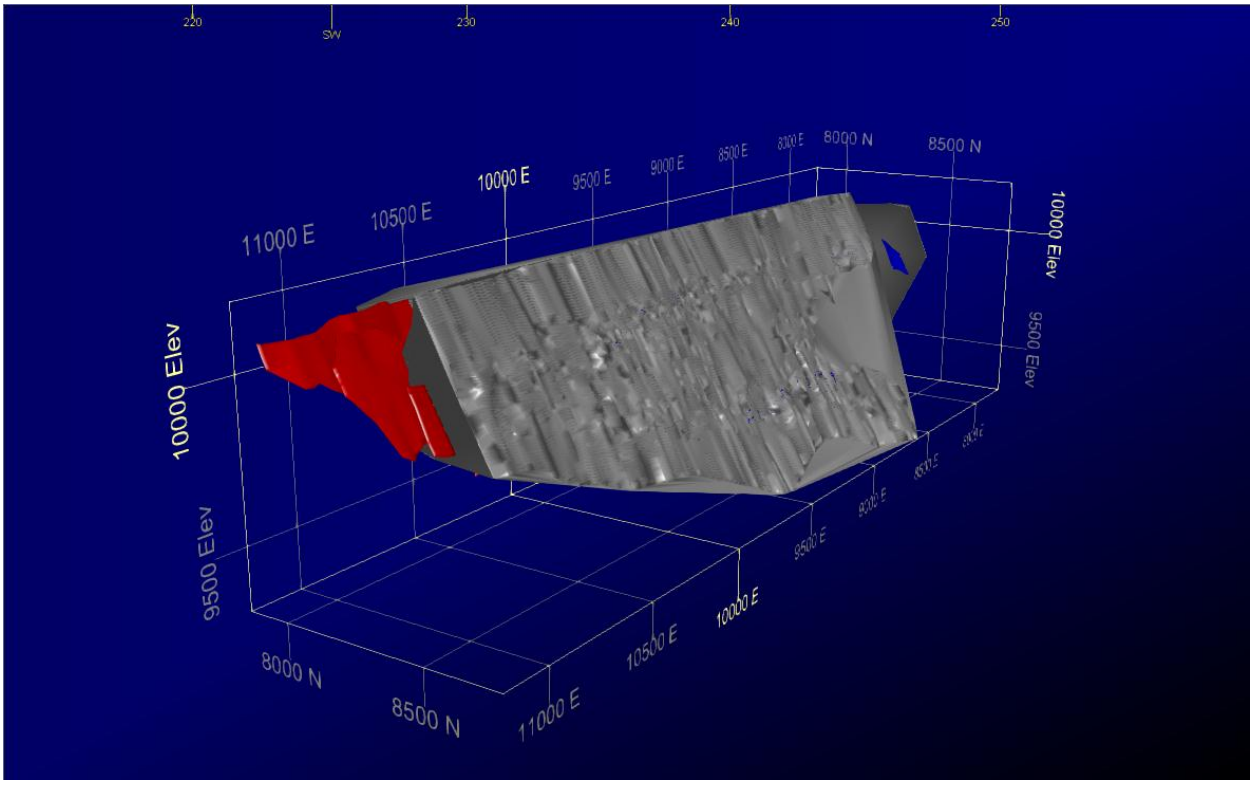


Figure 14.7 - Isometric view of the Normeg low-grade domain (sericitic volcanic rocks) in grey, looking to the southwest (Tiriganiaq grid)

14.2.1.4 Discovery deposit

At the Discovery deposit, there are ten narrower and continuous zones containing higher gold grades, mainly hosted in or near quartz veins and excluding most internal waste zones. These ten zones are grouped into three domains according to their orientation and spatial distribution: the 51 series located to the south (5110 to 5150), the "52 low" series trending east-west (5210, 5220 and 5310), and the "52 high" series trending northwest (5230 and 5240). An unscaled oblique northward view of the Discovery geological interpretation is shown in Figure 14.8.

The 51 series trends approximately west-northwest (280°) and dips approximately 60° to the northeast. The 52 low series has the same trend (281°) and dips approximately 57°. The 52 high series strikes approximately northwest (300°) and dips approximately 48° to the northeast. Where the two 52 series overlap, the 52 high series is located to the north of the 52 low series.

The overall Discovery deposit extends 850 m along strike and shows an average true width of 20 m. The 52 low series is deeper, reaching as deep as 500 m below surface.

Channel samples were used to interpret the position of the lodes in the 52 low and 52 high series at surface, but to restrict the influence of their high grades the channel sampling results were excluded from the resource estimation. It is unclear if this historical data underwent any QA/QC program and review.

The interpretation of the high-grade zones is guided by a wider lithological envelope corresponding to an iron formation that is understood as a favourable control for gold deposition (Figure 14.9). The iron formation 3D model is considered as a low-grade domain and is only used during the pit shells generation.

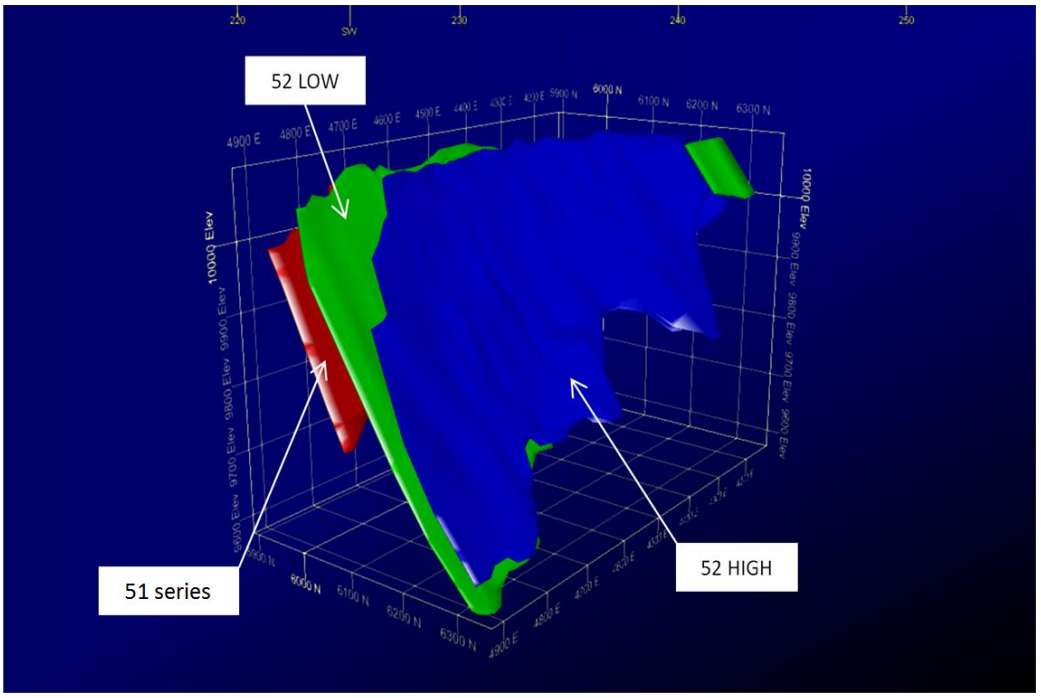


Figure 14.8 - Isometric view of the Discovery 3D high-grade zones looking to the southwest (MEL9 grid)

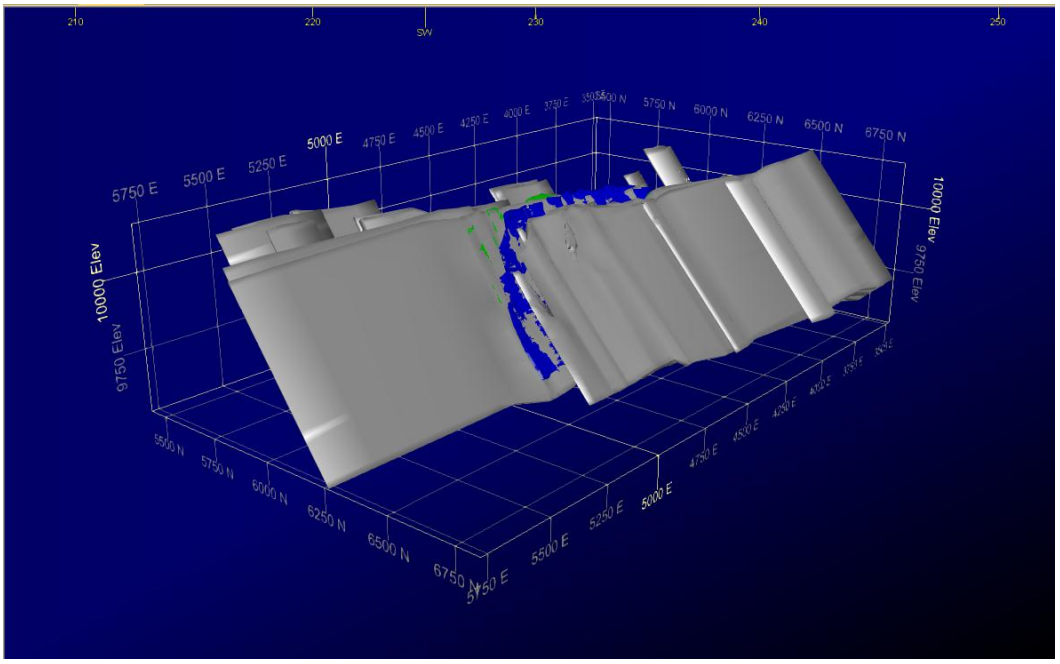


Figure 14.9 - Isometric view of the Discovery low-grade domain (iron formation bands) in grey, looking to the southwest (MEL9 grid)

14.2.1.5 F zone deposit

At the F zone deposit, the mineralized 3D domains have been re-interpreted to comply with the underground cut-off grade. The F zone underground models comprise 13 narrow and continuous zones containing higher gold grades (4100 to 4180), usually hosted in or near quartz veins, and exclude most internal waste zones (Appendix 14.2). The F zone underground zones were interpreted using a minimum horizontal width of 3 m and a minimum cut-off grade of 4 g/t gold.

A wider envelop corresponding to the iron formation package was built around the underground model (Figure 14.10). The gold grade is interpolated in this low-grade domain but is used only for pit shell generation.

An unscaled northward oblique view of the F zone geological interpretation is shown in Figure 14.11. The zones all strike approximately west-northwest (285°) and dip approximately 50° to the northeast. The wireframes cover a region of 2.2 km in strike length, and the package shows an average true width of 35 m. The deeper zones reach 640 m below surface.

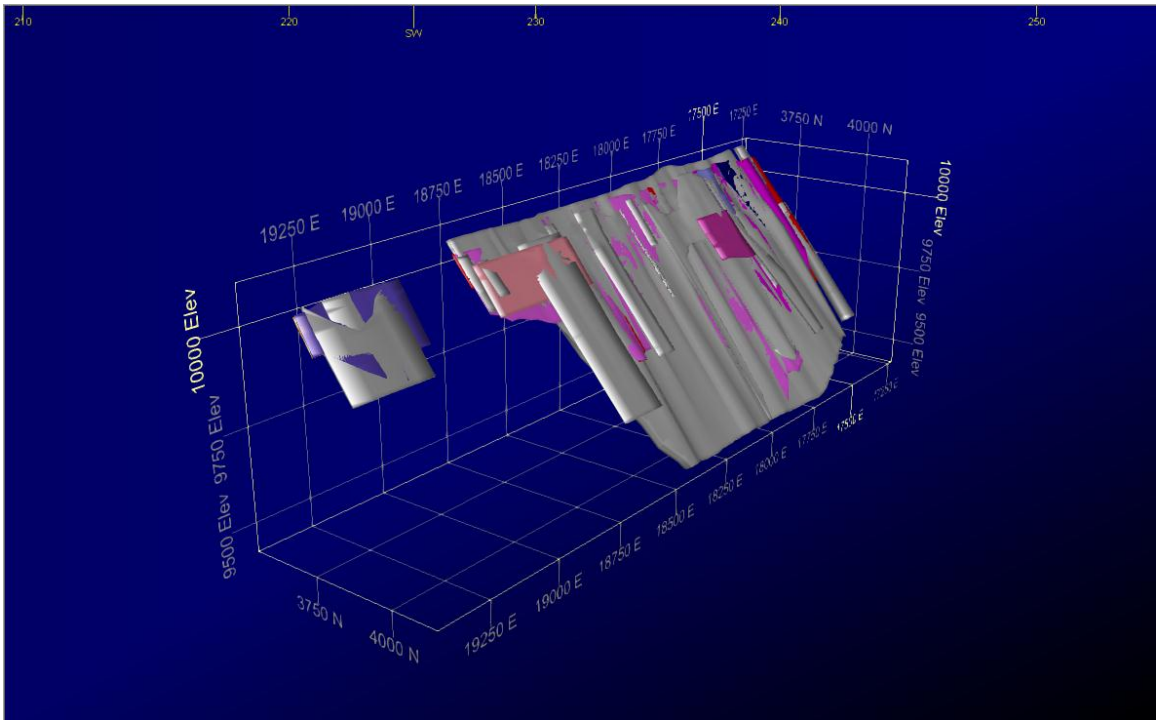


Figure 14.10 - Isometric view of the F zone low-grade domain (iron formation bands) in grey, looking to the southwest (MEL22 grid)

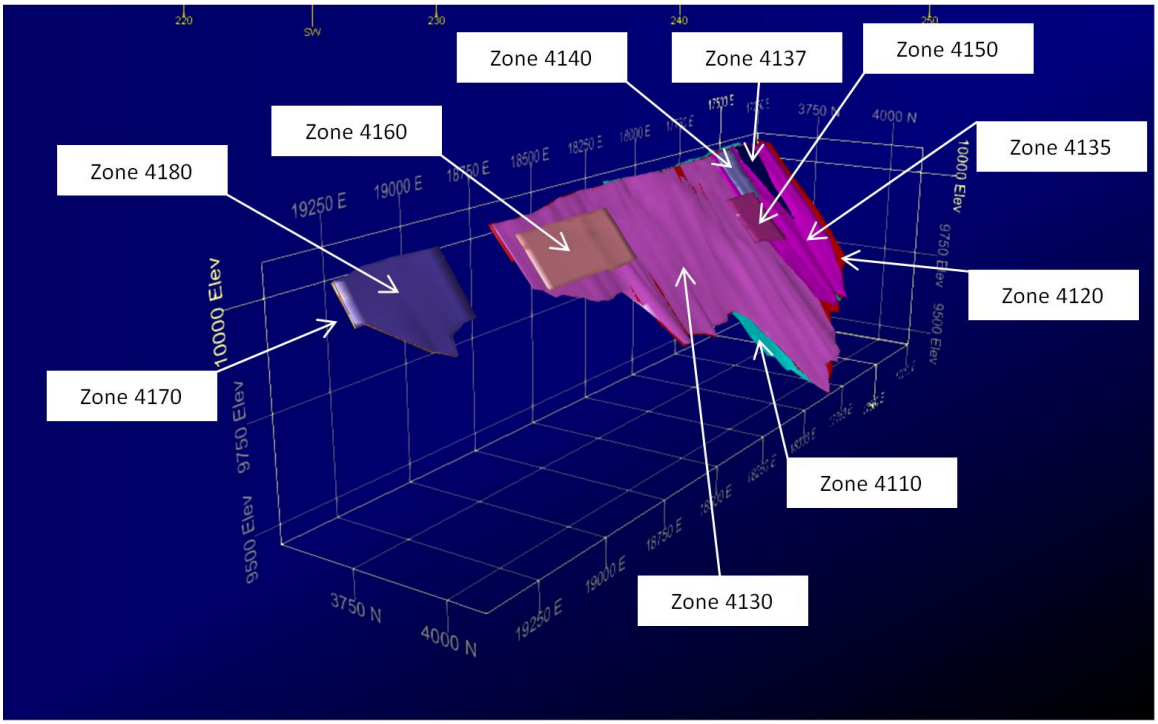


Figure 14.11 - Isometric view of the F zone 3D high-grade zones looking to the southwest (MEL22 grid)

14.2.1.6 Pump deposit

At the Pump deposit, 25 mineralized zones have been defined based on continuous higher gold grades generally hosted in or near quartz veins, using a minimum horizontal width of 3 m. The zones are grouped into five domains according to their structural distribution, as illustrated in Figure 7.10:

- the 31-1 domain is mostly located in the south of the Pump deposit (3100 and 3101) in the south flank of the western fold
- the 31-2 (3109, 3110 and 3130) and the 31-3 (3165, 3180, 3190 and 3195) domain are located in the western fold hinge
- the 33-1 (3300, 3301, 3310, 3320, 3330 and 3340) domain is located in the eastern fold hinge
- the 34-1 (3411, 3412, 3413, 3440 and 3460) domain is located in a central fold hinge and
- the 34-2 (3299, 3341, 3400, 3402 and 3405) domain is located in the flank between the central and eastern folds

Appendix 14.2 lists all the zones in the Pump deposit, and Figure 14.12 shows their spatial distribution.

These lodes have been modelled along shear zones that are interpreted to be parallel to the axial planes of regional folding (west-northwest strike (290°) dipping 50° northeast). All groups are localized within regional fold hinges or sheared flanks and are locally crosscut by later faults, explaining the restricted extent of the zones. The mineralization seems to be dominated by both structural and lithological controls such as iron formations and shear zones.

The iron formation 3D model has been considered as a low-grade domain (Figure 14.13). Gold interpolation in that domain has been used for pit shell generation.

The Pump wireframes extend along a 2-km northwest trend, and the package shows a variable true width between 10 and 65 m. The deepest zones reach 500 m below surface.

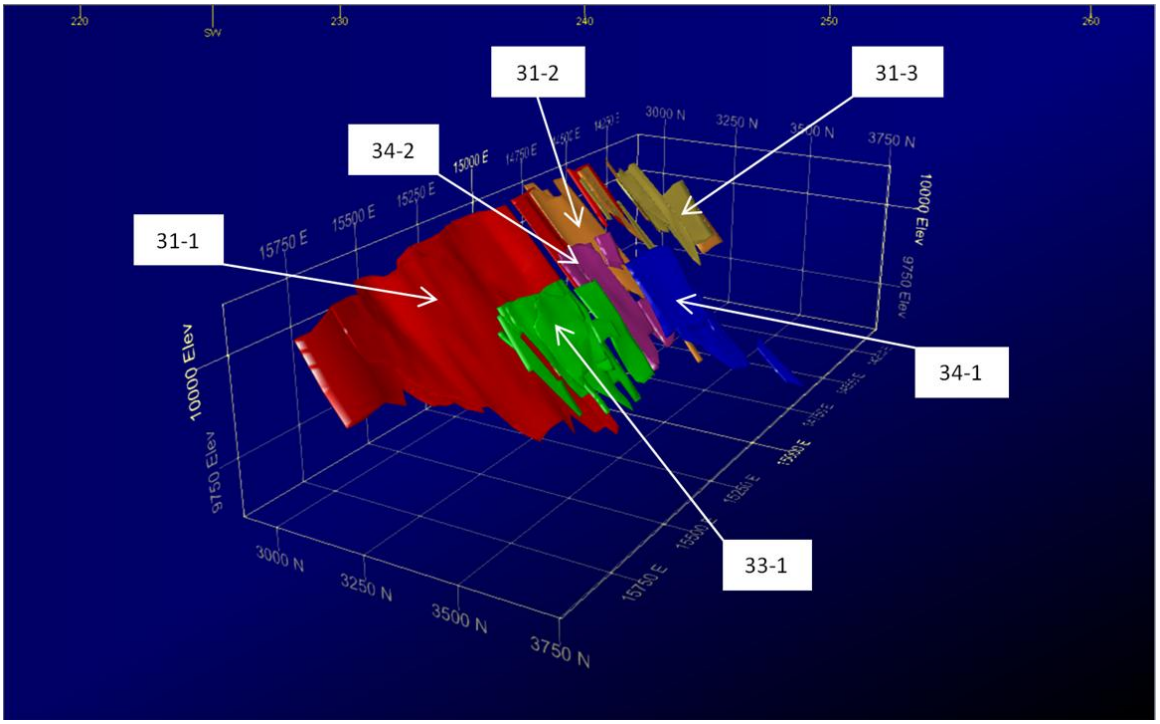


Figure 14.12 - Isometric view of Pump 3D high-grade zones looking to the Southwest (MEL22 grid)

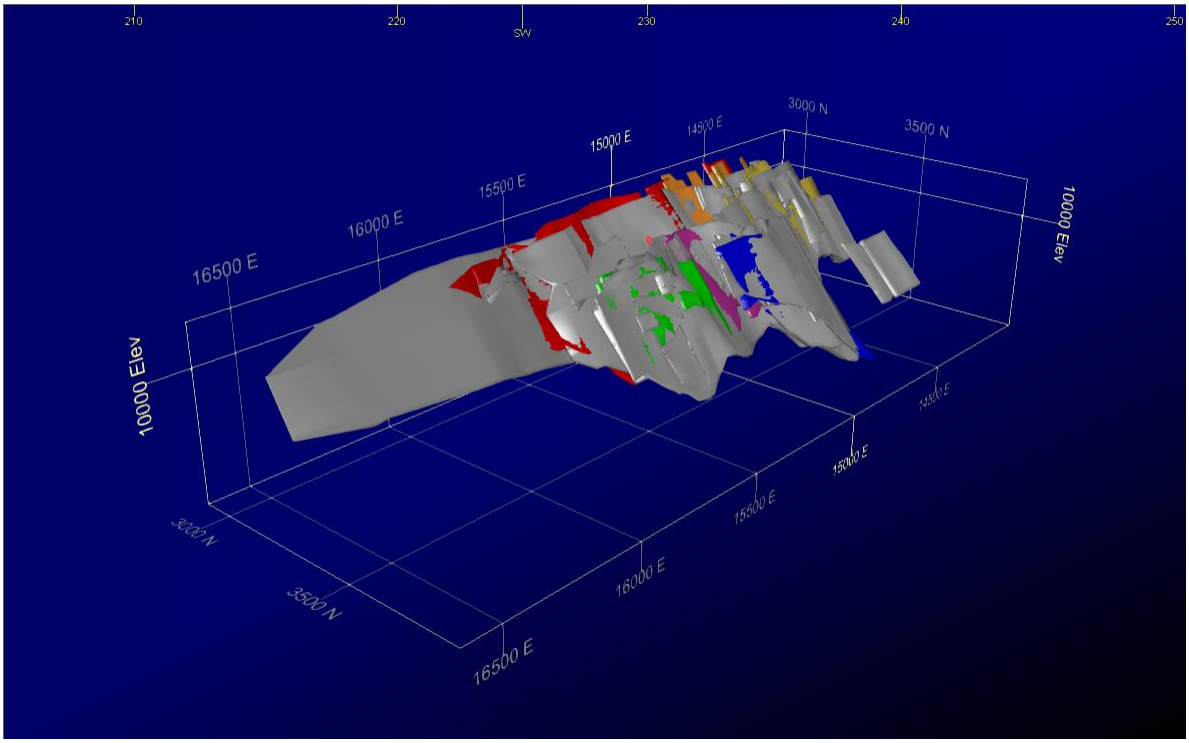


Figure 14.13 - Isometric view of the Pump low-grade domain (iron formation bands) in grey, looking to the southwest (MEL22 grid)

14.2.1.7 Wolf deposit

The Wolf deposit consists of 14 zones divided into two domains according to the stratigraphy:

- 23 series: zones 2310, 2320 and 2330 hosted by the Upper Oxide Formation sedimentary rocks
- 21 series: zones 2107 to 2305 hosted by the Wesmeg Formation mafic volcanic rocks

The zones are recognized by the intensity of quartz veining and the presence of iron formation bands in the Upper Oxide Formation and in the Wesmeg Formation.

All zones strike west-northwest (approximately 292°) and dip approximately 65° to 70° to the northeast. Mineralization is interpreted to extend 1.4 km long by 550 m deep. The average true width of the package is approximately 40 m for both domains but there is generally a 5- to 25-m waste horizon separating the mineralized zones.

A detailed listing of all zones is given in Appendix 14.2 and a plan view of the Wolf geological interpretation is shown in Figure 14.14.

There is no low-grade domain at the Wolf deposit.

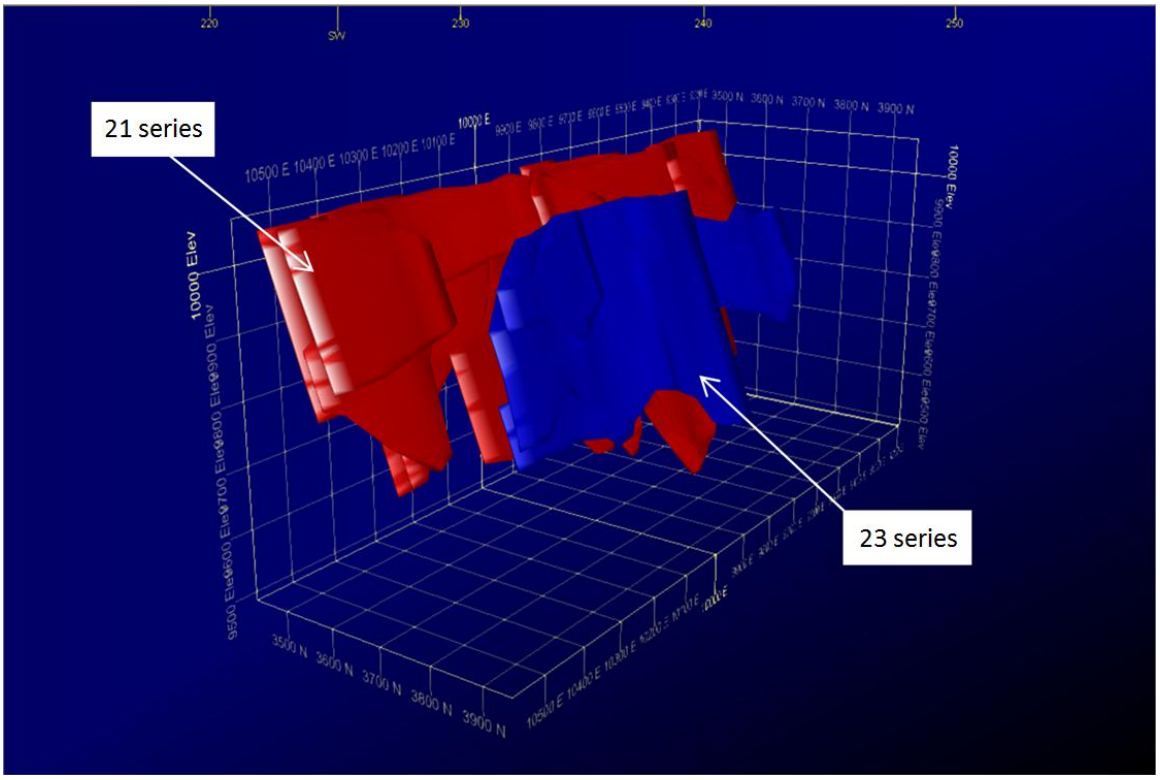


Figure 14.14 - Isometric view of the Wolf 3D high-grade zones looking to the southwest

14.2.2 Definition of Grade Estimation Domains

Grade estimation domains, which are subdivisions of the geological model and are represented by subsets of the sample data, ensure that samples used for estimating a block grade are from the same population as the point of estimation. In this report, the grade estimation domain is called a

"zone". A grade population may be defined by attributes such as spatial location, lithology, mineralization style and structural boundaries.

The Meliadine mineral resources have been estimated and reported individually for each deposit. Data for each deposit have been further divided into sub-domains according to the geological interpretations. All grade estimation domains are detailed in Appendix 14.2.

14.3 Sample Statistics

The number of drill-holes and samples selected based on geological interpretations and used in the current Meliadine mineral resource estimate are shown in Table 14.4. Channel and chip samples were used in the interpretation of the Tiriganiaq and Discovery deposits, but were excluded from the block model estimation.

Table 14.4 - Number of drill-holes used in the Meliadine mineral resource estimate as of December 31, 2014

Deposit	Number of drill-holes	Number of samples	Total metres drilled
Tiriganiaq	964	21,108	305,198
Wesmeg	415	4,595	109,517
Normeg	445	3,310	135,131
Discovery	169	1,972	34,866
F zone	320	3,650	52,157
Pump	249	2,041	51,128
Wolf	96	1,325	27,693
Total	**2,658**	**38,001**	**715,690**

14.3.1 Extreme Grade Value Treatment

Extreme grade values are considered to be those that lie outside the range of values expected, based on the distribution of the samples in each lithological unit. Top cuts of extreme values, by re-setting outlier grades to a lower grade, are made to prevent over-estimation in grade estimation domains due to disproportionately high-grade outliers during the interpolation technique.

For the Meliadine project, Agnico Eagle examined gold assay grades for each lithological unit in each deposit to identify the presence and nature of extreme grade values. Lithological codes are described in Appendix 14.3. This is an unusual practice, and comes from the recommendations of the 2008 and 2011 bulk sample programs:

"…lithology-specific capping in this environment may provide a tool to improve the gold grade estimate for this material…." (Strathcona, 2009)

"Successful resource grade estimation and underground grade control need to take this into account, since each of the lithologies, where part of a mineralized package, requires its own capping level". (Duquette and Thalenhorst, 2012)

Agnico Eagle has revised the RPA Inc. (RPA, 2013) and the SRK (SRK, 2013) grade-capping values established in 2012 and 2013, respectively, for all deposits except the F zone, which was not drilled in 2014. F zone is the only deposit to be capped by grade estimation domain.

The Snowden SuperVisor® (version 8.3) software (from Snowden) and Datamine software have been used for the extreme grade value treatment. Firstly, lithological units have been grouped according to their statistical similarities using Box-and-Whisker plots. Then the top-cut thresholds have been established using industry-standard approaches of decile analysis, identification of discontinuities in logarithmic probability plots, the number of samples in the domain and by examining the spatial location of extreme values. Once the top-cut thresholds have been determined to be required and established, statistics and plots are done again on capped samples, and their impact on the mean, the percentage metal lost and the coefficient of variation ("CV") of the sample data is examined.

At Tiriganiaq, which is the most important deposit at Meliadine, 19 different major rock units are present and grouped in eight main domains (Table 14.5) using the Box-and-Whisker plot. Then statistics and logarithmic probability plots are generated (Figure 14.15), top-cut thresholds are established and the statistics of capped samples are calculated (Table 14.6).

For the Normeg deposit, the lithological capping has been applied on a small search ellipsoid to restrict its influence, and then, for the second and third search ellipsoid, a capping by zone has been applied. Gold assays were capped prior to compositing (Table 14.7 and Table 14.8).

Table 14.5 - Tiriganiaq lithological groups for extreme value treatment

Group	Description	Number of samples
1-KMG	GRAPHITIC ARGILLITE	1
		1,111
2-K	SEDIMENTARY ROCKS	4
		44
3-K_K	MINERALIZED SEDIMENTARY ROCKS	5
		55
4-M	MAFIC AND ULTRAMAFIC VOLCANIC ROCKS	7
		77
		6
		8
		88
5-Q	QUARTZ VEINS	9
6-Q_Q	MINERALIZED QUARTZ VEINS	10
7-N	IRON FORMATION BANDS	11
		111
		2
8-N_N	MINERALIZED IRON FORMATION BANDS	12
		122
		3

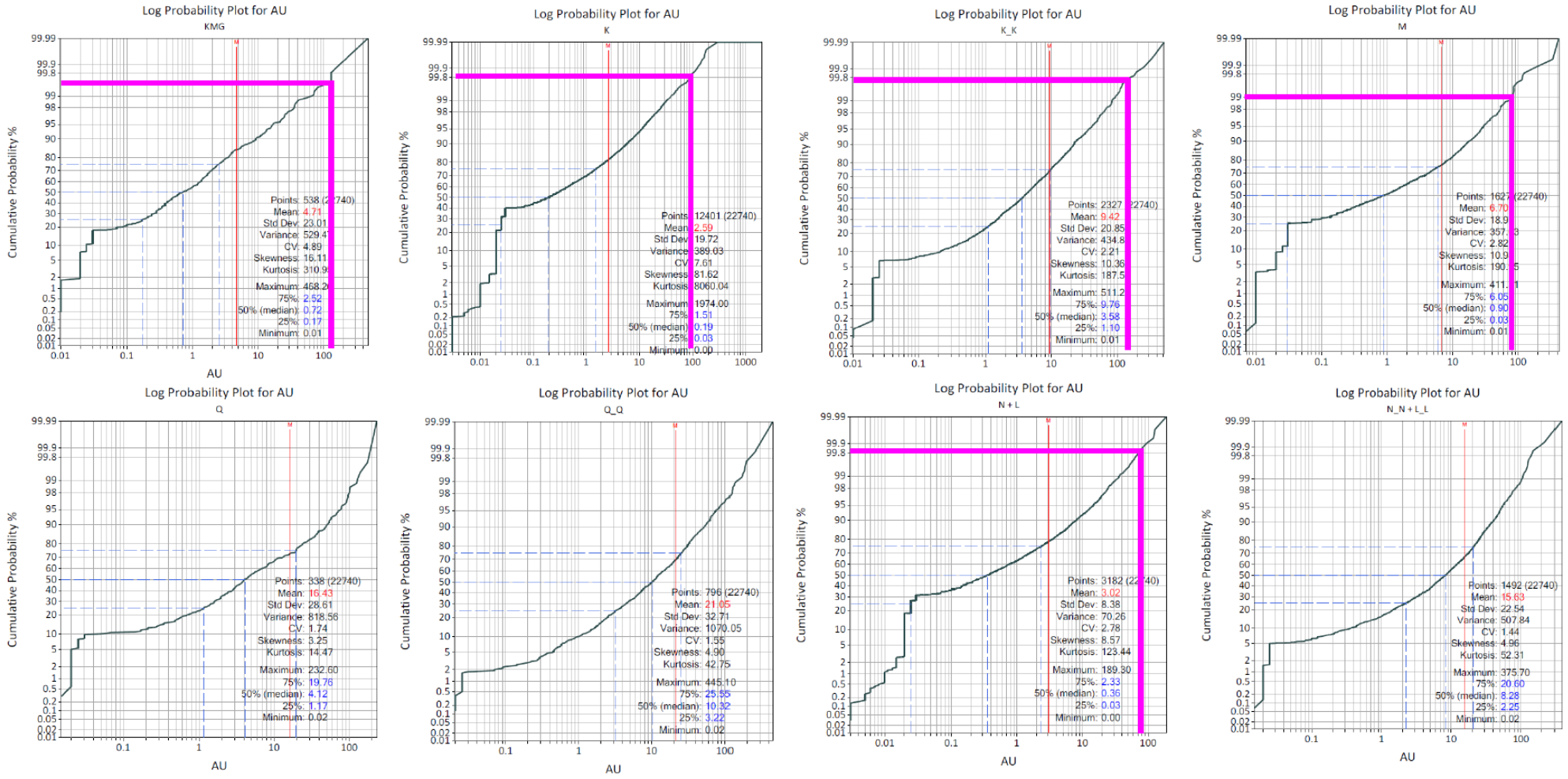


Figure 14.15 - Logarithmic probability plots for lithological units at Tiriganiaq; pink lines represent the top-cut gold grade values (g/t)

Table 14.6 - Basic statistics after capping of high-grade samples at Tiriganiaq

Group	Number of samples	Gold grade (g/t)				% metal lost	Capping (g/t gold)	Number of samples capped
		Min	Max	Mean	Cv			
1-kmg	538	0.01	125.00	2.76	3.13	13.5	125	3
2-k	12,401	0	100.00	2.01	3.28	10.4	100	19
3-k_k	2,327	0.01	150.00	8.73	1.79	2.6	150	5
4-m	1,666	0.01	80.00	5.57	2.12	7.6	80	19
6-q	338	0.02	232.60	17.65	1.72	0.0	250	0
7-q_q	796	0.02	445.10	20.81	1.53	0.0	450	0
8-n	3,182	0	80.00	2.85	2.56	2.7	80	5
9-n_n	1,492	0.02	375.70	14.85	1.50	0.0	400	0

Table 14.7 - Top cut values by lithological code for each deposit

Deposit	Rock type	Capping value (g/t)
Normeg*	KMG/L/K/OTH/KMGqv/N/Q	25
	L_L/K_K/Q_Q/K_Kqv/M_M/M_Mqv	150
	M/Mqv	120
	Low Grade domain (Mafic volcanic rock)	25
Discovery	L / Q / Q_Q/ N / OTHERS	55
	K / K_K	5
	N_N	100
	Low grade domain (Iron Formation bands)	55
Tiriganiaq	KMG / KMG-qv	125
	K / K-qv	100
	K_K / K_K-qv	150
	M / M-qv	80
	Q	250
	Q_Q	450
	N / N-qv / L	80
	N_N / N_N-qv / L_L	400
Pump	L / N	35
	L_L / Q_Q	95
	M/ M_M/ Mg /Q/ OTHERS	25
	K / Kmg	35
	Low grade domain (Iron Formation bands)	35
Wesmeg	L/ L_L/ N/ N_N/ Lqv/ L_Lqv	40
	K/ OTHERS	10
	M/ M_M/ Q/ Q_Q/ Mqv	60
	Low grade domain (Iron Formation bands)	40
Wolf	L/ L_L	35
	K_K/ K_K-qv/Q_Q/N_N/N_N-qv	70
	M-qv/M_M/M_M-qv	10
	Q /N/N-qv/OTHERS	15
	K/ K-qv/ Kmg	30
	M/ Mg	35

*For first pass estimation

Table 14.8 - Top-cut values by high-grade domains for the F zone and Normeg deposits

Deposit	Zone	Capping value (g/t gold)
F zone	4100	30
	4105	5
	4110	30
	4115	30
	4120	30
	4130	60
	4135	60
	4137	30
	4140	30
	4150	30
	4160	30
	4170	30
	4180	30
Normeg*	901	25
	902	25
	903	25
	904	25
	905	25
	906	15
	907	25
	909	35
	910	35
	911	45
	920	60
	921	60
	922	60
	923	45
	924	60
	925	60
	930	15
	987	25
	988	25

*For second and third passes estimation

14.3.2 Sample Compositing

After applying top-cutting values to the extreme grades, the samples located within the grade estimation domains were length-composited to ensure that the samples used in statistical analyses and estimations had similar support *(i.e.*, length). Comaplex, Agnico Eagle and previous operators have sampled drill-holes at various interval lengths depending on the length of intersected geological features; in geologically similar units, they have selected samples at 1-m or 1.5 m lengths. Sample lengths for all estimation domains in the Tiriganiaq, Wesmeg, Normeg, Discovery, Pump and Wolf deposits were examined and composited according to the most frequently sampled length interval. For F zone, sample lengths have been composited to 1.5-m as recommended by RPA (RPA, 2013).

Table 14.9 shows the composite length for each deposit, and the percentage of samples that were less than or equal to the selected composite length. The composited and raw sample data were compared to ensure no sample length loss or metal loss had occurred.

The Datamine software COMPDH downhole compositing process was used to composite the samples within the estimation domains (*i.e.*, composites do not cross over the mineralized domain boundaries). The COMPDH parameter MODE was set to a value of 1 to allow adjusting

of the composite length while keeping it as close as possible to the composite interval. This was done to minimize sample loss, and to ensure equal sample support.

Table 14.9 - Sample composite length by domain by deposit

Deposit		Composite length (m)	Number of composites	% of samples less than or equal to the composite length
Tiriganiaq	High Grade	1.0	18,143	64%
	Low Grade	1.0	60,313	59%
Normeg	High Grade	1.0	3,365	71%
	Low Grade	1.0	60,479	62%
Wesmeg	High Grade	1.0	4,279	66%
	Low Grade	1.0	3,795	62%
Discovery	High Grade	1.0	1,541	66%
	Low Grade	1.0	5,104	59%
F zone	High Grade	1.5	2,187	70%
	Low Grade	2.0	1,891	68%
Pump	High Grade	1.0	1,884	68%
	Low Grade	1.0	6,355	59%
Wolf	High Grade	1.0	1,175	55%

14.4 Variography

Continuity analysis refers to the analysis of the spatial correlation of a grade value between sample pairs to determine the major axis of spatial continuity. Continuity analysis was undertaken for gold by grade estimation domain for each deposit using 1-m composites for high-grade and low-grade domains. Snowden SuperVisor® (version 8.3) software was used for the variographic study, and the variogram parameters have been transformed to respect Datamine conventions.

Most deposits except Normeg were subdivided into domains according to changes in the strike and dip within estimation domains, to allow for better definition of the major axes of spatial continuity within each domain. Geological information and ore shoot orientation have also been considered during the modelling.

Pairwise relative variograms were made for gold, while normal score transformed variograms were made for density, mainly for deposits where density was estimated (see Appendix 14.3). The nugget effect was handled first using downhole variograms, and then directional variograms were made using the variance contour fans to set the direction of maximum continuity. Examples of variograms for the Tiriganiaq 1100 lode are shown in (Figure 14.16). Generally, horizontal and across-strike maximum continuity are similar to the orientation of the 3D solids.

Variogram modelling at Tiriganiaq was done for five groups (the 1250 and 1350 series are combined) and for the north and south low-grade domains (Upper Oxide Formation). The nugget effect varies between 0.19 and 0.41. All domains have a dominant exponential structure followed by a secondary spherical structure. In accord with the current geological understanding at Tiriganiaq, a pronounced anisotropy was modelled in the ore shoot directions. For the 1000, 1000 series, and 1100 domains, the direction of maximum continuity plunges between 20 and 30° to the east. For all other groups, the direction of maximum continuity plunges approximately 15° to the west. Variogram parameters are detailed in Table 14.10 for high-grade domains and in Table 14.11 for low-grade domains.

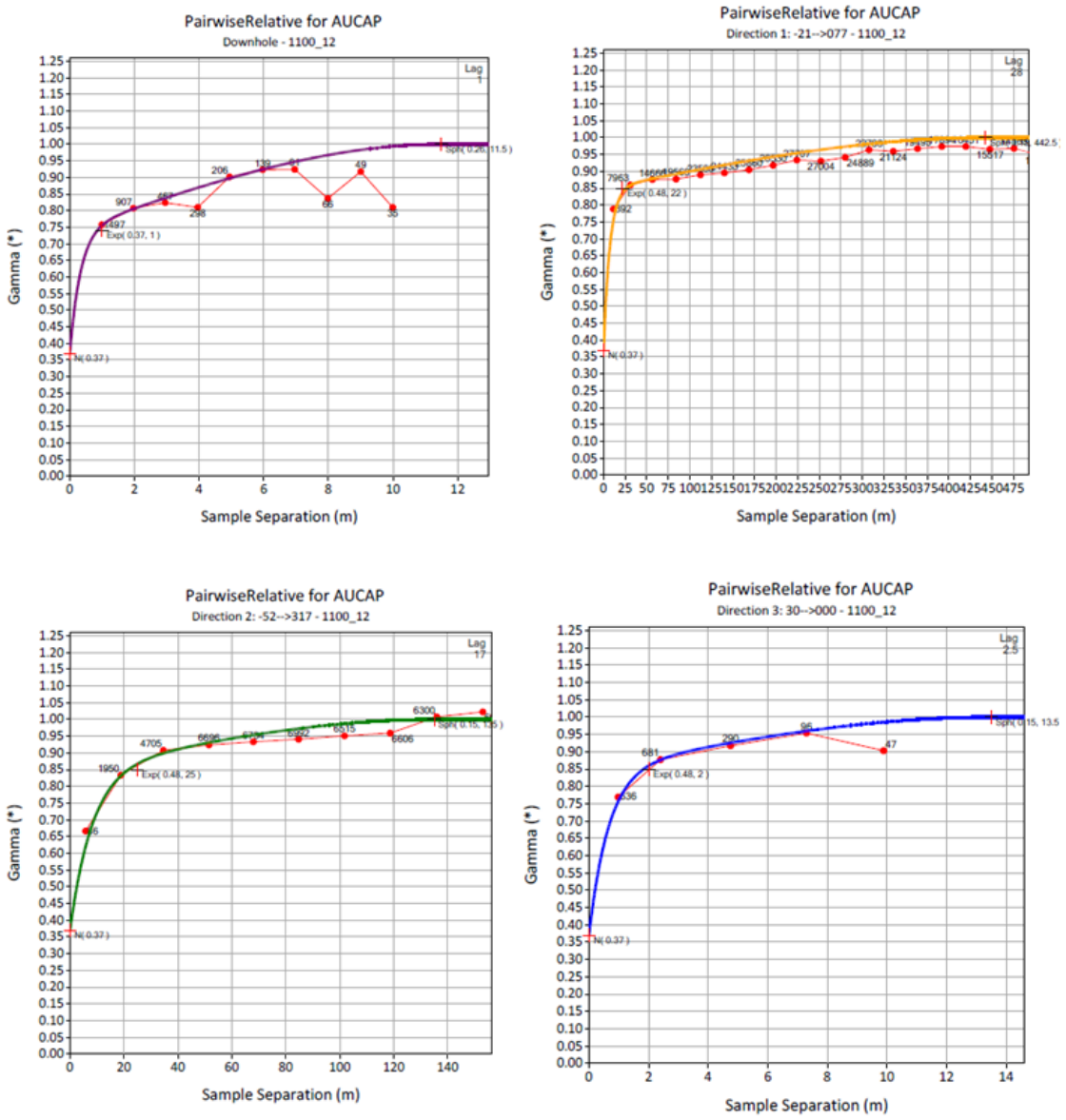


Figure 14.16 - Variograms for Tiriganiaq 1100 lode

Table 14.10 - Variogram parameters for gold for high-grade domains at the Tiriganiaq deposit

1000										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	079 / -26	316 / -49	005 / 30
0.19	0.3	1.5	0.51	3.5	0.19	EXP	0.55	10.5	13.5	2.5
						SPH	0.26	132	43.5	6.5
1000 SERIES (ZONES 1015 / 1025 / 1050 / 1075 / 1087)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	080 / -17	324 / -54	000 / 30
0.35	0.3	2	0.22	10	0.35	EXP	0.45	25.5	18.5	5
						SPH	0.07	170.5	58	9.5
1100 (ZONES 1100 / 1102)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	077 / -21	317 / -52	000 / 30
0.37	0.37	1	0.26	11.5	0.37	EXP	0.48	22	25	2
						SPH	0.15	442.5	135	13.5
1150 SERIES (ZONES 1150/1151/1152/1153/1154/1155/1156/1157/1170)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	280 / -14	223 / 65	005 / 20
0.49	0.36	3.5	0.15	28	0.49	EXP	0.39	19.5	14.5	12
						SPH	0.12	187.5	75.5	30.5
1250-1350 (ZONES 1251/1252/1253/1254/1255/1256/1257/1258/1260/1261/1262/1263/1264/1265/1270/1350/1360)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	276 / -14	212 / 61	000 / 25
0.41	0.45	2	0.14	11	0.41	EXP	0.52	38	15.5	21.5
						SPH	0.07	193	30	26

Table 14.11 - Variogram parameters for gold for low grade domains at the Tiriganiaq deposit

LOW-GRADE DOMAIN SOUTH										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	071 / -30	306 / -45	000 / 30
0.24	0.27	2.5	0.09	4.5	0.24	EXP	0.32	24	14.5	2.5
						SPH	0.09	40	40.5	13
LOW-GRADE DOMAIN NORTH										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	276 / -14	212 / 61	000 / 25
0.36	0.1	2.5	0.18	4.5	0.36	EXP	0.20	10.5	10.5	2
						SPH	0.11	33	18	19

Variogram modelling at Wesmeg was done for the five domains. The nugget effect is relatively low: 0.14 and 0.27. All of them have a dominant exponential structure followed by a secondary spherical structure. The absence of evident anisotropy at Wesmeg generates variograms with similar horizontal and across-strike continuities. The 200-300 domain is located in a poorly drilled area and the maximum direction continuity is influenced by the drill-hole distribution. Variogram parameters are detailed in Table 14.12. The variogram parameters of zone 650 have been used to estimate the low-grade domain (iron formation bands).

Table 14.12 - Variogram parameters for gold at the Wesmeg deposit

200-300										
(ZONES 225/230/235/240/250/270/280/290/300/310/320/330/360)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	095 / 00	005 / -60	005 / 30
0.14	0.55	1	0.18	4.5	0.14	EXP	0.67	59	50.5	2
						SPH	0.06	103.5	72	2.5
400 LOW										
(ZONES 420/430/435/440/450)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	075 / -30	311 / -45	005 / 30
0.25	0.34	1.5	0.09	6	0.25	EXP	0.30	44.5	43	1
						SPH	0.13	79.5	85	6
400 HIGH										
(ZONES 455/460/470/475/480/490/500/510)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	332 / -52	272 / 21	015 / 30
0.27	0.46	2	0.08	19.5	0.27	EXP	0.37	61	25	2
						SPH	0.17	122	81	37
650										
(ZONE 650)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	064 / -42	298 / -34	005 / 30
0.24	0.36	2	0.16	6.5	0.24	EXP	0.43	73.5	84.5	2.5
						SPH	0.09	108	106.5	12.5
600-700										
(ZONES 520/600/625/660/670/710/720/730/740)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	286 / -23	233 / 55	005 / 25
0.20	0.43	2	0.14	5	0.20	EXP	0.39	22	50.5	1.5
						SPH	0.18	89.5	113.5	11

Variogram modelling at Normeg was done combining all grade estimation domains together to have sufficient data. The nugget effect is 0.37. A dominant exponential structure and two secondary spherical structures were modelled. A slight anisotropy with a maximum continuity direction plunging approximately 25° to the east was modelled, reflecting the ore shoot direction, according to the current geological understanding. The short ranges are explained by the specific nature of the Normeg deposit characterized by quartz-vein-rich pipes hosted by mafic volcanic rocks with the absence of iron formation bands. The same variogram parameters have been used to estimate the low-grade domain. Variogram parameters are detailed in Table 14.13.

Table 14.13 - Variogram parameters for gold at the Normeg deposit

ALL ZONES												
DOWN-THE-HOLE							DIRECTIONAL					
C0	C1	H1	C2	H2	C3	H3	C0	STR TYPE	C1/C2	077 / -21	317 / -52	000 / 30
0.37	0.33	1	0.09	13.5	0.12	28.5	0.37	EXP	0.33	28.5	13	1.5
								SPH	0.1	58.5	60	12
								SPH	0.11	80.5	63	38

Variogram modelling at Pump was done for the six domains. The nugget effect varies between 0.21 and 0.38. A dominant exponential structure and a secondary spherical structure were modelled. There is anisotropy at Pump expressed by the plunge of the shoots to the west. Depending on the domain, this anisotropy is more or less pronounced. For domains 31-3 and 34-2, the scant drill information influences the maximum continuity direction, which is mostly horizontal. For domains 31-2 and 34-1, the maximum continuity direction follows the anisotropy with a steep plunge of 70° to the west. For the two main domains, 31-1 and 33-1, the

maximum continuity direction plunges 50° to 60° to the west. The variogram parameters of the 31-1 domain have been used to estimate the low-grade domain (iron formation band). Variogram parameters are detailed in Table 14.14.

Table 14.14 - Variogram parameters for gold at the Pump deposit

31-1										
(ZONES 3100 / 3101)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	320 / -30	250 / 30	015 / 45
0.21	0.38	3	0.41	4.5	0.21	EXP	0.37	99	35.5	3
						SPH	0.42	200.5	117	3.5
31-2										
(ZONES 3109 / 3110 / 3130)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	160 / 46	087 / -15	010 / 40
0.28	0.25	2	0.47	3	0.28	SPH	0.38	54	42.5	2
						SPH	0.34	83.5	60.5	4
31-3										
(ZONES 3165 / 3180 / 3190 / 3195)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	323 / -42	246 / 14	350 / 45
0.26	0.16	4	0.58	17	0.26	EXP	0.38	14.5	53	11
						SPH	0.36	229.5	308.5	19
33-1										
(ZONES 3300 / 3301 / 3310 / 3320 / 3330 / 3340)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	321 / -48	075 / -20	180 / -35
0.42	0.16	1.5	0.42	12.5	0.42	EXP	0.20	52	28	2
						SPH	0.38	156	100	31.5
34-1										
(ZONES 3411 / 3412 / 3413 / 3440 / 3460)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	308 / -50	238 / 16	340 / 35
0.20	0.42	2	0.38	11.5	0.20	EXP	0.48	57.5	71.5	2.5
						SPH	0.32	246	216	17
34-2										
(ZONES 3299 / 3341 / 3400 / 3402 / 3405)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	327 / -48	250 / 11	350 / 40
0.38	0.54	2.5	0.08	3.5	0.38	EXP	0.28	30	92	5
						SPH	0.34	100	94	17

For Discovery, because the orientations of the lodes change over the deposit, the dynamic anisotropy option in Datamine Studio 3 software was used. This option allows the search volume to be oriented precisely along the trend of mineralization, since the ellipsoid orientation is calculated in each block. During the kriging interpolation, the variogram parameters are adjusted for each block according to the search ellipsoid direction of that block. Variogram modelling at Discovery was done for the three domains. The nugget effect is relatively low: 0.18 to 0.31. A dominant exponential structure and a secondary spherical structure were modelled. There is anisotropy at Discovery corresponding to the ore shoot orientations to the east. Depending on the domain, this anisotropy is more or less pronounced. For domain 51, the scarce drill information influences the maximum continuity direction, which is mostly horizontal. For groups 52 Low and 52 High, the maximum continuity direction plunges at 60° to 65° to the east. This plunge corresponds to the ore shoots observed in the deposit, and the anisotropy is strong, especially for 52 low. The variogram parameters of zone 5210 have been used to estimate the low-grade domain (iron formation bands). Variogram parameters are detailed in Table 14.15.

Table 14.15 - Variogram parameters for gold at the Discovery deposit

51										
(ZONES 5110 / 5120 / 5130 / 5140 / 5150)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	048 / -55	281 / -23	000 / 25
0.18	0.36	1	0.65	4	0.18	EXP	0.59	37	54.5	2.5
						SPH	0.41	75.5	81.5	3.5
52 LOW										
(ZONES 5210 / 5220 / 5310)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	051 / -42	292 / -28	000 / 35
0.2	0.52	2	0.28	5.5	0.2	EXP	0.65	47	13	4
						SPH	0.15	222.5	54	12
52 HIGH										
(ZONES 5230 / 5240)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	055 / -46	308 / -15	025 / 40
0.31	0.36	1.5	0.33	5	0.31	EXP	0.51	41	42	3.5
						SPH	0.18	81.5	57.5	14.5

Variogram modelling at Wolf was done for the two domains. The nugget effect is differes significantly: 0.07 and 0.31 for the Upper Oxide Formation and the Wesmeg Formation, respectively. The zones in the Upper Oxide Formation are wider than those in the Wesmeg Formation. Where the zones are narrow, the inclusion of sterile samples in the intersection to respect the minimum mining width could contribute to increasing the nugget effect. A dominant exponential structure and a secondary spherical structure were modelled. There is anisotropy for the Upper Oxide Formation Group corresponding to an ore shoot orientation to the west. For the Wesmeg Formation domain, no anisotropy has been observed, so the maximum continuity directions for the horizontal and across-strike directions are the same. The ranges are longer, because the Wolf deposit gold grade is lower than in the deposits. Variogram parameters are detailed in Table 14.16.

Table 14.16 - Variogram parameters for gold at the Wolf deposit

Gold - DOMAIN 21										
(ZONES 2107 / 2110 / 2112 / 2115 / 2120 / 2125 / 2130 / 2140 / 2240 / 2300 / 2305)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	307 / -55	074 / -23	175 / -25
0.31	0.46	2	0.23	22.5	0.31	EXP	0.48	80.5	73	2
						SPH	0.21	297	310	17.5
Gold - DOMAIN 23										
(ZONES 2310 / 2320 / 2330)										
DOWN-THE-HOLE					DIRECTIONAL					
C0	C1	H1	C2	H2	C0	STR TYPE	C1/C2	291 / -50	072 / -33	175 / -20
0.07	0.68	2.5	0.25	10	0.07	EXP	0.72	69.5	69.5	3
						SPH	0.21	199	93.5	6.5

The F zone deposit was reviewed by RPA Inc. (RPA, 2013). Variograms were computed in individual major zones such as the 4110, 4120 and 4130 zones. A variogram of zone 4120 was used for the other zones. The variograms for these zones show a very high nugget effect and rather short ranges. These two features demonstrate a rather short or small continuity. Also, anisotropies were weak or difficult to observe. At F zone, the variograms have been used for ordinary kriging estimation as a comparison method since the inverse distance squared ("ID^2") method has been adopted as the official estimation method and variogram ranges are used as a guide for the categorization processes.

14.5 Estimation Parameters

14.5.1 Sample Search Parameters

For the Tiriganiaq, Wesmeg, Normeg, Pump, Discovery and Wolf deposits, the search ellipsoids were created based on the variogram ranges and orientation.

At Tiriganiaq, the search ellipsoids dimension for the high-grade domains and the south low-grade domain is 85% to 90% of the sill for the first pass, 90% to 95% of the sill for the second pass, and 95% to 100% of the sill for the third pass. The north low-grade domain at Tiriganiaq shows relatively low ranges, and for this reason 100% of the sill has been used for the first pass, 200% of the sill for the second pass and then 300% for the third pass (Table 14.17).

Table 14.17 - Search parameters for Tiriganiaq high-grade and low-grade domains

			1000		
			(ZONE 1000)		
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	5	40	80	120
X	1	60	15	30	45
Z	3	-30	5	10	15
			1000 SERIES		
			(ZONES 1015 / 1025 / 1050 / 1075 / 1087)		
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	0	30	60	90
X	1	60	15	30	45
Z	3	-20	5	10	15
			1100		
			(ZONES 1100 / 1102)		
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	0	50	100	150
X	1	60	30	60	90
Z	3	-25	5	10	15
			1150 SERIES		
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	5	30	75	90
X	1	70	15	37.5	45
Z	3	-165	10	25	30
			1250-1350 SERIES		
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	0	30	45	90
X	1	65	10	15	30
Z	3	-165	13	19.5	39
			LOW-GRADE DOMAIN SOUTH		
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	0	20	40	80
X	1	60	15	30	60
Z	3	-35	5	10	20
			LOW-GRADE DOMAIN NORTH		
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	0	35	70	140
X	1	65	20	40	80
Z	3	-165	20	40	80

For the Wesmeg deposit, the first pass of the search ellipsoid was established at 75% of the sill, the second pass at 85% of the sill and third pass at 95% of the sill Table 14.18.

Table 14.18 - Search parameters for Wesmeg high-grade and low-grade domains

200-300 (ZONES 225/230/235/240/250/270/280/290/300/310/320/330/360)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	5	25	37.5	75
X	1	60	20	30	60
Z	3	0	5	7.5	15
400 LOW (ZONES 420/430/435/440/450)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	5	35	52.5	87.5
X	1	60	30	45	75
Z	3	-35	5	7.5	12.5
400 HIGH (ZONES 455/460/470/475/480/490/500/510)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	15	30	60	90
X	1	60	15	30	45
Z	3	-115	5	10	15
ZONE 650 AND LOW-GRADE DOMAIN (BIF)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	5	30	45	75
X	1	60	30	45	75
Z	3	-50	5	7.5	12.5
600-700 (ZONES 520/600/625/660/670/710/720/730/740)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	5	15	30	45
X	1	65	30	60	90
Z	3	-155	5	10	15

At the Normeg deposit, a first search ellipsoid has been used to constrain the influence of the gold grade capping by lithology, and corresponds to a quarter of the second search ellipsoid. The second pass of the search ellipsoid was established at 93% of the sill, the third pass at 99% of the sill and last pass at 100% of the sill Table 14.19.

Table 14.19 - Search parameters for Normeg high-grade and low-grade domains

GOLD - ALL ZONES						
DATAMINE ROTATION			ELLIPSOID			
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS	4TH PASS
Z	3	0	10	40	60	80
X	1	60	7.5	30	45	60
Z	3	-25	2.5	10	15	20

For the Pump deposit, the first search ellipsoid was derived by taking approximately 75% of the sill of the directional variogram, the second pass was at 85% of the sill and the third pass was at 95% of the sill Table 14.20.

Table 14.20 - Search parameters for Pump high-grade and low-grade domains

31-1 (ZONES 3100 / 3101) AND LOW-GRADE DOMAIN (BIF)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	15	70	105	175
X	1	45	35	52.5	87.5
Z	3	-135	5	7.5	12.5
31-2 (ZONES 3109 / 3110 / 3130)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	10	30	60	90
X	1	50	25	50	75
Z	3	70	5	10	15
31-3 (ZONES 3165 / 3180 / 3190 / 3195)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	-10	50	100	150
X	1	45	70	140	210
Z	3	-110	5	10	15
33-1 (ZONES 3300 / 3301 / 3310 / 3320 / 3330 / 3340)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	180	40	80	120
X	1	125	25	50	75
Z	3	-65	10	20	30
34-1 (ZONES 3411 / 3412 / 3413 / 3440 / 3460)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	-20	50	100	150
X	1	55	55	110	165
Z	3	-110	5	10	15
34-2 (ZONES 3299 / 3341 / 3400 / 3402 / 3405)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	-10	25	37.5	62.5
X	1	50	35	52.5	87.5
Z	3	-105	5	7.5	12.5

For Discovery, the first pass is a rounded range of 75% of the variogram sill, the second pass is 85% of the sill and the third pass is 95% of the sill Table 14.21.

Table 14.21 - Search parameters for Discovery high-grade and low-grade domains

51 (ZONES 5110 / 5120 / 5130 / 5140 / 5150)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	0	25	37.5	50
X	1	65	30	45	60
Z	3	-65	5	7.5	10
LOW-GRADE DOMAIN (BIF) AND 52 LOW (ZONES 5210 / 5220 / 5310)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	0	25	37.5	75
X	1	55	10	15	30
Z	3	-55	5	7.5	15
52 HIGH (ZONES 5230 / 5240)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	25	20	30	60
X	1	50	15	22.5	45
Z	3	-70	5	7.5	15

For Wolf, the first pass is a rounded range of 75% of the variogram sill, the second pass is 85% of the sill and the third pass is 95% of the sill (Table 14.22).

Table 14.22 - Search parameters for Wolf high-grade domains

21 (ZONES 2107 / 2110 / 2112 / 2115 / 2120 / 2125 / 2130 / 2140 / 2240 / 2300 / 2305)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	175	45	90	180
X	1	115	40	80	160
Z	3	-65	5	10	20
23 (ZONES 2310 / 2320 / 2330)					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES	1ST PASS	2ND PASS	3RD PASS
Z	3	175	40	80	120
X	1	110	35	70	105
Z	3	-55	5	10	15

For the F zone deposit, the first search volumes were based on continuities observed in the variograms done by RPA (2013). It was suggested by RPA (2013) to use a larger second search volume for the gold interpolation and the first one for the categorization process.

Table 14.23 - Search parameters for F zone high-grade domains

ALL ZONES					
DATAMINE ROTATION			ELLIPSOID		
AXIS	SAXIS	ANGLES*	1ST PASS	2ND PASS	3RD PASS
Z	3	269	50	80	80
X	1	51	30	50	50
Z	3	0	10	15	20

*Average angle it is slightly different for each zone but varies between 264° and 283° and dips between 48° and 52°

For all deposits, during the estimation process if insufficient numbers of samples and holes were located within the first search volume centred on the cell being estimated, a second search was used. If sufficient samples and holes were still not encountered, a third search volume was used. If the minimum number of samples required was not encountered in the third search volume, no estimate was made. A minimum of two holes is required for the first and the second pass. Table 14.24 and Table 14.25 detail the sample search parameters for the resource estimate. Minimum and maximum sample numbers per hole were selected in order to prevent over-smoothing of grades in the estimate.

Table 14.24 - Sample search parameters for high-grade and low-grade gold estimates

Deposit	Domain	First Search Volume		Second Search Volume		Third Search Volume		Maximum Number of Samples Per Drill-hole	
		Minimum Number	Maximum Number	Minimum Number	Maximum Number	Minimum Number	Maximum Number	Svol 1 & 2	Svol 3
Tiriganiaq	High-Grade	4	12	4	12	3	12	3	3
Tiriganiaq	Low-Grade	4	12	4	12	3	12	3	3
Normeg	High-Grade	4	12	4	12	3	12	3	3
Normeg	Low-Grade	4	12	4	12	3	12	3	3
Wesmeg	High-Grade	4	12	4	12	3	12	3	3
Wesmeg	Low-Grade	4	12	4	12	3	12	3	3
Discovery	High-Grade	4	12	4	12	3	12	3	3
Discovery	Low-Grade	4	12	3	12	0	0	3	3
F zone	High-Grade	3	10	3	10	2	10	2	0
F zone	Low-Grade	3	10	-	-	-	-	2	-

Pump	High-Grade	3	8	3	8	2	8	2	2
Pump	Low-Grade	3	8	3	8	2	8	2	2
Wolf	High-Grade	4	12	4	12	3	12	3	3

Table 14.25 - Sample search parameters for density (specific gravity) estimates

Deposit	Domain	First Search Volume		Second Search Volume		Third Search Volume		Maximum Number of Samples Per Drill-hole	
		Minimum Number	Maximum Number	Minimum Number	Maximum Number	Minimum Number	Maximum Number	Svol 1 & 2	Svol 3
Tiriganiaq	SG	2	3	2	3	2	3	0	0
Pump	SG	2	3	2	3	2	3	0	0
Wolf	SG	2	3	2	3	2	3	0	0

14.6 Block Model

14.6.1 Block Size Selection

Block sizes were selected according to the average regular drill-hole spacing, the mine plan and the dimensions of the mineralized envelopes. Table 14.26 shows the block model parameters for the Meliadine mineral resource models. Discretization points in the blocks were set to four in each axis for all deposits.

Table 14.26 - Block model parameters

Deposit	Direction	Minimum Local Grid	Maximum Local Grid	Minimum UTM	Maximum UTM	Increment (m)	# Cells
Tiriganiaq	Easting	7500	11340	537500	541340	12	320
	Northing	8100	9105	6988100	6989105	3	335
	Elevation	9150	10250	-850	250	5	220
Normeg	Easting	7500	12000	537500	542000	12	375
	Northing	7500	9000	6987500	6989000	3	500
	Elevation	9000	10150	-1000	150	5	230
Wesmeg	Easting	7000	13900	537000	543900	12	575
	Northing	6300	8802	6986300	6988802	3	834
	Elevation	9000	10150	-1000	150	5	230
Discovery	Easting	3400	5704	529887	532773	12	192
	Northing	5100	7101	6992905	6993897	3	667
	Elevation	9500	10200	-500	200	5	140
F zone	Easting	17000	19544	566291	568928	12	212
	Northing	3400	4195	6977058	6977446	3	265
	Elevation	9400	10100	-600	100	5	140
Pump	Easting	14000	16160	563218	565524	12	180
	Northing	2700	3801	6976836	6977586	3	367
	Elevation	9600	10150	-400	150	5	110
Wolf	Easting	8500	11308	557786	560872	12	234
	Northing	2700	4701	6977695	6979233	3	667
	Elevation	9400	10200	-600	200	5	160

14.6.2 Block model coding

The domain coding was assigned by different 3D solids and 3D surfaces used to populate the block model. The high-grade domains, the low-grade domains, the overburden, the air, the voids (*i.e.*, underground ramp development) and the waste rock were coded in the block model. Within the final block model, a series of models was incorporated to add essential attributes to each block as the pit domain, the underground stopes and the open pit mine block.

Appendix 14.4 shows the block model attributes and a description of each field.

14.6.3 Grade Interpolation and Boundary Conditions

Grade interpolation was undertaken by grade estimation domain using an ordinary kriging estimate for all deposits except F zone, which was estimated using an ID^2 estimate. In all cases, ordinary kriging interpolation, ID^2 and the nearest neighbours method were undertaken for additional validation. The domain boundaries listed in Appendix 14.2 were treated as hard boundaries, so that samples lying in one domain were not used in the estimation of another, to prevent the smearing of grades from one domain to another.

For mineral reserves and pit shell generation, grade interpolation in the low-grade domains (the Upper Oxide Formation for Tiriganiaq, sericitic volcanic rocks for Normeg, and iron formation bands for all other deposits) was undertaken using an ordinary kriging estimate. Samples lying in high-grade domains were not used for this estimate.

14.7 Density

The density attribution for each rock type was initially determined using the density measurements made on samples during the drilling campaigns (Table 10.7).

Using these data, a fixed density was applied to all rock codes encountered in each deposit or each 3D lithological solid depending of the quality of the 3D lithological models (Appendix 14.3).

For the Tiriganiaq, Pump and Wolf low-grade and high-grade domains, length-weighted mean sample density values for the major units were assigned by lithological codes along the drill-hole (Appendix 14.3). Then the density was estimated as the gold into the block model inverse distance cubed interpolation and using specific estimation parameters derived from internal statistical studies. The blocks that were left unevaluated after the third search volume were assigned a fixed density value of 2.82 t/m^3.

For the Wesmeg, Normeg and Discovery deposits, the 3D lithological interpretation is well advanced and relatively simple, allowing a fixed density by 3D solids (mafic volcanics, iron formation bands, sedimentary rocks, graphitic argillite, lamprophyre, ultramafic volcanic rocks and gabbro dykes) (Appendix 14.3). Density in the high-grade domains of the F zone has been estimated, while density in the low-grade domains and the waste is fixed by 3D lithological solids.

14.8 Estimation of Mine Dilution

Waste rock dilution has been applied to the indicated resources at the end of the estimation process by applying a fixed percentage to the total tonnage. For the open pit indicated resources, an average dilution rate of 40% was fixed using a grade of 0 g/t gold for all deposits. For the underground indicated resources, an average dilution rate was fixed at 35% using a grade of 0 g/t gold for all deposits.

14.9 Mineral Resource Classification

In the current updated technical study on the Meliadine project, the mineral resource classification definitions used are the CIM Definition Standards for Mineral Resources and Reserves adopted by CIM Council on May 10, 2014 (CIM, 2014). The terms measured, indicated and inferred mineral resources are defined as follows:

Measured Mineral Resource: A Measured Mineral Resource is that part of a Mineral Resource for which quantity, grade or quality, densities, shape, and physical characteristics are estimated with confidence sufficient to allow the application of Modifying Factors to support detailed mine planning and final evaluation of the economic viability of the deposit. Geological evidence is derived from detailed and reliable exploration, sampling and testing and is sufficient to confirm geological and grade or quality continuity between points of observation. A Measured Mineral Resource has a higher level of confidence than that applying to either an Indicated Mineral Resource or an Inferred Mineral Resource. It may be converted to a Proven Mineral Reserve or to a Probable Mineral Reserve.

Indicated Mineral Resource: An Indicated Mineral Resource is that part of a Mineral Resource for which quantity, grade or quality, densities, shape and physical characteristics are estimated with sufficient confidence to allow the application of Modifying Factors in sufficient detail to support mine planning and evaluation of the economic viability of the deposit. Geological evidence is derived from adequately detailed and reliable exploration, sampling and testing and is sufficient to assume geological and grade or quality continuity between points of observation. An Indicated Mineral Resource has a lower level of confidence than that applying to a Measured Mineral Resource and may only be converted to a Probable Mineral Reserve.

Inferred Mineral Resource: An Inferred Mineral Resource is that part of a Mineral Resource for which quantity and grade or quality are estimated on the basis of limited geological evidence and sampling. Geological evidence is sufficient to imply but not verify geological and grade or quality continuity. An Inferred Mineral Resource has a lower level of confidence than that applying to an Indicated Mineral Resource and must not be converted to a Mineral Reserve. It is reasonably expected that the majority of Inferred Mineral Resources could be upgraded to Indicated Mineral Resources with continued exploration.

Agnico Eagle has considered all aspects affecting its confidence in the resource estimation, including:

- geological continuity (including geological understanding and complexity);
- data density and orientation;
- grade continuity.

14.9.1 Geological Continuity and Understanding

Comaplex and Agnico Eagle geologists have logged drill core in detail including textural, alteration, structural, mineralization and lithological properties. Agnico Eagle geologists are continuing to develop a good understanding of the geological controls on mineralization.

Field observations have been incorporated into the geological interpretation and variogram modelling, and considerable effort is constantly invested in the definition of mineralized lodes. For Tiriganiaq 1000 and 1100 lodes, underground exposure along approximately 200 m of strike length has validated the geological model and provided continued insight into geological continuity and the geological controls on mineralization.

For 1000 series called the “interveining lodes” and the 1150 to 1350 series, an oriented-drilling campaign from the underground exploration ramp in 2014 (Figure 14.17) allowed improvement of geological understanding and an increase the confidence in the model:

- Gold seems to be mainly hosted within quartz-carbonate veins more than within iron formation. Different quartz vein families have been identified but the most important network is mostly controlled by the E-W to ENE-WSW trend (Figure 14.18).
- Bedding, foliation and contact zones display parallel global E-W orientation, but some bedding and foliation in iron formation bands show a distinct dip of 34°-40° explained by the presence of tight folding, creating hinges that could act as a trap for gold deposition.

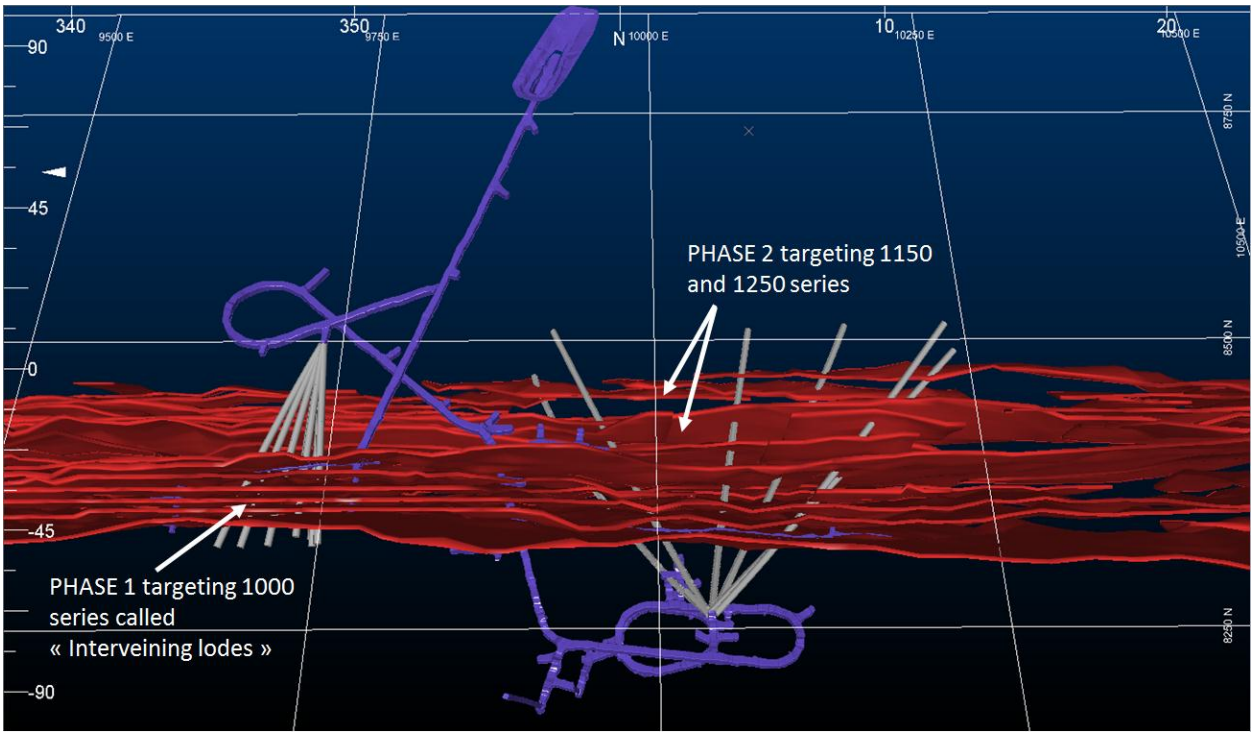


Figure 14.17 - 2014 underground oriented drilling campaign

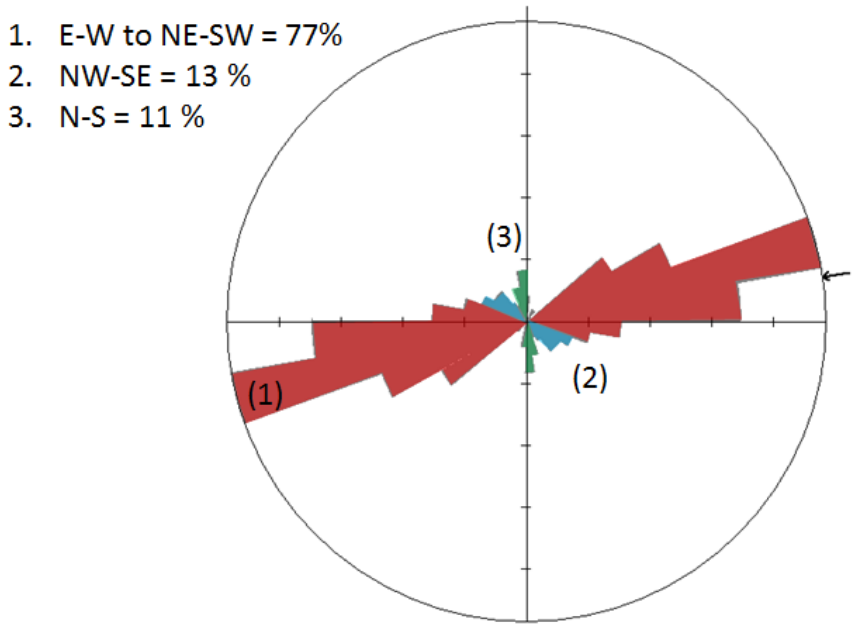


Figure 14.18 - Orientation of three quartz-carbonate vein networks observed at Tiriganiaq

14.9.2 Data Density and Orientation

The level of detail and confidence in the geological interpretation are closely related to data density, and this is reflected in the classification of confidence categories.

Except for geotechnical drilling, all drill-holes on deposits are drilled from north to south or northeast to southwest depending of their local grid (see Table 14.1). For oriented drilling (geotechnical and 2014 underground drilling), the orientation varies and is adjusted according to the objective.

14.9.3 Grade Continuity

Spatial grade continuity, as indicated by the variogram, is an important consideration when assigning confidence categories to a mineral resource estimate. The nugget effect and range variance characteristics of the variogram are the most important measures of continuity. At the Meliadine deposits, the variogram nugget effect for gold is 15% to 50% of the total population variance depending of the domain. In the current estimate, the variogram model was used as a guide for resource classification.

For all deposits, the method consists of defining the confidence level of the resources as they fall within a certain percentage of the sill; then the corresponding distance is calculated from the variogram model. The rounded distance calculated at a percentage varying between 75% and 90% of the sill determines the indicated resources search volume radii, and between 90% and 100% determines the inferred resources search volume radii. All average radii distances used for indicated and inferred resource categorization by deposit are derived from search ellipsoid dimensions (Item 14.5.1) and detailed in Table 14.27.

Indicated and inferred resource classification 3D solids, called “cookie cutters”, are constructed using these distances for each deposit. Cookie cutters are generated perpendicular to the drill-hole directions, assuming that all drill-holes have the same direction and the deviation is negligible. An example of cookie cutters for F zone is shown in Figure 14.19.

Table 14.27 - Distance (metres) from a hole used for classification of indicated and inferred mineral resources

Deposit	Indicated Resources		Inferred Resources	
	X	Z	X	Z
Tiriganiaq	30	30	75	75
Wesmeg	30	30	60	60
Normeg	30	30	60	60
F zone	50	30	80	50
Discovery	30	30	60	60
Pump	30	30	60	60
Wolf	40	40	80	70

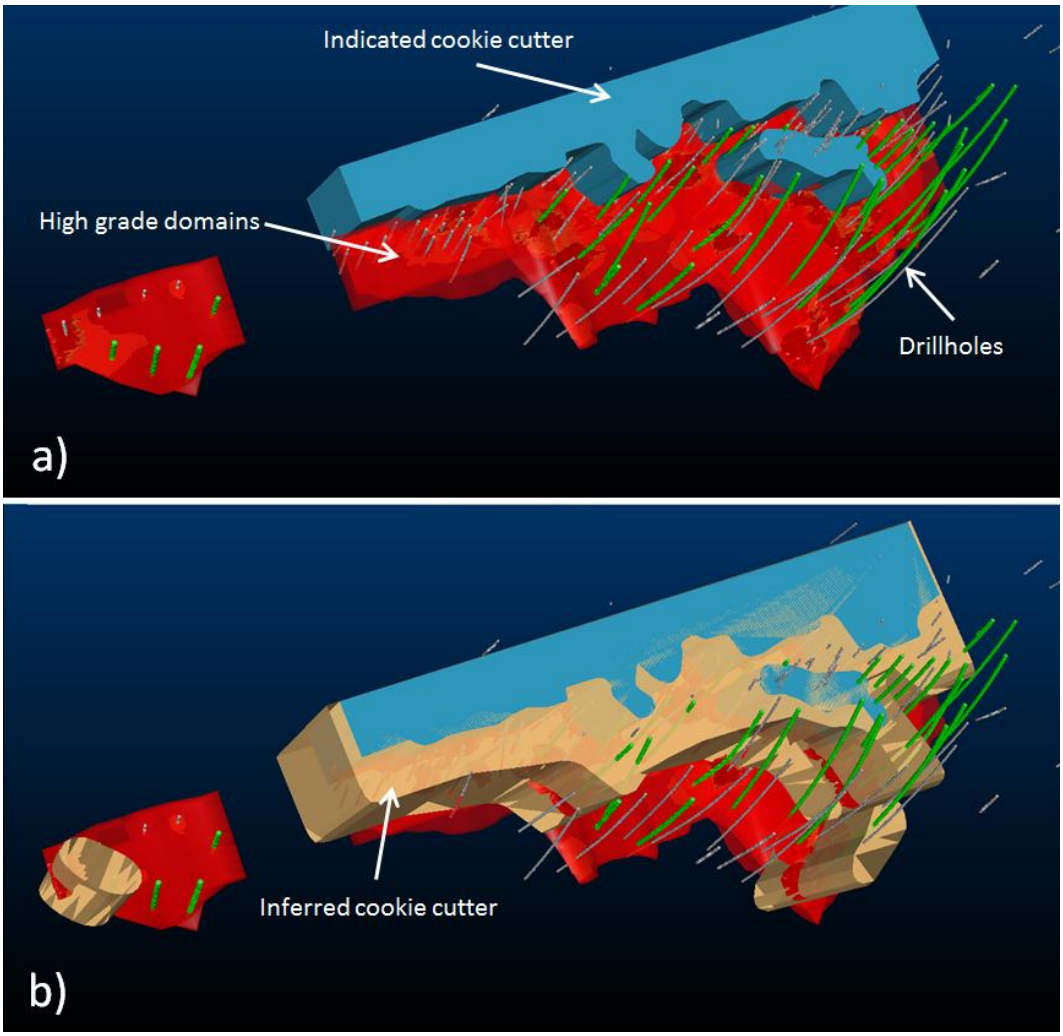


Figure 14.19 - Example of cookie cutters (3D solids) for F zone resource classification for a) indicated resources and b) inferred resources

14.9.4 Classification Process

The classification of the Meliadine mineral resource models incorporated confidence in:

- the drill-hole data;
- the geological interpretation;
- the geological continuity;
- data density and orientation;
- grade continuity, and;
- estimation quality.

The confidence in the classification of resources was iteratively refined with respect to these aspects. The resource models were coded for inferred or indicated resources according to CIM Standards (CIM, 2014).

The procedure for mineral resource classification is slightly different for open pit and underground at Meliadine. For all deposits, the mineral resources are classified on the basis of the data density first by defining classification 3D solids for indicated and inferred resources based on the radii detailed in previous section, then by the gold grade above the minimum cut-off value.

The cut-off values for all deposits are based on the operating cost estimates for mill processing of open pit ores and underground ores that are taken from Item 16 of this report. In order to satisfy the definition of "reasonable prospects for eventual economic extraction" in the CIM Standards, a minimum cut-off grade equivalent to 75% of the mineral reserve cut-off grade was used to classify the underground mineral resources. Open pit marginal cut-off grades (Table 16.3) have been used to classify the open pit mineral resources and a gold price of US$1,533/oz has been used to generate the pit shells. A C$/US$ exchange rate of 1.08 has been assumed. The open pit cut-off grades for open pit mineral resources classification are applied within the ultimate pit shells. The underground reserve cut-off grades are applied outside the ultimate pit shells.

14.9.4.1 Open Pit Resources

Open pit mineral resource models for all deposits were selected by Agnico Eagle complete with gold and density data for evaluation of their open pit potential using a Lerchs-Grossmann ultimate pit algorithm to determine the open pit shape.

Indicated resources were assigned to blocks and sub-blocks where the grade was interpolated inside the indicated classification 3D solids. The indicated resources correspond to well-drilled parts of the deposits where there is a high level of confidence in grade and geological continuity, defined by drill-holes spaced generally between 20 m and 40 m apart.

Inferred resources were assigned to blocks and sub-blocks where the grade was interpolated on the second pass inside the inferred classification 3D solids for the other deposits. The inferred resources also correspond to areas in which drill-holes and specific gravity information is sufficient to infer geological and grade continuity. The volumes of inferred resources that were estimated using samples within the second search volumes were multiplied by 1.5 or 2 depending on the deposit. Estimates within the third search volume were unclassified for the F

zone, Pump, Wolf, Wesmeg, Normeg and Discovery deposits, and will serve to provide Agnico Eagle with exploration and infill drill targets.

In order to be classified as open pit indicated or inferred mineral resources, each individual resource block above the fixed elevation had to satisfy a cut-off grade (Table 14.28). An average dilution of 40% at a grade of 0 g/t gold was applied to indicated resources prior to resource classification (see section 14.8).

Table 14.28 summarizes the parameters used for designing the ultimate pits for the different Meliadine deposits and shows the not diluted cut-off grades for resources classification.

Table 14.28 - Parameters and cut-off grades for ultimate pit design and open pit resources classification

Parameters	Tiri/Wesmeg/ Normeg Resources	F zone Resources	Pump Resources	Discovery Resources	Wolf Resources
Gold price (US$/oz)	US$1,533	US$1,533	US$1,533	US$1,533	US$1,533
Gold refining charge	C$2.50/oz	C$2.50/oz	C$2.50/oz	C$2.50/oz	C$2.50/oz
Exchange rate (C$/US$)	1.08	1.08	1.08	1.08	1.08
Metallurgical recovery	Formula	Formula	Formula	Formula	Formula
Mining dilution	42%	30%	44%	44%	44%
Mining recovery	95%	95%	95%	95%	95%
Processing cost (per tonne milled)	C$29.25/t	C$29.25/t	C$29.25/t	C$29.25/t	C$29.25/t
G&A cost (per tonne milled)	C$31.54/t	C$31.54/t	C$31.54/t	C$31.54/t	C$31.54/t
Closure & Rehabilitation cost (per tonne milled)	C$0.50/t	C$0.50/t	C$0.50/t	C$0.50/t	C$0.50/t
Stockpile rehandling cost for marginal ore (per tonne milled)	C$3.00/t	C$3.89/t	C$3.49/t	C$9.00/t	C$3.49/t
Total Marginal ore-based cost(per tonne milled)	C$64.29/t	C$65.18/t	C$64.78/t	C$70.29/t	C$64.78/t
Not diluted marginal gold cut-off grade	2.56 g/t	2.42 g/t	2.70 g/t	2.73 g/t	2.46 g/t

14.9.4.2 Underground Resources

Indicated underground resources were assigned to blocks and sub-blocks where the grade was interpolated on the first pass inside the indicated classification 3D solids and located outside the ultimate pit shells. The indicated resources correspond to well-drilled parts of the deposits where there is a high level of confidence in grade and geological continuity, defined by drill-holes spaced generally between 20 m and 40 m apart.

Inferred underground resources were assigned to blocks and sub-blocks where the grade was interpolated on the second pass inside the inferred classification 3D solids and located outside the ultimate pit shells. The inferred underground resources also correspond to areas in which drill-holes and specific gravity information is sufficient to infer geological and grade continuity. The volumes of inferred resources that were estimated using samples within the second search volumes were multiplied by 1.5 or 2 depending of the deposit. Estimates within the third search volume were unclassified for the F zone, Pump, Wolf, Wesmeg, Normeg and Discovery deposits, and will serve to provide Agnico Eagle with exploration and infill drill targets.

In order to be classified as underground indicated or inferred mineral resources, each individual resource block below the ultimate pit shells had to satisfy a cut-off grade detailed in Table 14.29. An average dilution of 35% at a grade of 0 g/t gold was applied to indicated resources prior to resource classification (see section 14.8).

Table 14.29 - Parameters and cut-off grades for underground resources classification

Parameter	Tiri/Wesmeg/ Normeg Resources	F zone Resources	Pump Resources	Discovery Resources	Wolf Resources
Gold price (US$/oz)	US$1,533	US$1,533	US$1,533	US$1,533	US$1,533
Gold refining charge	C$2.50/oz	C$2.50/oz	C$2.50/oz	C$2.50/oz	C$2.50/oz
Exchange rate (C$/US$)	1.08	1.08	1.08	1.08	1.08
Dilution (%)	30%	35%	40%	35%	35%
Metallurgical recovery	Formula	Formula	Formula	Formula	Formula
Mining cost (per tonne milled)	C$63.00/t	C$67.34/t	C$62.60/t	C$73.29/t	C$62.60/t
Processing cost (per tonne milled)	C$30.50/t	C$29.25/t	C$29.25/t	C$29.25/t	C$29.25/t
G&A cost (per tonne milled)	C$82.89/t	C$50.07/t	C$50.07/t	C$50.07/t	C$50.07/t
Closure & Rehabilitation cost (per tonne milled)	C$0.05/t	C$0.05/t	C$0.05/t	C$0.05/t	C$0.05/t
Total ore-based cost (per tonne milled)	C$176.44/t	C$146.71/t	C$141.97/t	C$152.66/t	C$141.97/t
Not diluted gold cut-off grade (ore)	4.68 g/t	4.15 g/t	4.23 g/t	4.14 g/t	3.96 g/t

14.10 Mineral Resource Reporting

Mineral resource estimates are reported in Table 14.30 for the deposits at the Meliadine gold project.

The mineral resources estimate (inclusive of mineral reserves) at the Meliadine project consist of 34.2 million t grading 6.03 g/t gold for a total of 6.6 million oz of gold in indicated mineral resources and at 14.1 million t grading at 7.65 g/t for a total of 3.5 million oz of gold in inferred mineral resources, as of December 31, 2014.

Table 14.30 - Meliadine gold project mineral resources inclusive of reserves (as of December 31, 2014)

Classification	Deposit	Category	Tonnes (000)	Gold grade (g/t)	Contained gold (000 Oz)
Measured Resources	Tiriganiaq	Open pit	34	7.31	8
Indicated Resources	Tiriganiaq	Open pit	5 070	4.82	785
		Underground	16 543	7.28	3 870
	F-Zone	Open pit	1 254	4.46	180
		Underground	1275	5.16	212
	Wesmeg	Open pit	2 241	4.12	297
		Underground	1 784	5.32	305
	Normeg	Open pit	1250	3.99	160
		Underground	346	5.06	56
	Discovery	Open pit	945	5.00	152
		Underground	1 572	6.35	321
	Pump	Open pit	671	5.32	115
		Underground	707	4.54	103
	Wolf	Open pit	115	3.63	13
		Underground	383	4.12	51
	Total		***34 190***	***6.03***	***6 627***
Inferred Resources	Tiriganiaq	Open pit	-	-	-
		Underground	2 402	9.59	740
	F-Zone	Open pit	46	6.26	9
		Underground	1 427	6.82	313
	Wesmeg	Open pit	181	5.92	35
		Underground	2 175	7.59	531
	Normeg	Open pit	237	4.24	32
		Underground	2 351	8.51	643
	Discovery	Open pit	-	-	-
		Underground	529	7.55	128

	Pump	Open pit	304	6.78	66
		Underground	2 022	7.75	504
	Wolf	Open pit	262	4.43	37
		Underground	2145	6.17	425
	Total		***14 083***	***7.65***	***3 464***

Notes to accompany Mineral Resource Table

1. The Qualified Person for the mineral resource estimate, as defined by NI 43-101, is Julie Larouche, PGeo (Superintendent Geology for Agnico Eagle's Technical Services group), and the effective date of the estimate is December 31, 2014.
2. The mineral reserves are inclusive of the mineral resources
3. Current CIM definitions and guidelines were followed in the estimation and reporting of these Mineral Resources
4. Ounce (troy) = tonnes x grade / 31.1035
5. Indicated resources are diluted

14.11 Estimate Validation

Agnico Eagle validated the current Meliadine mineral resources models using the following techniques:

- comparison of global uncapped sample statistics and composite statistics with the mean estimated grade by domain, and comparison of the ID^2 estimate with ordinary kriging (OK) and nearest neighbour (NN) estimates for all deposits**;**
- visual inspection of block and sample composite grades in section, plan, and in three dimensions;
- comparison with the combined results of the 2008 and 2011 bulk samples;
- comparison to previous mineral resource estimates, where possible.

Global grade comparisons regardless of the resources categories demonstrate that the estimated grades are generally below the capped composites overall grade. Swath plots show the similarities between the both ID^2 and OK estimation methods, which seem to smooth the grade in high density sampled areas. Higher variations between composites and estimation grades are observed locally in the extensions and at depth in areas that are relatively poorly drilled.

The distribution of estimated grades corresponds to the distribution of grades in the input data. Figure 14.20 shows a good match between the gold composite values and the gold block model interpolation for major zones of the Tiriganiaq deposit.

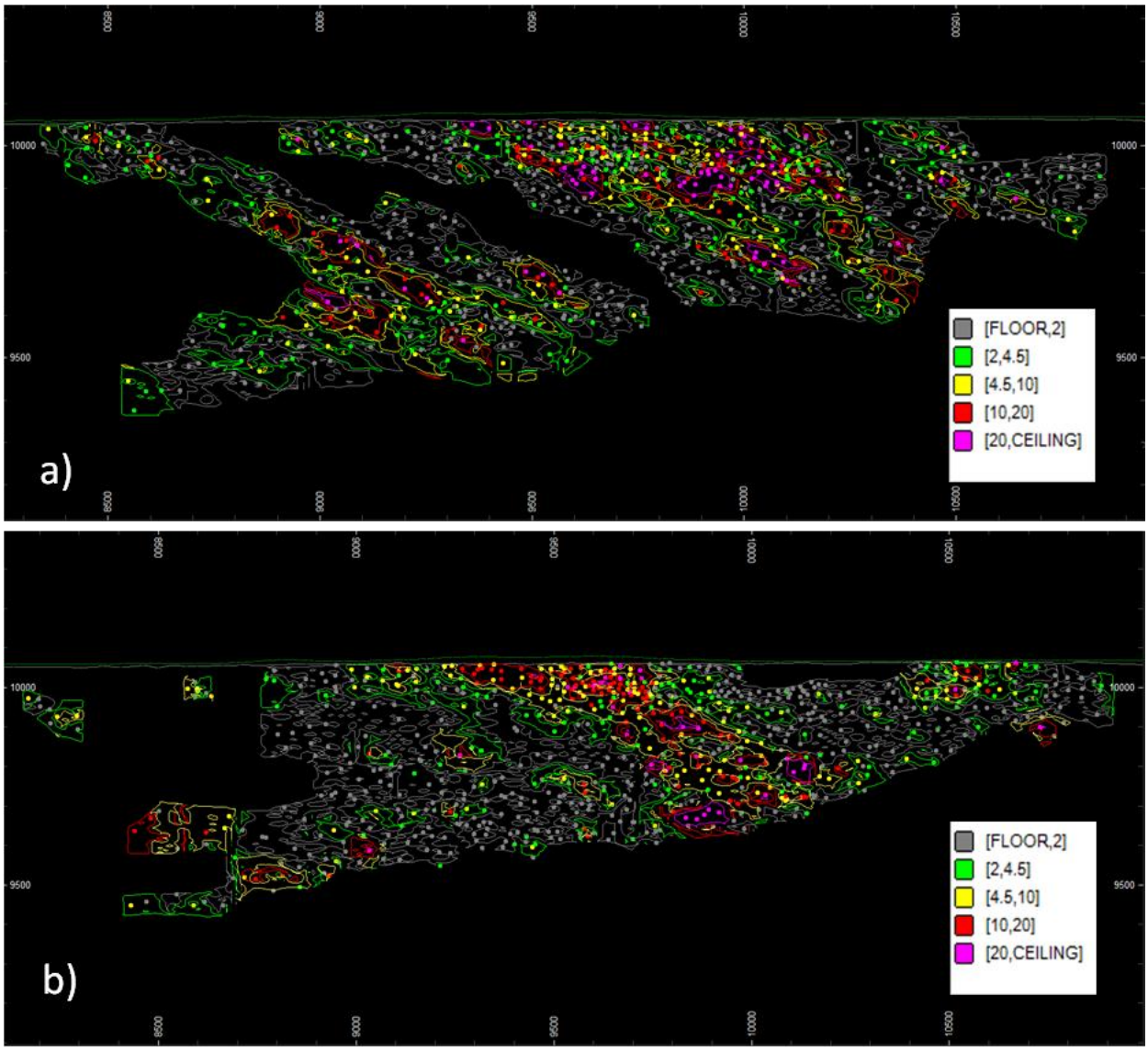


Figure 14.20 - Tiriganiaq longitudinal sections looking north showing the drill pierce points and the block model gold isosurfaces for the (a) 1000 zone and the (b) 1100 zone.

Underground bulk samples were taken in 2008 (Strathcona, 2009) and 2011 (Duquette and Thalenhorst, 2012). Table 14.31 shows the differences between the results of the addition of the two bulk samples and the December 31, 2013 and December 31, 2014 block models using ordinary kriging. Generally, for the high-grade part of the 1000 lode on the 9950 level (one of the two main zones in this part of the Tiriganiaq deposit), the tonnages were over-estimated by the both block models, but the grade capping used for the December 2014 block model has considerably aligned the grade with the bulk sample results. For the 1100 zone, the December 2014 block model still overestimates the tonnage but the grade is closer.

The author considers that the December 2014 block model's differences (less than 10%) for the for the tonnage and gold ounces in both lodes compared with the bulk sample are satisfactory,

and suggests that parameter changes have led to an improvement in the accuracy and the quality of the mineral resources estimate.

Table 14.31 - December 2013 and 2014 block models compared with bulk sample results

	Zone	Tonnes	Gold Grade (g/t)	Gold Ounces	Diff. Tonnes	Diff. Ounces
Undiluted bulk Samples results (2008 and 2011)	1000	7 048	15.90	3 596	0%	0%
	1100	8 812	11.60	3 279	0%	0%
Ordinary Kriging Dec. 2013	1000	8 123	17.64	4 606	15%	28%
	1100	9 636	10.25	3 175	9%	-3%
Ordinary Kriging Dec. 2014	1000	7 764	15.24	3 803	10%	6%
	1100	9 123	10.32	3 028	4%	-8%

The global increase in mineral resources at Meliadine is due to the considerable amount of drilling from 2011 through 2014.

Between 2011 and 2014, emphasis has been placed on conversion drilling at Tiriganiaq-Normeg-Wesmeg, F zone, Discovery and Pump deposit. The conversion success has led to a 63% increase in indicated mineral resources (including reserves). Exploration drilling has focussed on deposit extension and has led to an increase of 30% of the inferred resources over this period.

Item 15. Mineral Reserve Estimates

This item states the mineral reserves at the Meliadine project that have been converted from the indicated resources as of December 31, 2014. Agnico Eagle reports mineral reserve estimates in accordance with the definitions from the National Instrument 43-101 and the CIM Definition Standards for Mineral Resources and Mineral Reserves, adopted by CIM Council on May 10, 2014 (CIM, 2014). According to these standards, resource block models classified as indicated resources can be converted to probable reserves if they have a grade above the economic cut-off grade and demonstrate that they are economically mineable based on the mining parameters. The above reporting standards do not allow inferred resources to be included in reserve estimates; the inferred resource has not been included in this item.

The CIM definition for proven and probable mineral reserves follows:

Mineral Reserves are sub-divided in order of increasing confidence into Probable Mineral Reserves and Proven Mineral Reserves. A Probable Mineral Reserve has a lower level of confidence than a Proven Mineral Reserve.

A **Mineral Reserve** is the economically mineable part of a Measured and/or Indicated Mineral Resource. It includes diluting materials and allowances for losses, which may occur when the material is mined or extracted and is defined by studies at Pre-Feasibility or Feasibility level as appropriate that include application of Modifying Factors. Such studies demonstrate that, at the time of reporting, extraction could reasonably be justified. Modifying Factors are considerations used to convert Mineral Resources to Mineral Reserves. These include, but are not restricted to, mining, processing, metallurgical, infrastructure, economic, marketing, legal, environmental, social and governmental factors. A **Probable Mineral Reserve** is the economically mineable part of an Indicated, and in some circumstances, a Measured Mineral Resource. The confidence in the Modifying Factors applying to a Probable Mineral Reserve is lower than that applying to a Proven Mineral Reserve. A **Proven Mineral Reserve** is the economically mineable part of a Measured Mineral Resource. A Proven Mineral Reserve implies a high degree of confidence in the Modifying Factors.

The mineral reserve estimates were made using metal prices and foreign exchange rates in accordance with SEC Industry Guide 7. Industry Guide 7 requires the use of prices that reflect current economic conditions at the time of reserve determination. Given the current lower commodity price environment, Agnico Eagle has decided to use a price assumption that is below the historic three-year average price. The assumptions used in this mineral reserve estimate for the period ending December 31, 2014, are US$1,150 per ounce gold and a C$/US$ exchange rate of 1.08.

There are no known mining, metallurgical, infrastructure, permitting, and other relevant factors that could materially affect the mineral reserves.

15.1 Resource model

The resource block model described in Item 14 of this report was used for the mineral reserve conversion process. The mineral reserves are the portion of the Tiriganiaq and Normeg/Wesmeg

indicated resources that are economically recoverable by mining, as determined by the mining method (described in Item 16) and a fixed economic cut-off grade (calculated later in this item). Because of the very close proximity of the Tiriganiaq-Normeg-Wesmeg deposits and their equivalent genetic model, the resource block models for these three deposits have been merged together for the mineral reserve conversion. However, the underground indicated resources at Wesmeg are limited, and only a small proportion has been converted into mineral reserves. No indicated resources at Normeg have been converted into Mineral Reserves.

The probable mineral reserve is the portion of the indicated resource for which the diluted gold grade is above the economic cut-off, except for those portions that may be inaccessible or cannot be converted to reserves.

A negligible number of inferred resource blocks and sub-blocks located within the mining stopes and development drifts have been converted into reserves.

15.2 Identifying stopes and economic packets

Mineable Shape Optimizer (MSO) software was used to generate stope designs for underground mining, and economic packets for open pit mining. MSO is a module available in the Datamine Studio 3 software; itwas developed to optimize underground stope design, but can also be used for open pit packet design. Using the block model as an input, MSO identifies the optimal shape, size and location of stopes and economic packets according to the parameters established by the mine plan (Figure 15.1). The open pit and underground mining plan are described in Item 16.

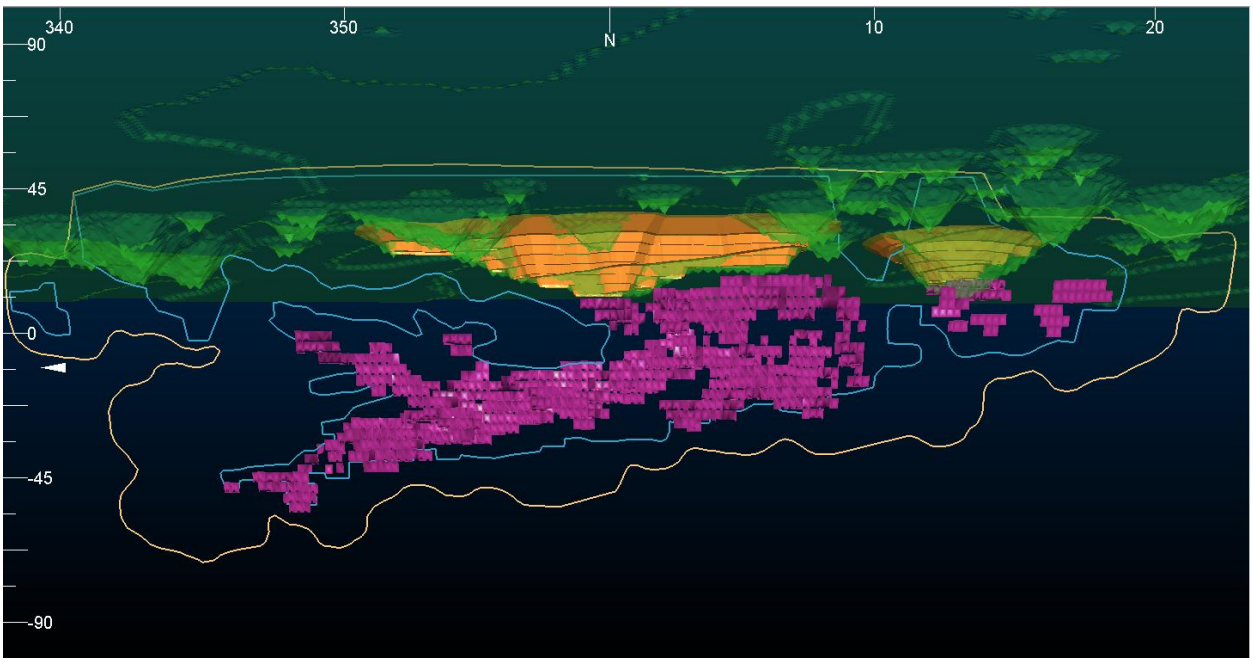


Figure 15.1 - Longitudinal section of the Tiriganiaq deposit showing the MSO-defined underground stopes (pink), the ultimate pit (green), and the pit design (orange) as well as the inferred resource (yellow contour) and indicated resource (blue contour) areas

In order to be classified as probable reserves, each resource packet or stope was designed using the parameters detailed in Table 15.1.

Table 15.1 - MSO parameters for designing underground stopes and open pit economic packets

MSO parameters - open pit			
Deposit	**Tiriganiaq**	**Wesmeg**	**Normeg**
	ore packet parameters		
Default dip	60°	60°	60°
Default azimuth	000°	000°	000°
Minimum thickness	3 m	3 m	3 m
Maximum thickness	no max	no max	no max
Stope height	5 m	5 m	5 m
Minimum pillar width	3 m	3 m	3 m
Footwall dilution	1.0 m, but lode 1000 and 1100 are 0.5 m	1.0 m	1.0 m
Hanging wall dilution	1.0 m, but lode 1000 and 1100 are 0.5 m	1.0 m	1.0 m
Minimum dip angle	30°	30°	30°
Maximum dip angle	70°	70°	70°
Maximum azimuth	045°	045°	045°
Maximum azimuth	045°	045°	045°
Maximum side length ratio	3	3	3
Stope length	12 m	12 m	12 m
MSO parameters - underground			
Deposit	**Tiriganiaq**	**Wesmeg**	**Normeg**
	Stope parameters		
Default dip	use wireframe	use wireframe	use wireframe
Default strike	use wireframe	use wireframe	use wireframe
Minimum thickness	3 m	3 m	3 m
Maximum thickness	no max	no max	no max
Stope height	25 m	25 m	25 m
Minimum pillar width	6 m	6 m	6 m
Footwall dilution	0.5 m (but lode 1000 is 1.0 m)	0.5 m	0.5 m
Hanging wall dilution	1 m	1 m	1 m
Minimum dip angle	55°	55°	55°
Maximum dip angle	90°	90°	90°
Maximum azimuth	045°	045°	045°
Maximum strike change	045°	045°	045°
Maximum side length ratio	3	3	3
Stope width	18 m	18 m	18 m
Mining method	primary, secondary and longitudinal		
Fill type	rockfill and paste backfill		

15.3 Dilution

Low-grade domains are used for the dilution model and in the mine plan. As described in Item 14, the Upper Oxide Formation, sericitic mafic volcanics and iron formation 3D models represent the low-grade domains for the Tiriganiaq, Normeg and Wesmeg deposits, respectively. The gold grade in these domains is estimated using specific estimation parameters described in Item 14, and is used to calculate an estimated gold dilution grade for the stope and packet designs. The specific dilution factors for each deposit are described in Item 16.

15.4 Mining extraction and ore losses

All stopes generated by MSO have been evaluated and classified according to the proposed mining plan. Isolated stopes at the eastern extent and at depth in Tiriganiaq have been excluded from mineral reserves and remain as indicated resources. The same evaluation process has been

done for the Normeg and Wesmeg deposits. Overall, 790,000 tonnes representing 170,000 ounces of gold have been excluded from reserves and downgraded to indicated resources.

A 95% mining recovery factor has been applied to the open pit and underground mineral reserves mined by open pit blasthole mining or underground blasthole stoping. A 100% mining recovery factor has been used for mineral reserves resulting from underground development.

15.5 Cut-off grades

The economic parameters used to establish the reserve cut-off grades are presented in Table 15.2. For the economic cut-off grade calculations, the dilution grade is considered to be 0 g/t gold. The average metallurgical recovery for open pit reserves and for underground reserves has been established according to the recovery curves described in Item 13. A royalty that is part of the IIBA, a closure and a rehabilitation costs are also taken into account in deriving the cut-off grades. The assumptions for these calculations are a gold price of US$1,150/oz, and a C$/US$ exchange rate of 1.08. A gold refining cost of C$2.50/oz has been used. The mine-site costs for open pit and underground reserves are derived in Item 16 and summarized in Table 15.2.

Table 15.2 - Economic parameters used to establish cut-off grades for probable reserves

	Tiriganiaq Open Pit Mineral Reserves		**Tiriganiaq and Wesmeg Underground Mineral Reserves**	
Parameters	**Economic ore**	**Marginal ore**	**Economic ore**	**Marginal ore**
Gold price	US$1,150/oz	US$1,150/oz	US$1,150/oz	US$1,150/oz
Refining cost	C$2.50/oz	C$2.50/oz	C$2.50/oz	C$2.50/oz
Exchange rate	C$1.08/US$1.00	C$1.08/US$1.00	C$1.08/US$1.00	C$1.08/US$1.00
Metallurgical recovery	Formula (1)	Formula (1)	Formula (1)	Formula (1)
Mining dilution (average)	42%	42%	30%	30%
Mining recovery	95%	95%	95%	95%
Processing cost	C$29.25/tonne	C$29.25/tonne	C$30.50/tonne	C$29.25/tonne
General & administrative cost	C$50.07/tonne	C$31.54/tonne	C$82.89/tonne	C$31.54/tonne
Mining cost	C$0.00/tonne	C$0.00/tonne	C$63.00/tonne	C$0.00/tonne
Rehandling	C$2.15/tonne	C$3.00/tonne	C$0.00/tonne	C$3.00/tonne
Total mine-site cost	C$**81.47**/tonne	C$**63.79**/tonne	C$**176.39**/tonne	C$**63.79**/tonne
Closure & Rehabilitation cost	C$0.50/tonne	C$0.50/tonne	C$0.05/tonne	C$0.05/tonne
Total cost	C$**81.97**/tonne	C$**64.29**/tonne	C$**176.44**/tonne	C$**63.84**/tonne
Cut-off grade after dilution	**2.28 g/t**	**1.81 g/t**	**4.80 g/t**	**1.79 g/t**
Cut-off grade before dilution	3.24 g/t	2.56 **g/t**	6.24 **g/t**	2.33 **g/t**

*(1) 3.0114*ln(Au)+88.662, max 96.5*

For the December 31, 2014 open pit mineral reserves estimate, the gold cut-off grade has been derived from the gold cut-off grade used for the open pit optimization detailed in Table 16.3. The optimization study determined a mine-site cost of C$85.64/tonne, and a diluted gold cut-off grade of 2.36 g/t for open pit economic ore. Since no new open pit design was generated for the current mineral reserve estimate, the open pit design of the updated economic study has been used, which explains the slight difference between the two cut-off grades. Table 15.2 shows the revised mine-site cost of C$81.97/tonne used to calculate the open pit mineral reserves cut-off

grade of 2.28 g/t after dilution. The gold cut-off grade before dilution for open pit mining is 3.24 g/t.

The marginal cut-off grade for open pit reserves was calculated using a reduced mine-site cost of C$64.29/tonne, reducing the gold cut-off grade to 1.81 g/t after dilution (2.56 g/t before dilution). The main cost reduction is due to a lower G&A, during the year of marginal ore processing.

As shown in the Table 15.2, the gold cut-off for underground reserves after dilution is 4.80 g/t (6.24 g/t before dilution), based on mine-site costs of C$176.44/tonne.

Marginal material resulting from underground development has been included in the underground mineral reserves. The marginal underground gold cut-off grade of 1.79 g/t after dilution (2.33 g/t before dilution) was calculated using a reduced operating cost of C$63.84/tonne, reducing the gold cut-off grade to 1.79 g/t after dilution (as detailed inTable 16.8). The main cost reduction is due to a lower G&A, during the year of marginal ore processing.

15.6 Mineral Reserve Reporting

Based on the mining, processing and economic parameters described above (Table 15.2), the mineral reserves have been derived from the indicated resources of the Tiriganiaq-Normeg-Wesmeg deposits, and are therefore classified in accordance with the National Instrument 43-101. The mineral reserves are based on the mining plan (Item 16) and supported by an economic analysis (Item 22). They were estimated using a gold price of US$1,150/oz and a C$/US$ exchange rate of 1.08. The proven reserves are limited to a surface stockpile.

The total proven and probable mineral reserves at the Meliadine project as of December 31, 2014 (Table 15.3) are estimated at 13.9 million tonnes grading 7.44 g/t gold, containing 3.3 million ounces of gold. The economic diluted cut-off grades used are 2.28 g/t (open pit) and 4.80 g/t (underground), with the marginal cut-off grades of 1.8 g/t (open pit) and 1.79 g/t (underground).

Table 15.3 - Meliadine gold project mineral reserves as of December 31, 2014

Classification	Deposit	Category	Tonnes (000)	Gold grade (g/t)	Contained gold (000 oz)
Proven Reserves	Tiriganiaq	Stockpile	34	7.31	8
	Subtotal		***34***	***7.31***	***8***
Probable Reserves	Tiriganiaq	Open pit	3,862	5.13	638
		Underground	9,787	8.39	2,640
	Wesmeg	Underground	261	5.84	49
	Subtotal		***13,910***	***7.44***	***3,327***
	Total		***13,944***	***7.44***	***3,335***

After the conversion of measured and indicated mineral resources to reserves, the remaining mineral resources as of December 31, 2014, consist of indicated mineral resources estimated at 20.2 million tonnes grading 5.06 g/t gold, containing 3.3 million ounces of gold, and inferred mineral resources estimated at 14.1 million tonnes grading 7.65 g/t gold, containing 3.5 million ounces of gold. The mineral resources exclusive of mineral reserves are shown in Table 15.4.

Table 15.4 - Meliadine gold project mineral resources exclusive of mineral reserves as of December 31, 2014

Classification	Deposit	Category[1]	Tonnes (000)	Gold grade (g/t)	Contained gold (000 Oz)
Indicated Resources[2]	Tiriganiaq	Open pit	1,208	3.79	147
		Underground	6,756	5.66	1,230
	F zone	Open pit	1,254	4.46	180
		Underground	1,275	5.16	212
	Wesmeg	Open pit	2,241	4.12	297
		Underground	1,522	5.23	256
	Normeg	Open pit	1,250	3.99	160
		Underground	346	5.06	56
	Discovery	Open pit	945	5.00	152
		Underground	1,572	6.35	321
	Pump	Open pit	671	5.32	115
		Underground	707	4.54	103
	Wolf	Open pit	115	3.63	13
		Underground	383	4.12	51
	Total		***20,246***	***5.06***	***3,293***
Inferred Resources	Tiriganiaq	Open pit	-	-	-
		Underground	2,402	9.59	740
	F zone	Open pit	46	6.26	9
		Underground	1,427	6.82	313
	Wesmeg	Open pit	181	5.92	35
		Underground	2,175	7.59	531
	Normeg	Open pit	237	4.24	32
		Underground	2,351	8.51	643
	Discovery	Open pit	-	-	-
		Underground	529	7.55	128
	Pump	Open pit	304	6.78	66
		Underground	2,022	7.75	504
	Wolf	Open pit	262	4.43	37
		Underground	2,145	6.17	425
	Total		***14,083***	***7.65***	***3,464***

(1) Open pit mineral reserves are classified inside the operational pit design and open pit mineral resources are classified inside the ultimate pit shells

(2) Indicated resources are diluted

Item 16. Mining Methods

16.1 Mining Operations

The Meliadine mineral reserve, contained mostly within the Tiriganiaq deposit, will be mined by both surface and underground operations. It is estimated that approximately 3.4 million tonnes of ore is extractable from surface mining and 9.1 million tonnes by underground mining over a nine-year mine life (see Item 15). An additional 1.4 million tonnes of lower grade material from underground development and open pit mining ("marginal ore") will be stockpiled. The marginal ore will be processed at the end of the mine life, assuming that market conditions and minesite costs[1] will allow it to be processed economically. The current plan is to mine the Tiriganiaq deposit including the Wesmeg 650 lode from two open pits and an underground mine (Figure 16.1).

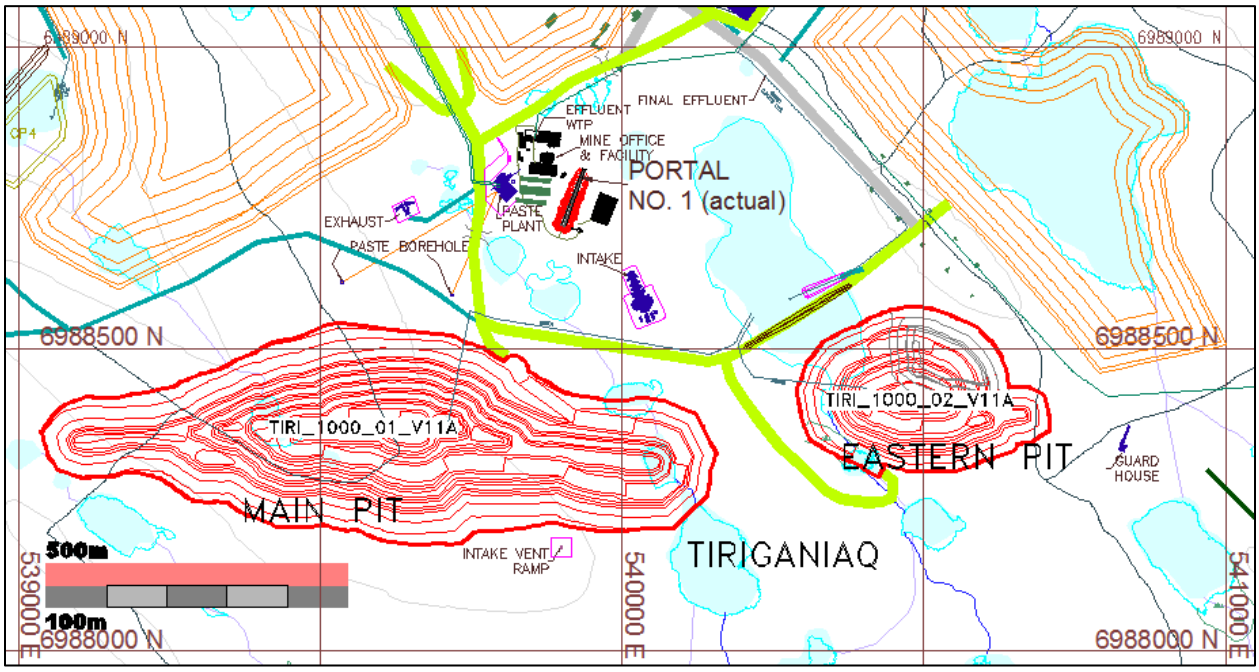


Figure 16.1 - Location of Tiriganiaq open pits in relation to surface watercourses and facilities, showing the main pit and the eastern pit. The red portal to the underground operations is to the north of the main pit.

The first three years (Y1 through Y3) of production will be from the underground operation only, delivering 3,000 tonnes per day ("tpd") of ore to the process plant. Starting at the end of Y2, the open pits will be developed, adding 2,000 tpd of ore to the mill feed starting in Y4. The mining plan is presented in Table 16.2.

1 Minesite costs include all mining, milling, site administration, site maintenance, site services, royalties, differed stripping and stockpiles adjustment costs,

Table 16.1 - Meliadine mine plan for open pit ("OP") and underground ("UG") mines including ore, marginal ore, waste and overburden ("Ovb")

Production	Total	Y-5	Y-4	Y-3	Y-2	Y-1	Y1	Y2	Y3
OP mine									
Ore tonnes (t)	3,862,383								
Ovb tonnes (t)	7,358,674							2,038,237	4,328,239
Waste (t)	26,115,639							68,930	4,205,799
UG Mine									
Ore tonnes (t)	10,115,604	338	987	731	120,865	602,440	1,185,403	1,051,472	1,254,293
Waste (t)	5,806,709	164,638	328,666	540,079	639,872	707,561	888,242	730,630	563,161

Production	Y4	Y5	Y6	Y7	Y8	Y9
OP mine						
Ore tonnes (t)	954,850	888,480	954,166	1,064,884		
Ovb tonnes(t)	840,971	151,227				
Waste (t)	6,102,493	6,890,390	6,144,502	2,703,525		
UG Mine						
Ore tonnes (t)	1,237,507	1,154,294	1,003,612	1,131,182	1,095,000	277,479
Waste (t)	310,955	310,955	310,995	310,955		

If mineral resources in other Meliadine deposits can be converted into reserves, they could be developed as separate mining operations. As with the Tiriganiaq deposit, the other deposits could be mined by a combination of open pit mining to a maximum depth of 150 m, with lower ore exploited by underground mining methods.

16.2 Geotechnical considerations

Geotechnical studies have been conducted on the property since 2000, with a focus on open pit slope design as well as preliminary studies on underground mine development and stope design. Geotechnical site investigations and design reviews were carried out in 2013. Pit slope design parameters were reviewed for the Tiriganiaq, F zone and Discovery deposits, and new parameters were provided for Normeg and Pump. For underground mining, stope dimensions, dilution estimates and ground support recommendations were provided in 2013 based on existing data. In 2014, geotechnical investigations, analysis and design were focused primarily on the Tiriganiaq underground mine.

16.2.1 Rock mass characterization

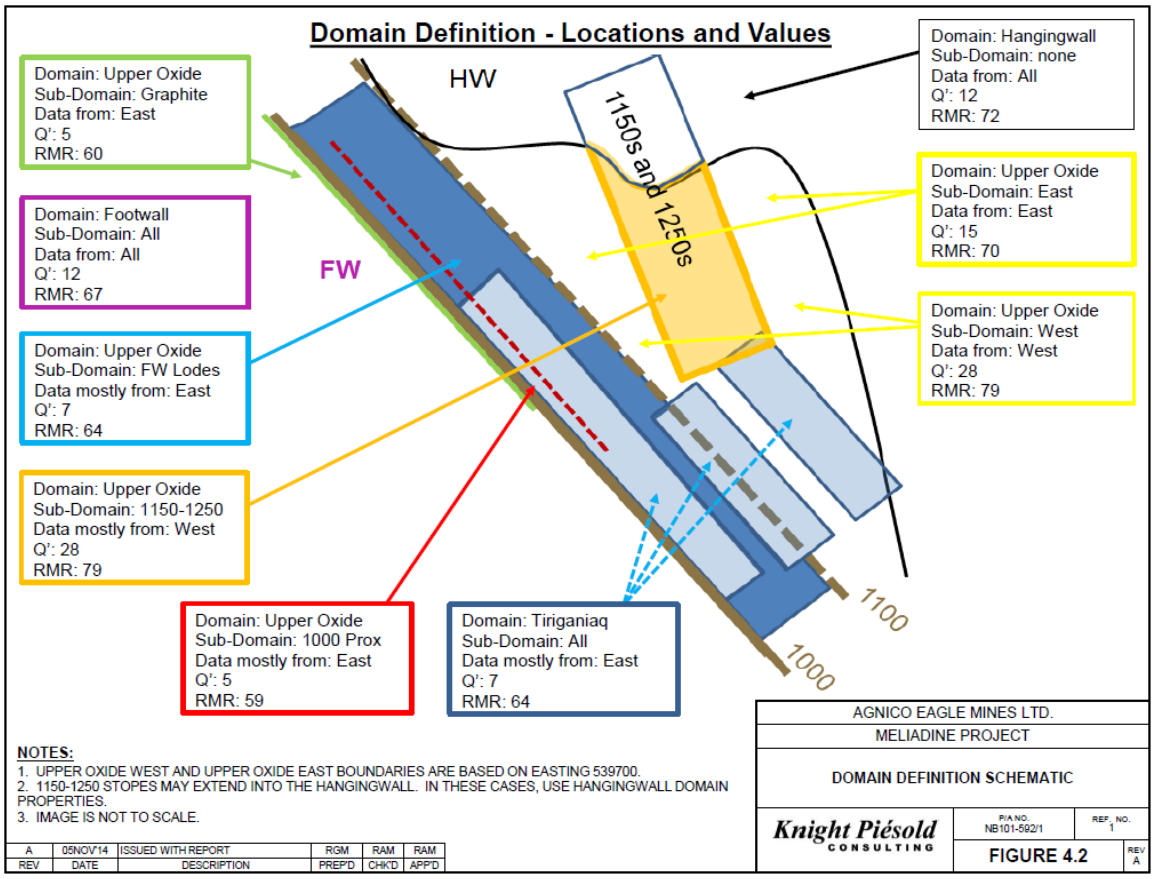
A geotechnical model was developed for the Tiriganiaq orebody focusing on the underground mine, as it requires a higher resolution and level of detail than the open pit mines. Geotechnical data were collected from oriented drill core for geological definition purposes, and also from mapping in the underground ramp. Geotechnical domains and rock mass properties were derived on the basis of all the existing data up to August 2014.

16.2.2 Rock mass domains

The final domain definition for the underground mine comprises four main domains and six sub-domains. The main domains are based on the main rock formations, while the sub-domains aim

to capture variations in and around the lodes of particular interest. The relative positions of the domains are provided schematically in Q' is the Norwegian Geotechnical Institute Index of rock mass quality from Barton et al. (1974) ; RMR is the Rock Mass Rating based on Bieniawski (1976); HW = hanging wall; FW = footwall

Figure 16.2.



Q' is the Norwegian Geotechnical Institute Index of rock mass quality from Barton et al. (1974) ; RMR is the Rock Mass Rating based on Bieniawski (1976); HW = hanging wall; FW = footwall

Figure 16.2 - Schematic representation of geotechnical domains for the Tiriganiaq underground deposit.

16.3 Hydrogeological conditions and permafrost

Hydrogeological investigations were carried out in the vicinity of the Tiriganiaq deposit in 2009 and 2011 and near the Discovery deposit in 2013. The hydrogeological testing programs were designed to obtain information about the hydraulic conductivity of the bedrock below the permafrost and within an open talik (Unfrozen ground surrounded by permafrost), and were required as support for the geotechnical and environmental programs for the project.

Preliminary estimates of groundwater inflow and quality into the underground mine below the permafrost were used inside the initial phases of the technical study. Additional studies are planned in 2015 and 2016 to address remaining uncertainties.

16.4 Surface Mining

Tiriganiaq resources located close to surface are planned to be mined from two open pits developed above the underground mining operation, as shown in Figure 16.1. The main pit ("Tiri1000_01") and the secondary eastern pit ("Tiri1000_02") have ultimate depths of 150 m and 100 m, respectively, and contain a combined total of mineable material (rock and overburden) in excess of 37 million tonnes. A conventional truck/shovel operation is recommended for both open pits.

The diluted mineable mineral reserves contained in the two Tiriganiaq open pits are summarized in Table 16.2.

Table 16.2 - Summary of Meliadine open pits material: waste including rock and overburden (OVB), and ore

Pit	Waste			Ore[1]		Total moved (tonne)
	OVB (tonne)	ROCK (tonne)	Total (tonne)	Total (tonne)	(oz)	
Tiri1000_01	6,602,722	20,367,946	26,970,667	3,358,861	563,431	30,329,529
Tiri1000_02	755,952	5,747,693	6,503,645	503,522	74,143	7,007,167
Total	7,358,674	26,115,639	33,474,313	3,862,383	637,574	37,336,696

(1) Includes marginal ore (grade 1.81 g/t to 2.28 g/t gold) and ore (grade >2.28 g/t gold)

16.4.1 Ultimate Pit Economic Parameters

As described in Item 15 of this report, the geological block model was first processed with Mineable Shape Optimizer (MSO) software in order to generate initial ore packets including dilution based on specific parameters and criteria. The software essentially adds a dilution skin around economic mineralization and/or incorporates some waste located between lodes to reflect the anticipated mining selectivity. These parameters and criteria are presented in Table 15.1.

Based on the initial ore packets, optimal open pit mining limits were established with the NPV Scheduler open pit software which is using the Lerch-Grossman algorithm for pit optimization. For the mineable mineral reserves of Tiriganiaq, the pit limits were optimized for a base case gold price of US$1,200/oz and a C$/US$ exchange rate of 1.03 (C$1,236/oz). The ore cut-off grade was established from phase 1 of the updated technical study, which was completed in the second quarter of 2013. An ore base cost of C$85.64/t milled was used. A marginal cut-off grade was also established taking into account a potential 25% reduction in G&A costs and a stockpile re-handling cost of C$5.03/t. Table 16.3 summarizes the parameters used for designing the ultimate pit shells for Tiriganiaq deposit.

Table 16.3 - Meliadine open pit optimization parameters for Tiriganiaq deposit

Parameters	Tiriganiaq/ Wesmeg Reserves
Gold price (US$/oz)	US$1,200
Gold refining charge	C$2.50/oz
Exchange rate (C$/US$)	1.03
Metallurgical recovery	Variable
Mining dilution	Variable (1)
Mining recovery	95%
Processing cost (per tonne milled)	C$28.08/t
G&A cost (per tonne milled)	C$51.22/t
Closure & Rehabilitation cost (per tonne milled)	C$1.31/t
Total ore-based cost (per tonne milled)	C$85.64/t
Total Marginal ore-based cost(per tonne milled)	C$64.29/t
Diluted gold ore cut-off grade	2.36 g/t
Not diluted marginal gold cut-off grade	-
Mining cost (per tonne mined)	C$5.06/t
Waste rehabilitation cost (per tonne milled)	C$0.03/t
Stockpile rehandling cost (per tonne milled)	C$5.03/t
Stockpile rehandling cost for marginal ore (per tonne milled)	C$5.03/t

(1) Mining dilution calculated with MSO (1 m footwall and hanging wall, except for the 1000 and 1100 lodes where the dilution is set to 0.5 m in the footwall and hanging wall)

16.4.2 Open Pit Slope Design

Pit slope designs for the project were derived based on a compilation and review of existing data complemented by the results of the 2013 geotechnical field investigation campaign (Golder Associates, 2013h). Previous pit slope designs had been made for the Tiriganiaq (Golder Associates, 2010a), F zone (Golder Associates, 2010b) and Discovery (Golder Associates, 2010a) deposits. These designs were reviewed and refined with additional geotechnical drilling in 2013 at F zone and Discovery (Golder Associates, 2013i). Four geotechnical holes drilled by Agnico Eagle in 2011 at Tiriganiaq were, however, included in the review of the Tiriganiaq pit slope design for this study. At the request of Agnico Eagle, Golder Associates Ltd. conducted a review of previous slope designs and provided optimized slope angles wherever possible based on a third party review and additional Arctic experience since the initial work in 2010 (Golder Associates, 2013j). The review and revised analyses resulted in the steepening of the Tiriganiaq pit slopes by 6° and 3° for the north and east walls, respectively.

The final bench height for Tiriganiaq open pits will typically be 20 m (two 10-m benches) and the face angle will vary from 64° to 70° depending on the pit wall. The catch bench width in the rock varies from 8 m to 10 m resulting in inter-ramp angles of 48° to 49° (See Table 16.4).

Table 16.4 - Tiriganiaq pit slope design parameters

Parameter	North wall	South wall	East wall	West wall
Bench face angle	70°	64°	70°	65°
Operating bench height	10 m	5 m	5 m	5 m
Bench configuration	double	double	double	double
Vertical separation	20 m	20 m	20 m	20 m
Catch bench width	10 m	8 m	10 m	8 m
Inter-ramp angle	49°	48°	49°	49°

Table 16.5 summarizes the inter-ramp pit slopes that were defined and considered for the other deposits, within which some potential pit resources were established.

Table 16.5 - Inter-ramp pit slopes for other Meliadine deposits

Inter-ramp pit slope	North wall	South wall	East wall	West wall
Tiriganiaq	49°	48°	49°	49°
Wesmeg	43°	49°	49°	49°
Normeg	43°	49°	49°	49°
F zone	49°	39°	53°	49°
Pump North	49°	37°	49°	49°
Pump south and west	49°	43°	49°	43°
Discovery	49°	40°	49°	49°

Overburden thickness atop the Tiriganiaq deposit is expected to range from a typical 5 m to 10 m up to 15 m to 20 m in places. The design recommendations for the overburden material are based on available shear strength information and operational experience at Meadowbank and elsewhere in the Arctic. Overburden slope design criteria are summarized in Table 16.6. The overburden material should be excavated in winter and kept frozen by use of a thermal protection cover. The bench face will be sloped at 40° followed by the placement of a 3-m-thick layer of rip-rap material.

Table 16.6 - Overburden slope design criteria

Parameter	Overburden slope design
Bench face angle	40° (with 3 m rip-rap thermal protection)
Bench height	8 m
Catch bench width	8 m
Rock/Overburden interface bench width	14 m
Inter-ramp overburden slope angle	25°
Overall slope angle	23°

16.4.3 Pit Design Parameters

The pit design includes ramp access to the bottom of both open pits, large enough to accommodate 65-tonne-class haul trucks (operational width not exceeding 5.7 m) in accordance with Nunavut mine regulations. For double-lane traffic, the ramp width will be 21.5 m, decreasing to 15.8 m for single-lane traffic at the pit bottom (last five benches) in order to reduce waste stripping. The ramp width includes a protection berm and a drainage ditch (Figure 16.3). Ramp gradients have been established at 10% and increased to 12% for the last three benches at the bottom of the pit.

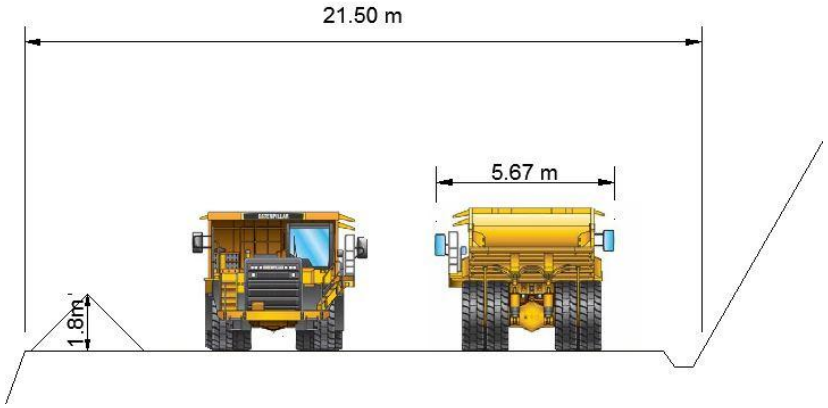


Figure 16.3 - Double-lane ramp design

16.4.4 Open Pit Mining Method

A conventional truck/shovel operation for both pits is planned with different mining approaches for ore and waste. The mining method must be suited to Arctic conditions and provide a good daily production in waste zones. To maximize the recovery of economic material and minimize dilution in the ore zones, the method must be very selective.

16.4.4.1 Ore and waste mining areas

Selective mining will be performed within the ore involving large blasts, whereby rock movement will be controlled and tracked. Within the ore zones, a tight drilling pattern with a large number of blast holes is required. The pattern will be confined to three or four faces and shot parallel to the deposit strike and to a confined face to limit blast movement (Figure 16.4).

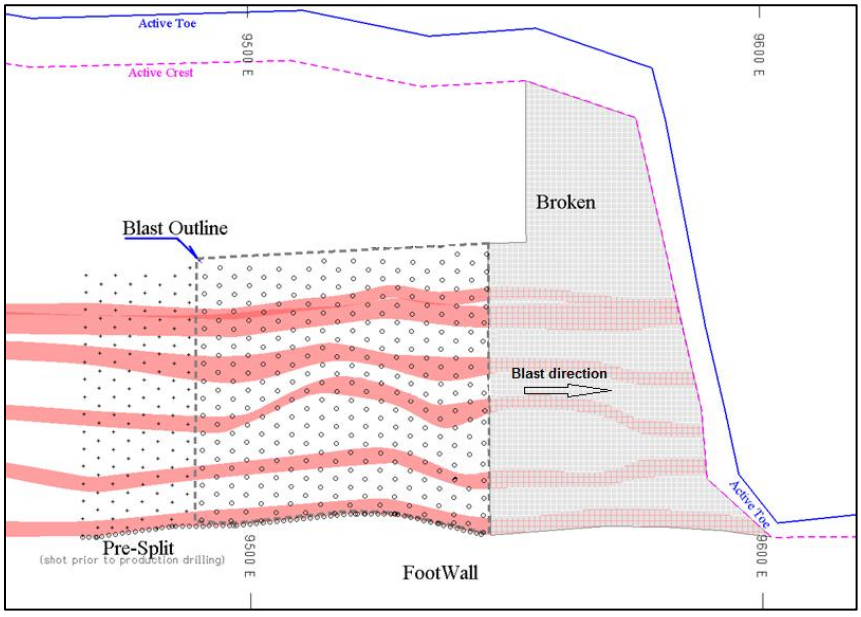


Figure 16.4 - Typical blast layout in ore (map view)

Digging will be performed with a mid-size backhoe excavator perpendicular to the strike of the lodes from the hanging wall to the footwall direction (see Figure 16.5 and Figure 16.6).

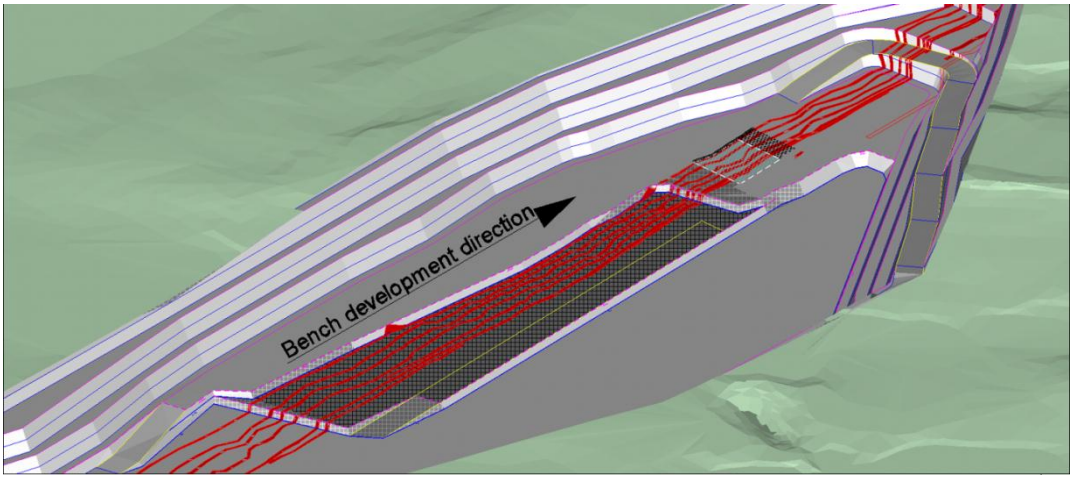


Figure 16.5 - Typical bench development in ore

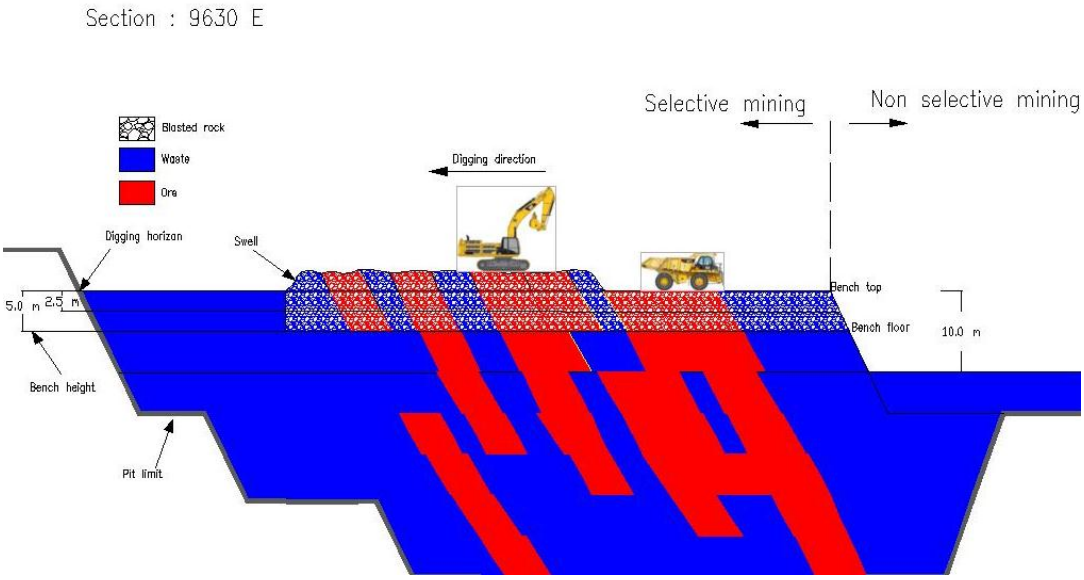


Figure 16.6 - Typical section 9630E showing digging horizons in ore zone

For the haulage, relatively small off-highway trucks (60- to 65-tonne payload class) will be used.

The ore mined from the pit will be either hauled to the primary crusher (located near the process plant) or placed on the low-grade or high-grade ore stockpiles.

Within waste areas, where no material selectivity is required, 10 m benches are planned. A wider drilling pattern will be used and blasting will be done in such a way as to maximize digging efficiency.

16.4.4.2 Drilling and Blasting

In order to minimize the drilling fleet and maintain flexibility to move drills from one work area to another, 165-mm (6.5-inch) diameter blast holes will be drilled in both ore and waste rock (selective and non-selective mining). Similarly, pre-shearing of the final pit wall will also be accomplished with 165-mm-diameter holes.

Blasting with a high-energy bulk emulsion explosive is planned with a targeted powder factor of 0.34 kg/t in ore and 0.27 kg/t in waste. Emulsion is a versatile product that can be used in dry and wet conditions. Emulsion will be produced on site in an explosives plant operated and maintained by an explosives supplier.

In order to develop a safe pit wall, pre-shearing techniques and controlled blasting will be used to limit rock mass damage beyond the final pit limit. Wall scaling will also be done using an appropriate shovel to remove unstable loose to prevent it from falling on the catch bench.

16.4.4.3 Ultimate Pit Physical constraints

No physical surface constraints have been considered in defining the ultimate pit limits within the Tiriganiaq deposit. The presence of different watercourses located within or near the pit footprints will require some water management including dewatering, drainage and water retention dykes.

However, the ultimate pit limits have been controlled by the presence of the underground mine, which limits the deepening of the pits. Potential future Tiriganiaq pit expansion could interact with and/or be constrained by the development of surface infrastructure such as vent houses and raises that will be installed in the vicinity of the current/final pit walls.

The floors of the main pit and the secondary (eastern) pit were fixed at a reference elevation of 9,930 and 10,000 meters respectively (sea level being set at a reference level of 10,000 m), in order to be compatible with the underground mine limits defined in previous trade-off studies. Figure 16.1 provides a plan view of the Tiraganiaq pits in relation to the surface facilities and watercourses, while Figure 16.7 is a longitudinal section and Figure 16.8 is an aerial view showing the relationship between the pits and the underground operation.

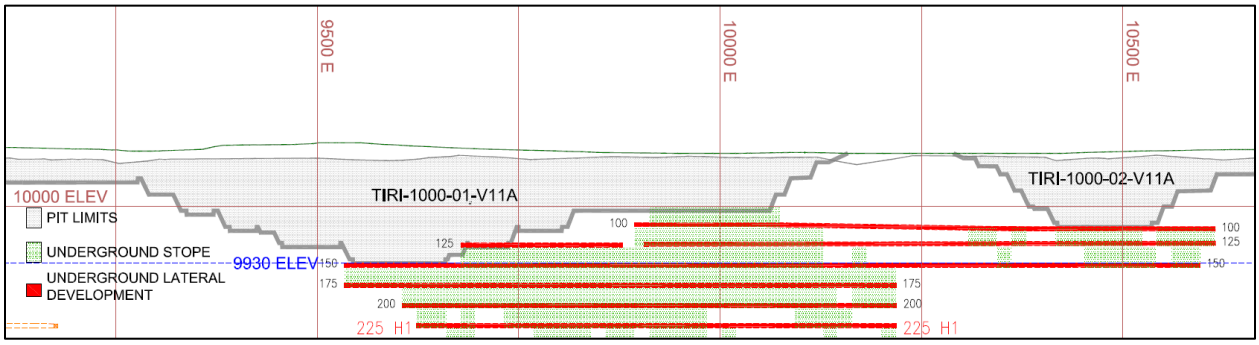


Figure 16.7 - Typical Tiriganiaq longitudinal section showing the relationship between open pit limits and underground mine infrastructure

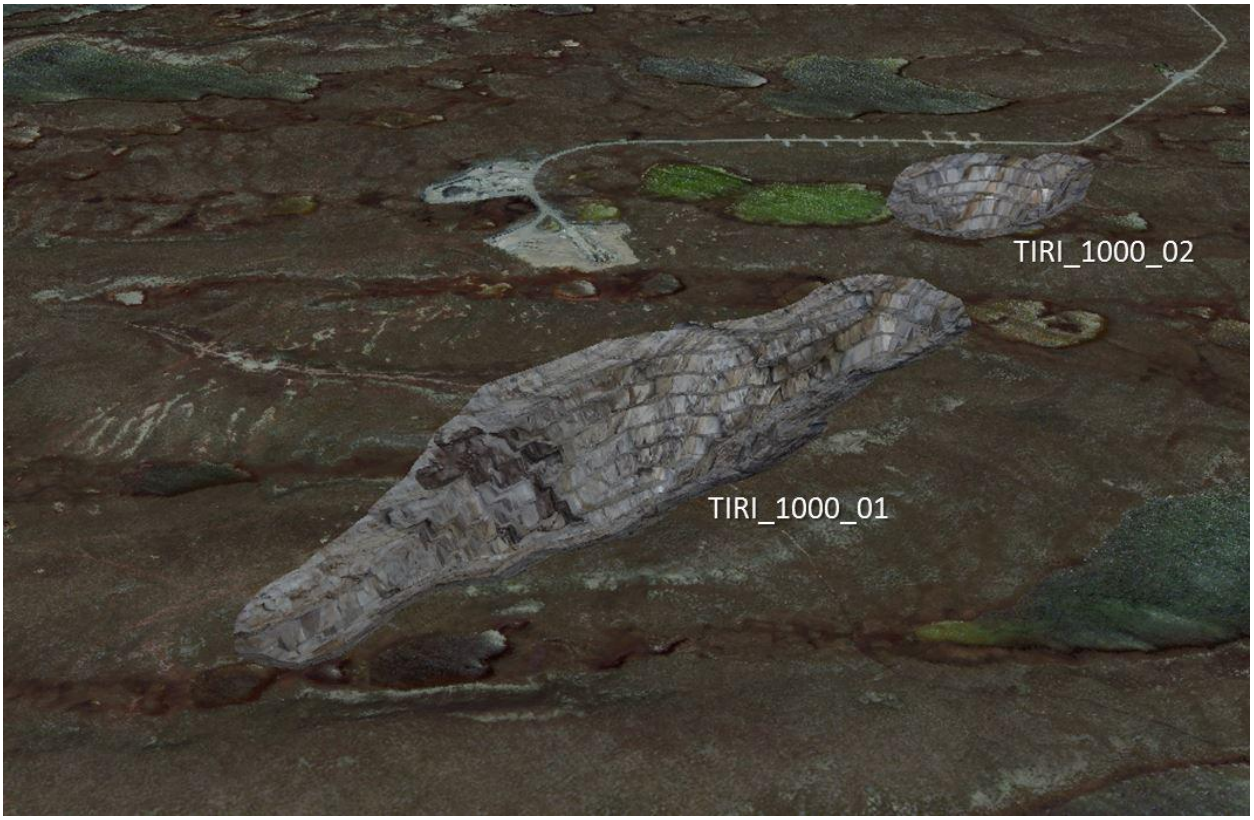


Figure 16.8 - Tiriganiaq open pit looking north

It is currently assumed that no permanent crown pillar will be left between the pit floor and the underground operation. The upper portion of the underground mine will be mined during the first years of operation, with paste fill being placed as tightly to the back of the upper stopes as possible to maintain stability. The final pit floor will eventually rest on the backfilled stopes. This approach will continue to be evaluated.

16.4.4.4 Open Pit Mobile equipment

The fleet selection was based on the efficiency, availability and fuel consumption of the equipment. The fleet will be used on two 12-hour shifts daily.

Agnico Eagle will supply the mobile pit equipment for development, production and services. The equipment selection was based both on the average and the peak utilization rates, and the tonnage to be mined over the life of the mine.

Table 16.7 shows the fleet selection for a total of 57 pieces of equipment required during the peak production for the operation of the two Tiriganiaq pits. The proposed equipment's selection was based on the best practices in the company and the synergy in terms of spare parts maintenance and labour training. Validation was conducted between the equipment selection and mine design, and mining design parameters defined accordingly.

Table 16.7 - Summary of pit equipment fleet during peak production period

Equipment	Capacity	Total
Haulage truck	65-t class	6
Front-end loader	11-m^3	1
Hydraulic shovel	110-t operating weight	2
Hydraulic shovel with rock breaker	50-t operating weight	1
Track dozer	40-t operating weight	2
Wheel dozer	42-t operating weight	1
Grader	14-foot blade	2
DTH drill	100-165-mm hole ∅	3
Fuel truck		1
Lube truck		2
Service truck		2
Water truck		1
Loader with side bucket (stemming)		2
4x4 Pickup truck 450 (bit truck)		1
4x4 Pickup truck 350 (blaster)		1
4x4 Pickup truck 250		16
Lowboy carrier	100t	1
Dewatering pumps		4
Pit busses	20-30 passengers	3
Light tower		6
TOTAL		57

16.4.5 Underground Mining

The underground operations in the Tiriganiaq and Wesmeg/Normeg deposits will mine 9.14 million tonnes of ore at an average grade of 8.89 g/t gold. Moreover, 1.00 million tonnes of marginal ore averaging 3.10 g/t gold originating from the underground development will be hauled and stockpiled on surface for processing at the end of mine life.

The underground mine will feed the process plant at a nominal rate of 3,000 tpd over a period of 9 years. Development of the underground infrastructure will start well in advance of the mill start-up.

Based on the Tiriganiaq underground mineral reserves estimated in Item 15 of this report, an updated development and production plan has been developed and used to define the operating and capital requirements. The current Tiriganiaq underground reserves lie between 100 m and 650 m below surface. The main underground mine plan consists of 23 levels (level 100 through level 650) set at 25-m intervals.

Access to all underground workings will be via one of two decline ramps, which can be seen in Figure 16.9 and Figure 16.10. The existing portal will be used as the initial mine access for pre-development, from which the existing ramp (decline 1) will be extended to the 300 level. A second Decline developed in the hanging wall of the Tiriganiaq deposit from a second surface portal (portal 2) will be used as the trucking ramp and the main access for the Meliadine mine. Decline 1 will remain as a secondary egress point and provide direct access to the upper parts of the mine. A third decline (Decline 3) will be developed allowing access and mining of the Wesmeg 650 lode.

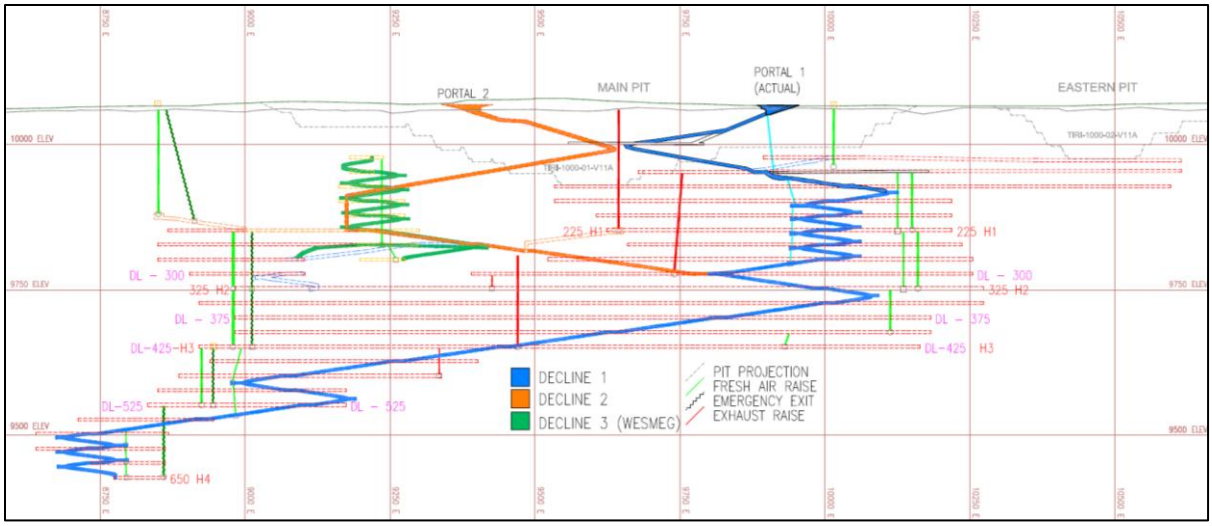


Figure 16.9 - Longitudinal section of the Tiriganiaq underground mine plan, looking to the north

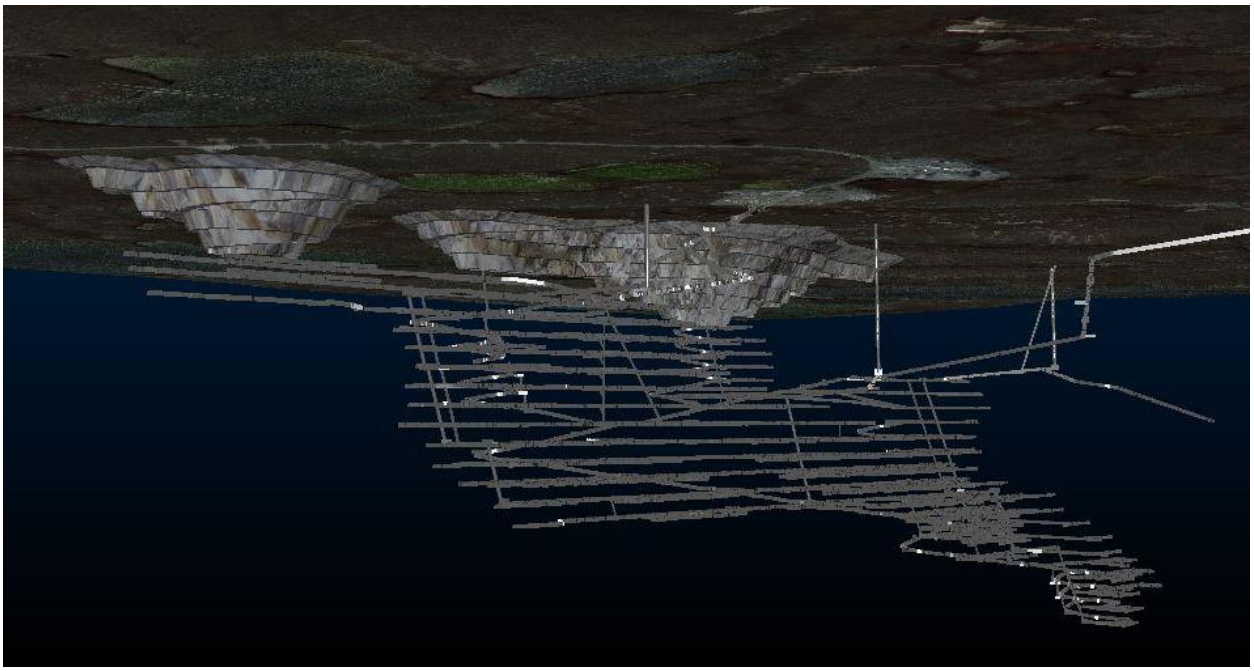


Figure 16.10 - Tiriganiaq underground mine looking south

16.4.5.1 Mining Methods

A long-hole mining method was selected to mine the Tiriganiaq deposit due to the shape, thickness and orientation of the orebody. The stope height was set at 25 m to minimize drill deviation and waste rock dilution, and to maximize mine recoveries. Two variations of long-hole mining (transverse or longitudinal mining) will be utilized; the variant selected for a particular stope will depend on the thickness of the ore zone. Considering the grade of the Tiriganiaq underground mineral reserves, ore recovery will be maximized by backfilling every stope mined. Cemented pastefill will be used in primary stopes, whereas secondary stopes will be backfilled with dry rockfill only. However, during the operation, the flexibility to leave some rib pillars

between primary and secondary stopes will be considered at specific locations where the geometry of the lodes (narrowing) and/or the ore grade justify it. The primary and secondary transverse stope width is set at 18 m. Longitudinal stopes are also set at 18 m long, but could be eventually adjusted during the operation depending on the geometry of the individual lodes.

A long-hole mining method will also be considered for the eventual exploitation of the underground indicated and inferred mineral resources located in other deposits (F zone, Pump and Discovery) not currently include in the LOM plan but with some variations because the lodes in these deposits are generally shallower-dipping (dips ranging between 45° and 60°) and are narrower than the Tiriganiaq lodes. Longitudinal mining would be used for these deposits. Permanent rib pillars would be left between adjacent stopes, and uncemented rockfill would be used to fill the stopes. Levels would be 20 m apart (instead of 25 m) to minimize drill-hole deviation and dilution due to the shallower dip.

In the Tiriganiaq deposit, transverse mining will be adopted for stopes with a true ore-zone thickness averaging 4 m or more and longitudinal mining will be adopted for stopes with a true ore-zone thickness averaging less than 4 m. Table 15.1 (in Item 15) identifies the parameters used for the stope design and the dilution calculation, considering the mining method and the mining fleet selected in relation with the deposit geometry (multiple narrow lodes stacked and dipping between 60° and 75°). The size of the stopes and their expected mine dilution have also been defined based on the geotechnical data currently available (see the next subsection of this report).

The underground mineral reserves were defined based on the geological block model available in December 2014. The economic parameters presented in Table 16.8 were used to define the ore and marginal cut-off grades. Minesite and closure costs defined in a trade-off study in 2014 were used to derive ore and marginal cut-off grades for each deposit. For the mineral reserve, a diluted cut-off grade of 4.80 g/t gold is defined based on a gold price of US$1,150/oz. Moreover, all the material with a grade higher than 1.79 g/t generated during the underground development work will be stockpiled at surface in order to be processed at the end of the mine life. This last cut-off grade includes the cost of hauling the material to surface. A mining recovery of 95% is applied to all stope tonnages.

Table 16.8 - Underground mine parameters used for gold cut-off grade calculations

Parameter	Tiriganiaq/Wesmeg Reserves
Gold price (US$/oz)	US$1,150
Gold refining charge	C$2.50/oz
Exchange rate (C$/US$)	1.08
Dilution (%)	Variable (1)
Metallurgical recovery	Variable
Mining cost (per tonne milled)	C$63.00/t
Processing cost (per tonne milled)	C$30.50/t
G&A cost (per tonne milled)	C$82.89/t
Closure & Rehabilitation cost (per tonne milled)	C$0.05/t
Total ore-based cost (per tonne milled)	C$176.44/t
Total Marginal ore-based cost (per tonne milled)	C$60.84/t
Diluted gold cut-off grade (ore)	4.80 g/t
Not diluted gold cut-off grade (ore)	-
Diluted gold Marginal ore cut-off grade	1.79 g/t
Stockpile Rehandling cost per tonne milled)	C$3.00/t

(1) Mining dilution calculated with MSO (0.5 m footwall and 1 m hanging wall, except for the 1000 lode where the dilution is set to 1.0 m in the footwall and hanging wall

16.4.5.2 Underground Geotechnical Parameters

The underground mine design was adjusted in 2013 and stope dimensions were set at 18 m for both primary and secondary transverse stopes on the basis of a review of existing rock mass data and empirical analyses. External dilution estimates were revised on the basis of anticipated rock mass quality: 0.5 m in the footwall of all lodes except Lode 1000 where 1 m of dilution is expected. External dilution of 1 m is expected on average from the hanging wall of all stopes.

In 2014, numerical modeling and analytical and empirical design tools were used:

- to evaluate stope and pillar dimensions and performance in terms of stability and potential external dilution;
- to provide geomechanical guidelines for mining sequence and development;
- for ground support design (Knight Piesold, 2014).

A mine-wide three-dimensional FLAC3D model and stope-scale 3D and 2D numerical models (Meshed 3DEC, Block 3DEC and Phase2) were used in conjunction with empirical tools such as Stability Graph (Mathews *et al*., 1980, Potvin, 1988 and Nickson, 1992) and ELOS chart (Clark, 1998), and limit equilibrium analysis to estimate dilution and stope ground-support requirements. Pillar stability was analyzed using numerical modeling stress results and empirical pillar design charts (Lunder and Pakalnis, 1997).

The empirical and numerical analysis results indicate that stope dimensions are generally adequate but aggressive under some circumstances (weaker rock mass sub-domains, intense foliation and tighter jointing, deep hanging wall relaxation, high mining-induced stress), which is expected to result in dilution in excess of the planned averages reported in Table 16.8. These cases could represent up to 30% of the proposed stopes. Mitigation strategies include additional hanging wall ground support and locally reducing stope dimensions once the distribution of rock mass characteristics is better defined.

Secondary pillar instability could result in operational difficulties including potentially some seismicity at greater depths. The completed stability analyses indicate that secondary pillars are generally designed to be stable; however, there are some exceptions such as the wider lodes 1150-1250 and some late-stage pillars in the 1000 and 1100 lodes.

16.4.5.3 Mine Development

A development schedule was prepared to ensure that stopes will be available on time to sustain the process plant feed at a nominal rate of 3,000 tpd. The majority of the development plan will use multiple faces and include flexibility to ensure the design target is achieved.

Table 16.9 details the development schedule for the life-of-mine and pre-production work. A total of 86.5 km of development will be required to access and develop the different stopes on time. The development of Decline 1 (Figure 16.9) to access the different horizons and levels is on the critical path and will be prioritized. Four teams (three Agnico Eagle teams plus one contractor team) will be required during the peak development period (late Y-1 to early Y2), and their number will gradually be decreased to fit with the reduction of metres of development during the later years of operation (Y3 to Y7).

Table 16.9 - Underground metres of lateral development planned annually

	Total	Y-5	Y-4	Y-3	Y-2	Y-1	Y1	Y2
CAPEX	51,251	1,984	3,835	5,966	6,662	6,531	8,805	6,949
OPEX	35,252	0	63	265	1,917	5,104	5,551	4,704
Total	86,503	1,984	3,898	6,231	8,579	11,635	14,356	11,653

	Y3	Y4	Y5	Y6	Y7	Y8
CAPEX	3,765	2,817	1,797	1,500	640	
OPEX	7,051	3,257	1,805	2,102	2,503	930
Total	10,816	6,074	3,602	3,602	3,143	930

16.4.5.4 Production Drilling and Blasting

Drilling and blasting parameters will differ depending on the mining method and the stope size. Transverse and longitudinal stopes will be drilled using 100-mm and 89-mm diameter holes, respectively.

An initial slot, 0.76 m in diameter, will be made in each stope using appropriate boring equipment to allow for the rock swelling during blasting.

Similarly to the open pit operation, bulk emulsion product manufactured on site will be used for the underground development and production blasting. The explosives plant will be built early during the construction period in order to produce emulsion at a time when explosives consumption is becoming significant, and to avoid having to order and store large amounts of explosives at site.

16.4.5.5 Backfilling

Cemented pastefill will be used in the longitudinal mining sequence, in which each stope will be backfilled and cured before an adjacent stope can be mined. For the transverse mining method, the primary stopes will also be backfilled with cemented paste, whereas secondary stopes will be backfilled with dry, uncemented rockfill. The majority of demand for rockfill will be met by transferring waste rock from development headings. Any additional rockfill needed will be trucked from the waste stockpile generated at surface in the open pit operations. This will be necessary from the end of Y4 through the following years when underground development will gradually be reduced and cease.

The paste backfill will be made by mixing pressed filtered tailings, cement and water in a facility located next to the Decline 1 portal.

16.4.5.6 Mine Ventilation and heating

In order to evaluate the ventilation requirements for the underground operation, a list of mobile equipment that will be in operation during the peak period of production and development was compiled and the required volume of fresh air per minute calculated. A 20% reduction on total required volume of fresh air is applied to account for the inclusion of some higher-performing engines (Tier 4 engines) that will replace engines currently considered at this stage of the study. The maximum underground mine ventilation requirements were calculated at 544 m^3/sec (1,153,000 ft^3/minute (cfm)). Two 576-kcfm fan systems will be required to ventilate the mine,

one for the eastern part of the mine and another one for the western part. One 800-kcfm fan system will be required in the return air raise. The ventilation network is shown in Figure 16.11

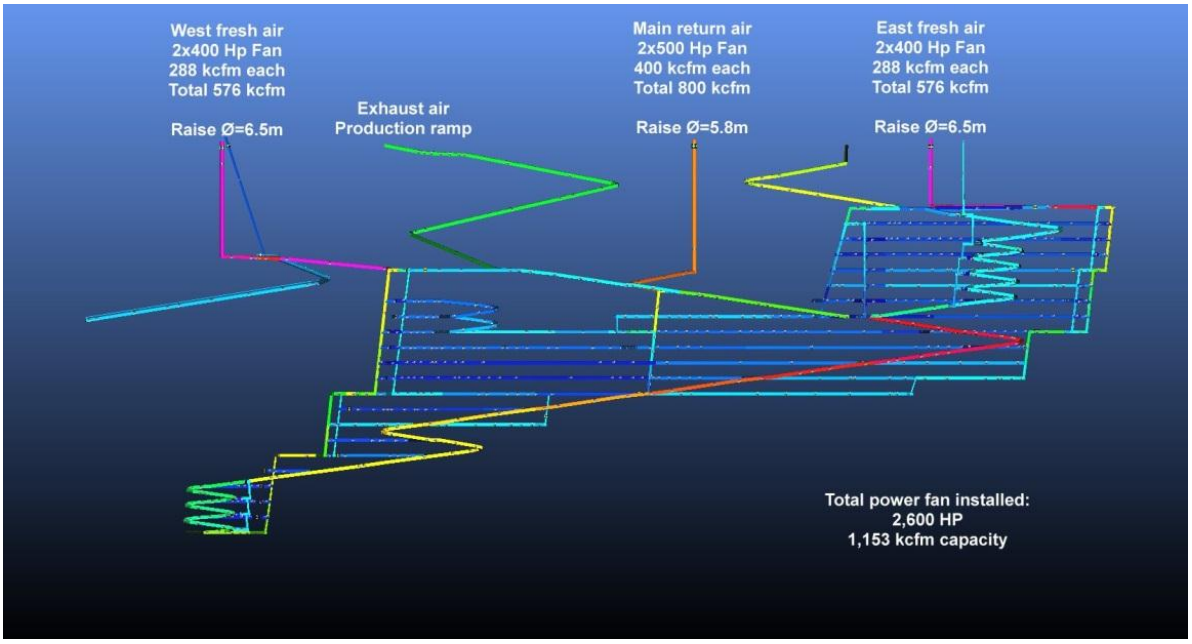


Figure 16.11 - Simplified ventilation network for the Tiriganiaq underground mine

The mine-air-heating infrastructure for the Tiriganiaq underground mine consists of multiple indirect oil-fired air heaters and heat exchangers for each raise. The heat will come from both the heat recovery system at the power house and from the fuel heaters. Annual fuel consumption for the mine air heating will be approximately 4 million litres.

For potential underground operations at the other deposits, fresh air would not be heated and saline water would be used for mining activities requiring water consumption, in order to prevent its freezing.

16.4.5.7 Underground Mobile Equipment

Table 16.10 summarizes the underground mine equipment fleet that will be required during the peak period considering the development and production plan defined in the technical study of the project. This fleet was selected in consideration of the quantities of material to be mined and moved, the geometry of the orebody and from the expertise Agnico Eagle gained at its other mines in operation. Up to eight 60 t trucks will be used to haul waste and ore at surface or rockfill into stopes. Scooptrams will be used for mucking development headings or production stopes.

Table 16.10 - Underground equipment fleet

Equipment	Capacity	Quantity required
Main equipment		
truck	60t	8
Production scoop	12 yards	4
Development scoop	8 yards	4
Production drill with V30 attachment	3½ to 8½ po	2
Production drill	3½ to 8½ po	1
Production drill Top Hammer	3½ to 5 po	2
Jumbo	2 Booms	4
cable drill		2
Development loading unit		3
bolters		8
Production loading unit		2
Scissor Lift		6
Auxiliary equipment		
Auxiliary scoop	3.5 yards	3
Men Carrier		6
Scaler		2
boom truck		2
Grader	16 feet blade	2
Lube Truck		2
service tractor		10
supervision tractor		13
Concrete truck		2
small lift		2
small shovel		2
Total		92

Item 17. Recovery Methods

Significant metallurgical testing has been conducted on Meliadine samples, as discussed in Item 13 of this report. Comminution testing confirms the use of 75th percentile of ore hardness to design the mills, which is consistent with standard practices. The gravity separation tests performed by Knelson and SGS confirm the presence of liberated coarse gold, which agrees with the nugget effect observed with the Tiriganiaq ore. The coarse gold is in the 600 µm to 2,000 µm range and is generally in the form of flakes. Test results easily demonstrate sufficient economic justification for including gravity separation at Meliadine. Results indicate the possibility of recovering 40% of the gold using a custom gravity circuit. Inclusion of a continuous gravity circuit, combined with concentrate regrind, increases the global gold recovery by 1.5%. This higher recovery is related to the fine gold particles (5 µm to 20 µm) locked in arsenopyrite, which was described by AMTEL (2013). Leaching testing confirms the need to use pre-aeration tanks to control the cyanide consumption. Mineralogical studies indicate the presence of pyrite, arsenopyrite and pyrrhotite which are oxygen and cyanide consumers. The use of oxygen prior to air was not economically justified. Carbonaceous mineral was identified in lode 1000 of the Tiriganiaq deposit, which sometimes generates preg-robbing. The addition of activated carbon during leaching eliminates preg-robbing, and justifies the selection of a CIL circuit. The filtration circuit is designed using the filtration test results from Pocock (2014). Recent filtration test results, not presented, confirm that the design criteria are more than adequate to obtain the desired filtration of tailings.

The metallurgical test results provide the basis for the detailed process development. Table 17.1 shows the general design criteria for the process plant. All equipment for this project has been sized based on the test results or best standard industry calculations.

The proposed process at Meliadine comprises crushing, grinding and gravity recovery, cyanidation and gold recovery in a CIL circuit followed by a pressure Zadra type stripping circuit. The main ore processing streams are continuous operations, while the carbon-handling and gold recovery circuits are batch operations. The plant operating schedule is on a continuous basis with a designed 92% plant availability.

Table 17.1 - General process plant design criteria for two different throughputs: 3,000 and 5,000 tpd

Criteria	3,000 tpd	5,000 tpd
Mill operating days/year	365	365
Mill availability	92%	92%
Gold production (oz/day), nominal design	850	920
Crushing Plant utilization	65%	75%
Crushing Plant Feed Rate operation design (tonnes/hour)	209	302
Crusher Feed Rate Operation design (tonnes/hour)	157	181
Crushing circuit product (mm P80) (mill feed)	75	110
Comminution specific energy (pinion) (kWh/t)	22.7	19.1
SAG specific energy (pinion)(kWh/t)	22.7	8.4
SAG mill circuit product transfer size (microns T80)	300	1,300
Bond ball work index, BWi 200 mesh screen (80th percentile) (kWh/t)	14	14
Bond Abrasion index (Ai) design (80th percentile) (g)	0.34	0.34
Cyclone overflow (microns P80)	75	75
Gravity gold recovery design	40%	40%
No. CIL leach stages	5	7
CIL retention time design (hours)	51	49
Final tails density (% solids)	45.9	47.5
Filter press utilization	86%	86%
Paste backfill plant capacity (wet tonnes/day)	3,000	5,000
Paste backfill plant availability	92%	92%

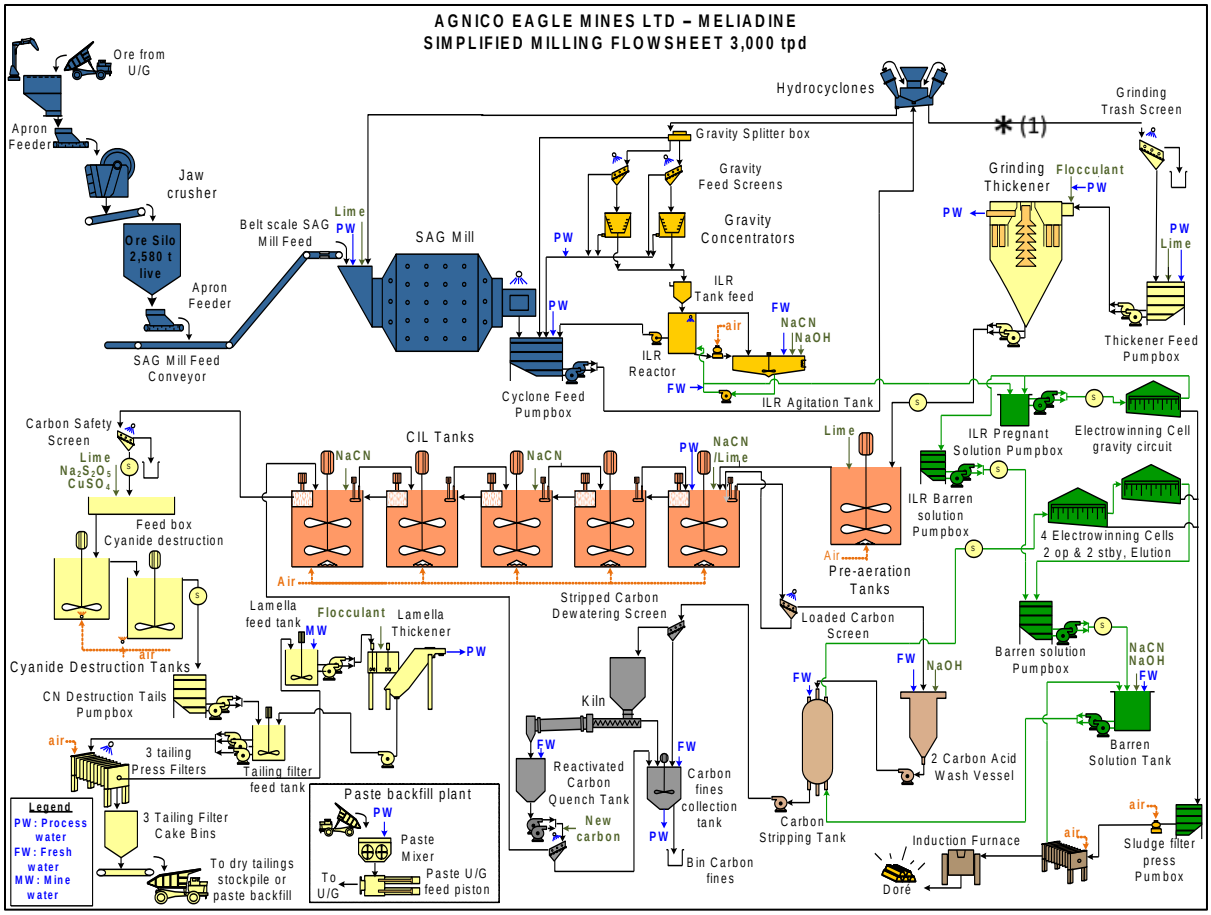
17.1 General

The proposed process plant will treat gold ore at a nominal process rate of 3,000 tpd from Year 1 to Year 3. A process plant expansion of 2,000 tpd will increase capacity to 5,000 tpd at Year 4 due to the addition of ore from the Tiriganiaq open pit operation. The Tiriganiaq deposit will be the dominant source of process plant feed for the plant during the early years. A combination of conventional gravity concentration and cyanidation processes has been selected for the project. The process plant will consist of three separate facilities:

- a crushing facility, including primary and related material-handling facilities that can crush ore from either underground or open pit operations;
- a main processing facility including a coarse ore surge bin and related feeding and reclaim systems, single-stage grinding, gravity concentration and an intensive leaching reactor, leaching feed thickening, CIL cyanide circuit, loaded carbon acid wash, elution and reactivation, gold electrowinning, smelting, cyanide destruction of the leach residue and filtration of final tails;
- a paste backfill plant.

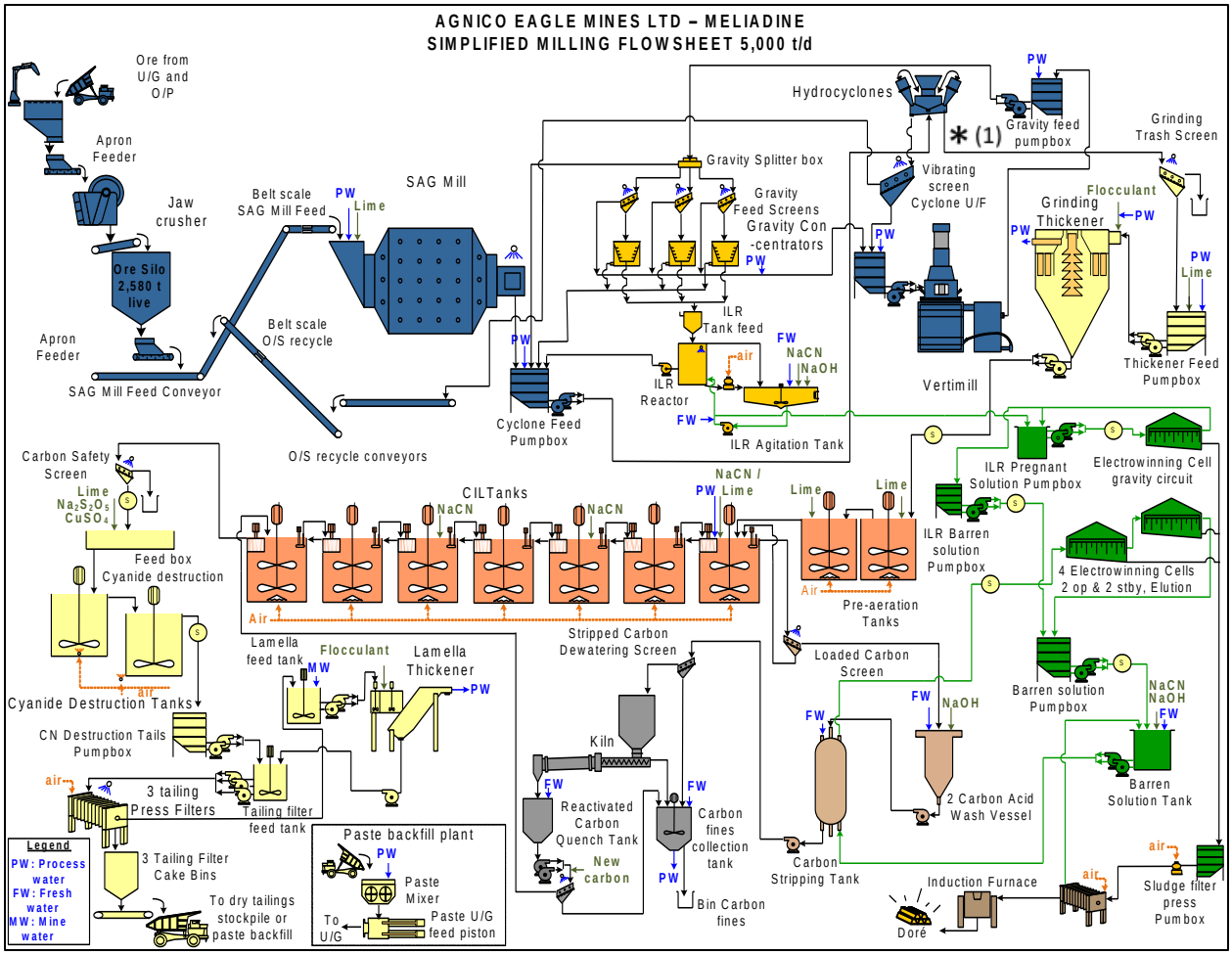
It should be noted that, for operational and maintenance considerations, all process equipment (CIL tanks, thickeners, the paste plant, water tanks, *etc.*) are located inside the process plant building, which is insulated and heated.

Figure 17.1 and Figure 17.2 show the simplified milling flowsheets for the 3,000 and 5,000 tpd throughput scenarios, respectively.



(1) Continuous gravity circuit added in the CAPEX, OPEX and recovery model

Figure 17.1 - Meliadine project's proposed milling flowsheet at 3,000 tpd throughput capacity



(1) Continuous gravity circuit added in the CAPEX, OPEX and recovery model

Figure 17.2 - Meliadine project's proposed milling flowsheet at 5,000 tpd throughput capacity

17.2 Crushing and Ore Handling

The ore is trucked from the underground mine to a surface crusher located in the vicinity of the process plant. The trucks dump into a hopper equipped with a static grizzly and a hydraulic rock breaker that can handle any oversize rocks. An apron feeder is located under the dump hopper. The ore is fed to a reciprocating grizzly feeder via the apron feeder. Oversize rock from the grizzly feeder is fed to a jaw crusher. The jaw crusher product and the undersize from the reciprocating grizzly feeder are both transferred by gravity to the jaw crusher discharge conveyor, which then carries the material to a 2,500-tonnes-capacity ore bin adjacent to the process plant. The ore is reclaimed from the bin using an apron feeder that discharges onto the SAG mill feed conveyor at an average feed rate of 136 t/h.

The crushing plant is designed to accommodate an increase in production from 3,000 tpd to 5,000 tpd in Year 4.

17.3 Grinding

Grinding is performed by a single-stage mill in closed circuit with a cyclone cluster. Cyclone underflow recirculates to the SAG mill, while the overflow reports to the thickener. The thickener underflow is fed to the CIL circuit and the overflow reports to the process water tank, which is the source of water for most applications in the plant. It should be noted that the layout proposed for the SAG mill discharge area takes into consideration the potential future retrofit of a vibrating screen and recycle conveyors, should the plant throughput be increased and the circuit expanded to a two-stage circuit. The expansion would be located to the east of the primary grinding circuit (refer to the Item 18 Infrastructure for more detail). A discharge screen would be necessary to avoid oversize feed to the Vertimill.

17.4 Gravity Recovery

A portion of the SAG mill discharge is diverted to the gravity circuit that is comprised of two centrifugal batch concentrators operating in parallel. Ahead of each concentrator is a vibrating screen that removes material coarser than 2 mm and returns it to the grinding circuit. The undersize from both screens feeds the centrifugal concentrators. The tailings from the concentrators are combined and returned to the cyclone feed pump box, while the concentrates are combined and sent to the intensive leaching reactor where they are leached prior to the pregnant solution being pumped to a dedicated electrowinning circuit. Space is also allocated, in the layout, for a third gravity concentrator unit.

The continuous gravity system is located outside of the grinding circuit. The concentrator is fed by the cyclone overflow after the removal of coarse material (+2 mm) by screening. All of the cyclone overflow is fed to the continuous gravity circuit.

The tailings report to the thickener while the concentrate is reground. The regrind circuit consists of a regrind mill in closed circuit with cyclones. The gravity concentrate would be reground at 80% passing 38 µm prior to being pre-aerated and leached through the leaching circuit.

17.5 Cyanidation and Carbon Adsorption

The grinding thickener underflow is sent to a pre-aeration tank into which process air is sparged to achieve sulphide oxidation, and lime is added for pH adjustment. The pre-aeration tank is followed by five agitation CIL tanks in series. Leaching is performed using sodium cyanide, and pH is controlled with lime addition. All CIL tanks are also sparged with process air in order to keep the oxygen concentration sufficient for gold leaching.

Slurry travels through the CIL circuit via inter-stage pumping screens, while gold-loaded carbon is pumped counter-current to the slurry flow by carbon transfer pumps, to the previous CIL tank and finally to the loaded carbon screen. This step is performed regularly, based on the carbon gold loading. Space has been allocated to the west of the CIL circuit for future expansion consisting of adding three tanks of larger volumes. This expansion will maintain an appropriate

residence time for the leaching process; the expanded cyanidation circuit will consist of two pre-aeration tanks followed by seven agitation CIL tanks in series.

17.6 Gold Recovery Circuit

Loaded carbon from CIL tank 1 is pumped to the loaded carbon screen. The screen undersize is returned to the same CIL tank while screen oversize feeds the stripping circuit. Loaded carbon flows by gravity from the loaded carbon screen to an acid wash vessel. A dilute solution of hydrochloric acid is used to remove calcium carbonate and other contaminants from the carbon. The hydrochloric acid solution is circulated in an up-flow manner through the carbon bed in closed circuit with the acid solution pump and acid wash tank. Once the washing step is complete, the solution is neutralized and discarded. The carbon is then rinsed with fresh water before it is transferred to a carbon stripping vessel. A pressurized Zadra desorption system is used to recover gold from the carbon. It is designed to run at approximately 140ºC and a maximum operational pressure of 380 kPa.

In the strip vessel, carbon is combined with hot strip solution. The overflow from the stripping vessel consists of pregnant (gold-bearing) strip solution that is pumped to electrowinning cells where gold is deposited onto stainless steel cathodes. The stripping cycle is operated for a predetermined period of time (typically 12 to 16 hours) and ends when the carbon loading reaches a low value. Barren solution is reused from one cycle to the other, but a solution bleed is periodically sent to the CIL circuit to control impurity buildups. Once the stripping cycle is completed, the carbon is rinsed and transferred to the reactivation kiln. The kiln thermally reactivates the carbon at ~700°C to remove organic compounds. Reactivated carbon is quenched with fresh water upon exiting the kiln. From there it is pumped to the reactivated carbon sizing screen to remove fines. As required, new carbon is added to this stream after having been attrited to remove fine particles. The screen oversize is returned by gravity to CIL tank 5, while screen undersize reports to the carbon fines collection tank.

The agitated carbon fines collection tank receives undersize from the stripped carbon dewatering screen and the reactivated carbon sizing screen, as well as fines from the kiln screw feeder. Underflow from the tank is pumped to the carbon fines filter, and the resulting cake is collected and bagged for resale.

17.7 Cyanide Destruction

Cyanide destruction is done in two tanks in series, using the SO_2/Air process. The tails from the last CIL tank are directed to a carbon safety screen to recover any carbon that could have escaped the CIL circuit. The screen oversize is recovered into a bin, while the undersize is sampled before flowing to the cyanide destruction tank feed box that receives $CuSO_4$, sodium metabisulphite ($Na_2S_2O_5$) and lime. The slurry then flows by gravity to cyanide destruction tank 1 where it is agitated and sparged with process air. The tank overflows into cyanide destruction tank 2, where it undergoes further agitation and sparging with process air. The cyanide destruction tails, from the cyanide destruction tank 2, flow by gravity to a pumpbox where they are pumped to the filtration circuit.

17.8 Tailings Dewatering

Tailings from the cyanide destruction circuit are pumped to an agitated filter feed tank, which acts as a buffer between the gold recovery process and the tailings filtration circuit. From there the slurry is pumped to the tailings filter presses. The filtration plant consists of three recessed plate filter presses (two in operation, one standby). The presses operate in a cycle consisting of filter closing and clamping, filter feed, core wash and core blow, cake blow, and cake discharge.

The filters bring the moisture content of the filter cake below 16%. Filtrate and cloth wash solutions are collected and pumped to the lamella clarifier. Part of the clarifier overflow is reused as filter cloth wash water, while the excess is forwarded to the gland seal water tank.

The filter cake is dropped onto a belt feeder located under each filter unit. Each belt feeder is located at an elevation such that the chute above it provides reserve. The three feeders discharge onto a collecting conveyor installed perpendicular to the three feeders. This conveyor extends outside the plant building to load trucks that will transport the cake to the tailings area or to the paste backfill plant, as required.

17.9 Paste Backfill

The paste backfill circuit is detached from the main process plant and housed in a separate building located close to underground mine portal #1. This building also houses the services required for the operation (compressed air, maintenance work area, fresh and process water). As required, filtered tailings are trucked from the process plant to the paste backfill plant and dumped into a receiving hopper. A screw feeder reclaims the filtered tailings and transfers them to a weigh scale conveyor that discharges into the paste mixer, where water is added. Cement is fed from a 200-tonne-capacity bin adjacent to the paste backfill building. The paste mixer overflows into the paste pump hopper and the paste is finally pumped underground using one paste piston pump. The water required for the paste recipe can be obtained from either the underground mine or the process plant.

17.10 Energy, Water and Laboratory

Refer to the Item 18 Infrastructure for more detail.

Item 18. Project Infrastructure

This section describes the design and sizing of the surface facilities for the Meliadine project including both at the site and off-site at Rankin Inlet, the nearest community and shipping port.

18.1 Design Basis

The infrastructure is designed to accommodate the personnel, equipment and fuel demands for nine years of mine life.

An all-weather access road ("AWAR") was built by Agnico Eagle to connect Rankin Inlet to the Meliadine site. The final route to the camp was selected in consultation with the local Inuit community. The AWAR is a private, 23.8-km-long, single-lane road (6.5-m-wide running surface) from the Char River bridge turnoff to the Meliadine site. Construction was completed in September 2013. The location of the road is shown in Figure 4.1.

The mining and processing operations will require the design and location of ore stockpiles and waste rock storage pads as well as tailings storage facilities, which are described in Item 20 of this report. The operations as well as the permanent accommodations require a water management plan for handling process as well as potable water, which is also described in Item 20.

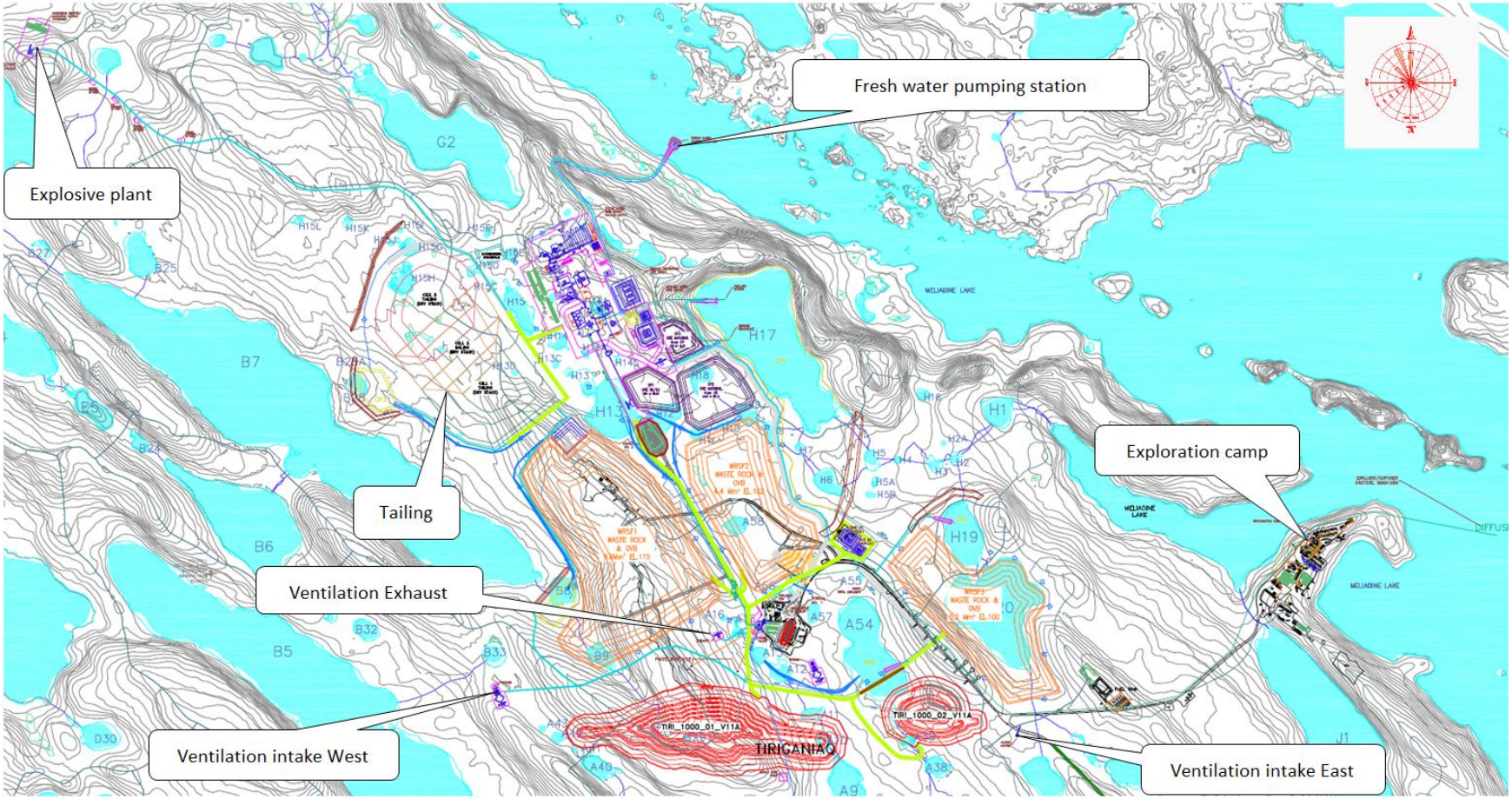
Because of its location, the Meliadine infrastructure will require special cold climate and permafrost design considerations. The climate data used for this study were based on the values specified in the National Building Code of Canada and on experience building Agnico Eagle's Meadowbank mine, located 290 km to the northwest.

The arctic design of the buildings will be reflected notably in insulation and special foundation requirements, use of heated utilidors (insulated, enclosed utilities corridors) to connect the buildings, and space-heating requirements.

Based on the current geotechnical evaluation, the surface of the bedrock is generally located between 2 m and 13 m below surface. Consequently, building foundations and heavy equipment (such as the SAG mill in the process plant) are designed using pilings for structural support.

Based on the seismic hazard assessment provided by the Pacific Geosciences Centre for this site, the proposed development is located within Seismic Zone 0 of the current National Building Code, so there is negligible seismic risk.

The first drawing in Appendix 18.1 (6509-000-210-001 SHT 02) shows the location of the planned infrastructure. The main facilities are located about 1.6 km north-northwest of the Tiriganiaq open pit (2.8 km west-northwest of the existing exploration camp), as shown on Figure 18.1. This location is the most favourable site because of its relatively shallow overburden and favourable geotechnical conditions.



The two Tiriganiaq open pits can be seen at the south side (bottom) of the map. The purple area at the center top includes the permanent camp, processing plan and power plant. The current portal is the small red oval just north of the larger pit, and the proposed portal is the larger red oval near the center of the map.

Figure 18.1 - Layout of proposed Meliadine mine and processing facilities.

18.2 On-site Infrastructure

Figure 18.1 depicts the proposed two open pits, the portals to the underground mine, plant site, tailings impoundment, waste rock and overburden storage areas and main haul roads. The plant site and other infrastructure is conveniently located relative to the mining sites but at a sufficient distance from the open pit (a minimum distance of 900 m has been used) to reduce the impact of vibration and fly rock caused by blasting. The exceptions to this are the ramp portal #1, paste plant, the intake and exhaust ventilation systems and water treatment plant. These buildings will be evacuated during blasting. The compact arrangement of buildings and other infrastructure (Figure 18.2) is primarily designed to reduce site preparation and pad building costs as well as to reduce the overall project footprint.

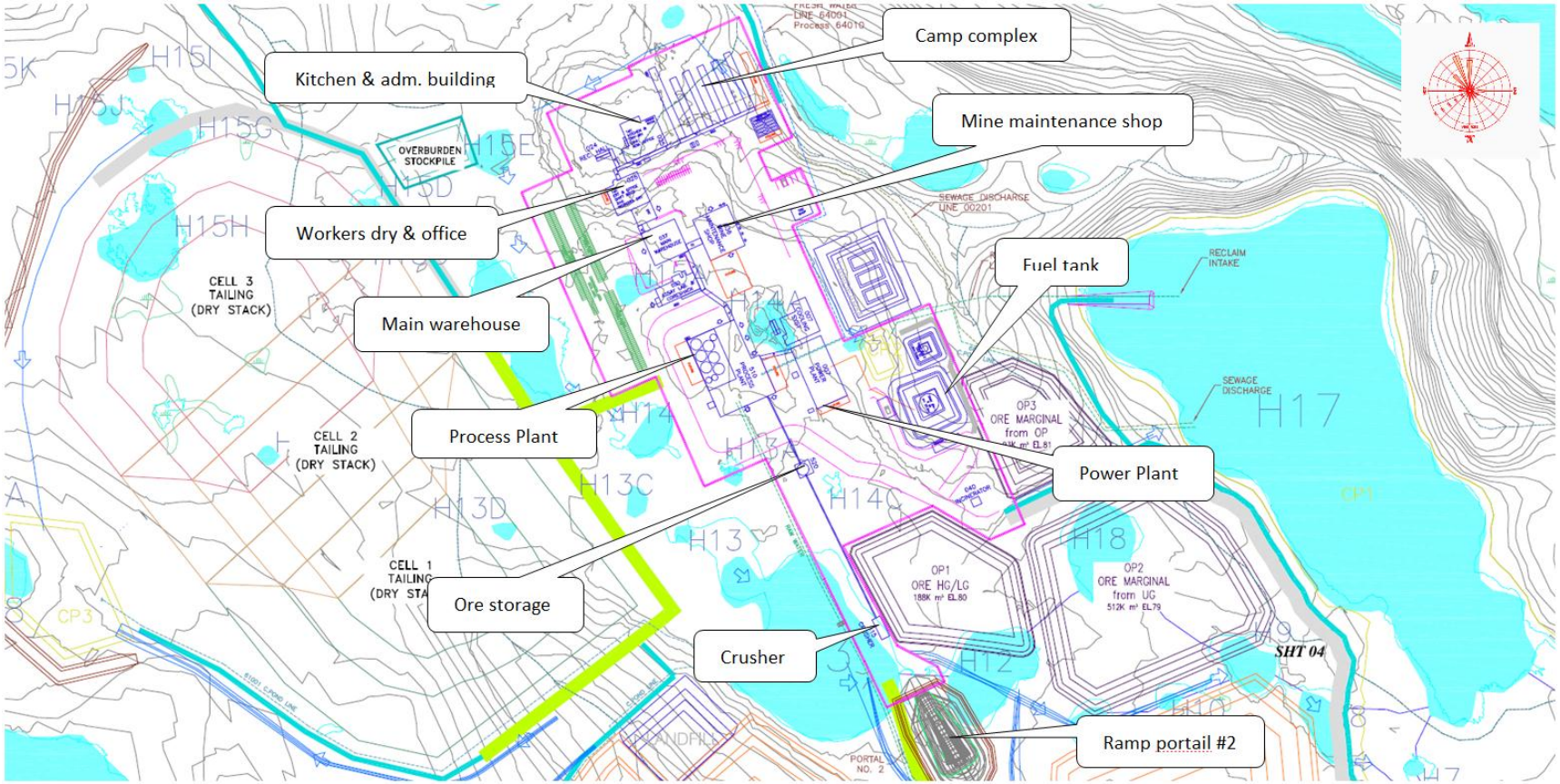


Figure 18.2 - Layout of proposed infrastructure at Meliadine project

18.2.1 Main Process Plant Building

The mineral processing facilities consist of three main areas: (1) the primary crusher, (2) the crushed ore storage bin and, (3) the mill building housing the rest of the ore processing equipment. The building of 6,946 m^2 will be a standard steel structure covered with cladding to be assembled on site. Internal walls will consist of steel studs with single-skin steel panels; gyproc will be added where required for fire rating. Internal offices will be prefabricated modules to simplify installation and reduce on-site construction. Truck doors will provide access to a central corridor that will run the length of the process plant, providing space for laydown of equipment and access to parts and consumables from the warehouse.

The process plant building foundation will be supported by drilled piles embedded in bedrock. Heavy equipment will be placed on the structural concrete slab floor (a raft) which will be structurally supported by pedestal piles. The process plant building is designed to maintain an average indoor temperature of 10°C.

18.2.2 Power Plant

The Meliadine site power station will be a diesel-fuelled generation facility using multiple medium-speed reciprocating engines housed in a powerhouse, complete with heat recovery and all auxiliary equipment.

The power plant will be a pre-engineered insulated building of 3,288 m^2 constructed on pile foundations. It is designed to accommodate six 5.2-MW units for a total of 31.3 MW installed power. At the current mining rate, this meets the anticipated power requirement, calculated to be 17.3 MW (Table 18.1).

The power station will be located adjacent to the largest loads, which are located in the grinding area of the process plant, to minimize both power losses and capital cost. The fuel specified will be arctic grade light fuel oil (LFO).

Each generator set will include a local engine control panel with its own PLC-based control and will be capable of manual or automated (remote) operation.

Table 18.1 - Meliadine project power demand and electrical generator sets

Production rate (tonnes ore)	1 million t/yr
Electrical power demand	17.3 MW
Genset capacity at 100% load (each)	5.211 MW
Load	83%
Number of generators installed	6
Number of generators running	4
Total installed capacity	31.3 MW

Waste heat from the diesel power plant high-temperature loop will be recovered to provide total space heating, domestic water heating and underground heating. To meet emergency requirements, an auxiliary boiler will be installed in the powerhouse to provide maximum safety and reliability.

18.2.3 Site Power Distribution

The site power distribution includes a local power plant suitably sized for the electrical loads required by the processing equipment and the local infrastructure. Power will be generated at 12.5 kV and will be connected to a common set of switchgears located in the power house.

The electrical distribution system will consist of switchgears, dry transformers, starters, and feeder breakers for the motors and non-motorized loads in common line-ups. Lighting and small electrical service applications will be fed as required from transformers and power panels, which will be located in the electrical rooms. Armored-type cables will be installed in galvanized steel ladder trays or buried. Local capacitor banks will be installed for power factor corrections in the process building. Pre-fab electrical rooms will be located at strategic places throughout the site to distribute the power to each infrastructure location. 13-kV power cables will be used to carry electrical power to each of these pre-fabricated electrical rooms.

Energy-efficient fluorescent lighting will be used where applicable throughout the site, along with occupancy sensors for increased energy savings.

Emergency backup power will be supplied by a smaller power plant containing three 2-MW gensets located at a specific location on the industrial site.

18.2.4 Diesel Fuel Storage

A 6-million-litre fuel tank for winter fuel and a 250,000-litre tank for summer fuel will be located 150 m east of the power plant, to facilitate easy fuel distribution to the power plant, mining operations and plant facilities. Likewise, a 3-million-litre fuel tank for winter fuel and a 250,000-litre tank for summer fuel will be located 303 m northeast of portal #1, to supply fuel to the underground operation, heating for underground ventilation and open pit mobile equipment.

Winter fuel will be use 7 months and summer fuel for 5 months during the year. The summer fuel dew point is at -15 °C and -50°C for the winter fuel. The decision to use summer fuel during a certain period of the year is to lower the purchasing cost of 0.025$/liter.

The two sites are located on higher land where bedrock is close to the surface. The foundation design will involve placing structural fill to insulate the underlying bedrock and promote good drainage. A high-density polyethylene (HDPE) liner will extend up the inside slope of the perimeter berm. to the storage tank at the plant site. The storage tank will meet American Petroleum Institute specifications and be constructed of cold-temperature-resistant steel.

18.2.5 Assay Laboratory / Geology Core Shack

The assay laboratory and geology core shack are in a building located on the Meliadine industrial site. The assay laboratory is designed to accommodate an average of 250 samples/day and a peak of 350 samples/day (Mill and geology samples) using fire assay and atomic absorption methods. The geology core shack should be designed to accommodate an average of 172 samples /day and a peak of 276 samples/day.

The assay laboratory (535 m^2) and core shack (585 m^2) will be housed in a building located near the south side of the warehouse building. It will be a prefabricated steel frame (foldaway type)

structure covered by cladding and roofing panels. The foundation of the building is a steel frame on piles.

The assay laboratory and core shack will comprise:

- a core shack with a receiving area and a saw room;
- an assay laboratory with a sample receiving area, sample preparation room, balance room, fire-assay room, warehouse, an office and a service room
- The laboratory will operate 24 hours per day, seven days per week, and will be able to handle all grade control, geology, mine and process plant samples including bullion assays. Most of the environmental assaying will also be done externally.

18.2.6 Permanent Camp Complex

The permanent camp will be similar to those at other remote mines and will include individual rooms, with flexibility for visiting senior staff and guests.

The complex will be constructed of insulated structural wood frames on pile foundations. The accommodation complex will have dormitory buildings and a building that combines the reception area, security office, kitchen, dining room, and recreational facilities.

The prime reason for combining all the camp facilities is to minimize the cost through more efficient foundation designs, common walls, reduced heat losses and a compact site area.

The camp complex will meet the National Building Code of Canada Group C fire safety and occupancy requirements.

18.2.6.1 Dormitory

The design of the personel camp will provide one room per non-rotational staff and allow sharing of one room by two staff members on opposite rotations (cross shifts), based on a two-week-in/two-week-out rotation and one bed per room.

A portion of the dormitory will be a three-storey accommodation complex will be built of pre-fabricated modules. Each bedroom includes a bed, a desk with chair and a closet, and will be equipped with a TV and an internet connection. The second portion of the dormitory will be five 50-room modules comparable to the existing exploration camp facilities. The complex includes the kitchen and dining facilities. The complex will have a capacity of 370 bedrooms.

18.2.6.2 Service buildings & Administration Building

A two storey building of 2,275 m² will house the kitchen, dry/warehouse and offices. The first floor will have the main entrance with security services, a kitchen and dining room and a dry warehouse.

The second floor (1,272 m²) will house administration offices, an engineering and training room, various departmental offices (human resources, training, geology, engineering, planning, environment, *etc*.), and a potable water treatment plant, emergency boiler and HVAC equipment.

The camp complex will be designed for both electric and glycol heating; the electric heating will be used initially until the heat recovery system in the power plant is fully functional.

18.2.6.3 Emergency Response Team Building

An Emergency Response Team (ERT) building has to be designed for the Meliadine Project. The following should be included:

- one ambulance;
- one fire truck;
- a training room;
- an office, apparel room and storage room;
- a washroom.

The building will be a foldaway type measuring 22 m x 22 m at the Meliadine site. The building is separated into two sections. The garage is for emergency vehicles. The other section is the training room for the mine rescue team. The building foundation will be a structural concrete slab on piles.

18.2.6.4 Recreation Hall

The recreation hall will be two prefabricated wood modules. The gymnasium will mainly contain a section for fitness equipment. The recreation hall modules are going to be seated on tripods.

18.2.6.5 Potable Water Treatment

The potable water treatment plant contains sand filters, UV units, chlorine injection, retention tanks and distribution pumps for the camp complex.

The design flow rate for the potable water for the main camp and accommodations (kitchen, laundry) is 156 m^3 per day based on the design criteria. Fresh water will be sourced from Meliadine Lake at the water pump station to fill the fresh/fire suppression water tank located inside of the process plant. The potable water treatment plant will be a turnkey unit designed for easy installation. A water distribution pump will distribute potable water to the site through the arctic corridors

18.2.6.6 Sewage Treatment System and Disposal

There are a number of site-specific parameters that need to be considered in the design of a sewage treatment facility. These include the proximity of the system to wastewater inputs, the anticipated influent characteristics (*i.e*., the quality and quantity of the wastewater), the estimated site conditions (*e.g*., number of workers, *etc*.), the effluent requirements, and the maximum and minimum ambient temperatures. At the Meliadine Project, a sewage treatment plant is required to treat black and grey water.

Sewage will be collected from the camp and change-room facilities and pumped to a sewage treatment plant.

The system will be composed of one pumping station, four septic tanks, four bioreactors and two pre-treatment units. These last two units are for the water coming from the kitchen grease trap. Lift stations are installed at different locations to collect sewage water from the various buildings and to pump the water to the sewage treatment plant. The foundation is a steel frame floor on piles.

The sewage treatment plant for the camp will be designed to meet Nunavut effluent guidelines for wastewater discharge (NWT Water Board, 1992). It will be housed in a prefabricated (modular) structure adjacent to the camp, close to the wastewater inputs.

The sewage treatment plant discharges to the H17 contact water pond (CP1).

18.2.6.7 Incinerator

An industrial incinerator will be housed in a 130m² building located southeast of the accommodation complex. The building will be prefabricated steel frame. (The foundation for the building is a structural concrete slab on piles.

Solid waste from the camp, kitchen, shops and offices will be burned in the incinerator. The unit will be diesel-fired and its exhaust will be located down-wind of the dormitory wings. Waste feed will be transported in waste bins by forklift and loaded into the incinerator. Used oil including other flammable or combustible petroleum hydrocarbons will be the fuel used by the incinerator.

Acceptable waste for incineration will be:

- solid waste (mainly organic matter including food, food containers and wrappings contaminated by food, paper, *etc.*);
- sewage sludge (during the construction phase mainly; during mine operation, sludge may be disposed of differently).

Based on the volumes of waste predicted to be generated at the site, the incinerator will require an approximate incineration capacity of 1,500 kg per day based on a daily 10-hour burn. Approximately 350,000 litres of used oil will be burned in the incinerator per year.

Air pollution control systems will be included in the design. Efficiency will be sought at the detailed project design stage in order to minimize as much as possible the costs and environmental impacts of running such equipment.

18.2.7 Mine Maintenance Shop

An industrial mine maintenance shop with a floor area of 2,575 m² (54.9 m x 46.9 m) containing three maintenance bays, a wash bay, a machine shop and a welding shop will be required. The concrete foundation will be designed according to the type of bay (*e.g.*, for a wash bay, drains in the foundation will need to be designed for used water with a sump for the oil separator).

The maintenance shop is designed for servicing equipment from the underground operation. However, a year 3 expansion is included in the estimate to enable servicing equipment for the open pit operation. The expansion will add 1,729 m^2 and three maintenance bays to the building.

The foundation for this building is a structural concrete slab on piles.

The maintenance shop will have areas for a tool crib, large shop-tool storage, lube storage, fast-moving spares and daily consumables, a mechanical and electrical room, a lunch room along with toilets and offices for maintenance planning and shift bosses, HVAC, as well as make-up air and shop exhaust systems.

Exhaust ventilation for the workshop and light vehicle service bays will be provided by source-collection hoods to efficiently evacuate fumes.

18.2.8 Worker's Dry

The first floor (1,727 m²) of the modular workers' dry building will include offices for shift bosses and surveyors, an electrical room, a mechanical room, basket drying, laundry facilities and a nursing station. The laundry room will have washing machines, dryers, hot water tanks and storage space.

The second floor (1,379 m²) will contain dry facilities for operations, maintenance and mine staff.

The workers' dry facilities for men will include a change area with 465 full-height lockers, one for each worker on site. On the dirty side, 274 hanging baskets and 191 lockers will be provided, one for each worker. A separate section will be reserved for women.

The building will be of modular construction. The foundation will be a steel frame floor on piles.

18.2.9 Main Warehouse

The main warehouse will be housed in a two-storey building with a first floor area of 1,935 m² and 920 m² for the mezzanine (mechanical, electrical and HVAC room). The building will be a prefabricated steel frame. The entrance is a heated transition bay (double entry) with garage doors.

A separate contained area inside the warehouse will store special lubricants and greases. In addition, a designated caged area will be provided for flammable products such as solvents and paints. A separate area outside the warehouse will be available for storing large mining equipment components. Large-size process equipment spares will be stored in a dedicated laydown area on the east side of the process plant.

18.2.10 Fresh Water Pumping Station and Pipeline

Fresh water will be pumped from Meliadine Lake to the mine site. The average consumption is estimated to be 51 m³/h. The pump station will be designed with vertical well pipes that include two submersible pumps and one diesel pump.. The water will be pumped through an insulated and heat-traced HDPE pipe to a main storage tank located inside the process plant at the mine site. This tank will provide a reservoir for fire suppression water as well as fresh water storage. The fire suppression water reservoir is adequate for two hours of fire-fighting.

A pump station located adjacent to the main storage tank will house two fresh water pumps for distribution and two fire pumps.

18.2.11 Explosives plant

It is expected that 24,000 tonnes of explosives will be used during the life of the project. Considering the quantities required, bulk explosives will be manufactured on site inside an emulsion plant operated by an explosives provider. The plant will be designed at a nominal annual production capacity of 4,000,000 kg of emulsion product in order to be able to supply both the underground and open pit mining operations at peak period. For this purpose, the selected explosives supplier will provide and install the facility required to manufacture the emulsion product. The explosives plant will be built approximately 2 km northwest of the camp complex and northwest of the process plant in accordance with Canadian mining standards and regulations. A storage area will be erected nearby the plant to contain the bulk materials (ammonium nitrate and sodium nitrate) used to manufacture the explosives. Powder and detonator magazines will also be located in a separate building along the road accessing the explosive plant, as required by regulations.

The emulsion plant building will house the emulsion mixing equipment. The foundation supporting the building will be provided by Agnico Eagle and will consist of a structural concrete slab on piles.

18.2.12 Landfill

The waste management philosophy on site will be to reduce, reuse or recycle material where practical. Waste material generated during construction, operation and closure will need to be disposed of in a solid waste landfill. The landfill is required for disposal of non-salvageable, non-degradable solid waste. The landfill will not receive any waste that would attract birds or wildlife and it will be maintained in such a manner that will minimize the amount of windblown litter.

The landfill will be located within one of the waste rock storage facilities (WRSF). Design of the landfill was part of the feasibility level design made by Tetra Tech EBA (Tetra Tech EBA, 2014). The landfill will be covered with waste rock progressively over time; the final cover will consist of a 3.7mthick waste rock layer. The final cover will promote permafrost development in the waste materials, which will limit leaching from the landfill.. The surface runoff from the landfill will be managed as part of the WRSF 1 and will naturally flow into the main contact water pond (CP1 in water body H17).

18.2.13 Landfarm

Similar to the waste management philosophy, plans are being devised to actively minimize spills through suitable work procedures. Plans developed from the environmental impact study (Agnico Eagle, 2014) address the management of spills on land, ice, water and into the marine environment. When spills cannot be prevented and/or do occur, the goal will be to limit the spread of the spill, and then to deal with any contaminated material resulting from the spill.

Hydrocarbon-contaminated soils (HCS) generated during the construction, operation and closure phases will need to be adequately dealt with. One of the management options for light hydrocarbons such as diesel is to treat this material on-site in a landfarm. Materials contaminated with heavy hydrocarbons will need to be segregated, packaged and shipped south for treatment and/or disposal.

It was estimated that 350 m³ per year of HCS will need to be managed for the 12 years of construction, operation and closure of the Meliadine project. This has been accounted for in the design of the landfarm. Additionally, the Meadowbank design assumed that a yearly volume of 500 m³ of contaminated ice and snow would require management, the same yearly volume that has used in the design of the Meliadine project. Based on these assumptions, Tetra Tech EBA made a feasibility-level design for the landfarm (Tetra Tech EBA, 2014).

It is estimated that soils contaminated with light-end petroleum hydrocarbons would require three full summer seasons for complete biodegradation of the HCS. When remediated, the soils will be removed from the facility and can be used for any construction purpose such as normal overburden (*i.e.*, part of the cover of the TSF) or stacked in the WRSF. Based on a remediation period of three summer seasons, it would be possible to close the landfarm facility three years after the end of the process plant operation.

18.3 Off-site Infrastructure

18.3.1 Rankin Inlet Fuel Tank Farm

Since the Meliadine project is in a remote location, a dedicated tank farm will be required at the port of Rankin Inlet on Hudson Bay to receive the fuel from barges during the sealift season. Yearly fuel consumption over the life of the mine has been estimated, to determine the fuel tank farm capacity requirements (see Figure 18.3 and Figure 18.4).

The Rankin Inlet fuel tank farm will need a total storage capacity of 33.5 million litres (one tank of 20million litres for winter fuel, and one of 13.5 million litres for summer fuel).

These will be field-erected steel tanks built to API-650 standards, within a lined and bermed containment designed to hold 110% of the larger tank. The storage tanks will be constructed in accordance with fire regulations.

Annual fuel shipments to Rankin Inlet will come via deep-sea vessels or barges during the open water season, from approximately July to October 15 each year.

At the last fuel boat delivery, approximately mid-October, the fuel tanks at Rankin Inlet and the Meliadine mine tank should all be full. The total diesel required is calculated with the mobile equipment consumption for a year and with the power plant consumption. The design should include a fuel dispenser at the Rankin Inlet fuel tank farm for heavy and light fill with access for all types of equipment as well as a design for small power generator facilities.

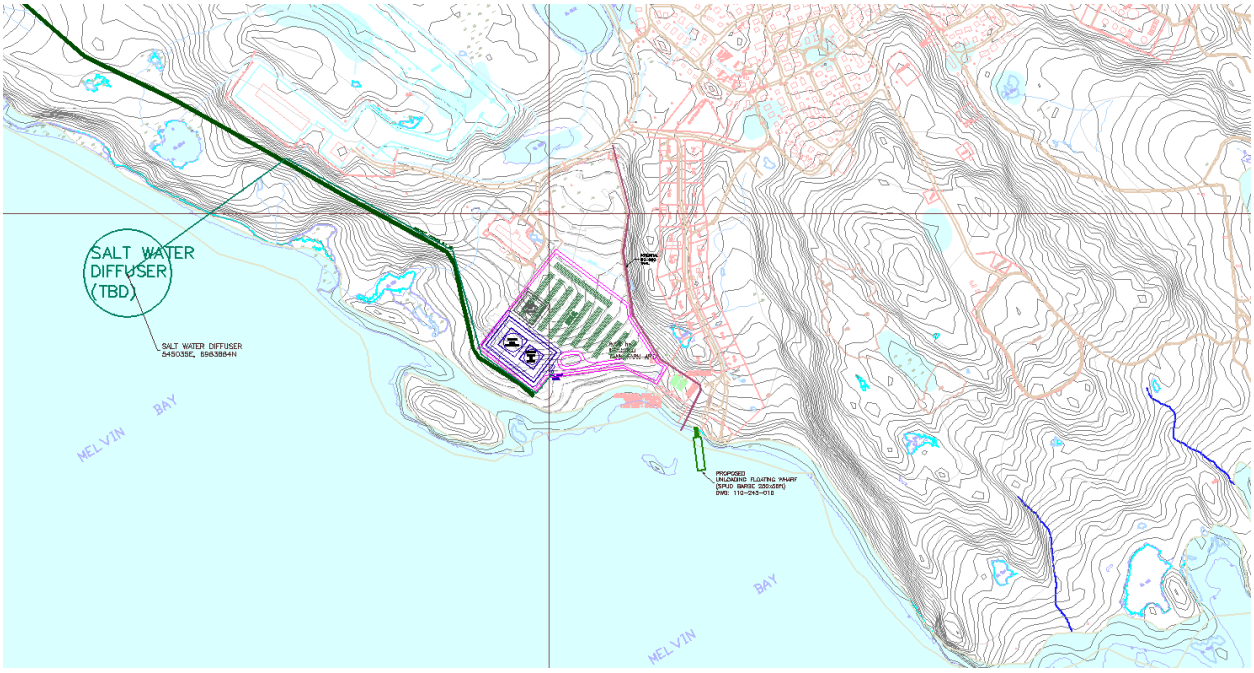


Figure 18.3 - Layout of Rankin Inlet fuel tank farm

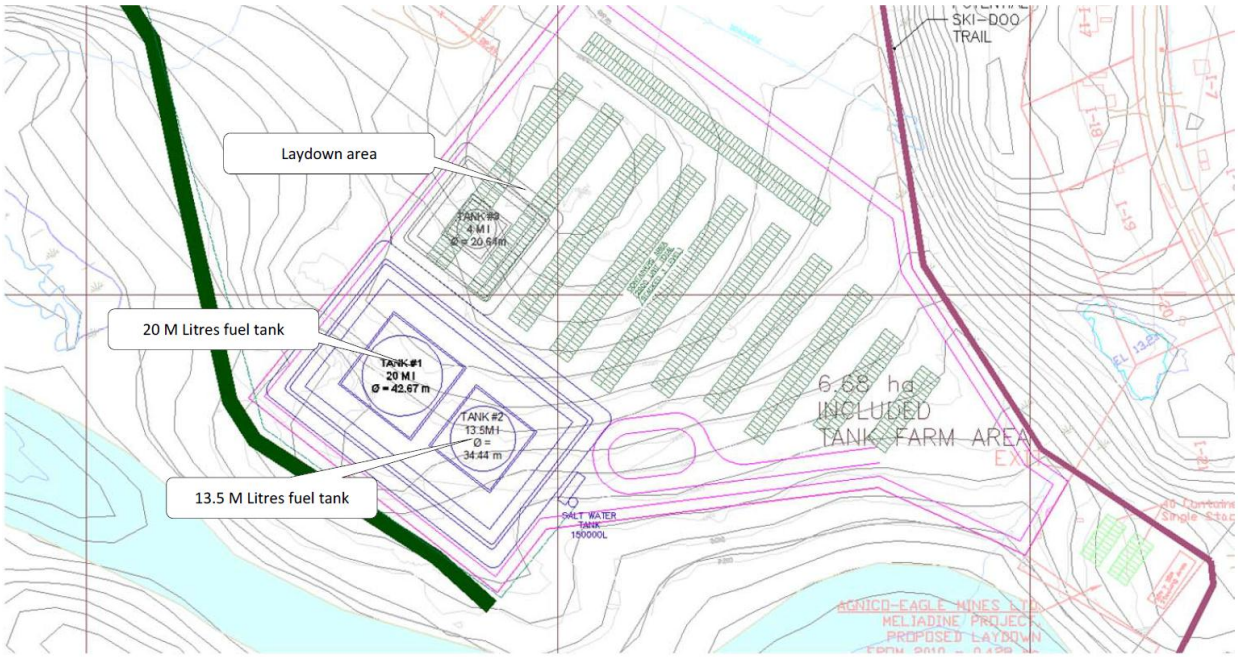


Figure 18.4 - Detailed layout of Rankin Inlet Tank Farm

Item 19. Market Studies and Contracts

19.1 Markets

The Meliadine mine and processing facilities are expected to produce high-grade gold doré bars at the mine site, which is readily marketable. The refining contract will be based on market terms and the precious metal will be sold on the spot market.

19.2 Contracts

The Meliadine project had nine major contractors for the exploration and ramp development project in 2014 and two work/supply agreements:

Diamond drilling	Orbit Garant
Airplane transportation of personnel and cargo	Nolinor – Sarliaq
Food supply	Ben Deshaie – Kisarvik
Housekeeping	Foret de Demain – Tangmaarvik
Medical and nursing	Sirius – Qikiqtaaluk
Underground ramp development	CMAC – Sarliaq
Port facility at Bécancourt, Quebec	TPQ
Sealift	NSSI
Ground support	DSI
Explosives supply	Orica – Sarliaq
Goods transportation Rankin Inlet to Meliadine Project	MTI

As with past and current contracts, Agnico Eagle negotiates within industry norms, using its past and current experience in Nunavut. The company intends to utilize its own employees and equipment for mining and processing operations at the Meliadine mining operation.

Item 20. Environmental Studies, Permitting and Social or Community Impact

20.1 Environmental studies and issues

The Meliadine gold mine project has undergone a comprehensive environmental and socio-economic impact assessment in accordance with Article 12 of the NLCA under the direction of the NIRB. This process took four years and involved regulatory agencies from the Government of Canada and Government of Nunavut, the KIA and the general public. A final Public Hearing on the project was held in Rankin Inlet in August 2014. In its hearing report the NIRB recommended to the Government of Canada that the project be allowed to proceed, concluding that the project should not cause any significant adverse environmental or socio-economic impacts and would be beneficial to the economic well-being of the region. The Government of Canada accepted this recommendation, with the NIRB issuing a Project Certificate to Agnico Eagle in February of 2015. Consequently Agnico Eagle is confident that the Meliadine project can proceed, with the belief that all environmental and social issues can be addressed.

As part of this impact assessment, extensive baseline studies were conducted in the project area covering both the physical and socio-economic environment. These studies led to the preparation of the Environmental Impact Statement that forms the basis for the NIRB impact assessment process.

20.2 Social and Community-related Agreements, Activities and Plans

Agnico Eagle recognizes and appreciates the impact its operations can have on local communities, the Kivalliq region, and Nunavut as a whole. The Company is thus committed to engaging stakeholders through public consultation during the development, construction, operation and closure of the Meliadine project. The participation of community members, including Elders and community organizations, maximizes opportunities for local knowledge to be considered and adequately incorporated into the project's design. Consultations have been recorded from 1995 to the present, and have included information sessions, consultation, informed participation, and negotiation. In its public engagement and consultation, Agnico Eagle has focused on those communities in close proximity to the project (Rankin Inlet and Chesterfield Inlet).

20.3 Tailings, Waste Rock and Water Management

20.3.1 Tailings

Following the processing of the ore, tailings will be detoxified for cyanide and dewatered by filtration to approximately 85 wt% solids in the processing plant. The dry tailings will be transported to the dry tailings storage facility (DTSF, generally called dry stack), laid down by the hauling equipment, spread with a dozer and compacted by a vibratory soil compactor.

The design selected for the DTSF uses a series of criteria derived from previous Agnico Eagle experience (*e.g.*, at the Pinos Altos operation) and from similar operations. Note that Glencore Canada's Raglan mine in northern Quebec has been operating such a facility quite successfully for more than 15 years under similar climatic conditions. Similarly, Sumitomo Metal Mining's Pogo mine in Alaska (which was visited by Agnico Eagle representatives in September 2014) successfully operates a dry stack facility with the same hauling and placing approach as the one suggested for the Meliadine project in this report.

Geochemical characterization programs for Meliadine were carried out from 1998 to 2011 (Agnico Eagle, 2014). The methods used for testing the acid rock drainage and metal leaching potential included mineralogical and chemical composition testing, acid-base accounting (ABA), net acid generation (NAG) tests, shake flask extraction (SFE) testing, humidity cell tests (HCTs), large column tests, and field cell tests. The key findings from the tests for tailings are summarized as follows:

- The test results from ABA and NAG indicated that overall the Meliadine tailings have no potential for acid-rock drainage (ARD); *i.e.*, they are non-potentially acid generating (NPAG), according to Indian and Northern Affairs Canada guidance (INAC, 1992). (The tailings from the Discovery deposit have low acid generating potential (i.e., low sulphide mineral content) but also have low natural buffering capacity resulting in an uncertain acid generating potential, however the tonnage of Discovery tailings represent only a small proportion of the overall project tonnage of tailings and when correctly blended the overall or combined tailings are clearly non-acid generating).
- Metal leaching (including Arsenic) from tailings is expected to remain low based on their NPAG classification and based on laboratory testing.
- The DTSF will contain some pore water that will require some form of control/treatment of pH, arsenic, cyanide and suspended solids levels to meet Metal Mine Effluent Regulation (MMER) criteria prior to discharge to the receiving environment.

From the available test results, tailings acid generation and long-term metal leaching are not expected to occur (Agnico Eagle, 2014). However, test results show that tailings pore water (which is essentially process water) could contain residual arsenic and cyanide. Therefore, seepage water from the TSF could contain some residual contamination that will be progressively washed out or will remain trapped in the tailings as pore water. During operations, seepage water will be collected and pumped into the water management system. Over the long-term, establishing an effective final cover system for the DTSF at closure should promote conditions that limit contaminated seepage. With a proper cover system and appropriate placement and construction methods, long-term seepage from the DTSF would essentially consist of surface runoff water.

Based on the LOM, it is estimated that approximately 12 million t of dry tailings will be generated. Of this amount, 2.5 million t will be used as underground backfill in the primary stopes and longitudinal stopes, and the remaining 9.5 million tonnes will require storage in the DTSF. With an estimated in-place density of 1.65 t/m³, the total volume required for the DTSF is approximately 6.0 million m³.

Some key considerations of the design basis of the DTSF are:

- Minimize the overall footprint, while the short-term and long-term stability is maintained.
- Avoid or minimize impacts to fish-bearing lakes.
- Limit tailings surface dust generation, control tailings surface erosion, and reduce the closure cost.
- Minimize the pre-production construction, consider the mine waste production schedule and local construction material availability, and when feasible, facilitate early progressive closure of the TSF during mine operation when tailings cover materials are readily available.
- Make positive use of the local climate conditions (cold and long winter) and recognize the potentially localized ice-rich soils conditions within the area.
- Promote the tailings freezing, the freeze back of the underlying foundation, and permafrost development in the DTSF.
- When feasible, divert the clean natural runoff water to avoid contact with the tailings by avoiding flowing through the DTSF area.
- Collect and manage the contact water from the DTSF area during mine operation to avoid potentially negative impacts on outside environment.
- Establish a proper tailings closure cover system to limit potential long-term seepage through the tailings.

Modelling performed by Tetra Tech EBA (2014) shows long-term mechanical and thermal stability for the designed facility. The proposed TSF lies west of the plant, as shown in Figure 20.1.

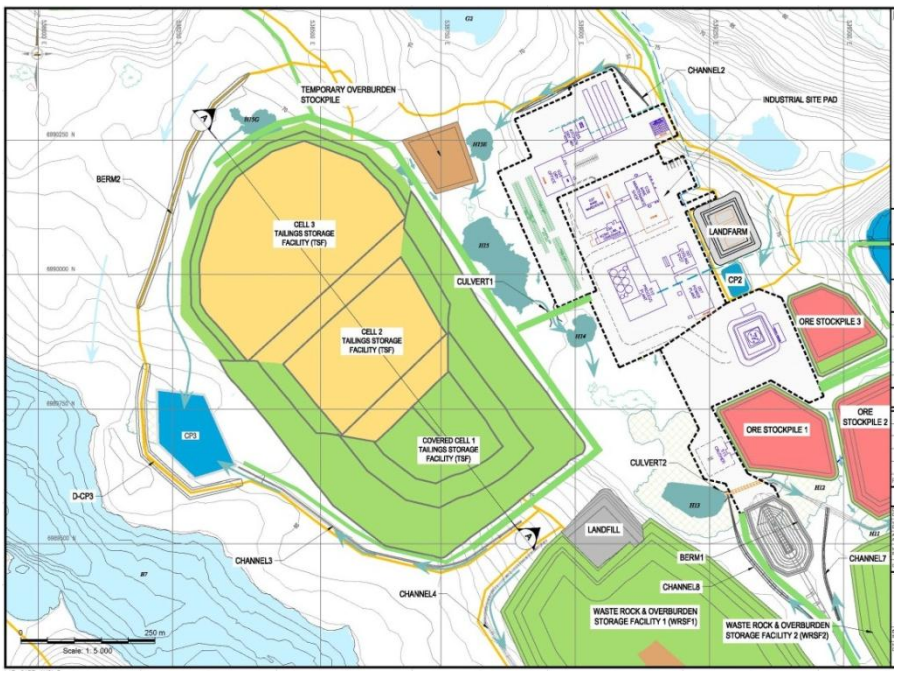


Figure 20.1 - Location of the tailings storage facility (TSF).

20.3.2 Waste Rock

During the Environmental Assessment process, the geochemical behavior of the waste rock was analyzed in detail (Agnico Eagle, 2014) by a series of static and kinetic tests. The potential to generate acid rock drainage (ARD) and metal leaching was assessed using numerous samples of various lithologies. ARD potential was assessed in accordance with Guidelines for Acid Rock Drainage Prediction in the North (INAC, 1992). All leach-test water-quality results were checked against Metal Mining Effluent Regulations (DFO, 2006) for effluent quality compliance.

From the results of the different analyses, the consultant concluded that waste rock will be non-potentially acid generating (NPAG). The waste rock contains elevated carbonate-mineral buffering capacity and generally low sulphide content.

Kinetic tests done on the different waste rock types and at various scales show that for the vast majority of rock types, seepage is also expected to meet MMER monthly mean effluent limits.

These results indicate that waste rock storage facilities will not require any special measures to prevent oxidation and metal leaching (Agnico Eagle, 2014).

Overburden from within the pit outlines has also been found to be NPAG. Metal release under laboratory conditions has been found to be low despite the relatively high total arsenic content. Leachate concentrations in the overburden are generally lower than in the waste rock, and all meet MMER monthly mean limits.

Waste rock and overburden have compatible geochemical characteristics, so they can be managed together in the same facilities (Agnico Eagle 2014). However, contact water from the waste rock and overburden storage facilities will need to be collected and managed appropriately prior to its discharge to the environment mainly because of issues with suspended solids (Agnico Eagle 2014).

Three Waste Rock Storage Facilities (WRSF) located in the vicinity of the open pits are planned to be used. The WRSF 1 and 2 located respectively south and southeast of the process plant (Figure 20.2) will respectively contain 16.7 million tonnes and 6.8 million tonnes of waste and overburden, while the WRSF 3 located on the footprint of the Lake H19 will contain 9.4 million tonnes of waste and overburden. The waste rock is planned to be used for pads and road construction, underground backfill and as cover for closure of the DTSF. Approximately 95,000 t of overburden will also be kept in an isolated pile located next to the DTSF for the progressive closure of this facility.

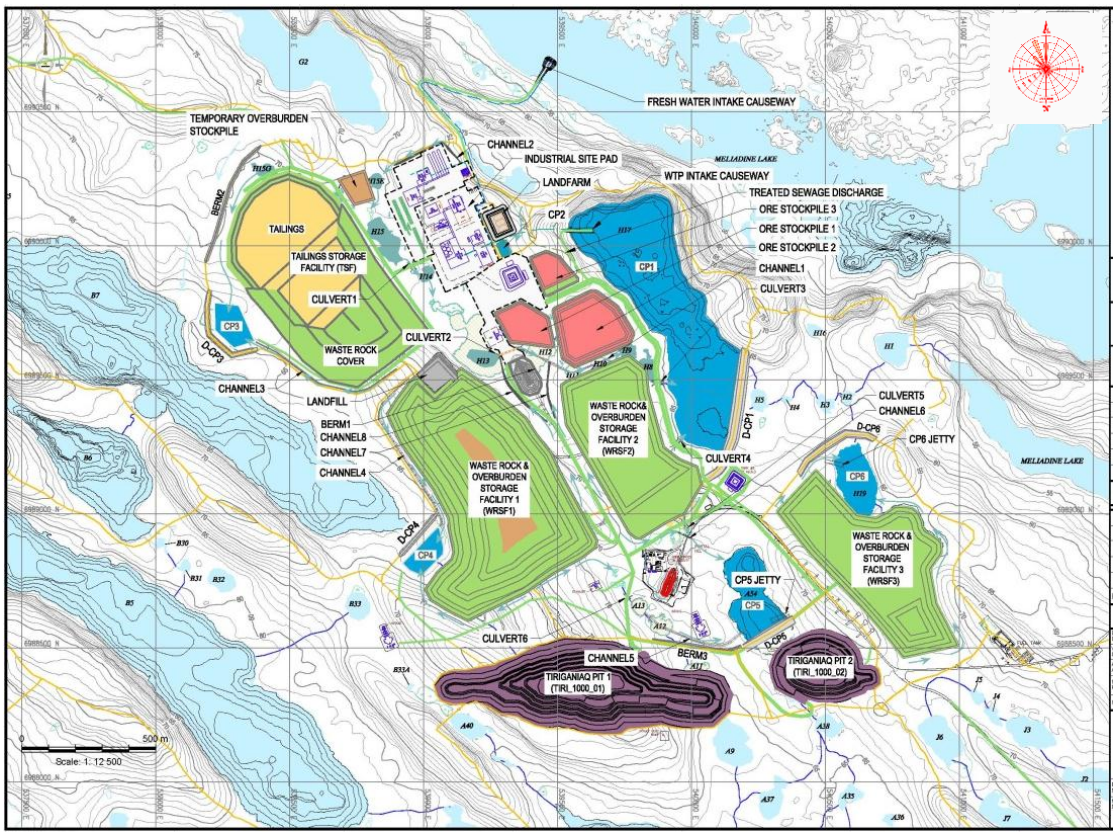


Figure 20.2 - Location of waste rock and overburden storage facilities (green) and contact water ponds (blue) at the Meliadine Project

The design basis for the WRSF is based on Agnico Eagle's experience as well as on recommendations from the designer (Tetra Tech EBA, 2014). Some of the key considerations are:

- Minimize the overall footprint of the WRSF while maintaining the short-term and long-term stability of the facilities;
- Avoid or minimize impact on the fish-bearing lakes;
- Minimize the haulage distance from the open pits to the WRSF;
- Make positive use of the local climate conditions (cold and long winter) and recognize the potentially localized ice-rich soils conditions within the WRSF;
- Promote the mine waste freezing, the freeze back of the underlying foundation, and permafrost development in the WRSF;
- When feasible, divert the clean natural runoff water to avoid contact with the mine waste by avoiding flowing through the WRSF;
- Facilitate the collection and management of the contact water from the WRSF during mine operation to avoid potentially negative impacts on the outside environment;
- Maintain a minimum distance of 100 m between the toe of the waste rock storage facilities and the open pits;
- Maintain a minimum distance of 20 m between the toe of the waste rock storage facilities and roads;

- Maintain a minimum distance of 100 m between the toe of the waste rock storage facilities and any protected lakes.

The maximum height for the WRSF 1, 2 and 3 is respectively 42 m (115 m elevation above sea level), 35 m (102 m elevation above sea level) and 37 m (100 m elevation above sea level). Construction of the benches in the WRSF will use a slope of 1.3 horizontal : 1 vertical for the waste rock, and 1.6 horizontal : 1 vertical for the overburden. The overall slope of the facilities is set at 3 horizontal : 1 vertical, an angle with a safety factor that takes into account the presence of overburden in the WRSF. Modelling performed by Tetra Tech EBA (2014) shows long-term slope stability for the designed facilities.

20.3.3 Water management

The sequence of activities and the detailed plan for water management is described in Tetra Tech EBA (2014). In developing the water management plan at Meliadine, the following principles were followed:

- Keep the different water types (contact, process, groundwater (saline) and non-contact) separated;
- Minimize fresh water consumption;
- Reduce water discharge to the environment.

It is believed that keeping types of water segregated allows for water quality control in the different areas of the site and reduces costs.

The water management plan is based on the following general assumptions:

- Contact water will be collected and will not be directly discharged into the environment until the water quality meets discharge criteria;
- All contact water collection ponds are expected to be completely empty by the end of the fall (October) each year, so they will have enough capacity to store at least three days of the water received during the spring freshet;
- All intermediate contact water ponds are kept empty most of the time to leave enough capacity to store the water from an extreme rainfall event;
- Make-up water for ore processing will be sourced from the treated water from the water treatment plant when available, and then from the fresh water pumped from Meliadine Lake;
- Where feasible, surface water diversion structures will be constructed to divert the natural runoff water to avoid mixing with the contact water, thus reducing impacts on the natural environment and limiting the need for on-site water management;
- All water management infrastructure should be designed with sufficient capacities to withstand design inflow floods;
- Most of the water in the underground mine will be re-used for drilling after the suspended solids have been removed using an underground total suspended solids (TSS) removal plant;
- Initially all underground mine workings will be within the zone of continuous permafrost and thus it is expected that most mine water generated will come from drill water and other water used in the actual mining cycle and not from groundwater. During this phase

it is expected that most underground mine water will be recycled following removal of suspended solids. However at some point in the mine life, underground mining will start to enter the zone below the permafrost (expected to start in Year -3 of Mine development). Indications from prior hydrogeological investigations suggest that some highly saline groundwater (historically old sea water that has been trapped under the permafrost zone) will be encountered. At this point underground mine water will start to become more saline and over time special management measures will likely be required. The amount of saline groundwater encountered is likely to increase as more mine workings are opened in the zone below the permafrost (it should be noted that this saline groundwater is historically trapped sea water and does not represent any active connection with the ocean which located approximately 20 km away). Initially this saline groundwater will be managed through internal recycle in the mine with allowance for removal of suspended solids. Additional hydrogeological studies are planned in the coming years to help improve our knowledge of how much saline groundwater can be expected (i.e. what volume will need to be managed). These studies are difficult to do effectively from surface and so they are scheduled to be completed from the underground development work that is currently underway. This information will be collected during the first years of mine development and will enable us to better predict what volume of saline groundwater will likely be encountered as mining increases beneath the zone of permafrost and at what rate the saline groundwater will enter the open mine workings. There are several options available for dealing with this saline groundwater, specifically:

- Segregating saline water from all other waters and recycling this water preferentially for ongoing underground mining purposes. Treatment for removal of suspended solids would be required;
- Segregating saline water from all other waters, storing this water and then blending this water on a controlled basis with other contact water to meet final discharge criteria. Treatment for removal of suspended solids and metals would likely be required;
- Segregating saline water from all other waters, storing this water and treating this water using reverse osmosis to create a “clean” water for use elsewhere in the mining/milling process and a brine that would be re-used within the mine;
- Segregating saline water from all other sources, storing this water and then trucking it to the ocean for discharge on a controlled basis into the ocean through an engineered diffuser to ensure proper mixing; and
- A combination of one or more of the above.

The management option selected will be determined during the first few years of mine development/operation once the additional hydrogeological studies have been completed. The selected management option would likely require further environmental assessment and permitting before it could be implemented. In the interim any saline groundwater encountered would be managed on site.

Contact water includes the water (mostly runoff) in contact with the piled material (ore, waste, overburden, tailings) on pads but also the dewatering water from the open pits. It also includes all the water caught by channels or diverted by berms into a collection pond. The contact water accumulates in different facilities and is treated before reuse or discharge into Meliadine Lake.

Groundwater inflow rates used for this analysis are based on data provided by Golder (Golder Associates, 2013). Based on the current mine plan, the underground mine is believed to reach the base of the permafrost at the beginning of Year - 3 when saline groundwater seepage is expected to start. The current plan is to treat the saline groundwater underground for TSS removal, recycle underground to the maximum extent possible and then ultimately manage in accordance to one of the options described above.

Most of the water coming from the TSF will be runoff from precipitation (rain and snow). Given the nature of this tailings placement technology (fairly dry and compacted tailings stacked and undergoing progressive freezing), limited contaminated seepage is anticipated. This water will be collected in ditches surrounding the TSF and stored in a collecting pond before being pumped during the warmer weather to the main contact water pond.

The process water that will be used in the process plant will be managed in a closed loop circuit since filtered tailings are selected as the tailings management strategy. The TSF will therefore not be used for recirculation of the water. Thus, process water will be recirculated in the process plant only.

Fresh water will be supplied from Meliadine Lake. Water from Meliadine Lake is used mainly at the process plant for the mixing of reagents and cooling units but it will also be required for potable water, truck shop, open pit drilling, emulsion plant and laboratory usages. When possible, contact water will replace the use of fresh water in order to minimize fresh water consumption. Truck shop consumption has been optimized through a closed loop including treatment within the shop allowing maximum recirculation of water.

The water balance has been prepared by the consultant Tetra Tech EBA (Tetra Tech EBA, 2014). The water balance uses the general assumptions presented above and has been used to design the water management infrastructure as well as to size the water pipelines.

Based on the water balance, Golder Associates (2014) developed a water quality model for the project. The model integrates the geochemistry results (ARD and leaching results on ore, waste and tailings) and the water quality results from the different sources (runoff, pumped water from the different contact water ponds, seepage from the waste rock and the other piles, treated sewage water, dewatering water from the open pits, *etc*.). The model indicates the treatment of the effluent during the period of the mine operation, but also estimates the length of monitoring time during the post-operation period.

During operations, the modelled results show no exceedances of the monthly mean concentrations allowed by MMER in the main contact water pond. However, from Year 4 of operation onward, the arsenic concentration in this pond approaches the MMER limit. For this reason, in addition to the treatment of the total suspended solids planned in the capital cost budget, the capacity to treat metals such as arsenic has been added to the sustaining budget (capital and operating costs).

Prior to discharge into Meliadine Lake, any contact water will flow through the water treatment plant (WTP) and be treated (if required) to remove excessive suspended solids and to precipitate metals. The WTP will only operate during summer months (June to September). For the rest of the year, there will be no discharge of treated effluent into Meliadine Lake. When in operation, the treatment process underflow will be pumped to the process plant clarifier for re-use in the

processing plant. Treated contact water will be discharged via pipeline equipped with a diffuser to a selected point located in Meliadine Lake (Figure 20.3). Discharge will have to meet MMER discharge criteria or Type A water license discharge criteria, whichever are more stringent.

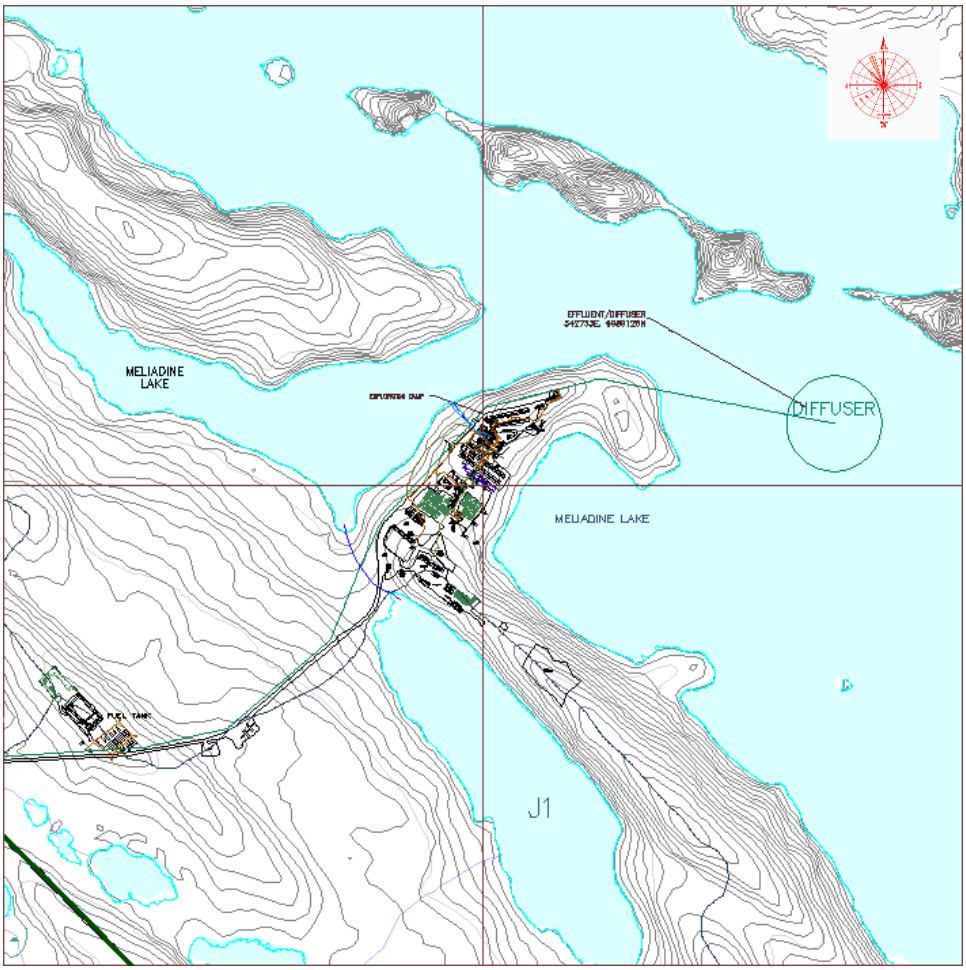


Figure 20.3 - Location of the treated water discharge and diffuser in the Meliadine Lake

Some of the key design elements for water management infrastructure and retention facilities including contact water ponds are:

- Comply with the Canadian Dam Safety Guidelines;
- Minimize seepage through dykes/berms while optimizing the construction efficiency;
- Maximize the use of mine waste materials produced during pit development;
- Minimize overall environmental footprint and effects;
- Facilitate an effective mine closure plan;
- Optimize the dyke/berm construction sequences to reduce initial construction requirements during the pre-production stage and intensify construction during mine operation;
- Establish adequate setback from the open pit limits to allow for mining safety and to minimize seepage into the open pits;
- Incorporate mine site roads (including haul roads) into the dykes wherever practical.

The main infrastructure for the water management is the contact water pond CP1 (approximately 300,000 m³ capacity) where a dyke is built early in the project to manage the contact water (Figure 20.2). The other water management infrastructure includes a number of smaller ponds, channels, berms and pumping stations (permanent or temporary) including pipelines to dewater the temporary storage facilities.

Tetra Tech EBA (2014) provided the design of the planned water management infrastructure over the LOM as well as the quantities and the technical specifications for the required construction materials. Agnico Eagle costed the designed infrastructure based on internal estimations for the preparation of the granular material and on bids provided by Nuna Logistics Limited and Inukshuk Construction Limited for the construction of the infrastructure, and a bid provided by Innovex for the geomembranes and geotextiles.

20.4 Permits

Land and environmental management in the region of the Meliadine project is governed by the provisions of the Nunavut Land Claim Agreement (the "NLCA"). The Meliadine project is located on Inuit owned land, where Inuit own both the subsurface mineral rights (managed by NTI) and the surface land rights (managed by the KIA on behalf of Inuit beneficiaries under the provisions of the NCLA). Consequently, to explore and develop the project, the Company must obtain land use leases from the KIA. The Company has been granted a commercial lease by KIA for exploration and underground development activity, a prospecting and land use lease for exploration and development activities, an exploration land use lease for exploration and drilling on the Inuit owned lands of Meliadine East, and a parcel drilling permit for drilling activity on Inuit owned lands. A number of right-of-way leases covering road access to the Meliadine project property and esker quarrying on the Inuit owned lands were also granted by the KIA.

Pursuant to the NLCA and the Nunavut Waters and Nunavut Surface Rights Tribunal Act requirements, the Company obtained several water use licences from the Nunavut Water Board (NWB), covering ongoing water use for its Meliadine project exploration camp, the underground bulk sampling program and for ongoing exploration drilling activities.

The primary project approval requirements are summarized in Table 20.1. A detailed list of all applicable statutes, regulations, codes and standards to which the project may be subject is given in Table 20.2.

Table 20.1 - Primary project approval requirements for Meliadine mine project

Permit/Approval Legislation	Administering Agency	Project Activity
Project Certificate NLCA (Article 12)	NIRB	Project approval
Inuit Impact and Benefit Agreement NLCA (Article 26)	KIA	Project commencement
Mineral Production Lease	NTI	Required for mineral production
Inuit Water Rights Compensation Agreement NLCA (Article 20)	KIA	May be required
Water Licence Nunavut Waters and Nunavut Surface Rights Tribunal Act	NWB	Required for water use and waste disposal
Class 1/Class 2 Archaeology Permit Nunavut Archaeological and Paleontological Sites Regulations	Government of Nunavut – Department of Culture, Language, Elders and Youth (CLEY)	Required to conduct archaeology research and to mitigate archaeological sites to allow development to occur
IOL – Commercial Land Use Lease or Right of Way NLCA	KIA	Long term land tenure required for land use on Inuit owned land; land required for infrastructure, roads and activities associated with construction, operations, and closure phases
IOL – Quarry Lease/Permit NLCA	KIA	Required for quarrying of material on Inuit owned land during construction, operation and closure
Crown Land – Lease/Land Use Permit Territorial Lands Act Territorial Land Use Regulations	AANDC	Required for quarrying of material on Crown Land during construction, operation and closure
Approval and/or Exemption Navigable Waters Protection Act (section 5)	Transport Canada (TC)	Construction of works in navigable waters
Fisheries Authorization for Harmful Alteration Disruption or Destruction (HADD) of Fish or Fish Habitat Fisheries Act (section 35)	Fisheries and Oceans Canada (DFO)	Required if HADD cannot be avoided; if HADD can be avoided, DFO may provide a letter of advice outlining best management practices
License for a Factory and Magazine Explosives Act and Regulations	Natural Resources Canada (NRCan)	Required for construction of explosives factories and magazine(s) and storage of explosives
Permit to Store Detonators Explosives Use Act Mine Health and Safety Act and Regulations	Nunavut Mine Health and Safety Nunavut Workers Compensation Board	Required to store detonators in a magazine
Explosive Use Permit Explosives Use Act Mine Health and Safety Act and Regulations	Nunavut Mine Health and Safety Nunavut Workers Compensation Board	A permit is required to use explosives unless used in accordance with the regulations
Spill Contingency Plan Approval Environmental Protection Act Spill Contingency Planning and Reporting Regulations	Nunavut Department of Environment (DoE)	A Spill Contingency Plan must be filed with the Chief Environmental Protection Officer to store fuel in an above-ground facility with a 20,000-litre capacity or greater
Assorted Scientific Research Permits Scientist Act Wildlife Act	Nunavut Research Institute	Required to conduct some of the environmental monitoring activities

Table 20.2 - Primary applicable acts, regulations and guidelines to the Meliadine project

Acts	Regulations	Guidelines
Federal		
Canadian Environmental Protection Act (1999 c.33)	Storage Tank Systems for Petroleum Products and Allied Petroleum Products Regulations (SOR/2008-197) Environmental Emergency Regulations (SOR/2003-307) Interprovincial Movement of Hazardous Waste and Hazardous Recyclable Material Regulations (SOR/2002-301)	Canadian Council of the Ministers of Environment - Environmental Code of Practice for Above-ground and Underground Storage Tank Systems Containing Petroleum and Allied Petroleum Products Notice with respect to substances in the National Pollutant Release Inventory Canada-Wide Standards for Particulate Matter (PM) and Ozone Canada-Wide Standards for Petroleum Hydrocarbons (PHC) In Soil
Canada Wildlife Act (1985 w9)		
Species at Risk Act (2002 c.29)		
Migratory Birds Convention Act (1994 c.22)	Migratory Birds Regulations (C.R.C., c. 1035)	
Canada Water Act (1985 c.11)		
Arctic Waters Pollution Prevention Act (R.S.C., 1985, c. A-12)		
Canada Shipping Act, 2001 (S.C. 2001, c. 26)	Response Organizations and Oil Handling Facilities Regulations (SOR/95-405)	
Marine Liability Act (S.C. 2001., c. 6)	Marine Liability Regulations (SOR/2002-307)	
Navigable Waters Protection Act (R.S. 1985 c. N-22)	Navigable Waters Works Regulations (C.R.C., c. 1232) Navigable Waters Bridges Regulations (C.R.C., c. 1231)	Sections 22 (throwing or depositing stone, etc.) and 23 (proclamation of exemption) prescriptions to be followed as necessary
Fisheries Act (R.S.C. c. F-14)	Metal Mining Effluent Regulations (SOR/ 2002-2222)	The Policy for the Management of Fish Habitat Guidelines for the Use of Explosives In or Near Canadian Fisheries Waters Freshwater Intake End-of-Pipe Fish Screen Guideline Standard Operating Procedure – Clear Span Bridges
Transport of Dangerous Goods Act (1992, c.34)	Transportation of Dangerous Goods Regulations (SOR/2001-286)	
Explosives Act (1985 c.E-17)	Explosives Regulations (C.R.C., c. 599) Ammonium Nitrate and Fuel Oil Order (C.R.C., c. 598)	
National Fire Code of Canada (2010)		
Nuclear Safety and Control Act (s.c. 1997, c.9)	General Nuclear Safety and Control Regulations (SOR/2000-202)	
Canadian Human Rights Act (R.S.C., 1985, c. H-6)		
Canada Labour Code (R.S.C., 1985, c. L-2)	Canada Labour Standards Regulations (C.R.C., c. 986) Canada Occupational Health and Safety Regulations (SOR/86 304)	
Territorial Lands Act (R.S. 1985, c. T-7)	Northwest Territories and Nunavut Mining Regulations (C.R.C., c. 1516) Territorial Land Use Regulations (C.R.C. 1524) Territorial Quarrying Regulations (C.R.C. c. 1527)	
Nunavut Waters and Nunavut Surface Rights Tribunal Act (2002, c. 10)	Northwest Territories Waters Regulations (SOR/93/303)	
Nunavut Act (1993 c.28)	Nunavut Archaeological and Paleontological Sites Regulations (SOR/2001-220)	
Nunavut Land Claims Agreement Act (1993, c. 29)		

Territorial – Nunavut

Environmental Protection Act (~~RSNWT~~ (Nu) 1988, c E-7)	Spill Contingency Planning and Reporting Regulations (NWT Reg (Nu) 068-93) Used Oil and Waste Fuel Management Regulations (NWT Reg 064-2003) [The removal of hazardous materials will require the registration with the Government of Nunavut, Department of Environment as a waste generator as well as carrier (if applicable) prior to transport.]	Guideline on Dust Suppression Guideline for the General Management of Hazardous Waste in Nunavut Guideline for Industrial Waste Discharges in Nunavut Guideline for Air Quality – Sulphur Dioxide and Suspended Particulates Guideline for the Management of Waste Antifreeze Guideline for the Management of Waste Batteries Guideline for the Management of Waste Paint Guideline for the Management of Waste Solvents Guideline for Industrial Projects on Commissioner's Land
Scientists Act (RSNWT (Nu) 1988, c S-4)	Scientists Act Administration Regulations (NWT Reg (Nu) 174-96)	
Historical Resources Act (RSNWT (Nu) 1988, c H-3)		
Territorial Parks Act (RSNWT (Nu) 1988, c T-4)	Territorial Parks Regulations (RRNWT (Nu) 1990 c T-13)	
Wildlife Act (RSNWT (Nu) 1988, c W-4)	Wildlife General Regulations (NWT Reg (Nu) 026-92) Wildlife Licences and Permits Regulations (NWT Reg (Nu) 027-92) Wildlife Management Barren-Ground Caribou Areas Regulations (NWT Reg (Nu) 099-98) Wildlife Management Grizzly Bear Areas Regulations (NWT Reg (Nu) 155-96) Wildlife Management Zones Regulations (RRNWT (Nu) 1990 c W-17) Wildlife Regions Regulations (NWT Reg (Nu) 108-98)	
Commissioner's Land Act (RSNWT 1988, c C-11)	Commissioner's Airport Lands Regulations (NWT Reg (Nu) 067-97) Commissioner's Land Regulations (RRNWT 1990, c C-13)	
Safety Act (RSNWT 1988, c.S-1)	General Safety Regulations (RRNWT (Nu) 1990 c S-1) Work Site Hazardous Materials Information System Regulations (RSNWT 1988, C 81 (Supp))	
Mine Health and Safety Act (SNWT (Nu) 1994, c 25)	Mine Health and Safety Regulations (NWT Reg (Nu) 125-95)	
Workers' Compensation Act (RSNWT, 1988, c. W-6)	Workers' Compensation General Regulations (Nu Reg 017-2010)	
Apprenticeship, Trade and Occupations Certification Act (RSNWT (Nu) 1988, c A-4)	Apprenticeship, Trade and Occupations Certification Regulations (RRNWT (Nu) 1990 c A-8)	
Labour Standards Act (RSNWT (Nu) 1988, c L-1)	Annual Vacations Regulations (RRNWT 1990, c.L-1) Educational Work Experience Regulations (RRNWT 1990, c.L-2) Employment of Young Persons Regulations (RRNWT 1990, c.L-3) Labour Standards Meal Regulations (RRNWT 1990, c.L-4) Notice of Termination Exemption Regulations (RRNWT 1990 c.L-5) Pregnancy and Parental Leave Regulations (RRNWT 1990, c.8(Supp.)) Reciprocating Jurisdiction Order (RRNWT 1990, c.L-6) Wages Regulations (RRNWT 1990, c.L-7)	
Electrical Protection Act (RSNWT (Nu) 1988, c E-3)	Electrical Protection Regulations (RRNWT 1990 c. E-21)	
Explosives Use Act (RSNWT (Nu) 1988, c E-10)	Explosives Regulations (RRNWT (Nu) 1990 c E-27)	
Petroleum Products Tax Act (RSNWT (Nu) 1988, c P-5)	Petroleum Products Tax Regulations (RRNWT (Nu) 1990 c P-3)	

Fire Prevention Act (RSNWT (Nu) 1988, c F-6)	Fire Prevention Regulations (RRNWT (Nu) 1990 c F-12)	
Hospital Insurance and Health and Social Services Administration Act (RSNWT 1988, c T-3)	Territorial Hospital Insurance Services Regulations (RRNWT (Nu) 1990 c T-12)	
Public Health Act (RSNWT (Nu) 1988, c P-12)	Camp Sanitation Regulations (RRNWT (Nu) 1990 c P-12) General Sanitation Regulations (RRNWT (Nu) 1990 c P-16)	
All-terrain Vehicles Act (RSNWT (Nu) 1988, c A-3)	All-terrain Vehicles Regulations (RRNWT (Nu) 1990 c A-1)	
Motor Vehicles Act (RSNWT (Nu) 1988, c M-16)	Large Vehicle Control Regulations (RRNWT (Nu) 1990 c M-30) Motor Vehicle Registration and Licence Plate Regulations (NWT Reg (Nu) 054-94)	
Public Highways Act (RSNWT (Nu) 1988, c P-13)	Highway Designation and Classification Regulations (NWT Reg (Nu) 047-92)	
Transportation of Dangerous Goods Act (1990, RSNWT (Nu) 1988, c 81 (Supp))	Transportation of Dangerous Goods Regulations (1991, NWT Reg (Nu) 095-91)	

In addition to these construction and operating licences, permits and authorizations, the Company must negotiate an Inuit Impact and Benefit Agreement (IIBA) for the Meliadine project and an Inuit water compensation agreement in accordance with Article 20 of the NLCA. The negotiation of this IIBA started in 2011 and is expected to be complete by April of 2015. The parties have reached provisional agreement on most of the outstanding issues and are currently working on a Memorandum of Understanding ("MOU") that will solidify such agreement leading to an expected completion of the formal Agreement by mid 2015. The Agreement will include payments to be made by Agnico Eagleto the KIA during the Project life. Similarly, the Company is required to negotiate and implement a Water Rights Compensation Agreement and a production lease with the KIA, also before construction. While these agreements still need to be finalized the parties have reached provisional agreement on the financial terms to be contained within these agreements (part of the MOU mentioned above).

20.5 Mine Closure Requirements and Costs

20.5.1 General Closure Considerations

A preliminary Mine Closure and Reclamation Plan (CRP) has been prepared for the Meliadine Project as part of the environmental impact assessment process. The planaddresses permanent and progressive closure, as well as interim shutdowns (i.e., potential short to medium term suspension of operations due to economic factors or other external factors (strikes, loss of a critical part of the mine, etc.).

All closure planning and proposed activities were developed with the following objectives in mind:

- Provide long-term stable conditions (physical and chemical);
- Minimize potential contaminant levels in the environment;
- Ensure public safety after mine operations cease.

20.5.2 Specific Closure Strategies

20.5.2.1 Mined-out Pits and Underground Infrastructure

Within the CRP, conceptual closure strategies were proposed for the closure and reclamation of all mined out open pits and underground mining areas in accordance with the following:

- Seal all surface openings, especially those connecting the UG workings to the surface;
- Remove infrastructure and equipment if needed. Any equipment or infrastructure left UG will be cleaned, drained of fluids, inspected and remediated as appropriate to ensure that there is no risk of any contaminant leakage;
- Remove hazardous materials and identify and remediate contamination from UG shops, equipment and magazines (fuels, oils, glycol, batteries, explosives, etc.);
- Secure UG openings using properly designed concrete caps/plugs;
- Flood open pits;
- Contour land surfaces to establish positive natural drainage patterns and to blend in with the surrounding topography or re-contour surfaces to prevent surface water flow into the UG workings;
- Secure pit access ramps by rock berm barricades, and construct berms (2 m to 3 m high) around the perimeter of each pit at a given setback in accordance with applicable mine regulations and rock mechanics studies.

20.5.2.2 Waste Rock Storage Facility (WRSF)

The CRP included proposed closure strategies and activities for all WRSF as per the following general guidance:

As waste rock is not acid generating and the water quality from waste rock and overburden drainage is expected to meet MMER monthly mean effluent limits, a cover system is not considered necessary for the WRSF at closure. Since the WRSFs are designed for long-term stability (3 horizontal: 1 vertical slope ratio), no additional re-grading, including the construction of a wildlife ramp, is considered necessary as part of closure activities. The WRSF will be allowed to naturally re-vegetate. Dust from the facility is anticipated to be a minor issue during closure; the need for additional dust control measures will be implemented if required.

20.5.2.3 Tailings Storage Facility (TSF)

The CRP included proposed closure strategies and activities for the Meliadine TSF as per the following general guidance:

- Stabilize slopes of the dry tailings stack;
- Minimize wind migration of tailings dust using appropriate permanent cover materials such as non-acid generating waste rock;
- Minimize the threat of the TSF becoming a source of contamination;
- Blend with local topography where appropriate.

The closure concept for the TSF is to progressively cover the facility with non-acid generating and non-metal leaching rockfill (waste rock) and/or overburden. The cover consists of 3.7 m to 4.2 m of waste rock on the slopes and of 0.5 m of overburden and 2.5 m of waste rock on the top. The intent is to maintain the active layer within the cover so that the tailings will remain frozen, but more importantly the purpose of the cover is to divert the surface runoff to minimize its entry into the tailings material. This would minimize the possibility of metal leaching and the movement of residual process water that is already trapped in the tailings pore speces.

TetraTech EBA (2014a) performed long term (100 years) thermal modelling of the TSF with the specifications mentioned above for the cover, the results show temperature below 0°C for the overburden layer and, except for the deposition surface, the freezing of the tailings after one winter.

20.5.2.4 Water Management Infrastructure

The CRP included proposed closure strategies and activities for the water management infrastructure as per the following guidance:

- Dismantle and remove and/or dispose of as much of the system as possible and restore natural or establish new permanent self-sustaining drainage patterns;
- Stabilize and protect from erosion and failure for the long-term;
- Maintain controlled water release from dams, ditches, and all other points of discharge to the environment;
- Achieve approved water quality objectives while implementing long-term treatment only if necessary and ensure maintenance if required.

Mine water management infrastructure, including ditches, sumps, dykes, ponds and water treatment plant will be maintained until water quality monitoring demonstrates that the water reporting from the reclaimed areas is of acceptable quality for release to the environment without further management. Dykes will then be breached, and ditches and ponds will be scarified to promote re-vegetation and natural drainage. This work will be done so as to minimize wind-blown dust and erosion from surface runoff and to enhance natural re-vegetation and wildlife habitat. Select non-contact water diversion ditches may be retained to promote surface water drainage.

The need for a water treatment plant will be determined based on mine closure water quality monitoring at key locations around the site. If the water treatment plant is no longer required, it will be maintained for three water treatment seasons as a contingency before being dismantled.

20.5.2.5 On Site Infrastructure

The CRP includes proposed closure strategies and activities for the mine infrastructure as per the following:

Salvageable buildings and surface structures will be dismantled and removed from the site. The buildings could be offered to the Kivalliq Inuit Association (the land owner) for potential re-use elsewhere after closure, or sold;

Non-salvageable buildings and structures will be dismantled or demolished and disposed of in the on-site landfill or in areas of the mine waste management facility designated for inert non-hazardous landfill materials;

Concrete structures and foundations will be removed or buried to a depth of about 1 m below the final ground surface or the final re-graded surface;

The mine-site area will be re-graded to conform to the surrounding topography and to encourage re-growth of natural vegetation. In areas where the original ground surface was lowered for site grading or structural requirements, the slopes will be stabilized and contoured. Cover materials may be required for erosion and dust control;

The biopile area (an area for the onsite treatment of soils contaminated by light hydrocarbons such as diesel fuel spills) will be excavated and the material appropriately disposed of. The area would then be re-graded to ensure positive surface drainage;

The mine site fuel storage tank farm will be dismantled and, if necessary, the residue disposed of offsite at an approved disposal facility;

Unused hazardous materials and explosives will be removed from site;

Original drainage patterns will be restored to the greatest extent possible.

20.5.2.6 Off-Site Infrastructure

The All-weather Access Road (AWAR) will be maintained and remain open during closure until water quality meets discharge criteria and dykes are breached. It should be noted that the future of the AWAR may be revisited following discussions with the local community that may decide to keep it. For planning purposes, it is assumed at this stage that the road will be dismantled after closure objectives are met.

Proposed closure strategies and activities will include the following:

The AWAR, all site roads and the bypass road not required for post-closure monitoring will be decommissioned and the terrain restored;

The road surface will be scarified, promoting natural re-vegetation;

Slopes will be stabilized against potential erosion;

All bridges and culverts will be removed, original drainage patterns restored and stream crossings rehabilitated;

Disturbance of near-shore vegetation will be minimized during removal of culverts and bridges;

Cross-drain structures (cross-ditches) will be installed where necessary between culvert sites. Where armouring rock (rip-rap) is required, this rock will be non-acid generating and non-metal leaching for the protection of aquatic life. Where affected watercourses are fish-bearing, the timing of work will have to be restricted to within the designated DFO fisheries work window;

The spud barge (the portable dock facility to be used by Agnico Eagleduring the mine life) will be removed, and the Rankin Inlet laydown area will be reclaimed, the Rankin Inlet fuel tank farm dismantled and, if necessary, disposed of off-site at an approved disposal facility.

20.5.3 Closure and Reclamation Cost Estimate

The closure and reclamation cost for the Meliadine Project is estimated at 46.9M$. The breakdown of this estimate is provided in Table 20.3.

Table 20.3 - Summary of closure and reclamation costs

Capital costs	Component name	Cost (millions)	Land liability	Water liability (million)
Open pit	Tiriganiaq Pit 1	$2.78	$0	$2.782
	Tiriganiaq Pit 2	$0.05	$0	$0.05
Underground mine	Tiriganiaq	$0.97	$0	$0.97
Tailings facility	Tailings Storage Facility	$1.49	$0	$1.49
Rock pile	Waste Rock Facility East	$0	$0	$0
	Waste Rock Facility West	$0	$0	$0
	Waste Rock Facility H19-H20	$0	$0	$0
Buildings and equipment		$18.92	$0	$18.92
Chemicals and contaminated soil management		$1.92	$0	$1.92
Surface and groundwater management		$0.13	-	$0.13
Interim care and maintenance		$0	-	$0
Subtotal: capital costs		**$26.26**	**$0**	**$26.26**
Percent of subtotal			**0%**	**100%**

Indirect costs		COST	Land liability	Water liability
Mobilization/demobilization		$9.69	$0	$9.69
Post-closure monitoring and maintenance		$2.56	$0	$2.56
Engineering	5%	$1.31	$0	$1.31
Project management	5%	$1.31	$0	$1.31
Health and safety plans/monitoring & QA/QC	1%	$0.26	$0	$0.26
Bonding/insurance	1%	$0.26	$0	$0.26
Contingency	20%	$5.25	$0	$5.25
Market price factor adjustment	0%	$0	$0	$0
Subtotal: indirect costs		$20.65	$0	$20.65
TOTAL COSTS		**$46.91**	**$0**	**$46.91**

The estimate shows a split between land and water liability to assist regulatory authorities in splitting security requirements between the land owner (the KIA) and the Nunavut Water Board whose primary interest is the water related liability. In reality this split is artificial as reclamation has to address both aspects and must be holistic in its approach. Overall Agnico Eagle expects that reclamation security in total of $46.9M will be required to secure this liability. The CRP will be approved during the Water Licence permitting process, and security in the form of an irrevocable letter of credit posted through one of the main Canadian banks will have to be arranged by Agnico Eagle prior to the start of mining operations.

Item 21. Capital and Operating Costs

The cost estimates used in earlier items of this report were derived from previous internal studies and were used to determine the cut-off grades needed to complete the new mineral reserves and resources as of December 31, 2014.

This item describes in more detail the capital and operating costs associated with exploiting the reserves of the Tiriganiaq and Wesmeg deposits exclusively. The costs described in this item are based on the LOM plan from the January 2015 updated technical study (Petrucci *et al*., 2015).

21.1 Capital costs

The capital cost estimate encompasses open pit and underground mine construction and development, all surface infrastructure including on-site and off-site facilities, process plant construction, and all closure costs associated with mining the reserves of the Tiriganiaq and Wesmeg deposits. The costs are based on engineering standards and derived from current costs from Agnico Eagle's Meadowbank Division (an operating Agnico Eagle mine in Nunavut 290 km northwest of the Meliadine project), other Agnico Eagle operations, operating experience and suppliers' price quotations.

The capital cost estimates use fourth quarter 2014 Canadian dollars. No inflationary escalation factors have been applied to these cost projections. All cost estimates for this study should be considered at a feasibility level in accuracy (*i.e.*, -10% to +15%). A 10% average contingency has been added to all infrastructure capital costs.

The operating life of the Meliadine mine is estimated at nine years, with mining from underground only in the first three years, and both open pit and underground mining from Year 4 onward.

The initial capital cost is estimated at C$1,048 million (US$911 million), plus a sustaining capital cost of C$411 million (US$357 million) and closure capital costs of C$47 million (US$41 million). The total capital costs are therefore estimated to be C$1,505 million (US$1,309 million) over the LOM model. Table 21.1 shows the breakdown of the capital expenditures anticipated for the project, including sustaining capital.

Table 21.1 - Meliadine mine project capital expenditures estimate

Capital estimate	Cost	
	C$ (millions)	US$ (millions)
Pre-production capital		
General site infrastructure	95.76	83.27
Off-site infrastructure	21.58	18.77
Mine surface infrastructure (1)	6.88	5.99
Underground development	214.98	186.94
Underground mine infrastructure (2)	111.74	97.17
Process plant	162.59	141.38
Tailings and water reclaim	28.59	24.86
Construction indirect costs	250.11	217.49
Owner's costs	108.10	94.00
Contingency	73.54	63.95
Pre-production	29.11	25.32
Exploration	8.41	7,312
Gold revenue from pre-production	-63.90	-55.56
Subtotal pre-production capital	***1,047.51***	***910.88***
Sustaining capital		

Sustaining capital (3)	411.03	357.42
Salvage value	0	0
Closure	46.91	40.79
Subtotal sustaining capital	***457.94***	**398.21**
Total capital	**1,505.45**	**1,309.09**

(1) : mine surface infrastructure refers to explosives plant and ramp portal

(2) : includes underground mobile equipment

(3) : includes open pit mobile equipment

The mine-site costs and the operating costs described in this section reflect the LOM plan (Petrucci *et al.,* 2015) enhanced with the December 31, 2014 mineral reserves and mineral resources estimates and the related opportunities.

21.2 Operating costs

Operating costs have been estimated at C$1,877 million over Meliadine's LOM, as summarized in Table 21.2. The average cost to mine both the open pit and the underground mine is estimated at C$135.27/tonne milled. Table 21.3 shows mine-site costs per tonne in a typical year, including both underground and open pit mining. In addition there will be gold doré bars transportation charges of C$1.50/ounce and refining charges of C$1.00/ounce recovered, which are currently estimated to total approximately C$8.0 million over the life of the mine.

Table 21.2 - Meliadine mine project estimated operating costs

	C$/t milled
Total Open Pit	**9.30**
Geology	0.95
Production	5.03
OP Services	1.29
OP Maintenance	2.02
Total Underground Mine	**37.74**
Geology	2.79
Development	9.16
U/G Mining	11.70
U/G Services	7.23
U/G Maintenance	6.86
Milling	33.27
Site General	54.96
Total Operating cost (LOM)	**135.27**

Table 21.3 - Mine-site costs per tonne in a typical year at 5,000 tpd production rate

	C$/t milled
Operating costs	135.27
Deferred stripping	NA
Stock Pile inventory adjustment	NA
Other administration charges	4.20
Total Mine-site cost (LOM)	**139.47**

The total workforce at Meliadine is estimated to be a maximum of 700 Agnico Eagle employees at full production at Year 4 and is summarized in Table 21.4.

Table 21.4 - Estimated workforce requirements over the LOM

Department	Y4
Engineering	41
Environment/ Health & Safety	12
G&A	10
Geology	33
Human Resources	16
Maintenance	93
OP mining	81
Process Plant	131
Services	76
UG Mining	185
Warehouse	21
Total	**700**

To reduce costs associated with the exterior work during winter in Nunavut, exterior construction work will mainly be done from April to November each year. Major parts of the civil, structural and architectural work will be done during this period considered as 'summer months'. Emphasis will be placed on enclosing the buildings prior to the start of the cold-weather period. To achieve this target, exterior construction will be carried out 24 hours per day during that time. Major mechanical, piping and electrical work will be done inside the buildings during the winter season.

The construction facilities on-site are also planned to be minimal. The existing installation (exploration camp) will be used as a construction office, camp and kitchen. Additional temporary infrastructure will be built in Y-4 close to the construction site to support the contractors and reduce travelling time on site such as traveling to lunch and breaks, but will be kept minimal. Other existing infrastructure such as cover-all buildings will going to be used by the construction group.

An advantage of having the construction done over a four year period is also to equalize the labour curves required for the infrastructure construction. This will reduce the amount of temporary installation (camp, garage, shop), will minimize supervision required on-site and give flexibility to the construction management strategy.

The mill capacity upgrade from 3,000 tpd to 5,000 tpd will also require construction activity. The objective is to reach 5,000 tpd in the first quarter Y4. By the beginning of Y3, there will be some construction activity related to the increase in mill capacity.

21.3 Employment practices

For the Meliadine project, employment and Human Resources ("HR") policies proposed are in compliance with all applicable labour standards legislation in force in Nunavut (*Labour Standards Act*), reflect best practices in HR management, and provide clear, transparent and efficient general practices. Policies will be applied fairly to all employees in a respectful workplace free from violence and harassment.

All positions at the Meliadine project will be staffed with qualified candidates selected and appointed on the basis of education, experience, knowledge, abilities, suitability and, when appropriate, seniority and residency. The Meliadine project is committed to the principles of

being an equal opportunity employer and will ensure that non-discriminatory practices respectful of Human Rights are adopted in all employment-related programs.

All employees, will be provided with a comprehensive compensation and benefits plan coverage, which will include dental, medical, accidental death and dismemberment insurance, life insurance (both short- and long-term disability coverage), as well as an Employee and Family Assistance Program ("EFAP"). Other benefit programs may involve: registered pension plan, medical travel assistance program, mobility premium, travel allowance, employee share purchase plan and recreation committee.

It was decided that 3 different schedules would be favoured for the Meliadine project function of the job description:

- 4 days worked and 3 days off (management)
- 14 days worked and 14 days off (normal schedule)
- 5 days worked and 2 days off (north employees)

Item 22. Economic Analysis

The proven and probable reserves reported for the Meliadine mine as of December 31, 2014 are 13.9 million tonnes grading 7.44 g/t gold, containing 3.3 million ounces of gold, all contained in the Tiriganiaq and Wesmeg deposits. This includes 8,000 ounces of gold in stockpiled proven reserves (34,000 tonnes grading 7.31 g/t gold); 638,000 ounces of gold in open pit probable reserves (3.9 million tonnes grading 5.13 g/t gold); and 2.7 million ounces of gold in probable underground reserves (10.0 million tonnes grading 8.33 g/t gold).

The economic analysis in this section of the report is based on the mine plan (LOM) and all associated costs as given in the January 2015 updated technical study (Petrucci *et al*., 2015).

22.1 Assumptions and cash flow

Details of the mine production schedule are given in Item 16 for both the underground and open pit mines. Based on the January 2015 LOM, Meliadine will have mine life of nine years from the Tiriganiaq and Wesmeg deposits. The basic mine production parameters and economic analysis assumptions are as follows:

- 365 operating days per year (with 20 unscheduled down days per year due to weather conditions)
- 3,000 tpd of ore to the mill in Years 1-3; 5,000 tpd of ore to the mill in Years 4-9
- low-grade marginal ore stockpiles to be processed at the end of the mine life
- recovery 96% average
- average oz production of 326,000 oz in years 1 to 3 and 397,000 oz in years 4 to 8
- total LOM oz production of 3,214,000 oz
- fuel price assumptions – $96.5/l in the winter, and $94.0/l in the summer
- gold price of US$1,300
- C$/US$ exchange rate of 1.15
- refining costs of C$2.50/oz
- IIBA costs are as stated in the latest MOU (February 2015)

Approximately four years of development and construction will be required before ore production begins. Ore production will start in Y-1 and commercial production will be achieved in the last month of year Y-1, and full capacity production of 1,095,000 tonnes will be reached in Y1.

22.1.1 Construction strategy

The mine production forecast is shown as Table 22.1. The average annual production from the Meliadine project will be 364,726 ounces of gold (excluding Y-1).

Table 22.1 - Mine and mill production forecast for the Meliadine mine, including ore and marginal ore from open pit and underground sources

	Y-1	Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8	Y9	
	2019	**2020**	**2021**	**2022**	**2023**	**2024**	**2025**	**2026**	**2027**	**2028**	**Total**
Underground production											
Ore tonnage (t)(x000)	202	1,095	1,095	1,095	1,119	1,098	967	1,095	1,825	557	10,149
Gold grade(g/t)	10.34	10.57	9.05	9.29	9.19	8.28	7.62	7.80	6.56	5.97	8.31
In-situ gold (oz)	67,241	372,239	318,697	327,074	330,736	292,360	237,072	274,508	385,193	107,080	2,712,202
Open pit ore											-
Ore tonnage (t)(x000)	-	-	-	-	690	727	858	730	0	858	3,862
Gold grade (g/t)	-	-	-	-	5.75	5.55	5.67	5.73	0.00	3.25	5.13
In-situ gold (oz)	-	-	-	-	127,484	129,834	156,241	134,392	0	89,622	637,574
Total Mill Feed											-
Ore tonnage (t)(x000)	202	1,095	1,095	1,095	1,809	1,825	1,825	1,825	1,825	1,415	14,012
Old grade (g/t)	10.34	10.57	9.05	9.29	7.88	7.20	6.70	6.97	6.56	4.32	7.44
In-situ gold (oz)	67,241	372,239	318,697	327,074	458,220	422,195	393,313	408,900	385,193	196,703	3,349,775
Recovered gold (oz)	64,216	355,489	307,543	315,627	441,266	405,730	377,188	392,136	369,015	185,884	3,214,093
Cash cost (C$/oz)	$812.81	$510.54	$601.24	$635.17	$551.01	$610.02	$690.79	$613.88	$546.20	$848.33	$610.30
Cash cost (US$/oz)	$706.97	$443.95	$522.82	$552.32	$479.14	$530.45	$600.69	$533.81	$474.96	$737.68	$530.70

As this table shows, the total cash cost varies from C$510 (US$444) to C$848 (US$738) per ounce of gold, averaging C$610/oz (US$531/oz) over the LOM. This economic analysis was done using assumptions that are different from the ones used to estimate the mineral reserves. The economics were analyzed using assumptions that are closer to the ones that are current at the time of the completion of the updated technical study: US$1,300/oz gold price and a C$/US$ exchange rate of 1.15. This gold price and exchange rate are similar to those being used in other current technical reports and by mining analysts employed in the capital markets industry.

Using these assumptions, the estimated cash flow projection over the life of the Meliadine mine project is presented in Table 22.2. Total revenues and total net cash flow are estimated to be, respectively, C$4,733 million and C$1,350 million over the LOM that was modeled. Calculation of the cash flow takes into account the revenues, and capital and operating costs, but not the taxes and financing expenses.

Table 22.2 - Meliadine project pre-tax cash flow evolution (C$ millions)

Year	Revenue	CAPEX	OPEX	Net cash flow before tax	Cumulative Cash flow
-5	-	69.70		-69.70	-69.70
-4	-	199.27		-199.27	-268.97
-3	-	317.57		-317.57	-586.54
-2	-	277.89		-277.89	-864.43
-1	31.95	183.08	17.30	-168.43	-1,032.87
1	530.57	67.86	179.90	282.80	-750.06
2	459.01	120.46	183.53	155.02	-595.04
3	471.07	93.96	199.06	178.05	-416.99
4	658.59	41.57	241.17	375.85	-41.14
5	605.55	25.89	245.69	333.97	292.83
6	562.95	25.89	240.66	296.41	589.24
7	585.26	25.89	220.55	338.82	928.06
8	550.76	9.50	194.95	346.31	1,274.37
9	277.43	2.92	154.36	120.15	1,394.52
10	-	20.00	-	-20.00	1,374.52
11 to 19	-	23.99	-	-23.99	1,350.52
Total	4,733.14	1,505.45	1,877.16	1,350.52	

The result of the economic analysis provides a positive internal rate of return (IRR) of 10.3%. After taxes, the NPV is C$307 million (US$267 million) showing a total cash flow after taxes of C$857 million.

22.2 Taxation and Royalties

The Meliadine project is subject to Canadian federal income taxes and mining royalties in Nunavut Territory. Income taxes included in the LOM cash flow model are based on a flat statutory income tax rate solely to demonstrate the economic viability of the Meliadine operations. The income tax rate is currently estimated to be 25.95%.

The Meliadine property is situated on Inuit-Owned Land. However, the claims are "grandfathered" claims so the production from these claims will be subject to a net profits royalty payable to the Crown royalty regime in accordance with the Northwest Territories and Nunavut Mining Regulations. The royalties are calculated using a graduated rate to a maximum of 13%. As the royalties are based on net profits, they will be reflected as income and mining taxes.

22.3 Payback

The after-tax payback period for the Meliadine project is estimated as 5.0 years after the start of commercial production (*i.e.*, four years of development and construction followed by five years of production) using a gold price of US$1,300/oz and a C$/US$ exchange rate of 1.15. This payback period does not take into account any interest on loans nor inflation.

22.4 Sensitivity Analysis

The base case economic analysis using a gold price of US$1,300/oz and a C$/US$ exchange rate of 1.15 shows an after-tax IRR of 10.3% and an after-tax NPV of C$307 million. In order to properly evaluate the robustness of the project, a sensitivity analysis was made to establish the sensitivity of the after-tax IRR and NPV to variations up to ±20% in the gold price, ore grade, capital expenditures, operations costs and gold recovery in the mill. The results of this analysis are given in Figure 22.1 and Figure 22.2. The figures show that the main sensitivities of the NPV and IRR of this project are to the gold price, metallurgical recovery and reserve grade (all three have the same impact). This is followed by the capital costs, with the operating costs having slightly less impact on the economics of the project.

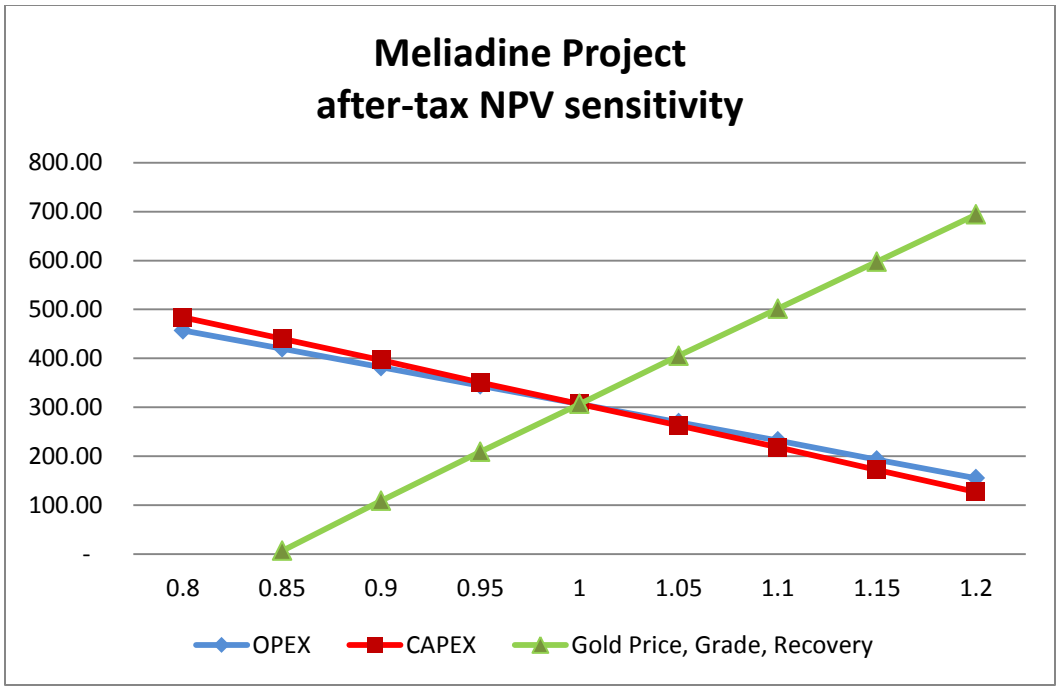


Figure 22.1 - Sensitivity of after-tax NPV to variations in operating costs, capital costs and gold price (grade, metallurgical recovery)

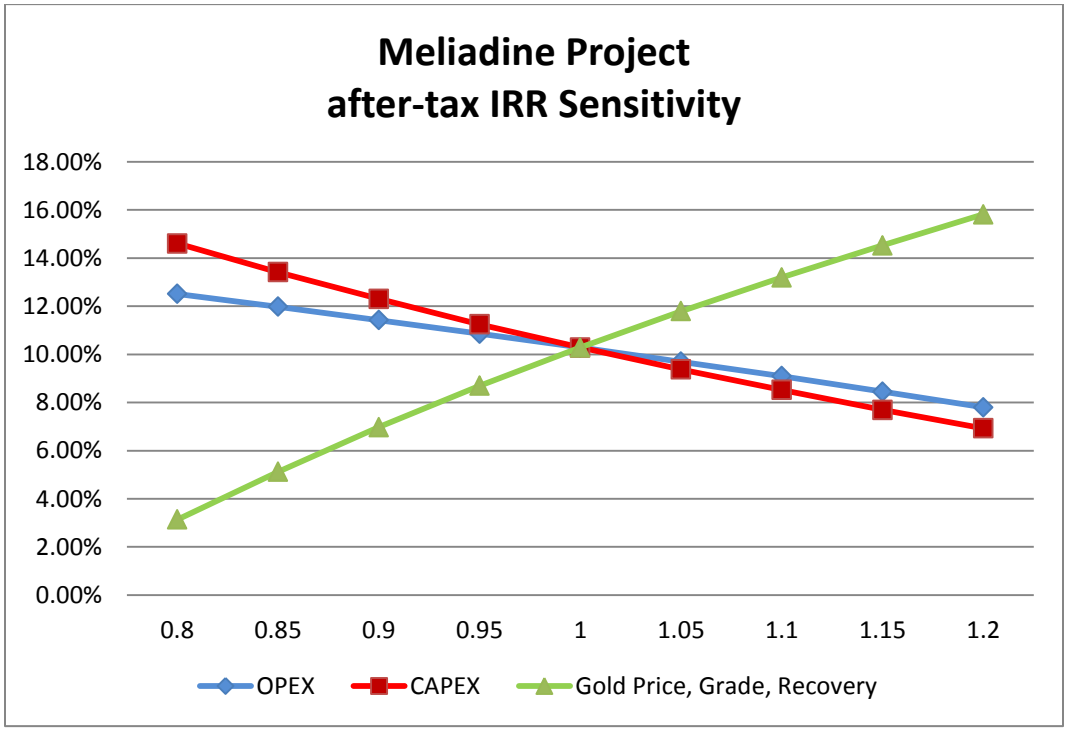


Figure 22.2 - Sensitivity of after-tax IRR to variations in operating costs, capital costs and gold price (grade, metallurgical recovery)

Table 22.3 shows the sensitivity of the after-tax IRR to variations in the gold price and exchange rate, while Table 22.4 shows the sensitivity of the after-tax NPV to variations in the same factors.

Table 22.3 - After-tax IRR sensitivity to gold price and exchange rate variation

Exchange rate	Gold Price (US$/oz)									
C$/US$	1,000	1,100	1,150	1,200	1,245	1,300	1,400	1,500	1,600	1,700
0.90	-11.11%	-4.90%	-2.55%	-0.73%	0.70%	2.35%	4.85%	7.08%	9.13%	10.99%
0.95	-7.36%	-2.13%	-0.28%	1.36%	2.75%	4.20%	6.61%	8.80%	10.79%	12.65%
1.00	-4.33%	-0.01%	1.69%	3.25%	4.46%	5.87%	8.23%	10.39%	12.37%	14.19%
1.05	-1.92%	1.86%	3.46%	4.85%	6.06%	7.43%	9.76%	11.90%	13.84%	15.66%
1.10	-0.01%	3.53%	4.97%	6.37%	7.53%	8.91%	11.19%	13.30%	15.23%	17.07%
1.15	1.69%	4.97%	6.43%	7.77%	8.95%	10.28%	12.56%	14.63%	16.59%	18.40%
1.20	3.25%	6.37%	7.77%	9.13%	10.26%	11.60%	13.84%	15.92%	17.86%	19.67%
1.30	5.87%	8.91%	10.28%	11.60%	12.72%	14.01%	16.26%	18.32%	20.26%	22.09%
1.40	8.23%	11.19%	12.56%	13.84%	14.94%	16.26%	18.47%	20.55%	22.50%	24.36%

Table 22.4 - After-tax NPV sensitivity to gold price and exchange rate variation (C$ millions)

Exchange rate	Gold Price (US$/oz)									
C$/US$	1,000	1,100	1,150	1,200	1,245	1,300	1,400	1,500	1,600	1,700
0.90							$(8.21)	$114.91	$235.19	$ 352.07
0.95						$(42.31)	$88.35	$215.45	$339.12	$ 463.49
1.00				$(91.79)	$(28.67)	$47.31	$181.08	$313.23	$444.21	$ 572.75
1.05			$(80.79)	$(8.21)	$57.63	$134.79	$274.21	$411.99	$547.04	$ 682.01
1.10		$(77.04)	$(1.39)	$74.98	$140.76	$222.13	$365.01	$508.48	$649.87	$ 792.80
1.15		$(1.39)	$78.32	$154.67	$224.44	$306.72	$457.07	$604.88	$754.38	$ 901.66
1.20	$(91.79)	$74.98	$154.67	$235.19	$305.42	$392.15	$547.04	$702.47	$856.83	$1,010.56
1.30	$47.31	$222.13	$306.72	$392.15	$467.99	$559.90	$728.74	$895.25		
1.40	$181.08	$365.01	$457.07	$547.04	$628.02	$728.74	$908.06			

Item 23. Adjacent Properties

There are no properties adjacent to the Meliadine gold project that have any effect on the project.

Item 24. Other Relevant Data and Information

Agnico Eagle is not aware of any other relevant data or information about the Meliadine project.

Item 25. Interpretation and Conclusions

Since 1987, over 2,960 holes representing 650,000 m have been drilled at the Meliadine project including 310,000 m (1,055 holes) at the Tiriganiaq deposit. Based on this drilling and the results of two underground bulk samples, the total Meliadine proven and probable mineral reserve as of December 31, 2014, stands at 13.9 million t averaging 7.44 g/t gold for a total of 3.34 million ounces of gold, contained in the Tiriganiaq deposit and a portion of the Wesmeg deposit. In addition, the total mineral resources in all the deposits comprise indicated mineral resources of 20 million t averaging 5.06 g/t gold for a total of 3.3 million ounces of gold, and inferred mineral resources of 14 million tonnes averaging 7.65 g/t gold for a total of 3.5 million ounces of gold (Table 15.3 and Table 15.4).

From 2012 through 2014, Agnico Eagle weighed various scenarios of extracting millfeed from a combination of underground and open pit mining. Improvements were made to the project based on the company's Nunavut experience at its Meadowbank mine. The resulting updated technical study, summarized in this technical report, envisions mining the reserves from two open pits and an underground mine over nine years.

25.1 Conclusions

The concept is to develop a smaller project at the start, reducing the initial capital cost, and expanding the mine and mill later on when experience has been gained and the operational performance is better known. For this purpose, the mill throughput is set at 3,000 tpd from Year 1 to Year 3 extracting all ore from the underground mine, and then increasing the mill throughput to 5,000 tpd starting in Year 4 with mill feed coming from both underground and the open pit mines. The conventional gold processing plant for the project comprises crushing, grinding, gravity separation and cyanide leaching by CIL, followed by cyanide destruction and filtration of the tails for dry stacking. The average metallurgical gold recovery, over the nine-year LOM averages 96.0%.

The current project results in annual production averaging 326,000 ounces of gold for the first three years and 397,000 ounces of gold from Year 4 to Year 8. The total cash cost varies from C$510 (US$444) to C$848 (US$738) per ounce of gold, averaging C$610 (US$531) per ounce over the LOM. The project generates an after-tax IRR of 10.3% and an after-tax NPV of C$307 million (US$267 million) at a discounted rate of 5% assuming a gold price of US$1,300/oz and a C$/US$ exchange rate of 1.15. The initial capital expenditure is estimated at C$1,048 million (US$911 million).

Considering all the geological knowledge acquired since 2011, the Meliadine property demonstrates excellent potential to increase the reserves and the resources and eventually expand the life of the mine, which would improve the profitability of this project. All deposits are still open at depth, and many other regional targets have been identified on the large property. Additional exploration and conversion drilling from surface and from the exploration ramp is planned in the coming years to test this potential.

25.2 Risks and Potential impacts

- Geological risks that could have an impact on mineral reserves at Meliadine are due to the nugget effect related to the nature of the deposit. This effect creates uncertainties concerning the accuracy of the ore model due to the complexity of the deposit, which could affect the mining method.
- Changes in commodity price represent a significant risk. Sensitivities show that a 13% decrease in the gold price would decrease the amount of gold contained in mineral reserves by approximately 5%.
- Groundwater inflow volume and quality (especially salinity) in the underground mine were estimated mainly from a wesbay (volume) and packer (quality) test completed in ten in diamond drill holes. Information about the hydrogeological properties of the rock mass was also used. Accordingly, some uncertainties can be stated about the capital and the operational costs required to manage this groundwater. A more detailed hydrogeological study is planned in 2015 to improve the estimation of the volume and quality of the groundwater inflow.
- Recirculation of the process water will tend to increase the level of some contaminants such as salts and cyanide complexes. The level of contamination is mainly driven by the addition or the production of contaminants and by the plant water balance. It is understood that salts could come from the underground mine with the potential presence of saline groundwater inflow. Thiocyanate and ferrocyanide will be produced in the cyanidation circuit. Those contaminants will build up in the process water until it reaches a steady state level. The processing plant includes water clarification treatment, which does not remove salts and cyanide complexes. At some point, additional water treatments may be required to regulate the process water quality.
- There is a potential risk related to the length of time required to complete the environmental permitting process. On February 27, 2015, NIRB issued the project certificate for the project, completing the environmental assessment process. This clears the way for Agnico Eagle to now obtain the required permits and authorizations (Water Licence, DFO authorizations, *etc*.) The company will submit applications in the second quarter of 2015 for all the permits and authorizations required to construct and operate the first phase of the mine. In the meantime, Agnico Eagle needs to manage its ongoing risk by maintaining in good standing its existing permits, licences, leases and authorizations that will allow for continued access to land for the purposes of mining and milling at the Meliadine site. These permits are discussed in Items 4 and 20 of this report. Agnico Eagle is also required to negotiate and implement an Inuit Impact Benefits Agreement (IIBA) with the KIA for the Meliadine project before the project can commence construction. Similarly, the Company is required to negotiate and implement a Water Rights Compensation Agreement in accordance with Article 20 of the NLCA and a Commercial Production Lease with the KIA. Both the Water Rights Compensation Agreement and the Commercial Production Lease are required before construction can start. These negotiations are well advanced; Agnico Eagle expects that the IIBA, Water Rights Compensation Agreement and Commercial Production Lease will all be successfully concluded in 2015.
- Cemented paste fill will be used in primary underground stopes to maximize ore recovery. The curing performance of that type of fill in the permafrost environment is not very well known. Although laboratory testing has been performed for the last three years

to investigate the paste in different conditions, some uncertainties remain regarding the behaviour of the backfill in the permafrost. Accordingly, economical risks can be stated about the percentage of cement required to achieve the required strength as well as the time needed to reach this strength that may slow down the underground mining sequence.

Item 26. Recommendations

The main recommendation for this project is to convert as much of the inferred resources (14 million tonnes averaging 7.65 g/t gold as of December 31, 2014) as possible into mineable reserves. This will significantly improve the project's economic viability, especially if the additional mill feed requires minimal or no additional infrastructure other than what is described in this document. It is also recommended to proceed with the validation of some basic project assumptions in order to reduce the overall project risks and to continue to study some concepts in order to improve the project economic performance.

Specific recommendations to further reduce the project risk include:

- Investigate the influence of the temperature of the stope walls on the strength development of the paste backfill.
- Validate the groundwater inflow rate (dewatering volume) with a more detailed hydrogeological study.
- It is currently assumed that no permanent crown pillar will be left between the pit floor and the underground operation. The upper portion of the underground mine will be mined during the first years of operation, with paste fill being placed as tightly to the back of the upper stopes as possible to maintain stability. The final pit floor will eventually rest on the backfilled stopes. This approach requires further study prior to moving on to the next planning phase.
- Complete modeling of water recycling from the tailings filtration, and the potential accumulation of elements detrimental to the recovery process.
- Acquire additional supporting data to improve confidence in the metallurgical recovery estimates for the Wesmeg, Normeg, Pump, F zone and Discovery deposits, and better assess the robustness of the processing for these deposits.
- Additional characterization and metallurgical testing should be completed to provide more in-depth information to be used in the final plant design and to identify opportunities for mill operating cost optimization, such as a continuous gravity circuit.
- Improve the 3D geological modelling for all deposits to increase the reserve and resources accuracy and confidence.
- Continue the condemnation drilling campaign in 2015 on the planned infrastructure site.

Specific recommendations to further improve the project economic performance include:

- Continue to optimize the paste backfill recipe. The latest laboratory test results indicated a significant strength increase with the addition of crushed rock.
- Re-assess the current haulage system (trucking with 60-t trucks), considering the evolution of the deposits' size and geometry. Alternative systems like conveying or "railveying" could eventually become more attractive. Similarly the type of haulage fleet considered on levels versus in the main haulage drifts (declines) should be re-assessed to validate, for example, the benefit of using smaller equipment on the levels, allowing a reduction of the haulage drift dimensions.

- Conduct a new Lerchs-Grossmann open pit evaluation and a new underground design following the conversion of inferred resources currently contained in the Wesmeg, Normeg, Discovery, Pump, F zone and Wolf deposits.
- Continue regional exploration (prospecting, geophysics and diamond drilling) along structures with good mineralization potential, especially close to the know deposits.

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Note to Investors Concerning Estimates of Mineral Reserves and Mineral Resources

The mineral reserve and mineral resource estimates contained in this Technical Report have been prepared in accordance with the Canadian securities regulatory authorities' (the "CSA") National Instrument 43-101 *Standards of Disclosure for Mineral Projects* ("NI 43-101"). These standards are similar to those used by the United States Securities and Exchange Commission's (the "SEC") Industry Guide No. 7, as interpreted by Staff at the SEC ("Guide 7"). However, the definitions in NI 43-101 differ in certain respects from those under Guide 7. Accordingly, mineral reserve information contained herein may not be comparable to similar information disclosed by U.S. companies. Under the requirements of the SEC, mineralization may not be classified as a "reserve" unless the determination has been made that the mineralization could be economically and legally produced or extracted at the time the reserve determination is made. The SEC does not recognize measures of "mineral resource".

The mineral reserve figures presented herein are estimates, and no assurance can be given that the anticipated tonnages and grades will be achieved or that the indicated level of recovery will be realized. The Company does not include equivalent gold ounces for byproduct metals contained in mineral reserves in its calculation of contained ounces.

Cautionary Note to Investors Concerning Estimates of Measured and Indicated Mineral Resources

This document uses the terms "measured mineral resources" and "indicated mineral resources". Investors are advised that while those terms are recognized and required by Canadian regulations, the SEC does not recognize them. **Investors are cautioned not to assume that any part or all of mineral deposits in these categories will ever be converted into mineral reserves**.

Cautionary Note to Investors Concerning Estimates of Inferred Mineral Resources

This document uses the term "inferred mineral resources". Investors are advised that while this term is recognized and required by Canadian regulations, the SEC does not recognize it. "Inferred mineral resources" have a great amount of uncertainty as to their existence and as to their economic and legal feasibility. It cannot be assumed that any part or all of an inferred mineral resource will ever be upgraded to a higher category. Under Canadian regulations, estimates of inferred mineral resources may not form the basis of feasibility or pre-feasibility studies, except in rare cases. **Investors are cautioned not to assume that any part or all of an inferred mineral resource exists, or is economically or legally mineable**.

Note to Investors Concerning Certain Measures of Performance

This document presents certain measures, including "total cash costs per ounce", "all-in sustaining costs" and "minesite costs per tonne" that are not recognized measures under US GAAP. This data may not be comparable to data presented by other gold producers. The Company believes that these generally accepted industry measures are realistic indicators of operating performance and are useful in allowing year over year comparisons. However, these non-US GAAP measures should be considered together with other data prepared in accordance with US GAAP, and these measures, taken by themselves, are not necessarily indicative of operating costs or cash flow measures prepared in accordance with US GAAP. This document also contains information as to estimated future total cash costs per ounce, all- in sustaining costs and minesite costs per tonne. The estimates of total cash costs per ounce, all-in sustaining costs and minesite costs per tonne are based upon the total cash costs per ounce, all-in sustaining costs and minesite costs per tonne that the Company expects to incur to mine gold at its mines and projects and, consistent with the reconciliation of these actual costs referred to above, do not include production costs attributable to accretion expense and other asset retirement costs, which will vary over time as each project is developed and mined. It is therefore not practicable to reconcile these forward-looking non-US GAAP financial measures to the most comparable US GAAP measure.

Appendix 4.1 - Meliadine Claims

MELIADINE	AANDC			
Mining Lease	**NAME**	**RECORDED DATE**	**EXPIRY DATE**	**AREA (ha)**
F64729	CWM7	4/14/1998	23/09/2030	1,045.30
F64730	CWM8	4/14/1998	23/09/2030	1,053.40
F64731	CWM9	4/14/1998	23/09/2030	1,034.78
F64732	CWM10	4/14/1998	23/09/2030	1,050.56
F64733	CWM11	4/14/1998	23/09/2030	1,046.92
F64734	CWM12	4/14/1998	23/09/2030	1,037.61
F19044	NAT34	9/26/2001	9/26/2022	817.10
F19045	NAT35	9/26/2001	9/26/2022	514.07
F19046	NAT36	9/26/2001	9/26/2022	851.05
F19047	NAT37	9/26/2001	9/26/2022	980.29
F19049	NAT38	9/26/2001	9/26/2022	524.59
F19620	NAT40	9/26/2001	9/26/2022	708.01
F19621	NAT41	9/26/2001	9/26/2022	755.54
F19038	NAT28	10/17/2000	10/17/2021	994.24
F19039	NAT29	10/17/2000	10/17/2021	1,055.18
F19040	NAT30	10/17/2000	10/17/2021	1,034.39
F19048	NAT31	10/17/2000	10/17/2021	448.80
F19042	NAT32	10/17/2000	10/17/2021	999.17
F19043	NAT33	10/17/2000	10/17/2021	931.51
F00526	NAT2	10/18/1999	10/18/2020	1,042.87
F00527	NAT3	10/18/1999	10/18/2020	1,038.42
F14842	NAT4	10/18/1999	10/18/2020	1,001.19
F14841	NAT5	10/18/1999	10/18/2020	1,021.43
F17843	NAT6	10/18/1999	10/18/2020	757.57
F14839	NAT	10/20/1997	10/20/2018	1,020.62
F29192	NAT51	10/25/2002	10/25/2023	733.70
F29193	NAT52	10/25/2002	10/25/2023	824.34
F29194	NAT53	10/25/2002	10/25/2023	852.67
F29195	NAT54	10/25/2002	10/25/2023	1,023.45
F29196	NAT55	10/25/2002	10/25/2023	1,098.72
F29197	NAT56	10/25/2002	10/25/2023	1,019.40
F29198	NAT57	10/25/2002	10/25/2023	1,011.31
F29199	NAT58	10/25/2002	10/25/2023	1,004.43
F29200	NAT59	10/25/2002	10/25/2023	715.48
F44578	NAT78	11/12/2003	11/12/2024	702.13
F44579	NAT79	11/12/2003	11/12/2024	728.84
F44580	NAT80	11/12/2003	11/12/2024	630.90
F51714	NAT81	12/29/2006	11/12/2027	677.85
F51715	NAT82	12/29/2006	11/12/2027	144.88
F51716	NAT83	12/29/2006	11/12/2027	774.97
F51717	NAT84	12/29/2006	11/12/2027	583.96
F44575	NAT75	1/29/2007	1/29/2028	297.85
F34244	NAT85	1/29/2007	1/29/2028	28.09
F51724	NAT86	1/29/2007	1/29/2028	205.18
F18141	NAT8	3/14/1990	3/1/2021	1,017.11
F18142	NAT9	3/14/1990	3/1/2021	1,046.92
F18143	NAT10	3/14/1990	3/1/2021	841.02
F18144	NAT11	3/14/1990	3/1/2021	1,005.68
F18145	NAT12	3/14/1990	3/1/2021	989.14
F18146	NAT13	3/14/1990	3/1/2021	919.61
F18147	NAT14	3/14/1990	3/1/2021	752.67
F18148	NAT15	3/14/1990	3/1/2021	878.31
F18149	NAT16	3/14/1990	3/1/2021	1,021.31
F18150	NAT17	3/14/1990	3/1/2021	1,027.09
F18151	NAT18	3/14/1990	3/1/2021	1,003.62
F18181	NAT19	3/14/1990	3/1/2021	1,007.26
F18182	NAT20	3/14/1990	3/1/2021	963.96
F18140	NAT7	3/14/1990	3/9/2021	989.43
F18184	NAT26	3/14/1990	3/9/2021	974.89
F18190	NAT27	3/14/1990	3/9/2021	1,024.66
				51,285.46
Claims	**NAME**	**RECORDED DATE**	**EXPIRY DATE**	**AREA (ha)**
F69575	CWM13	4/19/2006	4/19/2016	109.27
F69576	CWM14	4/19/2006	4/19/2016	109.27
F69574	PB1	12/29/2006	12/29/2016	668.95
F92823	SHR23	10/27/2011	10/27/2021	1,045.10
F92822	SHR22	10/27/2011	10/27/2021	1,045.10
F92821	SHR21	10/27/2011	10/27/2021	1,045.10
F92820	SHR20	10/27/2011	10/27/2021	1,045.10
F92819	SHR19	10/27/2011	10/27/2021	1,045.10
F92818	SHR18	10/27/2011	10/27/2021	1,045.10
F92812	SHR12	10/27/2011	10/27/2021	1,045.10
F92807	SHR7	10/27/2011	10/27/2021	1,045.10
F92802	SHR2	10/27/2011	10/27/2021	1,045.10
F92806	SHR6	10/27/2011	10/27/2021	1,045.10
F92811	SHR11	10/27/2011	10/27/2021	1,045.10
F92816	SHR16	10/27/2011	10/27/2021	1,045.10
F92815	SHR15	10/27/2011	10/27/2021	1,045.10
F92814	SHR14	10/27/2011	10/27/2021	1,045.10
F92810	SHR10	10/27/2011	10/27/2021	1,045.10
F92805	SHR5	10/27/2011	10/27/2021	1,045.10
F92801	SHR1	10/27/2011	10/27/2021	1,045.10

F92813	SHR13	10/27/2011	10/27/2021	1,045.10
F92824	SHR24	10/27/2011	10/27/2021	1,045.10
F92825	SHR25	10/27/2011	10/27/2021	1,045.10
F92803	SHR3	10/27/2011	10/27/2021	836.89
F92804	SHR4	10/27/2011	10/27/2021	331.03
F92808	SHR8	10/27/2011	10/27/2021	1,045.10
F92809	SHR9	10/27/2011	10/27/2021	784.28
F92817	SHR17	10/27/2011	10/27/2021	720.34
				25,507.13

NTI-MINERALEXPLORATIONRIGHTS

CONCESSION	AGREEMENT No.	RECORDED DATE	EXPIRY DATE	2014 ANNUAL FEES	AREA (ha)
Ant1	RI01-99-01	01/06/1999	01/06/2018	5,600.00$	1,400.00
Ant3	RI01-99-04	01/06/1999	01/06/2018	588.00$	147.00
Tan1	RI01-99-10	01/06/1999	01/06/2018	1,628.00$	407.00
Felsic1	RI01-99-08	31/12/1999	31/12/2018	2,760.00$	690.00
Fay1	RI01-99-06	31/12/1999	31/12/2018	544.00$	136.00
Fay2	RI01-99-07	31/12/1999	31/12/2018	1,000.00$	250.00
Fay3	RI01-99-02	01/06/1999	01/06/2018	772.00$	193.00
Raptor	RI01-RI12	31-12-2013	31-12-2032	63,482.00$	31,741.00
				76,374.00$	**34,964.00**

Appendix 10.1 - Drill Collars Intercepts

DEPOSIT	BHID	FROM	TO	ZONE	Capped AU(g/t)	Not Capped AU (g/t)	Horizontal width(m)	Core length (m)	Collar Coordinates (UTM)		
									EASTING	NORTHING	ELEVATION
TIRIGANIAQ	M11-1018A	627.20	630.20	1100	0.17	0.17	2.73	3.00	6,988,878.56	538,503.81	72.18
TIRIGANIAQ	M11-1018A	639.80	644.00	1025	4.29	4.29	3.87	4.20	6,988,878.56	538,503.81	72.18
TIRIGANIAQ	M11-1018A	659.00	662.00	1015	1.31	1.31	2.84	3.00	6,988,878.56	538,503.81	72.18
TIRIGANIAQ	M11-1018A	664.00	666.50	1000	5.05	5.05	2.39	2.50	6,988,878.56	538,503.81	72.18
TIRIGANIAQ	M11-1036	452.80	456.00	1251	4.40	4.40	2.90	3.20	6,988,778.21	538,749.61	66.48
TIRIGANIAQ	M11-1036	483.00	486.00	1100	0.50	0.50	2.75	3.00	6,988,778.21	538,749.61	66.48
TIRIGANIAQ	M11-1036	515.00	518.00	1050	1.93	1.93	2.79	3.00	6,988,778.21	538,749.61	66.48
TIRIGANIAQ	M11-1036	522.40	525.00	1025	6.26	6.26	2.43	2.60	6,988,778.21	538,749.61	66.48
TIRIGANIAQ	M11-1036	527.00	530.00	1015	0.56	0.56	2.81	3.00	6,988,778.21	538,749.61	66.48
TIRIGANIAQ	M11-1036	534.00	537.00	1000	1.37	1.37	2.83	3.00	6,988,778.21	538,749.61	66.48
TIRIGANIAQ	M11-1045	97.60	103.40	1100	4.81	4.81	5.90	5.80	6,988,433.00	539,601.97	78.01
TIRIGANIAQ	M11-1045	97.80	100.40	1102	1.48	1.48	2.64	2.60	6,988,433.00	539,601.97	78.01
TIRIGANIAQ	M11-1045	103.20	106.20	1087	7.68	7.68	3.05	3.00	6,988,433.00	539,601.97	78.01
TIRIGANIAQ	M11-1045	108.60	111.00	1075	2.57	2.57	2.44	2.40	6,988,433.00	539,601.97	78.01
TIRIGANIAQ	M11-1045	116.90	119.50	1050	6.28	6.28	2.65	2.60	6,988,433.00	539,601.97	78.01
TIRIGANIAQ	M11-1045	125.00	126.00	1025	5.92	5.92	1.02	1.00	6,988,433.00	539,601.97	78.01
TIRIGANIAQ	M11-1047	98.40	103.50	1100	4.79	4.79	5.12	5.10	6,988,432.78	539,581.03	78.86
TIRIGANIAQ	M11-1047	99.20	101.20	1102	1.07	1.07	2.01	2.00	6,988,432.78	539,581.03	78.86
TIRIGANIAQ	M11-1047	103.30	107.30	1087	4.90	4.90	4.01	4.00	6,988,432.78	539,581.03	78.86
TIRIGANIAQ	M11-1047	110.60	113.40	1075	0.50	0.50	2.81	2.80	6,988,432.78	539,581.03	78.86
TIRIGANIAQ	M11-1047	117.40	120.00	1050	10.68	10.68	2.61	2.60	6,988,432.78	539,581.03	78.86
TIRIGANIAQ	M11-1052	94.60	97.30	1102	0.03	0.03	2.72	2.70	6,988,430.93	539,556.96	78.20
TIRIGANIAQ	M11-1052	97.30	102.40	1100	21.61	21.61	5.14	5.10	6,988,430.93	539,556.96	78.20
TIRIGANIAQ	M11-1052	102.40	105.40	1087	2.03	2.03	3.03	3.00	6,988,430.93	539,556.96	78.20
TIRIGANIAQ	M11-1052	107.60	110.20	1075	6.30	6.30	2.63	2.60	6,988,430.93	539,556.96	78.20
TIRIGANIAQ	M11-1052	113.40	116.40	1050	5.41	5.41	3.03	3.00	6,988,430.93	539,556.96	78.20
TIRIGANIAQ	M11-1055	91.60	94.50	1102	4.59	4.59	2.77	2.90	6,988,422.73	539,535.02	77.50
TIRIGANIAQ	M11-1055	94.20	97.40	1100	21.24	21.24	3.06	3.20	6,988,422.73	539,535.02	77.50
TIRIGANIAQ	M11-1055	97.40	100.20	1087	1.54	1.54	2.67	2.80	6,988,422.73	539,535.02	77.50
TIRIGANIAQ	M11-1055	100.40	106.00	1075	21.35	21.35	5.35	5.60	6,988,422.73	539,535.02	77.50
TIRIGANIAQ	M11-1055	110.70	116.00	1050	18.30	18.30	5.07	5.30	6,988,422.73	539,535.02	77.50
TIRIGANIAQ	M11-1055	119.40	120.00	1025	0.85	0.85	0.57	0.60	6,988,422.73	539,535.02	77.50
TIRIGANIAQ	M11-1059	99.90	102.10	1102	0.46	0.46	2.21	2.20	6,988,435.04	539,510.05	77.08
TIRIGANIAQ	M11-1059	102.10	105.00	1100	6.87	6.87	2.91	2.90	6,988,435.04	539,510.05	77.08
TIRIGANIAQ	M11-1059	107.00	109.60	1087	0.48	0.48	2.61	2.60	6,988,435.04	539,510.05	77.08
TIRIGANIAQ	M11-1059	112.00	115.00	1075	9.93	9.93	3.01	3.00	6,988,435.04	539,510.05	77.08
TIRIGANIAQ	M11-1059	117.00	119.60	1050	0.05	0.05	2.61	2.60	6,988,435.04	539,510.05	77.08
TIRIGANIAQ	M11-1063	83.00	85.50	1102	3.04	3.04	2.52	2.50	6,988,437.55	540,090.76	64.72
TIRIGANIAQ	M11-1063	93.40	97.20	1100	0.14	0.14	3.84	3.80	6,988,437.55	540,090.76	64.72
TIRIGANIAQ	M11-1063	123.80	127.00	1050	0.84	0.84	3.24	3.20	6,988,437.55	540,090.76	64.72
TIRIGANIAQ	M11-1063	134.40	137.00	1025	1.03	1.03	2.64	2.60	6,988,437.55	540,090.76	64.72
TIRIGANIAQ	M11-1063	145.20	147.80	1000	0.05	0.05	2.64	2.60	6,988,437.55	540,090.76	64.72
TIRIGANIAQ	M11-1066	77.00	80.80	1102	0.34	0.34	3.73	3.80	6,988,430.77	540,105.30	65.98
TIRIGANIAQ	M11-1066	88.00	91.30	1100	1.24	1.24	3.24	3.30	6,988,430.77	540,105.30	65.98
TIRIGANIAQ	M11-1066	120.00	124.00	1050	0.68	0.68	3.95	4.00	6,988,430.77	540,105.30	65.98
TIRIGANIAQ	M11-1066	131.00	133.60	1025	0.91	0.91	2.57	2.60	6,988,430.77	540,105.30	65.98
TIRIGANIAQ	M11-1066	143.40	146.50	1000	3.75	3.75	3.06	3.10	6,988,430.77	540,105.30	65.98
TIRIGANIAQ	M11-1069A	378.40	381.40	1100	1.33	1.33	2.07	3.00	6,988,619.30	538,830.24	65.57
TIRIGANIAQ	M11-1072	89.40	92.60	1102	0.91	0.91	3.17	3.20	6,988,444.79	540,132.16	66.58
TIRIGANIAQ	M11-1072	100.20	103.20	1100	0.08	0.08	2.97	3.00	6,988,444.79	540,132.16	66.58
TIRIGANIAQ	M11-1072	136.70	140.00	1050	36.24	61.39	3.28	3.30	6,988,444.79	540,132.16	66.58
TIRIGANIAQ	M11-1072	142.00	145.60	1025	7.80	7.80	3.58	3.60	6,988,444.79	540,132.16	66.58
TIRIGANIAQ	M11-1072	156.70	159.00	1000	3.77	3.77	2.29	2.30	6,988,444.79	540,132.16	66.58
TIRIGANIAQ	M11-1075	76.50	78.80	1102	0.31	0.31	2.27	2.30	6,988,432.28	540,158.00	66.72
TIRIGANIAQ	M11-1075	84.50	88.20	1100	1.91	1.91	3.66	3.70	6,988,432.28	540,158.00	66.72
TIRIGANIAQ	M11-1075	112.00	115.80	1075	0.03	0.03	3.79	3.80	6,988,432.28	540,158.00	66.72
TIRIGANIAQ	M11-1075	125.00	128.00	1050	0.31	0.31	3.00	3.00	6,988,432.28	540,158.00	66.72
TIRIGANIAQ	M11-1075	133.00	136.00	1025	2.14	2.14	3.01	3.00	6,988,432.28	540,158.00	66.72
TIRIGANIAQ	M11-1075	143.00	146.20	1000	3.72	3.72	3.22	3.20	6,988,432.28	540,158.00	66.72
TIRIGANIAQ	M11-1076	360.70	363.90	1100	1.71	1.71	2.33	3.20	6,988,610.45	538,929.94	70.61
TIRIGANIAQ	M11-1079	78.80	81.70	1100	0.13	0.13	2.86	2.90	6,988,431.30	540,185.19	66.76
TIRIGANIAQ	M11-1079	108.00	111.00	1075	0.96	0.96	2.95	3.00	6,988,431.30	540,185.19	66.76
TIRIGANIAQ	M11-1079	120.00	122.40	1050	11.91	11.91	2.34	2.40	6,988,431.30	540,185.19	66.76
TIRIGANIAQ	M11-1079	129.10	132.00	1025	0.39	0.39	2.82	2.90	6,988,431.30	540,185.19	66.76
TIRIGANIAQ	M11-1079	146.00	148.60	1000	0.66	0.66	2.53	2.60	6,988,431.30	540,185.19	66.76
TIRIGANIAQ	M11-1090	113.00	116.70	1102	2.70	2.70	3.86	3.70	6,988,555.11	538,170.09	58.31
TIRIGANIAQ	M11-1090	119.90	124.00	1100	6.30	6.30	4.28	4.10	6,988,555.11	538,170.09	58.31
TIRIGANIAQ	M11-1092	273.00	276.00	1170	0.50	0.50	2.42	3.00	6,988,598.57	539,064.37	72.11
TIRIGANIAQ	M11-1092	330.40	333.90	1100	0.69	0.69	2.85	3.50	6,988,598.57	539,064.37	72.11
TIRIGANIAQ	M11-1092	345.00	349.00	1025	0.06	0.06	3.27	4.00	6,988,598.57	539,064.37	72.11
TIRIGANIAQ	M11-1092	352.00	368.30	1000	7.42	7.42	13.44	16.30	6,988,598.57	539,064.37	72.11
TIRIGANIAQ	M11-1094	346.80	350.10	1153	0.69	0.69	2.77	3.30	6,988,682.24	538,969.88	70.20
TIRIGANIAQ	M11-1094A	337.00	340.00	1170	1.35	1.35	2.83	3.00	6,988,682.32	538,968.15	70.00
TIRIGANIAQ	M11-1094A	388.00	389.90	1100	1.67	1.67	1.83	1.90	6,988,682.32	538,968.15	70.00
TIRIGANIAQ	M11-1094A	404.00	406.60	1025	0.08	0.08	2.52	2.60	6,988,682.32	538,968.15	70.00
TIRIGANIAQ	M11-1094A	416.00	418.00	1000	8.90	8.90	1.95	2.00	6,988,682.32	538,968.15	70.00
TIRIGANIAQ	M11-1100	79.10	83.00	1102	9.21	9.21	2.86	3.90	6,988,496.41	538,199.56	58.21
TIRIGANIAQ	M11-1100	90.80	95.60	1100	0.23	0.23	3.54	4.80	6,988,496.41	538,199.56	58.21
TIRIGANIAQ	M11-1108A	284.00	287.50	1170	2.51	2.51	2.90	3.50	6,988,598.79	539,063.78	72.08
TIRIGANIAQ	M11-1108A	342.00	345.00	1100	1.76	1.76	2.58	3.00	6,988,598.79	539,063.78	72.08
TIRIGANIAQ	M11-1108A	357.00	360.80	1025	0.72	0.72	3.31	3.80	6,988,598.79	539,063.78	72.08
TIRIGANIAQ	M11-1108A	367.00	378.00	1000	6.22	6.22	9.68	11.00	6,988,598.79	539,063.78	72.08
TIRIGANIAQ	M11-1110	137.40	140.40	1000	3.50	3.50	3.04	3.00	6,988,521.29	538,410.07	58.65

TIRIGANIAQ	M11-1116	136.00	141.00	1050	5.34	5.34	5.06	5.00	6,988,481.78	538,650.05	62.26
TIRIGANIAQ	M11-1116	143.00	145.50	1025	6.43	6.43	2.53	2.50	6,988,481.78	538,650.05	62.26
TIRIGANIAQ	M11-1116	152.40	155.00	1000	0.49	0.49	2.63	2.60	6,988,481.78	538,650.05	62.26
TIRIGANIAQ	M11-1119	310.20	313.00	1100	0.34	0.34	2.49	2.80	6,988,599.21	539,059.80	72.27
TIRIGANIAQ	M11-1119	316.90	320.00	1050	1.30	1.30	2.76	3.10	6,988,599.21	539,059.80	72.27
TIRIGANIAQ	M11-1119	321.40	324.90	1025	0.67	0.67	3.12	3.50	6,988,599.21	539,059.80	72.27
TIRIGANIAQ	M11-1119	327.50	331.10	1000	14.50	14.50	3.22	3.60	6,988,599.21	539,059.80	72.27
TIRIGANIAQ	M11-1121	88.60	91.40	1102	2.99	2.99	2.83	2.80	6,988,445.19	540,130.01	66.57
TIRIGANIAQ	M11-1121	97.50	101.00	1100	0.13	0.13	3.54	3.50	6,988,445.19	540,130.01	66.57
TIRIGANIAQ	M11-1121	125.00	127.60	1075	0.03	0.03	2.63	2.60	6,988,445.19	540,130.01	66.57
TIRIGANIAQ	M11-1121	136.20	138.80	1050	0.14	0.14	2.63	2.60	6,988,445.19	540,130.01	66.57
TIRIGANIAQ	M11-1121	142.90	145.80	1025	3.22	3.22	2.94	2.90	6,988,445.19	540,130.01	66.57
TIRIGANIAQ	M11-1121	154.00	157.20	1000	0.78	0.78	3.24	3.20	6,988,445.19	540,130.01	66.57
TIRIGANIAQ	M11-1125	134.40	137.40	1050	0.37	0.37	3.13	3.00	6,988,444.79	540,130.04	66.92
TIRIGANIAQ	M11-1125	141.00	144.50	1025	0.76	0.76	3.66	3.50	6,988,444.79	540,130.04	66.92
TIRIGANIAQ	M11-1125	152.00	154.60	1000	3.11	3.11	2.73	2.60	6,988,444.79	540,130.04	66.92
TIRIGANIAQ	M11-1132	284.00	287.00	1170	1.53	1.53	2.81	3.00	6,988,650.74	539,149.94	66.88
TIRIGANIAQ	M11-1134	147.00	150.70	1000	14.98	14.98	3.78	3.70	6,988,438.61	540,089.89	65.93
TIRIGANIAQ	M11-1138	440.00	443.60	1251	0.21	0.21	3.05	3.60	6,988,751.49	538,790.08	66.66
TIRIGANIAQ	M11-1138	474.20	477.20	1100	0.26	0.26	2.60	3.00	6,988,751.49	538,790.08	66.66
TIRIGANIAQ	M11-1138	505.30	508.50	1050	0.04	0.04	2.84	3.20	6,988,751.49	538,790.08	66.66
TIRIGANIAQ	M11-1138	512.00	515.00	1025	6.20	6.20	2.68	3.00	6,988,751.49	538,790.08	66.66
TIRIGANIAQ	M11-1138	519.50	523.00	1015	1.38	1.38	3.15	3.50	6,988,751.49	538,790.08	66.66
TIRIGANIAQ	M11-1138	525.00	527.50	1000	3.30	3.30	2.26	2.50	6,988,751.49	538,790.08	66.66
TIRIGANIAQ	M11-1139A	439.20	442.20	1153	0.36	0.36	2.74	3.00	6,988,775.40	538,649.33	67.21
TIRIGANIAQ	M11-1139A	461.40	464.30	1100	8.61	8.61	2.68	2.90	6,988,775.40	538,649.33	67.21
TIRIGANIAQ	M11-1139A	467.00	469.80	1075	0.20	0.20	2.59	2.80	6,988,775.40	538,649.33	67.21
TIRIGANIAQ	M11-1139A	490.40	493.60	1050	8.71	8.71	3.00	3.20	6,988,775.40	538,649.33	67.21
TIRIGANIAQ	M11-1140A	311.00	314.00	1100	3.09	3.09	2.69	3.00	6,988,600.52	539,149.85	69.50
TIRIGANIAQ	M11-1140A	328.30	331.30	1025	0.06	0.06	2.71	3.00	6,988,600.52	539,149.85	69.50
TIRIGANIAQ	M11-1140A	343.00	346.60	1000	0.82	0.82	3.27	3.60	6,988,600.52	539,149.85	69.50
TIRIGANIAQ	M11-1141	99.30	101.90	1102	4.61	4.61	2.70	2.60	6,988,434.94	539,600.94	78.50
TIRIGANIAQ	M11-1141	99.30	105.00	1100	26.05	26.05	5.92	5.70	6,988,434.94	539,600.94	78.50
TIRIGANIAQ	M11-1141	104.70	107.00	1087	15.49	15.49	2.39	2.30	6,988,434.94	539,600.94	78.50
TIRIGANIAQ	M11-1145	76.10	79.30	1102	0.13	0.13	3.30	3.20	6,988,432.85	540,169.85	66.93
TIRIGANIAQ	M11-1145	80.70	84.30	1100	0.07	0.07	3.72	3.60	6,988,432.85	540,169.85	66.93
TIRIGANIAQ	M11-1145	108.40	112.00	1075	8.97	8.97	3.75	3.60	6,988,432.85	540,169.85	66.93
TIRIGANIAQ	M11-1145	119.00	122.30	1050	0.74	0.74	3.44	3.30	6,988,432.85	540,169.85	66.93
TIRIGANIAQ	M11-1145	129.40	132.00	1025	0.53	0.53	2.71	2.60	6,988,432.85	540,169.85	66.93
TIRIGANIAQ	M11-1145	144.50	147.00	1000	16.74	16.74	2.61	2.50	6,988,432.85	540,169.85	66.93
TIRIGANIAQ	M11-1151	94.80	96.70	1102	5.88	5.88	1.98	1.90	6,988,432.05	539,556.03	78.86
TIRIGANIAQ	M11-1151	96.70	100.90	1100	16.29	16.29	4.39	4.20	6,988,432.05	539,556.03	78.86
TIRIGANIAQ	M11-1156	141.00	144.20	1000	12.86	12.86	3.27	3.20	6,988,432.21	540,152.94	66.87
TIRIGANIAQ	M11-1158	395.00	398.00	1000	0.34	0.34	2.57	3.00	6,988,633.36	540,399.91	67.51
TIRIGANIAQ	M11-1160	97.00	99.40	1102	15.65	15.65	2.46	2.40	6,988,432.50	539,508.12	77.06
TIRIGANIAQ	M11-1160	99.70	102.50	1100	1.62	1.62	2.87	2.80	6,988,432.50	539,508.12	77.06
TIRIGANIAQ	M11-1161	376.70	379.60	1154	1.44	1.44	2.67	2.90	6,988,691.97	540,115.02	66.32
TIRIGANIAQ	M11-1161	379.70	386.70	1100	14.42	14.42	6.46	7.00	6,988,691.97	540,115.02	66.32
TIRIGANIAQ	M11-1161	381.00	383.70	1153	6.49	6.49	2.49	2.70	6,988,691.97	540,115.02	66.32
TIRIGANIAQ	M11-1161	394.40	398.00	1087	0.30	0.30	3.33	3.60	6,988,691.97	540,115.02	66.32
TIRIGANIAQ	M11-1161	400.00	403.00	1075	3.05	3.05	2.78	3.00	6,988,691.97	540,115.02	66.32
TIRIGANIAQ	M11-1161	404.00	407.00	1050	5.52	5.52	2.78	3.00	6,988,691.97	540,115.02	66.32
TIRIGANIAQ	M11-1161	414.10	417.50	1025	35.48	35.48	3.16	3.40	6,988,691.97	540,115.02	66.32
TIRIGANIAQ	M11-1161	421.30	424.40	1000	1.01	1.01	2.88	3.10	6,988,691.97	540,115.02	66.32
TIRIGANIAQ	M11-1171	179.40	182.80	1254	0.03	0.03	2.98	3.40	6,988,612.44	540,398.75	67.45
TIRIGANIAQ	M11-1171	280.30	284.00	1100	0.03	0.03	3.29	3.70	6,988,612.44	540,398.75	67.45
TIRIGANIAQ	M11-1171	289.10	292.70	1087	0.07	0.07	3.21	3.60	6,988,612.44	540,398.75	67.45
TIRIGANIAQ	M11-1171	295.20	298.70	1075	0.17	0.17	3.13	3.50	6,988,612.44	540,398.75	67.45
TIRIGANIAQ	M11-1171	319.80	326.00	1050	6.24	6.24	5.58	6.20	6,988,612.44	540,398.75	67.45
TIRIGANIAQ	M11-1171	344.00	349.00	1000	0.35	0.35	4.54	5.00	6,988,612.44	540,398.75	67.45
TIRIGANIAQ	M11-1173	38.00	41.00	1540	0.22	0.22	2.97	3.00	6,988,691.51	540,115.27	66.92
TIRIGANIAQ	M11-1173	235.50	238.20	1254	0.29	0.29	2.74	2.70	6,988,691.51	540,115.27	66.92
TIRIGANIAQ	M11-1173	249.10	253.30	1257	5.25	5.25	4.28	4.20	6,988,691.51	540,115.27	66.92
TIRIGANIAQ	M11-1173	260.10	265.60	1262	20.33	20.33	5.61	5.50	6,988,691.51	540,115.27	66.92
TIRIGANIAQ	M11-1173	294.50	298.00	1155	0.03	0.03	3.60	3.50	6,988,691.51	540,115.27	66.92
TIRIGANIAQ	M11-1173	314.00	317.50	1153	0.64	0.64	3.61	3.50	6,988,691.51	540,115.27	66.92
TIRIGANIAQ	M11-1173	325.00	328.90	1100	2.44	2.44	4.04	3.90	6,988,691.51	540,115.27	66.92
TIRIGANIAQ	M11-1173	354.50	357.80	1050	0.55	0.55	3.44	3.30	6,988,691.51	540,115.27	66.92
TIRIGANIAQ	M11-1173	365.20	368.00	1025	3.26	3.26	2.92	2.80	6,988,691.51	540,115.27	66.92
TIRIGANIAQ	M11-1178	186.70	190.50	1254	1.06	1.06	3.93	3.80	6,988,632.01	540,400.29	67.13
TIRIGANIAQ	M11-1178	202.40	205.00	1257	0.42	0.42	2.69	2.60	6,988,632.01	540,400.29	67.13
TIRIGANIAQ	M11-1178	210.00	213.00	1258	1.06	1.06	3.11	3.00	6,988,632.01	540,400.29	67.13
TIRIGANIAQ	M11-1178	227.40	230.60	1251	1.88	1.88	3.32	3.20	6,988,632.01	540,400.29	67.13
TIRIGANIAQ	M11-1178	255.00	257.60	1100	2.24	2.24	2.70	2.60	6,988,632.01	540,400.29	67.13
TIRIGANIAQ	M11-1178	264.60	267.00	1087	0.29	0.29	2.49	2.40	6,988,632.01	540,400.29	67.13
TIRIGANIAQ	M11-1178	292.00	294.40	1050	0.60	0.60	2.50	2.40	6,988,632.01	540,400.29	67.13
TIRIGANIAQ	M11-1178	321.00	323.30	1000	0.18	0.18	2.40	2.30	6,988,632.01	540,400.29	67.13
TIRIGANIAQ	M11-1180	118.30	121.00	1254	0.20	0.20	2.54	2.70	6,988,520.94	540,695.47	70.57
TIRIGANIAQ	M11-1180	124.90	128.00	1257	1.46	1.46	2.94	3.10	6,988,520.94	540,695.47	70.57
TIRIGANIAQ	M11-1180	155.80	159.60	1155	0.62	0.62	3.64	3.80	6,988,520.94	540,695.47	70.57
TIRIGANIAQ	M11-1180	170.10	173.20	1100	1.05	1.05	3.00	3.10	6,988,520.94	540,695.47	70.57
TIRIGANIAQ	M11-1180	176.60	179.00	1075	1.35	1.35	2.34	2.40	6,988,520.94	540,695.47	70.57
TIRIGANIAQ	M11-1180	200.00	203.00	1050	0.77	0.77	2.99	3.00	6,988,520.94	540,695.47	70.57
TIRIGANIAQ	M11-1180	242.80	246.00	1000	1.38	1.38	3.24	3.20	6,988,520.94	540,695.47	70.57
TIRIGANIAQ	M11-1181	216.40	219.10	1254	19.90	19.90	2.62	2.70	6,988,637.80	540,500.03	70.89
TIRIGANIAQ	M11-1181	230.00	232.70	1257	4.01	4.01	2.63	2.70	6,988,637.80	540,500.03	70.89
TIRIGANIAQ	M11-1181	280.50	283.00	1100	0.17	0.17	2.44	2.50	6,988,637.80	540,500.03	70.89
TIRIGANIAQ	M11-1181	302.10	306.70	1075	11.00	11.00	4.49	4.60	6,988,637.80	540,500.03	70.89
TIRIGANIAQ	M11-1181	308.00	310.90	1050	2.10	2.10	2.83	2.90	6,988,637.80	540,500.03	70.89
TIRIGANIAQ	M11-1185	301.00	306.60	1153	0.13	0.13	5.08	5.60	6,988,674.85	539,479.94	76.44

TIRIGANIAQ	M11-1185	340.40	344.00	1152	1.75	1.75	3.32	3.60	6,988,674.85	539,479.94	76.44
TIRIGANIAQ	M11-1185	352.00	354.60	1100	1.51	1.51	2.40	2.60	6,988,674.85	539,479.94	76.44
TIRIGANIAQ	M11-1185	363.20	366.20	1075	3.95	3.95	2.78	3.00	6,988,674.85	539,479.94	76.44
TIRIGANIAQ	M11-1185	382.40	385.30	1025	0.91	0.91	2.69	2.90	6,988,674.85	539,479.94	76.44
TIRIGANIAQ	M11-1185	393.50	396.00	1000	0.18	0.18	2.32	2.50	6,988,674.85	539,479.94	76.44
TIRIGANIAQ	M11-1186	254.80	258.80	1155	0.03	0.03	3.47	4.00	6,988,615.34	539,990.08	67.44
TIRIGANIAQ	M11-1186	282.50	285.60	1153	0.79	0.79	2.72	3.10	6,988,615.34	539,990.08	67.44
TIRIGANIAQ	M11-1186	291.90	298.00	1152	3.89	3.89	5.38	6.10	6,988,615.34	539,990.08	67.44
TIRIGANIAQ	M11-1186	299.60	302.90	1100	2.97	2.97	2.91	3.30	6,988,615.34	539,990.08	67.44
TIRIGANIAQ	M11-1186	306.00	309.00	1087	3.45	3.45	2.65	3.00	6,988,615.34	539,990.08	67.44
TIRIGANIAQ	M11-1186	320.00	323.00	1075	0.06	0.06	2.66	3.00	6,988,615.34	539,990.08	67.44
TIRIGANIAQ	M11-1186	324.00	327.00	1050	2.37	2.37	2.66	3.00	6,988,615.34	539,990.08	67.44
TIRIGANIAQ	M11-1186	332.40	335.00	1025	1.52	1.52	2.31	2.60	6,988,615.34	539,990.08	67.44
TIRIGANIAQ	M11-1186	340.40	343.00	1000	9.01	9.01	2.31	2.60	6,988,615.34	539,990.08	67.44
TIRIGANIAQ	M11-1187	105.40	108.80	1254	3.28	3.28	3.53	3.40	6,988,520.36	540,695.50	70.56
TIRIGANIAQ	M11-1187	111.00	113.60	1257	4.78	4.78	2.70	2.60	6,988,520.36	540,695.50	70.56
TIRIGANIAQ	M11-1187	119.00	124.00	1251	2.33	2.33	5.21	5.00	6,988,520.36	540,695.50	70.56
TIRIGANIAQ	M11-1187	126.00	129.00	1155	2.16	2.16	3.13	3.00	6,988,520.36	540,695.50	70.56
TIRIGANIAQ	M11-1187	143.30	146.00	1100	0.93	0.93	2.82	2.70	6,988,520.36	540,695.50	70.56
TIRIGANIAQ	M11-1187	157.70	160.30	1075	1.17	1.17	2.72	2.60	6,988,520.36	540,695.50	70.56
TIRIGANIAQ	M11-1187	180.00	182.50	1050	4.48	4.48	2.62	2.50	6,988,520.36	540,695.50	70.56
TIRIGANIAQ	M11-1187	187.70	191.00	1025	2.51	2.51	3.47	3.30	6,988,520.36	540,695.50	70.56
TIRIGANIAQ	M11-1187	223.00	225.60	1000	0.10	0.10	2.76	2.60	6,988,520.36	540,695.50	70.56
TIRIGANIAQ	M11-1191	429.70	431.90	1075	0.03	0.03	2.17	2.20	6,988,774.78	538,649.32	67.18
TIRIGANIAQ	M11-1192	165.70	168.80	1254	0.14	0.14	2.74	3.10	6,988,565.44	540,787.83	65.87
TIRIGANIAQ	M11-1192	234.40	237.60	1075	0.42	0.42	2.90	3.20	6,988,565.44	540,787.83	65.87
TIRIGANIAQ	M11-1192	254.00	257.00	1025	1.57	1.57	2.74	3.00	6,988,565.44	540,787.83	65.87
TIRIGANIAQ	M11-1192	305.00	307.80	1000	6.08	6.08	2.60	2.80	6,988,565.44	540,787.83	65.87
TIRIGANIAQ	M11-1194	213.00	215.60	1155	0.03	0.03	2.61	2.60	6,988,614.66	539,990.08	67.38
TIRIGANIAQ	M11-1194	228.30	231.00	1154	1.52	1.52	2.72	2.70	6,988,614.66	539,990.08	67.38
TIRIGANIAQ	M11-1194	238.10	241.20	1153	1.58	1.58	3.12	3.10	6,988,614.66	539,990.08	67.38
TIRIGANIAQ	M11-1194	264.20	266.40	1100	7.51	7.51	2.23	2.20	6,988,614.66	539,990.08	67.38
TIRIGANIAQ	M11-1194	271.40	274.00	1087	0.56	0.56	2.64	2.60	6,988,614.66	539,990.08	67.38
TIRIGANIAQ	M11-1194	276.00	278.80	1075	3.19	3.19	2.85	2.80	6,988,614.66	539,990.08	67.38
TIRIGANIAQ	M11-1194	285.40	288.00	1050	1.30	1.30	2.65	2.60	6,988,614.66	539,990.08	67.38
TIRIGANIAQ	M11-1194	292.70	295.00	1025	4.35	4.35	2.35	2.30	6,988,614.66	539,990.08	67.38
TIRIGANIAQ	M11-1194	302.00	304.50	1000	2.99	2.99	2.55	2.50	6,988,614.66	539,990.08	67.38
TIRIGANIAQ	M11-1199	265.20	268.10	1153	0.04	0.04	2.92	2.90	6,988,674.48	539,480.26	76.58
TIRIGANIAQ	M11-1199	331.10	334.20	1100	0.55	0.55	3.14	3.10	6,988,674.48	539,480.26	76.58
TIRIGANIAQ	M11-1201	42.40	44.70	1510	3.91	3.91	2.00	2.30	6,988,635.04	539,739.96	68.69
TIRIGANIAQ	M11-1201	254.50	256.90	1154	1.17	1.17	2.16	2.40	6,988,635.04	539,739.96	68.69
TIRIGANIAQ	M11-1201	268.30	272.00	1153	0.62	0.62	3.35	3.70	6,988,635.04	539,739.96	68.69
TIRIGANIAQ	M11-1201	285.90	289.00	1152	0.46	0.46	2.81	3.10	6,988,635.04	539,739.96	68.69
TIRIGANIAQ	M11-1201	292.10	298.60	1151	10.60	10.60	5.89	6.50	6,988,635.04	539,739.96	68.69
TIRIGANIAQ	M11-1201	300.40	304.30	1100	32.05	32.05	3.54	3.90	6,988,635.04	539,739.96	68.69
TIRIGANIAQ	M11-1201	311.40	314.00	1087	1.72	1.72	2.37	2.60	6,988,635.04	539,739.96	68.69
TIRIGANIAQ	M11-1201	345.90	349.10	1000	2.15	2.15	2.93	3.20	6,988,635.04	539,739.96	68.69
TIRIGANIAQ	M11-1202	154.30	157.20	1254	1.40	1.40	2.89	2.90	6,988,564.95	540,787.86	65.65
TIRIGANIAQ	M11-1202	189.90	193.00	1155	2.23	2.23	3.10	3.10	6,988,564.95	540,787.86	65.65
TIRIGANIAQ	M11-1202	196.80	199.80	1100	1.36	1.36	3.00	3.00	6,988,564.95	540,787.86	65.65
TIRIGANIAQ	M11-1202	207.80	210.40	1075	7.66	7.66	2.60	2.60	6,988,564.95	540,787.86	65.65
TIRIGANIAQ	M11-1202	218.60	221.20	1050	1.79	1.79	2.60	2.60	6,988,564.95	540,787.86	65.65
TIRIGANIAQ	M11-1202	272.00	274.70	1000	0.03	0.03	2.72	2.70	6,988,564.95	540,787.86	65.65
TIRIGANIAQ	M11-1203	399.00	403.10	1153	1.52	1.52	3.66	4.10	6,988,719.87	538,830.05	67.26
TIRIGANIAQ	M11-1203	442.00	444.70	1100	0.97	0.97	2.46	2.70	6,988,719.87	538,830.05	67.26
TIRIGANIAQ	M11-1204	366.50	368.70	1100	0.11	0.11	2.19	2.20	6,988,696.54	539,219.95	69.28
TIRIGANIAQ	M11-1204	384.80	387.50	1025	0.03	0.03	2.69	2.70	6,988,696.54	539,219.95	69.28
TIRIGANIAQ	M11-1204	390.60	393.20	1000	0.15	0.15	2.59	2.60	6,988,696.54	539,219.95	69.28
TIRIGANIAQ	M11-1211	43.30	45.90	1510	2.44	2.44	1.45	2.60	6,988,635.84	539,739.97	68.39
TIRIGANIAQ	M11-1211	312.40	315.70	1263	0.25	0.25	1.86	3.30	6,988,635.84	539,739.97	68.39
TIRIGANIAQ	M11-1211	322.20	329.00	1256	11.63	11.63	3.86	6.80	6,988,635.84	539,739.97	68.39
TIRIGANIAQ	M11-1211	345.50	351.20	1255	2.85	2.85	3.29	5.70	6,988,635.84	539,739.97	68.39
TIRIGANIAQ	M11-1211	354.60	364.60	1252	2.34	2.34	5.81	10.00	6,988,635.84	539,739.97	68.39
TIRIGANIAQ	M11-1211	380.00	386.80	1251	1.29	1.29	4.06	6.80	6,988,635.84	539,739.97	68.39
TIRIGANIAQ	M11-1211	424.00	428.00	1154	1.23	1.23	2.41	4.00	6,988,635.84	539,739.97	68.39
TIRIGANIAQ	M11-1211	430.00	434.40	1153	0.64	0.64	2.65	4.40	6,988,635.84	539,739.97	68.39
TIRIGANIAQ	M11-1211	436.00	440.00	1100	0.87	0.87	2.42	4.00	6,988,635.84	539,739.97	68.39
TIRIGANIAQ	M11-1214	191.00	193.70	1100	8.44	8.44	2.83	2.70	6,988,629.06	538,250.03	59.16
TIRIGANIAQ	M11-1216	315.20	318.60	1150	0.63	0.63	3.12	3.40	6,988,696.77	539,219.97	69.18
TIRIGANIAQ	M11-1216	321.80	325.50	1152	3.20	3.20	3.40	3.70	6,988,696.77	539,219.97	69.18
TIRIGANIAQ	M11-1216	383.00	385.20	1100	0.82	0.82	2.04	2.20	6,988,696.77	539,219.97	69.18
TIRIGANIAQ	M11-1216	407.00	410.00	1025	1.00	1.00	2.78	3.00	6,988,696.77	539,219.97	69.18
TIRIGANIAQ	M11-1216	412.90	415.60	1015	6.73	6.73	2.51	2.70	6,988,696.77	539,219.97	69.18
TIRIGANIAQ	M11-1216	417.40	420.50	1000	3.23	3.23	2.88	3.10	6,988,696.77	539,219.97	69.18
TIRIGANIAQ	M11-1221	175.00	178.60	1050	1.09	1.09	3.46	3.60	6,988,531.88	538,597.14	61.49
TIRIGANIAQ	M11-1224	251.50	254.50	1152	0.48	0.48	3.03	3.00	6,988,634.38	539,739.91	68.57
TIRIGANIAQ	M11-1224	267.30	271.00	1151	1.11	1.11	3.75	3.70	6,988,634.38	539,739.91	68.57
TIRIGANIAQ	M11-1224	285.30	288.40	1100	8.56	8.56	3.15	3.10	6,988,634.38	539,739.91	68.57
TIRIGANIAQ	M11-1224	302.30	305.00	1050	0.68	0.68	2.75	2.70	6,988,634.38	539,739.91	68.57
TIRIGANIAQ	M11-1224	315.90	318.60	1000	0.16	0.16	2.76	2.70	6,988,634.38	539,739.91	68.57
TIRIGANIAQ	M11-1225	351.50	354.30	1100	3.52	3.52	2.89	2.80	6,988,696.06	539,219.73	68.99
TIRIGANIAQ	M11-1225	370.40	373.60	1000	0.03	0.03	3.31	3.20	6,988,696.06	539,219.73	68.99
TIRIGANIAQ	M11-1227	157.50	160.30	1050	0.34	0.34	3.04	2.80	6,988,531.31	538,597.08	61.49
TIRIGANIAQ	M11-1227	163.30	167.00	1025	7.23	7.23	4.02	3.70	6,988,531.31	538,597.08	61.49
TIRIGANIAQ	M11-1227	172.00	177.00	1000	3.64	3.64	5.44	5.00	6,988,531.31	538,597.08	61.49
TIRIGANIAQ	M11-1232	200.40	204.00	1050	2.71	2.71	3.15	3.60	6,988,532.33	538,597.14	61.47
TIRIGANIAQ	M11-1234	143.00	146.20	1254	0.03	0.03	2.73	3.20	6,988,549.01	540,544.81	69.26
TIRIGANIAQ	M11-1234	152.00	155.00	1257	0.13	0.13	2.56	3.00	6,988,549.01	540,544.81	69.26
TIRIGANIAQ	M11-1234	209.80	212.50	1100	0.03	0.03	2.35	2.70	6,988,549.01	540,544.81	69.26
TIRIGANIAQ	M11-1234	214.80	217.80	1087	0.10	0.10	2.61	3.00	6,988,549.01	540,544.81	69.26

TIRIGANIAQ	M11-1234	228.50	232.60	1075	1.12	1.12	3.59	4.10	6,988,549.01	540,544.81	69.26
TIRIGANIAQ	M11-1234	240.00	243.00	1050	0.08	0.08	2.63	3.00	6,988,549.01	540,544.81	69.26
TIRIGANIAQ	M11-1236	348.70	351.80	1260	0.39	0.39	2.53	3.10	6,988,749.27	539,585.19	71.73
TIRIGANIAQ	M11-1236	358.30	362.00	1253	0.13	0.13	3.02	3.70	6,988,749.27	539,585.19	71.73
TIRIGANIAQ	M11-1236	376.00	380.00	1256	6.44	6.44	3.30	4.00	6,988,749.27	539,585.19	71.73
TIRIGANIAQ	M11-1236	385.00	396.00	1255	4.76	4.76	9.08	11.00	6,988,749.27	539,585.19	71.73
TIRIGANIAQ	M11-1236	398.50	403.00	1252	6.37	6.37	3.72	4.50	6,988,749.27	539,585.19	71.73
TIRIGANIAQ	M11-1236	421.00	425.00	1155	0.03	0.03	3.32	4.00	6,988,749.27	539,585.19	71.73
TIRIGANIAQ	M11-1236	462.40	465.60	1100	10.61	10.61	2.67	3.20	6,988,749.27	539,585.19	71.73
TIRIGANIAQ	M11-1236	472.40	475.60	1075	0.80	0.80	2.67	3.20	6,988,749.27	539,585.19	71.73
TIRIGANIAQ	M11-1236	482.00	485.00	1050	2.62	2.62	2.51	3.00	6,988,749.27	539,585.19	71.73
TIRIGANIAQ	M11-1236	489.40	493.60	1025	0.08	0.08	3.52	4.20	6,988,749.27	539,585.19	71.73
TIRIGANIAQ	M11-1236	499.00	503.00	1015	6.10	6.10	3.36	4.00	6,988,749.27	539,585.19	71.73
TIRIGANIAQ	M11-1236	507.70	512.00	1000	0.50	0.50	3.62	4.30	6,988,749.27	539,585.19	71.73
TIRIGANIAQ	M11-1241	128.50	132.10	1254	0.08	0.08	3.47	3.60	6,988,548.64	540,544.82	69.29
TIRIGANIAQ	M11-1241	138.80	141.80	1257	2.59	2.59	2.91	3.00	6,988,548.64	540,544.82	69.29
TIRIGANIAQ	M11-1241	166.00	169.80	1251	0.36	0.36	3.71	3.80	6,988,548.64	540,544.82	69.29
TIRIGANIAQ	M11-1241	176.60	179.80	1155	0.90	0.90	3.14	3.20	6,988,548.64	540,544.82	69.29
TIRIGANIAQ	M11-1241	185.50	188.50	1100	0.59	0.59	2.95	3.00	6,988,548.64	540,544.82	69.29
TIRIGANIAQ	M11-1241	193.60	196.10	1087	8.68	8.68	2.46	2.50	6,988,548.64	540,544.82	69.29
TIRIGANIAQ	M11-1241	205.40	208.00	1075	0.41	0.41	2.57	2.60	6,988,548.64	540,544.82	69.29
TIRIGANIAQ	M11-1241	224.50	227.50	1050	9.31	9.31	2.98	3.00	6,988,548.64	540,544.82	69.29
TIRIGANIAQ	M11-1241	259.00	262.00	1000	0.33	0.33	3.01	3.00	6,988,548.64	540,544.82	69.29
TIRIGANIAQ	M11-1248	327.20	329.70	1100	0.03	0.03	2.51	2.50	6,988,679.71	540,340.00	66.02
TIRIGANIAQ	M11-1248	332.40	335.80	1087	1.69	1.69	3.42	3.40	6,988,679.71	540,340.00	66.02
TIRIGANIAQ	M11-1248	340.00	343.00	1075	0.03	0.03	3.03	3.00	6,988,679.71	540,340.00	66.02
TIRIGANIAQ	M11-1248	349.00	351.60	1050	0.22	0.22	2.65	2.60	6,988,679.71	540,340.00	66.02
TIRIGANIAQ	M11-1248	375.60	378.40	1000	0.21	0.21	2.88	2.80	6,988,679.71	540,340.00	66.02
TIRIGANIAQ	M11-1251	357.50	361.60	1155	1.28	1.28	3.88	4.10	6,988,748.92	539,585.49	71.69
TIRIGANIAQ	M11-1251	363.40	372.80	1154	5.41	5.41	8.91	9.40	6,988,748.92	539,585.49	71.69
TIRIGANIAQ	M11-1251	376.40	382.20	1153	18.92	18.92	5.50	5.80	6,988,748.92	539,585.49	71.69
TIRIGANIAQ	M11-1251	387.40	391.00	1150	1.69	1.69	3.41	3.60	6,988,748.92	539,585.49	71.69
TIRIGANIAQ	M11-1251	395.00	398.30	1152	1.83	1.83	3.13	3.30	6,988,748.92	539,585.49	71.69
TIRIGANIAQ	M11-1251	407.20	409.50	1151	2.00	2.00	2.18	2.30	6,988,748.92	539,585.49	71.69
TIRIGANIAQ	M11-1251	416.00	419.00	1100	0.39	0.39	2.85	3.00	6,988,748.92	539,585.49	71.69
TIRIGANIAQ	M11-1251	432.50	434.80	1075	0.12	0.12	2.20	2.30	6,988,748.92	539,585.49	71.69
TIRIGANIAQ	M11-1251	440.80	443.00	1050	0.46	0.46	2.11	2.20	6,988,748.92	539,585.49	71.69
TIRIGANIAQ	M11-1251	445.00	447.60	1025	1.15	1.15	2.50	2.60	6,988,748.92	539,585.49	71.69
TIRIGANIAQ	M11-1251	452.40	455.00	1015	0.13	0.13	2.51	2.60	6,988,748.92	539,585.49	71.69
TIRIGANIAQ	M11-1251	453.00	455.80	1000	0.14	0.14	2.71	2.80	6,988,748.92	539,585.49	71.69
TIRIGANIAQ	M11-1259	214.80	217.60	1254	5.30	5.30	2.94	2.80	6,988,679.12	540,339.64	65.82
TIRIGANIAQ	M11-1259	305.60	307.80	1100	0.05	0.05	2.34	2.20	6,988,679.12	540,339.64	65.82
TIRIGANIAQ	M11-1259	325.40	328.30	1050	0.03	0.03	3.09	2.90	6,988,679.12	540,339.64	65.82
TIRIGANIAQ	M11-1259	339.60	342.00	1025	0.95	0.95	2.56	2.40	6,988,679.12	540,339.64	65.82
TIRIGANIAQ	M11-1259	347.50	350.00	1000	1.41	1.41	2.67	2.50	6,988,679.12	540,339.64	65.82
TIRIGANIAQ	M11-1260	258.00	261.00	1050	1.66	1.66	2.54	3.00	6,988,555.29	538,733.12	65.61
TIRIGANIAQ	M11-1266	165.20	167.80	1153	0.05	0.05	2.43	2.60	6,988,529.43	540,039.92	66.79
TIRIGANIAQ	M11-1266	196.60	199.50	1100	1.43	1.43	2.72	2.90	6,988,529.43	540,039.92	66.79
TIRIGANIAQ	M11-1266	222.00	224.30	1050	23.00	23.00	2.17	2.30	6,988,529.43	540,039.92	66.79
TIRIGANIAQ	M11-1266	232.50	235.50	1025	1.25	1.25	2.84	3.00	6,988,529.43	540,039.92	66.79
TIRIGANIAQ	M11-1266	245.30	249.00	1000	0.43	0.43	3.51	3.70	6,988,529.43	540,039.92	66.79
TIRIGANIAQ	M11-1268	272.20	275.10	1170	17.19	17.19	2.43	2.90	6,988,600.19	538,999.93	72.45
TIRIGANIAQ	M11-1268	328.80	332.00	1100	0.57	0.57	2.78	3.20	6,988,600.19	538,999.93	72.45
TIRIGANIAQ	M11-1268	339.00	342.00	1025	1.49	1.49	2.63	3.00	6,988,600.19	538,999.93	72.45
TIRIGANIAQ	M11-1268	349.60	354.50	1000	10.88	10.88	4.33	4.90	6,988,600.19	538,999.93	72.45
TIRIGANIAQ	M11-1270	223.90	228.00	1050	1.09	1.09	3.93	4.10	6,988,554.47	538,733.13	65.35
TIRIGANIAQ	M11-1270	231.00	235.50	1025	2.08	2.08	4.33	4.50	6,988,554.47	538,733.13	65.35
TIRIGANIAQ	M11-1270	237.00	240.00	1000	5.15	5.15	2.90	3.00	6,988,554.47	538,733.13	65.35
TIRIGANIAQ	M11-1272	238.90	241.80	1100	3.96	3.96	2.85	2.90	6,988,570.50	539,599.97	74.94
TIRIGANIAQ	M11-1272	276.80	280.03	1000	0.04	0.04	3.19	3.23	6,988,570.50	539,599.97	74.94
TIRIGANIAQ	M11-1273	238.50	241.50	1100	0.10	0.10	2.78	3.00	6,988,549.96	538,880.14	65.73
TIRIGANIAQ	M11-1273	250.50	253.50	1050	0.21	0.21	2.79	3.00	6,988,549.96	538,880.14	65.73
TIRIGANIAQ	M11-1273	258.00	261.00	1025	0.32	0.32	2.80	3.00	6,988,549.96	538,880.14	65.73
TIRIGANIAQ	M11-1273	262.50	265.50	1000	9.30	9.30	2.81	3.00	6,988,549.96	538,880.14	65.73
TIRIGANIAQ	M11-1277	442.80	446.30	1100	1.73	1.73	3.49	3.50	6,988,820.19	538,500.05	69.00
TIRIGANIAQ	M11-1277	463.00	466.00	1075	13.35	13.35	3.00	3.00	6,988,820.19	538,500.05	69.00
TIRIGANIAQ	M11-1278A	274.50	277.50	1100	0.07	0.07	3.02	3.00	6,988,599.74	538,999.96	72.21
TIRIGANIAQ	M11-1278A	292.00	294.80	1050	1.50	1.50	2.82	2.80	6,988,599.74	538,999.96	72.21
TIRIGANIAQ	M11-1278A	295.50	298.50	1025	3.88	3.88	3.02	3.00	6,988,599.74	538,999.96	72.21
TIRIGANIAQ	M11-1278A	298.50	303.00	1000	1.15	1.15	4.53	4.50	6,988,599.74	538,999.96	72.21
TIRIGANIAQ	M11-1282	222.40	225.20	1100	0.44	0.44	2.87	2.80	6,988,549.17	538,880.10	65.77
TIRIGANIAQ	M11-1282	228.80	231.30	1025	5.03	5.03	2.56	2.50	6,988,549.17	538,880.10	65.77
TIRIGANIAQ	M11-1282	235.40	238.80	1000	0.36	0.36	3.49	3.40	6,988,549.17	538,880.10	65.77
TIRIGANIAQ	M11-1289	615.00	618.00	1015	0.52	0.52	2.98	3.00	6,988,850.24	539,506.38	73.30
TIRIGANIAQ	M11-1289	627.00	629.70	1000	3.22	3.22	2.70	2.70	6,988,850.24	539,506.38	73.30
TIRIGANIAQ	M11-1290	143.30	146.30	1100	5.76	5.76	2.82	3.00	6,988,472.34	539,275.66	72.99
TIRIGANIAQ	M11-1290	175.70	178.50	1000	0.14	0.14	2.66	2.80	6,988,472.34	539,275.66	72.99
TIRIGANIAQ	M11-1291	66.50	69.50	1157	0.31	0.31	2.78	3.00	6,988,447.66	538,923.81	65.37
TIRIGANIAQ	M11-1291	131.80	135.50	1100	0.79	0.79	3.50	3.70	6,988,447.66	538,923.81	65.37
TIRIGANIAQ	M11-1293	101.80	104.00	1156	0.19	0.19	2.31	2.20	6,988,471.80	539,275.60	73.42
TIRIGANIAQ	M11-1293	127.30	130.00	1100	0.75	0.75	2.84	2.70	6,988,471.80	539,275.60	73.42
TIRIGANIAQ	M11-1293	146.00	148.30	1025	0.09	0.09	2.43	2.30	6,988,471.80	539,275.60	73.42
TIRIGANIAQ	M11-1293	156.00	158.60	1000	0.11	0.11	2.74	2.60	6,988,471.80	539,275.60	73.42
TIRIGANIAQ	M11-1296	66.00	69.30	1157	2.70	2.70	3.42	3.30	6,988,448.00	538,924.00	65.00
TIRIGANIAQ	M11-1296	115.50	118.50	1102	1.81	1.81	3.13	3.00	6,988,448.00	538,924.00	65.00
TIRIGANIAQ	M11-1296	120.30	124.30	1100	3.18	3.18	4.17	4.00	6,988,448.00	538,924.00	65.00
TIRIGANIAQ	M11-1299	164.40	167.40	1100	0.37	0.37	3.11	3.00	6,988,493.64	539,100.21	74.06
TIRIGANIAQ	M11-1301	586.00	589.00	1025	0.33	0.33	2.46	3.00	6,988,820.19	538,499.98	69.32
TIRIGANIAQ	M11-1304	281.70	285.20	1170	0.00	0.00	3.25	3.50	6,988,638.52	539,094.15	68.20
TIRIGANIAQ	M11-1304	335.50	338.10	1100	0.65	0.65	2.47	2.60	6,988,638.52	539,094.15	68.20

TIRIGANIAQ	M11-1304	340.50	343.50	1050	0.09	0.09	2.85	3.00	6,988,638.52	539,094.15	68.20
TIRIGANIAQ	M11-1304	344.50	348.10	1025	1.19	1.19	3.43	3.60	6,988,638.52	539,094.15	68.20
TIRIGANIAQ	M11-1304	348.50	356.20	1000	22.14	22.14	7.35	7.70	6,988,638.52	539,094.15	68.20
TIRIGANIAQ	M11-1307	702.50	705.00	1015	8.02	8.02	2.27	2.50	6,988,850.39	539,506.49	72.39
TIRIGANIAQ	M11-1314	324.00	326.50	1100	2.69	2.69	2.59	2.50	6,988,638.34	539,094.15	68.35
TIRIGANIAQ	M11-1314	327.40	330.00	1050	31.06	33.56	2.69	2.60	6,988,638.34	539,094.15	68.35
TIRIGANIAQ	M11-1314	332.00	334.60	1025	0.26	0.26	2.70	2.60	6,988,638.34	539,094.15	68.35
TIRIGANIAQ	M11-1314	335.40	338.00	1000	0.39	0.39	2.70	2.60	6,988,638.34	539,094.15	68.35
TIRIGANIAQ	M11-1316	223.00	225.80	1100	0.69	0.69	2.58	2.80	6,988,528.76	539,151.50	73.77
TIRIGANIAQ	M11-1316	239.00	242.00	1000	5.51	5.51	2.77	3.00	6,988,528.76	539,151.50	73.77
TIRIGANIAQ	M11-1329A	153.00	155.50	1156	4.90	4.90	2.49	2.50	6,988,528.32	539,151.52	73.74
TIRIGANIAQ	M11-1333	395.50	399.00	1252	9.78	9.78	2.49	3.50	6,988,680.35	538,920.54	70.20
TIRIGANIAQ	M11-1333	406.00	410.30	1153	0.03	0.03	3.06	4.30	6,988,680.35	538,920.54	70.20
TIRIGANIAQ	M11-1335	46.00	49.40	1154	0.03	0.03	3.53	3.40	6,988,424.52	540,500.00	68.44
TIRIGANIAQ	M11-1335	58.10	63.60	1100	0.31	0.31	5.71	5.50	6,988,424.52	540,500.00	68.44
TIRIGANIAQ	M11-1335	67.00	69.60	1087	0.49	0.49	2.70	2.60	6,988,424.52	540,500.00	68.44
TIRIGANIAQ	M11-1335	80.40	82.80	1075	0.79	0.79	2.50	2.40	6,988,424.52	540,500.00	68.44
TIRIGANIAQ	M11-1335	94.50	97.50	1050	1.98	1.98	3.14	3.00	6,988,424.52	540,500.00	68.44
TIRIGANIAQ	M11-1335	134.30	137.00	1000	5.94	5.94	2.84	2.70	6,988,424.52	540,500.00	68.44
TIRIGANIAQ	M11-1337	309.00	311.90	1100	0.11	0.11	3.00	2.90	6,988,637.81	539,094.16	68.53
TIRIGANIAQ	M11-1338	267.30	271.30	1100	0.03	0.03	3.05	4.00	6,988,529.28	539,151.54	73.61
TIRIGANIAQ	M11-1338	291.80	295.20	1000	0.05	0.05	2.60	3.40	6,988,529.28	539,151.54	73.61
TIRIGANIAQ	M11-1349	225.50	229.30	1155	1.06	1.06	3.25	3.80	6,988,596.42	540,090.15	67.33
TIRIGANIAQ	M11-1349	257.40	260.80	1153	0.05	0.05	2.91	3.40	6,988,596.42	540,090.15	67.33
TIRIGANIAQ	M11-1349	269.60	273.10	1152	1.71	1.71	3.00	3.50	6,988,596.42	540,090.15	67.33
TIRIGANIAQ	M11-1349	274.70	280.50	1100	22.64	22.64	4.97	5.80	6,988,596.42	540,090.15	67.33
TIRIGANIAQ	M11-1349	286.10	290.00	1087	1.86	1.86	3.35	3.90	6,988,596.42	540,090.15	67.33
TIRIGANIAQ	M11-1349	306.00	309.00	1050	0.57	0.57	2.58	3.00	6,988,596.42	540,090.15	67.33
TIRIGANIAQ	M11-1349	312.00	315.00	1025	0.08	0.08	2.58	3.00	6,988,596.42	540,090.15	67.33
TIRIGANIAQ	M11-1349	324.10	327.00	1000	2.51	2.51	2.50	2.90	6,988,596.42	540,090.15	67.33
TIRIGANIAQ	M11-1358	189.00	192.60	1155	0.15	0.15	3.50	3.60	6,988,595.60	540,090.14	66.91
TIRIGANIAQ	M11-1358	224.40	227.50	1153	0.69	0.69	3.01	3.10	6,988,595.60	540,090.14	66.91
TIRIGANIAQ	M11-1358	253.20	256.50	1100	0.04	0.04	3.20	3.30	6,988,595.60	540,090.14	66.91
TIRIGANIAQ	M11-1358	275.40	278.00	1050	0.40	0.40	2.49	2.60	6,988,595.60	540,090.14	66.91
TIRIGANIAQ	M11-1358	279.00	282.00	1025	0.07	0.07	2.87	3.00	6,988,595.60	540,090.14	66.91
TIRIGANIAQ	M11-1358	293.00	295.40	1000	0.23	0.23	2.28	2.40	6,988,595.60	540,090.14	66.91
TIRIGANIAQ	M11-1359	253.70	256.70	1100	1.19	1.19	2.76	3.00	6,988,560.60	539,169.91	71.72
TIRIGANIAQ	M11-1359	264.80	268.00	1000	0.03	0.03	2.96	3.20	6,988,560.60	539,169.91	71.72
TIRIGANIAQ	M11-1361	272.90	276.00	1100	10.36	10.36	2.87	3.10	6,988,559.28	539,025.20	72.65
TIRIGANIAQ	M11-1361	276.00	279.00	1050	0.84	0.84	2.79	3.00	6,988,559.28	539,025.20	72.65
TIRIGANIAQ	M11-1361	279.00	281.00	1025	0.30	0.30	1.86	2.00	6,988,559.28	539,025.20	72.65
TIRIGANIAQ	M11-1361	281.00	283.60	1000	2.22	2.22	2.42	2.60	6,988,559.28	539,025.20	72.65
TIRIGANIAQ	M11-1363	156.00	158.60	1254	2.22	2.22	2.35	2.60	6,988,550.01	540,600.32	70.35
TIRIGANIAQ	M11-1363	212.00	215.40	1087	1.68	1.68	3.13	3.40	6,988,550.01	540,600.32	70.35
TIRIGANIAQ	M11-1363	225.00	228.00	1075	1.00	1.00	2.78	3.00	6,988,550.01	540,600.32	70.35
TIRIGANIAQ	M11-1363	237.80	240.90	1050	2.16	2.16	2.90	3.10	6,988,550.01	540,600.32	70.35
TIRIGANIAQ	M11-1363	275.30	277.80	1000	0.03	0.03	2.40	2.50	6,988,550.01	540,600.32	70.35
TIRIGANIAQ	M11-1364	326.10	330.20	1155	0.09	0.09	3.41	4.10	6,988,683.37	539,529.09	74.25
TIRIGANIAQ	M11-1364	344.10	348.00	1154	14.04	14.04	3.28	3.90	6,988,683.37	539,529.09	74.25
TIRIGANIAQ	M11-1364	356.20	360.60	1153	8.50	8.50	3.74	4.40	6,988,683.37	539,529.09	74.25
TIRIGANIAQ	M11-1364	371.60	374.60	1150	1.31	1.31	2.58	3.00	6,988,683.37	539,529.09	74.25
TIRIGANIAQ	M11-1364	381.80	385.00	1152	0.19	0.19	2.75	3.20	6,988,683.37	539,529.09	74.25
TIRIGANIAQ	M11-1364	394.00	397.00	1100	0.76	0.76	2.59	3.00	6,988,683.37	539,529.09	74.25
TIRIGANIAQ	M11-1364	409.00	411.80	1075	0.03	0.03	2.43	2.80	6,988,683.37	539,529.09	74.25
TIRIGANIAQ	M11-1364	415.90	418.70	1050	0.03	0.03	2.45	2.80	6,988,683.37	539,529.09	74.25
TIRIGANIAQ	M11-1364	427.00	429.60	1025	5.41	5.41	2.29	2.60	6,988,683.37	539,529.09	74.25
TIRIGANIAQ	M11-1364	431.00	434.00	1015	7.17	7.17	2.65	3.00	6,988,683.37	539,529.09	74.25
TIRIGANIAQ	M11-1364	434.00	437.00	1000	14.69	14.69	2.65	3.00	6,988,683.37	539,529.09	74.25
TIRIGANIAQ	M11-1366	226.00	229.00	1075	7.33	7.33	3.02	3.00	6,988,580.80	540,925.31	65.01
TIRIGANIAQ	M11-1366	235.00	237.60	1050	3.39	3.39	2.62	2.60	6,988,580.80	540,925.31	65.01
TIRIGANIAQ	M11-1366	242.00	244.60	1025	3.92	3.92	2.62	2.60	6,988,580.80	540,925.31	65.01
TIRIGANIAQ	M11-1368	176.00	179.40	1254	1.43	1.43	2.60	3.40	6,988,550.08	540,600.32	69.89
TIRIGANIAQ	M11-1368	251.00	254.00	1075	0.03	0.03	2.40	3.00	6,988,550.08	540,600.32	69.89
TIRIGANIAQ	M11-1368	290.00	293.00	1025	1.60	1.60	2.46	3.00	6,988,550.08	540,600.32	69.89
TIRIGANIAQ	M11-1370	144.90	148.00	1254	0.07	0.07	2.85	3.10	6,988,549.54	540,734.95	67.90
TIRIGANIAQ	M11-1370	195.00	201.00	1100	29.10	29.10	5.54	6.00	6,988,549.54	540,734.95	67.90
TIRIGANIAQ	M11-1370	207.00	210.00	1087	9.38	9.38	2.76	3.00	6,988,549.54	540,734.95	67.90
TIRIGANIAQ	M11-1370	211.00	214.00	1075	1.30	1.30	2.76	3.00	6,988,549.54	540,734.95	67.90
TIRIGANIAQ	M11-1370	225.00	228.00	1050	0.06	0.06	2.77	3.00	6,988,549.54	540,734.95	67.90
TIRIGANIAQ	M11-1370	273.40	276.00	1000	1.63	1.63	2.42	2.60	6,988,549.54	540,734.95	67.90
TIRIGANIAQ	M11-1372	134.00	137.00	1254	0.21	0.21	3.00	3.00	6,988,548.97	540,734.95	67.71
TIRIGANIAQ	M11-1372	167.40	171.00	1155	5.47	5.47	3.61	3.60	6,988,548.97	540,734.95	67.71
TIRIGANIAQ	M11-1372	185.00	187.60	1100	0.78	0.78	2.61	2.60	6,988,548.97	540,734.95	67.71
TIRIGANIAQ	M11-1372	199.30	202.00	1075	1.79	1.79	2.71	2.70	6,988,548.97	540,734.95	67.71
TIRIGANIAQ	M11-1372	207.00	209.60	1050	0.91	0.91	2.61	2.60	6,988,548.97	540,734.95	67.71
TIRIGANIAQ	M11-1372	214.00	217.00	1025	1.56	1.56	3.01	3.00	6,988,548.97	540,734.95	67.71
TIRIGANIAQ	M11-1372	256.30	259.60	1000	0.09	0.09	3.33	3.30	6,988,548.97	540,734.95	67.71
TIRIGANIAQ	M12-1371B	317.00	322.10	1154	30.73	30.73	4.35	5.10	6,988,683.37	539,529.07	75.67
TIRIGANIAQ	M12-1371B	337.10	346.50	1153	13.18	13.18	8.03	9.40	6,988,683.37	539,529.07	75.67
TIRIGANIAQ	M12-1371B	354.00	357.40	1150	0.44	0.44	2.91	3.40	6,988,683.37	539,529.07	75.67
TIRIGANIAQ	M12-1371B	370.10	373.80	1152	0.03	0.03	3.17	3.70	6,988,683.37	539,529.07	75.67
TIRIGANIAQ	M12-1371B	378.50	382.10	1100	0.69	0.69	3.09	3.60	6,988,683.37	539,529.07	75.67
TIRIGANIAQ	M12-1371B	394.60	397.60	1075	0.12	0.12	2.58	3.00	6,988,683.37	539,529.07	75.67
TIRIGANIAQ	M12-1371B	409.30	411.70	1025	0.22	0.22	2.07	2.40	6,988,683.37	539,529.07	75.67
TIRIGANIAQ	M12-1371B	412.70	417.00	1015	22.36	22.36	3.71	4.30	6,988,683.37	539,529.07	75.67
TIRIGANIAQ	M12-1371B	412.70	418.80	1000	21.82	21.82	5.27	6.10	6,988,683.37	539,529.07	75.67
TIRIGANIAQ	M12-1483	152.90	156.10	1100	0.23	0.23	3.37	3.20	6,988,591.48	538,200.22	58.25
TIRIGANIAQ	M12-1488	140.95	144.00	1100	0.71	0.71	2.99	3.05	6,988,566.29	538,224.97	59.21
TIRIGANIAQ	M12-1490	689.00	693.00	1270	2.06	2.06	4.00	4.00	6,989,129.20	538,469.81	62.33
TIRIGANIAQ	M12-1490	711.00	714.00	1265	2.32	2.32	3.01	3.00	6,989,129.20	538,469.81	62.33

TIRIGANIAQ	M12-1492	162.40	166.00	1100	1.10	1.10	3.07	3.60	6,988,566.29	538,225.01	59.23
TIRIGANIAQ	M12-1496	101.20	104.00	1102	4.90	4.90	2.91	2.80	6,988,546.00	538,224.87	58.45
TIRIGANIAQ	M12-1503	192.40	195.00	1100	5.52	5.52	2.75	2.60	6,988,626.07	538,300.16	59.55
TIRIGANIAQ	M12-1504	57.00	60.00	1050	15.88	15.88	2.90	3.00	6,988,424.93	538,526.92	59.79
TIRIGANIAQ	M12-1504	74.40	77.10	1000	8.81	8.81	2.62	2.70	6,988,424.93	538,526.92	59.79
TIRIGANIAQ	M12-1513	207.40	209.53	1100	1.60	1.60	2.14	2.13	6,988,626.34	538,300.16	59.35
TIRIGANIAQ	M12-1522	412.40	416.00	1075	0.23	0.23	3.30	3.60	6,988,762.82	538,434.91	64.94
TIRIGANIAQ	M12-1530	172.20	174.00	1254	3.94	3.94	1.69	1.80	6,988,593.41	540,205.02	65.52
TIRIGANIAQ	M12-1530	186.00	189.00	1257	3.71	3.71	2.83	3.00	6,988,593.41	540,205.02	65.52
TIRIGANIAQ	M12-1530	196.60	199.30	1262	6.99	6.99	2.55	2.70	6,988,593.41	540,205.02	65.52
TIRIGANIAQ	M12-1530	228.00	232.00	1155	0.06	0.06	3.81	4.00	6,988,593.41	540,205.02	65.52
TIRIGANIAQ	M12-1530	258.00	261.00	1153	0.22	0.22	2.87	3.00	6,988,593.41	540,205.02	65.52
TIRIGANIAQ	M12-1530	267.90	271.50	1100	0.22	0.22	3.45	3.60	6,988,593.41	540,205.02	65.52
TIRIGANIAQ	M12-1530	282.30	285.60	1050	0.36	0.36	3.17	3.30	6,988,593.41	540,205.02	65.52
TIRIGANIAQ	M12-1530	301.70	305.00	1025	1.71	1.71	3.19	3.30	6,988,593.41	540,205.02	65.52
TIRIGANIAQ	M12-1530	308.00	310.70	1000	13.83	13.83	2.61	2.70	6,988,593.41	540,205.02	65.52
TIRIGANIAQ	M12-1537	222.50	227.00	1155	0.42	0.42	3.86	4.50	6,988,590.19	539,920.25	66.51
TIRIGANIAQ	M12-1537	233.00	236.00	1154	3.70	3.70	2.59	3.00	6,988,590.19	539,920.25	66.51
TIRIGANIAQ	M12-1537	243.00	248.00	1153	7.46	7.46	4.35	5.00	6,988,590.19	539,920.25	66.51
TIRIGANIAQ	M12-1537	259.50	262.60	1152	2.76	2.76	2.71	3.10	6,988,590.19	539,920.25	66.51
TIRIGANIAQ	M12-1537	269.50	273.10	1151	0.69	0.69	3.16	3.60	6,988,590.19	539,920.25	66.51
TIRIGANIAQ	M12-1537	274.20	277.30	1100	9.53	9.53	2.73	3.10	6,988,590.19	539,920.25	66.51
TIRIGANIAQ	M12-1537	283.40	286.60	1087	0.05	0.05	2.82	3.20	6,988,590.19	539,920.25	66.51
TIRIGANIAQ	M12-1537	303.50	306.50	1050	0.42	0.42	2.66	3.00	6,988,590.19	539,920.25	66.51
TIRIGANIAQ	M12-1537	312.00	315.00	1000	3.52	3.52	2.67	3.00	6,988,590.19	539,920.25	66.51
TIRIGANIAQ	M12-1540	659.40	662.10	1265	1.20	1.20	2.73	2.70	6,989,065.50	538,464.91	62.61
TIRIGANIAQ	M12-1540	702.40	707.30	1100	1.25	1.25	5.00	4.90	6,989,065.50	538,464.91	62.61
TIRIGANIAQ	M12-1540	721.00	724.00	1025	0.17	0.17	3.07	3.00	6,989,065.50	538,464.91	62.61
TIRIGANIAQ	M12-1557	224.20	225.20	1154	0.03	0.03	0.86	1.00	6,988,587.41	539,846.97	66.86
TIRIGANIAQ	M12-1557	235.80	239.20	1153	0.55	0.55	2.93	3.40	6,988,587.41	539,846.97	66.86
TIRIGANIAQ	M12-1557	247.40	251.00	1152	0.18	0.18	3.11	3.60	6,988,587.41	539,846.97	66.86
TIRIGANIAQ	M12-1557	258.40	262.00	1151	0.49	0.49	3.13	3.60	6,988,587.41	539,846.97	66.86
TIRIGANIAQ	M12-1557	267.00	269.50	1100	21.26	21.26	2.18	2.50	6,988,587.41	539,846.97	66.86
TIRIGANIAQ	M12-1557	279.00	282.50	1087	11.48	11.48	3.07	3.50	6,988,587.41	539,846.97	66.86
TIRIGANIAQ	M12-1557	284.00	287.00	1075	6.00	6.00	2.63	3.00	6,988,587.41	539,846.97	66.86
TIRIGANIAQ	M12-1557	293.00	296.00	1050	0.15	0.15	2.64	3.00	6,988,587.41	539,846.97	66.86
TIRIGANIAQ	M12-1557	307.00	310.20	1000	0.73	0.73	2.82	3.20	6,988,587.41	539,846.97	66.86
TIRIGANIAQ	M12-1558	190.00	192.50	1254	1.43	1.43	2.24	2.50	6,988,620.36	540,284.77	65.85
TIRIGANIAQ	M12-1558	287.40	290.60	1153	3.48	3.48	3.04	3.20	6,988,620.36	540,284.77	65.85
TIRIGANIAQ	M12-1558	298.40	301.80	1100	-	-	3.23	3.40	6,988,620.36	540,284.77	65.85
TIRIGANIAQ	M12-1558	301.40	304.20	1087	-	-	2.66	2.80	6,988,620.36	540,284.77	65.85
TIRIGANIAQ	M12-1563	709.00	711.00	1270	3.37	3.37	2.03	2.00	6,989,130.38	538,579.92	62.41
TIRIGANIAQ	M12-1569	90.00	93.00	1050	2.59	2.59	3.10	3.00	6,988,463.61	538,524.96	59.71
TIRIGANIAQ	M12-1569	103.50	106.00	1000	0.44	0.44	2.59	2.50	6,988,463.61	538,524.96	59.71
TIRIGANIAQ	M12-1571	292.70	298.00	1251	3.34	3.34	4.57	5.30	6,988,668.64	539,815.47	66.60
TIRIGANIAQ	M12-1571	320.00	323.00	1155	2.92	2.92	2.61	3.00	6,988,668.64	539,815.47	66.60
TIRIGANIAQ	M12-1571	327.20	331.00	1154	21.06	21.06	3.31	3.80	6,988,668.64	539,815.47	66.60
TIRIGANIAQ	M12-1571	335.10	338.80	1153	4.35	4.35	3.22	3.70	6,988,668.64	539,815.47	66.60
TIRIGANIAQ	M12-1571	344.00	347.00	1152	1.89	1.89	2.62	3.00	6,988,668.64	539,815.47	66.60
TIRIGANIAQ	M12-1571	348.00	351.20	1100	1.99	1.99	2.79	3.20	6,988,668.64	539,815.47	66.60
TIRIGANIAQ	M12-1571	359.00	363.00	1087	26.95	26.95	3.50	4.00	6,988,668.64	539,815.47	66.60
TIRIGANIAQ	M12-1571	366.00	369.00	1075	0.26	0.26	2.63	3.00	6,988,668.64	539,815.47	66.60
TIRIGANIAQ	M12-1571	374.00	377.40	1050	1.27	1.27	2.98	3.40	6,988,668.64	539,815.47	66.60
TIRIGANIAQ	M12-1571	394.00	397.60	1000	0.65	0.65	3.18	3.60	6,988,668.64	539,815.47	66.60
TIRIGANIAQ	M12-1574A	322.00	325.00	1154	0.46	0.46	2.81	3.00	6,988,659.09	540,189.73	65.02
TIRIGANIAQ	M12-1574A	328.00	331.00	1153	3.71	3.71	2.81	3.00	6,988,659.09	540,189.73	65.02
TIRIGANIAQ	M12-1574A	336.00	340.00	1100	9.80	9.80	3.76	4.00	6,988,659.09	540,189.73	65.02
TIRIGANIAQ	M12-1574A	342.00	347.90	1075	10.05	10.05	5.55	5.90	6,988,659.09	540,189.73	65.02
TIRIGANIAQ	M12-1574A	351.00	354.20	1050	0.59	0.59	3.02	3.20	6,988,659.09	540,189.73	65.02
TIRIGANIAQ	M12-1574A	369.00	371.40	1025	0.39	0.39	2.27	2.40	6,988,659.09	540,189.73	65.02
TIRIGANIAQ	M12-1574A	375.00	377.60	1000	0.80	0.80	2.47	2.60	6,988,659.09	540,189.73	65.02
TIRIGANIAQ	M12-1576	105.80	108.80	1100	0.03	0.03	3.11	3.00	6,988,464.02	538,625.01	60.94
TIRIGANIAQ	M12-1576	111.00	114.00	1050	2.73	2.73	3.11	3.00	6,988,464.02	538,625.01	60.94
TIRIGANIAQ	M12-1576	114.00	119.00	1025	5.74	5.74	5.18	5.00	6,988,464.02	538,625.01	60.94
TIRIGANIAQ	M12-1576	123.00	127.60	1000	11.22	11.22	4.77	4.60	6,988,464.02	538,625.01	60.94
TIRIGANIAQ	M12-1583	155.40	158.00	1050	0.20	0.20	2.75	2.60	6,988,518.01	538,624.92	62.27
TIRIGANIAQ	M12-1583	158.80	161.30	1025	0.03	0.03	2.64	2.50	6,988,518.01	538,624.92	62.27
TIRIGANIAQ	M12-1583	170.20	174.50	1000	8.13	8.13	4.55	4.30	6,988,518.01	538,624.92	62.27
TIRIGANIAQ	M12-1588	599.00	602.00	1100	1.26	1.26	3.22	3.00	6,989,004.15	538,582.20	62.50
TIRIGANIAQ	M12-1589	37.00	40.60	1520	6.19	6.19	2.95	3.60	6,988,641.64	539,814.78	66.56
TIRIGANIAQ	M12-1589	254.30	258.00	1251	14.10	14.10	3.22	3.70	6,988,641.64	539,814.78	66.56
TIRIGANIAQ	M12-1589	276.70	280.60	1155	2.81	2.81	3.41	3.90	6,988,641.64	539,814.78	66.56
TIRIGANIAQ	M12-1589	287.00	291.00	1154	12.69	12.69	3.50	4.00	6,988,641.64	539,814.78	66.56
TIRIGANIAQ	M12-1589	293.40	297.60	1153	2.15	2.15	3.68	4.20	6,988,641.64	539,814.78	66.56
TIRIGANIAQ	M12-1589	306.50	310.00	1152	8.61	8.61	3.08	3.50	6,988,641.64	539,814.78	66.56
TIRIGANIAQ	M12-1589	322.00	324.70	1100	7.76	7.76	2.39	2.70	6,988,641.64	539,814.78	66.56
TIRIGANIAQ	M12-1589	329.00	331.60	1087	0.31	0.31	2.31	2.60	6,988,641.64	539,814.78	66.56
TIRIGANIAQ	M12-1589	336.00	338.60	1075	11.86	11.86	2.31	2.60	6,988,641.64	539,814.78	66.56
TIRIGANIAQ	M12-1589	343.40	346.40	1050	0.28	0.28	2.67	3.00	6,988,641.64	539,814.78	66.56
TIRIGANIAQ	M12-1589	361.40	364.50	1000	0.03	0.03	2.79	3.10	6,988,641.64	539,814.78	66.56
TIRIGANIAQ	M12-1590	166.00	170.00	1050	2.00	2.00	4.20	4.00	6,988,510.70	538,674.68	63.42
TIRIGANIAQ	M12-1590	178.40	181.00	1000	1.51	1.51	2.73	2.60	6,988,510.70	538,674.68	63.42
TIRIGANIAQ	M12-1597	216.00	219.00	1100	0.49	0.49	2.81	3.00	6,988,525.77	538,799.88	65.09
TIRIGANIAQ	M12-1597	220.80	224.20	1025	0.04	0.04	3.19	3.40	6,988,525.77	538,799.88	65.09
TIRIGANIAQ	M12-1597	230.00	233.00	1050	0.67	0.67	2.83	3.00	6,988,525.77	538,799.88	65.09
TIRIGANIAQ	M12-1597	238.00	241.00	1000	2.58	2.58	2.83	3.00	6,988,525.77	538,799.88	65.09
TIRIGANIAQ	M12-1600	174.00	176.60	1254	1.80	1.80	2.10	2.60	6,988,597.13	540,284.71	65.08
TIRIGANIAQ	M12-1600	281.00	284.60	1153	1.10	1.10	3.11	3.60	6,988,597.13	540,284.71	65.08
TIRIGANIAQ	M12-1600	288.00	290.60	1100	4.08	4.08	2.26	2.60	6,988,597.13	540,284.71	65.08
TIRIGANIAQ	M12-1600	292.00	295.00	1087	2.48	2.48	2.62	3.00	6,988,597.13	540,284.71	65.08

TIRIGANIAQ	M12-1600	299.80	303.40	1075	6.20	6.20	3.16	3.60	6,988,597.13	540,284.71	65.08
TIRIGANIAQ	M12-1600	304.40	307.60	1050	5.98	5.98	2.82	3.20	6,988,597.13	540,284.71	65.08
TIRIGANIAQ	M12-1600	324.40	328.00	1025	0.30	0.30	3.21	3.60	6,988,597.13	540,284.71	65.08
TIRIGANIAQ	M12-1600	343.40	346.20	1000	0.29	0.29	2.53	2.80	6,988,597.13	540,284.71	65.08
TIRIGANIAQ	M12-1612	258.00	261.00	1100	1.55	1.55	2.86	3.00	6,988,575.03	538,824.95	65.53
TIRIGANIAQ	M12-1612	262.30	265.00	1050	0.11	0.11	2.58	2.70	6,988,575.03	538,824.95	65.53
TIRIGANIAQ	M12-1612	282.00	284.90	1000	0.03	0.03	2.79	2.90	6,988,575.03	538,824.95	65.53
TIRIGANIAQ	M12-1616	23.80	26.00	1000	5.81	5.81	2.14	2.20	6,988,409.31	538,360.22	58.27
TIRIGANIAQ	M12-1617	346.20	350.00	1263	0.93	0.93	3.63	3.80	6,988,773.94	539,768.08	67.85
TIRIGANIAQ	M12-1617	359.00	362.20	1256	0.70	0.70	3.07	3.20	6,988,773.94	539,768.08	67.85
TIRIGANIAQ	M12-1617	382.50	385.80	1252	8.73	8.73	3.19	3.30	6,988,773.94	539,768.08	67.85
TIRIGANIAQ	M12-1617	393.40	396.60	1251	2.25	2.25	3.10	3.20	6,988,773.94	539,768.08	67.85
TIRIGANIAQ	M12-1617	404.00	407.50	1155	1.76	1.76	3.40	3.50	6,988,773.94	539,768.08	67.85
TIRIGANIAQ	M12-1617	416.80	420.20	1154	1.29	1.29	3.31	3.40	6,988,773.94	539,768.08	67.85
TIRIGANIAQ	M12-1617	424.00	427.00	1153	0.03	0.03	2.93	3.00	6,988,773.94	539,768.08	67.85
TIRIGANIAQ	M12-1617	428.90	432.00	1100	2.63	2.63	3.03	3.10	6,988,773.94	539,768.08	67.85
TIRIGANIAQ	M12-1617	428.90	432.00	1152	2.63	2.63	3.03	3.10	6,988,773.94	539,768.08	67.85
TIRIGANIAQ	M12-1617	444.40	447.00	1075	0.28	0.28	2.56	2.60	6,988,773.94	539,768.08	67.85
TIRIGANIAQ	M12-1617	458.70	461.40	1050	0.12	0.12	2.67	2.70	6,988,773.94	539,768.08	67.85
TIRIGANIAQ	M12-1621	252.00	255.00	1100	1.21	1.21	2.79	3.00	6,988,550.23	538,924.60	68.05
TIRIGANIAQ	M12-1621	260.00	263.00	1050	1.14	1.14	2.80	3.00	6,988,550.23	538,924.60	68.05
TIRIGANIAQ	M12-1621	264.00	267.00	1025	2.23	2.23	2.80	3.00	6,988,550.23	538,924.60	68.05
TIRIGANIAQ	M12-1621	270.00	273.00	1000	11.68	11.68	2.81	3.00	6,988,550.23	538,924.60	68.05
TIRIGANIAQ	M12-1622	26.00	29.00	1075	1.42	1.42	3.13	3.00	6,988,381.46	540,825.29	67.68
TIRIGANIAQ	M12-1622	49.70	52.50	1050	0.03	0.03	2.94	2.80	6,988,381.46	540,825.29	67.68
TIRIGANIAQ	M12-1625	371.00	374.00	1153	0.12	0.12	2.72	3.00	6,988,695.23	540,239.86	65.72
TIRIGANIAQ	M12-1625	374.00	376.60	1100	0.61	0.61	2.36	2.60	6,988,695.23	540,239.86	65.72
TIRIGANIAQ	M12-1625	388.40	392.00	1075	0.13	0.13	3.27	3.60	6,988,695.23	540,239.86	65.72
TIRIGANIAQ	M12-1625	394.00	397.00	1050	0.12	0.12	2.73	3.00	6,988,695.23	540,239.86	65.72
TIRIGANIAQ	M12-1625	406.30	410.00	1025	0.62	0.62	3.38	3.70	6,988,695.23	540,239.86	65.72
TIRIGANIAQ	M12-1625	413.00	416.90	1000	0.93	0.93	3.57	3.90	6,988,695.23	540,239.86	65.72
TIRIGANIAQ	M12-1628	642.00	644.20	1270	0.39	0.39	2.17	2.20	6,989,049.64	538,580.88	62.52
TIRIGANIAQ	M12-1628	710.50	713.00	1100	6.35	6.35	2.50	2.50	6,989,049.64	538,580.88	62.52
TIRIGANIAQ	M12-1628	718.70	721.40	1025	0.19	0.19	2.71	2.70	6,989,049.64	538,580.88	62.52
TIRIGANIAQ	M12-1628	745.50	747.80	1000	3.46	3.46	2.31	2.30	6,989,049.64	538,580.88	62.52
TIRIGANIAQ	M12-1644	312.00	315.50	1251	0.17	0.17	3.17	3.50	6,988,695.21	539,690.16	69.50
TIRIGANIAQ	M12-1644	326.00	330.80	1155	5.01	5.01	4.37	4.80	6,988,695.21	539,690.16	69.50
TIRIGANIAQ	M12-1644	335.00	351.00	1154	10.88	10.88	14.67	16.00	6,988,695.21	539,690.16	69.50
TIRIGANIAQ	M12-1644	357.60	360.70	1153	23.89	23.89	2.86	3.10	6,988,695.21	539,690.16	69.50
TIRIGANIAQ	M12-1644	360.70	363.60	1150	3.27	3.27	2.68	2.90	6,988,695.21	539,690.16	69.50
TIRIGANIAQ	M12-1644	371.00	376.00	1152	1.71	1.71	4.64	5.00	6,988,695.21	539,690.16	69.50
TIRIGANIAQ	M12-1644	384.00	387.00	1100	0.48	0.48	2.80	3.00	6,988,695.21	539,690.16	69.50
TIRIGANIAQ	M12-1644	393.40	397.00	1075	2.13	2.13	3.38	3.60	6,988,695.21	539,690.16	69.50
TIRIGANIAQ	M12-1652	468.40	472.00	1256	1.51	1.51	3.36	3.60	6,988,853.61	539,759.89	68.92
TIRIGANIAQ	M12-1652	528.60	531.30	1100	0.53	0.53	2.58	2.70	6,988,853.61	539,759.89	68.92
TIRIGANIAQ	M12-1652	566.00	568.50	1000	1.00	1.00	2.41	2.50	6,988,853.61	539,759.89	68.92
TIRIGANIAQ	M12-1668	189.00	192.00	1152	0.74	0.74	2.84	3.00	6,988,551.51	539,500.00	78.32
TIRIGANIAQ	M12-1668	225.40	228.30	1100	2.30	2.30	2.82	2.90	6,988,551.51	539,500.00	78.32
TIRIGANIAQ	M12-1668	260.40	263.00	1000	2.61	2.61	2.56	2.60	6,988,551.51	539,500.00	78.32
TIRIGANIAQ	M12-1672	69.00	72.50	1100	7.23	7.23	2.94	3.50	6,988,408.06	538,599.92	59.97
TIRIGANIAQ	M12-1672	74.00	77.60	1050	1.17	1.17	3.04	3.60	6,988,408.06	538,599.92	59.97
TIRIGANIAQ	M12-1672	79.40	82.30	1025	0.51	0.51	2.46	2.90	6,988,408.06	538,599.92	59.97
TIRIGANIAQ	M12-1672	84.40	87.70	1000	0.03	0.03	2.81	3.30	6,988,408.06	538,599.92	59.97
TIRIGANIAQ	M12-1679	72.80	76.50	1100	7.03	7.03	2.98	3.70	6,988,408.10	538,599.93	59.92
TIRIGANIAQ	M12-1679	76.50	82.00	1050	1.12	1.12	4.46	5.50	6,988,408.10	538,599.93	59.92
TIRIGANIAQ	M12-1679	83.00	87.00	1025	1.62	1.62	3.25	4.00	6,988,408.10	538,599.93	59.92
TIRIGANIAQ	M12-1679	88.40	91.00	1000	2.45	2.45	2.12	2.60	6,988,408.10	538,599.93	59.92
TIRIGANIAQ	M12-1682	8.00	12.00	1540	2.17	2.17	2.94	4.00	6,988,663.05	540,115.06	65.71
TIRIGANIAQ	M12-1683	288.80	291.80	1153	-	-	2.62	3.00	6,988,633.44	539,514.93	76.23
TIRIGANIAQ	M12-1683	322.00	325.30	1152	0.15	0.15	3.01	3.30	6,988,633.44	539,514.93	76.23
TIRIGANIAQ	M12-1683	335.30	338.30	1100	7.88	7.88	2.76	3.00	6,988,633.44	539,514.93	76.23
TIRIGANIAQ	M12-1684	76.00	81.50	1000	2.09	2.09	5.19	5.50	6,988,450.29	538,449.75	59.31
TIRIGANIAQ	M12-1688	8.60	12.70	1540	1.77	1.77	2.98	4.10	6,988,663.16	540,115.09	65.70
TIRIGANIAQ	M12-1688	365.60	368.70	1154	16.37	16.37	2.61	3.10	6,988,663.16	540,115.09	65.70
TIRIGANIAQ	M12-1688	367.80	374.50	1100	17.98	17.98	5.65	6.70	6,988,663.16	540,115.09	65.70
TIRIGANIAQ	M12-1688	370.50	373.40	1153	13.15	13.15	2.45	2.90	6,988,663.16	540,115.09	65.70
TIRIGANIAQ	M12-1688	386.00	390.50	1087	1.90	1.90	3.81	4.50	6,988,663.16	540,115.09	65.70
TIRIGANIAQ	M12-1688	392.00	395.00	1075	1.72	1.72	2.55	3.00	6,988,663.16	540,115.09	65.70
TIRIGANIAQ	M12-1688	396.00	399.00	1050	8.24	8.24	2.55	3.00	6,988,663.16	540,115.09	65.70
TIRIGANIAQ	M12-1688	404.00	408.70	1025	34.11	34.11	4.01	4.70	6,988,663.16	540,115.09	65.70
TIRIGANIAQ	M12-1688	411.00	415.40	1000	1.53	1.53	3.76	4.40	6,988,663.16	540,115.09	65.70
TIRIGANIAQ	M12-1692	279.00	281.70	1154	3.28	3.28	2.70	2.70	6,988,676.07	539,665.04	70.28
TIRIGANIAQ	M12-1692	292.80	295.30	1153	7.46	7.46	2.52	2.50	6,988,676.07	539,665.04	70.28
TIRIGANIAQ	M12-1692	317.70	320.70	1152	18.53	18.53	3.07	3.00	6,988,676.07	539,665.04	70.28
TIRIGANIAQ	M12-1692	326.10	329.00	1151	1.50	1.50	2.97	2.90	6,988,676.07	539,665.04	70.28
TIRIGANIAQ	M12-1692	340.70	342.90	1100	1.51	1.51	2.26	2.20	6,988,676.07	539,665.04	70.28
TIRIGANIAQ	M12-1701	215.00	217.80	1050	0.53	0.53	2.59	2.80	6,988,528.76	538,700.22	64.97
TIRIGANIAQ	M12-1701	224.90	228.00	1000	0.63	0.63	2.88	3.10	6,988,528.76	538,700.22	64.97
TIRIGANIAQ	M12-1704A	400.00	404.00	1155	0.33	0.33	3.39	4.00	6,988,731.48	539,385.35	77.73
TIRIGANIAQ	M12-1704A	406.00	410.00	1154	0.55	0.55	3.40	4.00	6,988,731.48	539,385.35	77.73
TIRIGANIAQ	M12-1704A	422.00	426.00	1153	17.62	17.62	3.41	4.00	6,988,731.48	539,385.35	77.73
TIRIGANIAQ	M12-1704A	433.00	436.00	1152	0.44	0.44	2.56	3.00	6,988,731.48	539,385.35	77.73
TIRIGANIAQ	M12-1704A	439.00	441.90	1100	0.08	0.08	2.48	2.90	6,988,731.48	539,385.35	77.73
TIRIGANIAQ	M12-1704A	460.40	464.00	1075	1.80	1.80	3.10	3.60	6,988,731.48	539,385.35	77.73
TIRIGANIAQ	M12-1704A	472.00	475.00	1050	0.93	0.93	2.60	3.00	6,988,731.48	539,385.35	77.73
TIRIGANIAQ	M12-1704A	480.00	484.00	1025	3.05	3.05	3.47	4.00	6,988,731.48	539,385.35	77.73
TIRIGANIAQ	M12-1704A	486.00	489.00	1015	1.87	1.87	2.60	3.00	6,988,731.48	539,385.35	77.73
TIRIGANIAQ	M12-1704A	493.00	499.00	1000	4.06	4.06	5.22	6.00	6,988,731.48	539,385.35	77.73
TIRIGANIAQ	M12-1705	427.30	430.00	1153	0.03	0.03	2.56	2.70	6,988,740.08	540,040.33	66.64
TIRIGANIAQ	M12-1705	428.80	432.00	1100	0.03	0.03	3.03	3.20	6,988,740.08	540,040.33	66.64

TIRIGANIAQ	M12-1705	442.00	444.60	1075	0.03	0.03	2.47	2.60	6,988,740.08	540,040.33	66.64
TIRIGANIAQ	M12-1705	450.00	453.00	1050	0.49	0.49	2.86	3.00	6,988,740.08	540,040.33	66.64
TIRIGANIAQ	M12-1705	460.30	463.30	1000	0.06	0.06	2.86	3.00	6,988,740.08	540,040.33	66.64
TIRIGANIAQ	M12-1706	262.40	266.00	1153	0.11	0.11	3.44	3.60	6,988,634.27	539,615.17	72.98
TIRIGANIAQ	M12-1706	282.00	285.20	1152	0.25	0.25	3.09	3.20	6,988,634.27	539,615.17	72.98
TIRIGANIAQ	M12-1706	291.40	294.70	1151	2.80	2.80	3.19	3.30	6,988,634.27	539,615.17	72.98
TIRIGANIAQ	M12-1706	313.70	316.40	1100	0.21	0.21	2.62	2.70	6,988,634.27	539,615.17	72.98
TIRIGANIAQ	M12-1709	56.00	59.00	1100	1.57	1.57	3.00	3.00	6,988,385.23	538,774.96	67.87
TIRIGANIAQ	M12-1709A	58.80	62.10	1100	2.65	2.65	3.19	3.30	6,988,385.23	538,774.96	67.87
TIRIGANIAQ	M12-1711	116.00	119.00	1000	0.45	0.45	2.80	3.00	6,988,428.69	538,700.13	63.87
TIRIGANIAQ	M12-1715	449.70	452.40	1075	0.06	0.06	2.82	2.70	6,988,847.58	538,539.71	70.80
TIRIGANIAQ	M12-1717	372.00	375.00	1260	3.98	3.98	2.40	3.00	6,988,757.95	539,611.07	70.66
TIRIGANIAQ	M12-1717	395.00	398.00	1256	0.38	0.38	2.41	3.00	6,988,757.95	539,611.07	70.66
TIRIGANIAQ	M12-1717	416.00	421.20	1255	2.59	2.59	4.23	5.20	6,988,757.95	539,611.07	70.66
TIRIGANIAQ	M12-1717	432.50	437.00	1252	0.28	0.28	3.68	4.50	6,988,757.95	539,611.07	70.66
TIRIGANIAQ	M12-1717	446.00	450.40	1251	0.77	0.77	3.62	4.40	6,988,757.95	539,611.07	70.66
TIRIGANIAQ	M12-1717	488.00	491.00	1100	0.03	0.03	2.51	3.00	6,988,757.95	539,611.07	70.66
TIRIGANIAQ	M12-1717	496.30	499.30	1075	0.36	0.36	2.51	3.00	6,988,757.95	539,611.07	70.66
TIRIGANIAQ	M12-1717	518.00	521.50	1025	3.45	3.45	2.96	3.50	6,988,757.95	539,611.07	70.66
TIRIGANIAQ	M12-1717	522.80	526.30	1000	2.67	2.67	2.97	3.50	6,988,757.95	539,611.07	70.66
TIRIGANIAQ	M12-1718	376.00	378.90	1100	0.65	0.65	2.53	2.90	6,988,675.32	538,945.07	70.51
TIRIGANIAQ	M12-1718	396.40	399.40	1025	3.70	3.70	2.61	3.00	6,988,675.32	538,945.07	70.51
TIRIGANIAQ	M12-1720	150.60	154.60	1254	0.72	0.72	3.08	4.00	6,988,549.48	540,470.01	67.40
TIRIGANIAQ	M12-1720	159.30	162.40	1261	4.81	4.81	2.39	3.10	6,988,549.48	540,470.01	67.40
TIRIGANIAQ	M12-1720	170.50	173.90	1257	0.41	0.41	2.63	3.40	6,988,549.48	540,470.01	67.40
TIRIGANIAQ	M12-1720	240.00	244.50	1100	0.03	0.03	3.56	4.50	6,988,549.48	540,470.01	67.40
TIRIGANIAQ	M12-1720	259.50	262.50	1075	3.20	3.20	2.38	3.00	6,988,549.48	540,470.01	67.40
TIRIGANIAQ	M12-1721	93.40	96.60	1100	0.61	0.61	2.99	3.20	6,988,439.18	540,250.06	66.03
TIRIGANIAQ	M12-1721	125.40	128.60	1050	0.21	0.21	3.02	3.20	6,988,439.18	540,250.06	66.03
TIRIGANIAQ	M12-1721	139.00	141.60	1025	0.77	0.77	2.46	2.60	6,988,439.18	540,250.06	66.03
TIRIGANIAQ	M12-1721	161.00	163.90	1000	0.26	0.26	2.76	2.90	6,988,439.18	540,250.06	66.03
TIRIGANIAQ	M12-1722	112.25	115.40	1254	1.45	1.45	2.91	3.15	6,988,529.54	540,494.96	68.05
TIRIGANIAQ	M12-1722	121.10	123.50	1261	0.84	0.84	2.23	2.40	6,988,529.54	540,494.96	68.05
TIRIGANIAQ	M12-1722	125.00	127.80	1257	1.44	1.44	2.60	2.80	6,988,529.54	540,494.96	68.05
TIRIGANIAQ	M12-1722	149.70	153.00	1251	0.98	0.98	3.10	3.30	6,988,529.54	540,494.96	68.05
TIRIGANIAQ	M12-1722	159.80	162.60	1155	1.28	1.28	2.64	2.80	6,988,529.54	540,494.96	68.05
TIRIGANIAQ	M12-1722	174.00	177.00	1100	0.03	0.03	2.85	3.00	6,988,529.54	540,494.96	68.05
TIRIGANIAQ	M12-1722	181.50	184.50	1087	0.39	0.39	2.86	3.00	6,988,529.54	540,494.96	68.05
TIRIGANIAQ	M12-1722	201.10	203.65	1075	0.06	0.06	2.45	2.55	6,988,529.54	540,494.96	68.05
TIRIGANIAQ	M12-1722	214.50	217.50	1050	1.03	1.03	2.90	3.00	6,988,529.54	540,494.96	68.05
TIRIGANIAQ	M12-1722	246.90	249.65	1000	19.07	19.07	2.69	2.75	6,988,529.54	540,494.96	68.05
TIRIGANIAQ	M12-1723B	312.80	316.40	1153	0.03	0.03	3.53	3.60	6,988,683.65	539,365.12	76.96
TIRIGANIAQ	M12-1723B	328.70	331.70	1152	-	-	2.99	3.00	6,988,683.65	539,365.12	76.96
TIRIGANIAQ	M12-1723B	363.35	366.10	1100	0.79	0.79	2.82	2.75	6,988,683.65	539,365.12	76.96
TIRIGANIAQ	M12-1723B	369.40	372.00	1075	1.91	1.91	2.68	2.60	6,988,683.65	539,365.12	76.96
TIRIGANIAQ	M12-1723B	392.50	395.55	1025	0.21	0.21	3.18	3.05	6,988,683.65	539,365.12	76.96
TIRIGANIAQ	M12-1723B	395.55	399.00	1015	1.06	1.06	3.60	3.45	6,988,683.65	539,365.12	76.96
TIRIGANIAQ	M12-1723B	398.20	400.70	1000	5.52	5.52	2.61	2.50	6,988,683.65	539,365.12	76.96
TIRIGANIAQ	M12-1725	320.70	323.60	1100	0.39	0.39	2.58	2.90	6,988,614.65	539,025.02	73.98
TIRIGANIAQ	M12-1725	327.90	331.00	1050	2.33	2.33	2.77	3.10	6,988,614.65	539,025.02	73.98
TIRIGANIAQ	M12-1725	333.00	336.00	1025	1.92	1.92	2.68	3.00	6,988,614.65	539,025.02	73.98
TIRIGANIAQ	M12-1725	336.00	342.20	1000	21.36	21.36	5.54	6.20	6,988,614.65	539,025.02	73.98
TIRIGANIAQ	M12-1726A	577.50	581.10	1000	1.23	1.23	3.71	3.60	6,988,878.88	540,281.13	67.05
TIRIGANIAQ	M12-1729	433.40	437.00	1075	0.91	0.91	3.24	3.60	6,988,733.74	540,340.01	67.40
TIRIGANIAQ	M12-1729	445.40	448.60	1050	0.04	0.04	2.88	3.20	6,988,733.74	540,340.01	67.40
TIRIGANIAQ	M12-1729	467.70	470.50	1025	32.59	35.01	2.53	2.80	6,988,733.74	540,340.01	67.40
TIRIGANIAQ	M12-1729	478.00	481.60	1000	0.84	0.84	3.27	3.60	6,988,733.74	540,340.01	67.40
TIRIGANIAQ	M12-1730	188.00	191.00	1153	0.99	0.99	2.80	3.00	6,988,546.07	540,095.39	67.69
TIRIGANIAQ	M12-1730	219.00	222.00	1100	0.25	0.25	2.82	3.00	6,988,546.07	540,095.39	67.69
TIRIGANIAQ	M12-1730	231.30	234.70	1050	0.03	0.03	3.21	3.40	6,988,546.07	540,095.39	67.69
TIRIGANIAQ	M12-1730	240.40	244.50	1025	2.88	2.88	3.89	4.10	6,988,546.07	540,095.39	67.69
TIRIGANIAQ	M12-1730	255.90	258.50	1000	0.42	0.42	2.47	2.60	6,988,546.07	540,095.39	67.69
TIRIGANIAQ	M12-1731	206.80	210.00	1153	3.91	3.91	3.21	3.20	6,988,584.80	540,045.31	67.53
TIRIGANIAQ	M12-1731	240.40	243.10	1100	0.19	0.19	2.72	2.70	6,988,584.80	540,045.31	67.53
TIRIGANIAQ	M12-1731	263.80	265.70	1050	0.66	0.66	1.91	1.90	6,988,584.80	540,045.31	67.53
TIRIGANIAQ	M12-1731	274.90	278.80	1025	3.57	3.57	3.92	3.90	6,988,584.80	540,045.31	67.53
TIRIGANIAQ	M12-1731	282.80	285.40	1000	0.61	0.61	2.62	2.60	6,988,584.80	540,045.31	67.53
TIRIGANIAQ	M12-1733	527.50	531.00	1255	1.51	1.51	3.12	3.50	6,988,869.01	539,455.01	73.83
TIRIGANIAQ	M12-1733	574.00	577.00	1075	1.83	1.83	2.71	3.00	6,988,869.01	539,455.01	73.83
TIRIGANIAQ	M12-1733	582.00	584.60	1050	2.23	2.23	2.36	2.60	6,988,869.01	539,455.01	73.83
TIRIGANIAQ	M12-1733	591.00	593.80	1025	0.03	0.03	2.56	2.80	6,988,869.01	539,455.01	73.83
TIRIGANIAQ	M12-1733	600.00	602.70	1015	0.84	0.84	2.48	2.70	6,988,869.01	539,455.01	73.83
TIRIGANIAQ	M12-1733	609.00	611.50	1000	0.07	0.07	2.30	2.50	6,988,869.01	539,455.01	73.83
TIRIGANIAQ	M12-1737B	303.00	310.50	1150	1.55	1.55	4.07	7.50	6,988,576.74	539,165.09	70.27
TIRIGANIAQ	M12-1737B	316.50	323.30	1152	0.45	0.45	3.71	6.80	6,988,576.74	539,165.09	70.27
TIRIGANIAQ	M12-1737B	331.70	337.70	1170	5.48	5.48	3.30	6.00	6,988,576.74	539,165.09	70.27
TIRIGANIAQ	M12-1737B	371.50	377.50	1160	0.84	0.84	3.40	6.00	6,988,576.74	539,165.09	70.27
TIRIGANIAQ	M12-1737B	380.50	384.50	1100	0.43	0.43	2.28	4.00	6,988,576.74	539,165.09	70.27
TIRIGANIAQ	M12-1737B	418.80	422.80	1025	0.68	0.68	2.34	4.00	6,988,576.74	539,165.09	70.27
TIRIGANIAQ	M12-1737B	428.80	432.80	1015	5.50	5.50	2.35	4.00	6,988,576.74	539,165.09	70.27
TIRIGANIAQ	M12-1737B	438.80	442.50	1000	0.03	0.03	2.19	3.70	6,988,576.74	539,165.09	70.27
TIRIGANIAQ	M12-1738	578.20	581.30	1251	9.34	9.34	2.91	3.10	6,988,871.41	538,680.15	64.37
TIRIGANIAQ	M12-1738	582.15	585.65	1153	2.32	2.32	3.29	3.50	6,988,871.41	538,680.15	64.37
TIRIGANIAQ	M12-1738	588.20	590.95	1100	0.33	0.33	2.59	2.75	6,988,871.41	538,680.15	64.37
TIRIGANIAQ	M12-1738	608.40	611.15	1050	0.68	0.68	2.62	2.75	6,988,871.41	538,680.15	64.37
TIRIGANIAQ	M12-1738	614.80	617.60	1025	8.21	8.21	2.67	2.80	6,988,871.41	538,680.15	64.37
TIRIGANIAQ	M12-1738	622.00	624.50	1015	2.38	2.38	2.39	2.50	6,988,871.41	538,680.15	64.37
TIRIGANIAQ	M12-1738	633.00	635.70	1000	0.92	0.92	2.59	2.70	6,988,871.41	538,680.15	64.37
TIRIGANIAQ	M12-1739	71.30	75.00	1251	0.46	0.46	3.44	3.70	6,988,462.97	540,999.91	67.83
TIRIGANIAQ	M12-1739	112.90	115.90	1075	1.55	1.55	2.85	3.00	6,988,462.97	540,999.91	67.83

TIRIGANIAQ	M12-1739	120.50	123.30	1050	2.92	2.92	2.67	2.80	6,988,462.97	540,999.91	67.83
TIRIGANIAQ	M12-1741	451.00	455.00	1263	1.78	1.78	3.89	4.00	6,988,855.34	539,680.19	69.65
TIRIGANIAQ	M12-1741	460.00	463.00	1256	0.70	0.70	2.92	3.00	6,988,855.34	539,680.19	69.65
TIRIGANIAQ	M12-1741	528.50	531.50	1100	4.01	4.01	2.97	3.00	6,988,855.34	539,680.19	69.65
TIRIGANIAQ	M12-1741	554.00	557.00	1025	0.19	0.19	2.99	3.00	6,988,855.34	539,680.19	69.65
TIRIGANIAQ	M12-1741	561.00	563.70	1000	0.44	0.44	2.69	2.70	6,988,855.34	539,680.19	69.65
TIRIGANIAQ	M12-1742	397.40	400.60	1153	7.29	7.29	2.77	3.20	6,988,688.05	540,105.86	66.27
TIRIGANIAQ	M12-1742	401.40	404.30	1100	0.05	0.05	2.52	2.90	6,988,688.05	540,105.86	66.27
TIRIGANIAQ	M12-1742	418.00	420.60	1075	0.07	0.07	2.27	2.60	6,988,688.05	540,105.86	66.27
TIRIGANIAQ	M12-1742	426.00	429.00	1050	1.12	1.12	2.62	3.00	6,988,688.05	540,105.86	66.27
TIRIGANIAQ	M12-1742	431.00	433.60	1025	6.09	6.09	2.28	2.60	6,988,688.05	540,105.86	66.27
TIRIGANIAQ	M12-1742	440.00	443.00	1000	1.51	1.51	2.63	3.00	6,988,688.05	540,105.86	66.27
TIRIGANIAQ	M12-1743	381.20	385.00	1153	27.87	38.53	3.94	3.80	6,988,771.94	539,439.96	75.10
TIRIGANIAQ	M12-1743	398.00	400.70	1152	1.84	1.84	2.81	2.70	6,988,771.94	539,439.96	75.10
TIRIGANIAQ	M12-1743	411.80	414.50	1100	3.04	3.04	2.81	2.70	6,988,771.94	539,439.96	75.10
TIRIGANIAQ	M12-1743	424.00	426.40	1075	0.03	0.03	2.51	2.40	6,988,771.94	539,439.96	75.10
TIRIGANIAQ	M12-1743	442.20	445.40	1025	2.00	2.00	3.35	3.20	6,988,771.94	539,439.96	75.10
TIRIGANIAQ	M12-1743	452.00	454.50	1000	0.25	0.25	2.62	2.50	6,988,771.94	539,439.96	75.10
TIRIGANIAQ	M12-1745	140.50	143.30	1254	2.72	2.72	2.71	2.80	6,988,561.45	540,420.02	66.50
TIRIGANIAQ	M12-1745	147.50	150.20	1257	0.39	0.39	2.62	2.70	6,988,561.45	540,420.02	66.50
TIRIGANIAQ	M12-1745	153.90	157.10	1258	1.18	1.18	3.11	3.20	6,988,561.45	540,420.02	66.50
TIRIGANIAQ	M12-1745	173.80	178.20	1251	5.00	5.00	4.32	4.40	6,988,561.45	540,420.02	66.50
TIRIGANIAQ	M12-1745	185.15	188.20	1155	8.35	8.35	3.01	3.05	6,988,561.45	540,420.02	66.50
TIRIGANIAQ	M12-1745	198.40	201.40	1100	0.27	0.27	2.97	3.00	6,988,561.45	540,420.02	66.50
TIRIGANIAQ	M12-1745	206.40	209.10	1087	0.24	0.24	2.68	2.70	6,988,561.45	540,420.02	66.50
TIRIGANIAQ	M12-1745	235.40	238.60	1050	0.42	0.42	3.20	3.20	6,988,561.45	540,420.02	66.50
TIRIGANIAQ	M12-1745	270.40	272.70	1000	0.15	0.15	2.33	2.30	6,988,561.45	540,420.02	66.50
TIRIGANIAQ	M12-1747	170.90	174.60	1254	1.90	1.90	3.08	3.70	6,988,556.44	540,695.05	69.72
TIRIGANIAQ	M12-1747	246.40	250.60	1075	0.68	0.68	3.51	4.20	6,988,556.44	540,695.05	69.72
TIRIGANIAQ	M12-1747	279.00	283.00	1025	0.03	0.03	3.35	4.00	6,988,556.44	540,695.05	69.72
TIRIGANIAQ	M12-1748	420.60	423.50	1252	5.64	5.64	2.59	2.90	6,988,759.51	538,940.02	65.28
TIRIGANIAQ	M12-1748	466.80	469.60	1100	4.89	4.89	2.55	2.80	6,988,759.51	538,940.02	65.28
TIRIGANIAQ	M12-1748	478.50	483.00	1050	1.30	1.30	4.12	4.50	6,988,759.51	538,940.02	65.28
TIRIGANIAQ	M12-1748	488.80	491.40	1025	5.75	5.75	2.39	2.60	6,988,759.51	538,940.02	65.28
TIRIGANIAQ	M12-1748	499.40	502.20	1015	0.10	0.10	2.59	2.80	6,988,759.51	538,940.02	65.28
TIRIGANIAQ	M12-1748	502.80	505.80	1000	3.26	3.26	2.79	3.00	6,988,759.51	538,940.02	65.28
TIRIGANIAQ	M12-1749	631.00	635.70	1252	9.39	9.39	4.07	4.70	6,988,895.93	538,769.87	63.66
TIRIGANIAQ	M12-1749	649.80	652.20	1050	2.40	2.40	2.10	2.40	6,988,895.93	538,769.87	63.66
TIRIGANIAQ	M12-1749	658.80	661.70	1025	7.69	7.69	2.54	2.90	6,988,895.93	538,769.87	63.66
TIRIGANIAQ	M12-1749	665.20	668.00	1015	0.03	0.03	2.46	2.80	6,988,895.93	538,769.87	63.66
TIRIGANIAQ	M12-1749	668.00	671.30	1000	1.81	1.81	2.91	3.30	6,988,895.93	538,769.87	63.66
TIRIGANIAQ	M12-1750	438.50	441.55	1251	35.96	35.96	2.82	3.05	6,988,794.10	538,697.98	65.20
TIRIGANIAQ	M12-1750	443.00	446.00	1153	50.19	97.19	2.78	3.00	6,988,794.10	538,697.98	65.20
TIRIGANIAQ	M12-1750	477.40	480.00	1100	1.14	1.14	2.44	2.60	6,988,794.10	538,697.98	65.20
TIRIGANIAQ	M12-1750	487.40	492.50	1050	28.21	28.21	4.81	5.10	6,988,794.10	538,697.98	65.20
TIRIGANIAQ	M12-1750	511.00	513.60	1025	5.12	5.12	2.47	2.60	6,988,794.10	538,697.98	65.20
TIRIGANIAQ	M12-1750	525.40	528.05	1000	2.13	2.13	2.53	2.65	6,988,794.10	538,697.98	65.20
TIRIGANIAQ	M12-1751	302.80	306.60	1150	0.03	0.03	3.18	3.80	6,988,654.94	539,269.89	71.34
TIRIGANIAQ	M12-1751	313.20	316.70	1152	7.95	7.95	2.95	3.50	6,988,654.94	539,269.89	71.34
TIRIGANIAQ	M12-1751	366.00	370.00	1100	0.86	0.86	3.40	4.00	6,988,654.94	539,269.89	71.34
TIRIGANIAQ	M12-1751	372.50	375.50	1075	0.26	0.26	2.56	3.00	6,988,654.94	539,269.89	71.34
TIRIGANIAQ	M12-1751	393.00	396.00	1025	2.52	2.52	2.58	3.00	6,988,654.94	539,269.89	71.34
TIRIGANIAQ	M12-1751	402.80	405.40	1015	0.03	0.03	2.24	2.60	6,988,654.94	539,269.89	71.34
TIRIGANIAQ	M12-1751	406.50	409.80	1000	0.35	0.35	2.85	3.30	6,988,654.94	539,269.89	71.34
TIRIGANIAQ	M12-1753	474.60	477.90	1255	3.56	3.56	2.77	3.30	6,988,799.60	538,885.08	65.37
TIRIGANIAQ	M12-1753	522.00	524.60	1100	0.19	0.19	2.24	2.60	6,988,799.60	538,885.08	65.37
TIRIGANIAQ	M12-1753	536.40	539.00	1050	0.10	0.10	2.26	2.60	6,988,799.60	538,885.08	65.37
TIRIGANIAQ	M12-1753	546.00	548.60	1025	0.06	0.06	2.28	2.60	6,988,799.60	538,885.08	65.37
TIRIGANIAQ	M12-1753	555.60	558.20	1015	0.94	0.94	2.29	2.60	6,988,799.60	538,885.08	65.37
TIRIGANIAQ	M12-1753	560.60	562.40	1000	0.17	0.17	1.59	1.80	6,988,799.60	538,885.08	65.37
TIRIGANIAQ	M12-1754	402.00	405.60	1155	0.63	0.63	3.39	3.60	6,988,772.26	539,439.95	75.02
TIRIGANIAQ	M12-1754	412.00	414.90	1154	0.59	0.59	2.74	2.90	6,988,772.26	539,439.95	75.02
TIRIGANIAQ	M12-1754	426.40	433.00	1153	9.30	9.30	6.26	6.60	6,988,772.26	539,439.95	75.02
TIRIGANIAQ	M12-1754	438.40	441.20	1152	1.19	1.19	2.67	2.80	6,988,772.26	539,439.95	75.02
TIRIGANIAQ	M12-1754	447.60	450.80	1100	0.10	0.10	3.06	3.20	6,988,772.26	539,439.95	75.02
TIRIGANIAQ	M12-1754	463.40	466.00	1075	0.10	0.10	2.50	2.60	6,988,772.26	539,439.95	75.02
TIRIGANIAQ	M12-1754	475.80	478.60	1050	0.17	0.17	2.70	2.80	6,988,772.26	539,439.95	75.02
TIRIGANIAQ	M12-1754	481.40	484.00	1025	0.03	0.03	2.51	2.60	6,988,772.26	539,439.95	75.02
TIRIGANIAQ	M12-1754	485.70	488.40	1015	0.03	0.03	2.61	2.70	6,988,772.26	539,439.95	75.02
TIRIGANIAQ	M12-1754	495.20	498.80	1000	0.37	0.37	3.49	3.60	6,988,772.26	539,439.95	75.02
TIRIGANIAQ	M12-1756	125.00	128.30	1154	0.04	0.04	3.07	3.30	6,988,512.32	540,175.19	66.34
TIRIGANIAQ	M12-1756	155.70	159.00	1153	4.30	4.30	3.12	3.30	6,988,512.32	540,175.19	66.34
TIRIGANIAQ	M12-1756	175.90	178.80	1100	0.15	0.15	2.80	2.90	6,988,512.32	540,175.19	66.34
TIRIGANIAQ	M12-1756	207.00	210.00	1050	1.21	1.21	3.01	3.00	6,988,512.32	540,175.19	66.34
TIRIGANIAQ	M12-1756	216.00	219.00	1025	5.51	5.51	3.03	3.00	6,988,512.32	540,175.19	66.34
TIRIGANIAQ	M12-1756	223.60	229.80	1000	8.13	8.13	6.28	6.20	6,988,512.32	540,175.19	66.34
TIRIGANIAQ	M12-1757	504.60	507.30	1260	16.97	16.97	2.36	2.70	6,988,879.82	539,240.15	75.18
TIRIGANIAQ	M12-1757	516.50	519.50	1253	1.35	1.35	2.63	3.00	6,988,879.82	539,240.15	75.18
TIRIGANIAQ	M12-1757	534.50	537.50	1255	1.61	1.61	2.65	3.00	6,988,879.82	539,240.15	75.18
TIRIGANIAQ	M12-1757	595.00	597.60	1050	3.12	3.12	2.34	2.60	6,988,879.82	539,240.15	75.18
TIRIGANIAQ	M12-1757	600.40	603.00	1025	10.34	10.34	2.35	2.60	6,988,879.82	539,240.15	75.18
TIRIGANIAQ	M12-1757	608.00	611.00	1015	0.21	0.21	2.72	3.00	6,988,879.82	539,240.15	75.18
TIRIGANIAQ	M12-1757	616.00	618.50	1000	0.10	0.10	2.27	2.50	6,988,879.82	539,240.15	75.18
TIRIGANIAQ	M12-1759	365.00	369.00	1155	2.02	2.02	3.79	4.00	6,988,740.08	539,180.06	68.15
TIRIGANIAQ	M12-1759	372.80	376.00	1153	1.95	1.95	3.06	3.20	6,988,740.08	539,180.06	68.15
TIRIGANIAQ	M12-1759	381.00	384.00	1150	1.17	1.17	2.89	3.00	6,988,740.08	539,180.06	68.15
TIRIGANIAQ	M12-1759	388.20	392.00	1152	2.71	2.71	3.68	3.80	6,988,740.08	539,180.06	68.15
TIRIGANIAQ	M12-1759	398.00	401.20	1170	2.81	2.81	3.11	3.20	6,988,740.08	539,180.06	68.15
TIRIGANIAQ	M12-1759	422.00	425.10	1160	0.67	0.67	3.05	3.10	6,988,740.08	539,180.06	68.15
TIRIGANIAQ	M12-1759	432.20	434.60	1100	0.61	0.61	2.37	2.40	6,988,740.08	539,180.06	68.15

TIRIGANIAQ	M12-1759	451.00	454.00	1025	0.20	0.20	2.97	3.00	6,988,740.08	539,180.06	68.15
TIRIGANIAQ	M12-1759	463.50	465.50	1015	0.31	0.31	1.99	2.00	6,988,740.08	539,180.06	68.15
TIRIGANIAQ	M12-1759	465.50	467.80	1000	23.67	23.67	2.28	2.30	6,988,740.08	539,180.06	68.15
TIRIGANIAQ	M12-1761	200.70	204.10	1254	1.29	1.29	2.91	3.40	6,988,599.26	540,439.94	68.03
TIRIGANIAQ	M12-1762	470.00	472.70	1255	3.37	3.37	2.39	2.70	6,988,802.62	538,834.98	66.23
TIRIGANIAQ	M12-1762	514.40	517.00	1100	1.21	1.21	2.35	2.60	6,988,802.62	538,834.98	66.23
TIRIGANIAQ	M12-1762	530.00	533.00	1050	0.03	0.03	2.73	3.00	6,988,802.62	538,834.98	66.23
TIRIGANIAQ	M12-1762	538.40	541.10	1025	0.36	0.36	2.46	2.70	6,988,802.62	538,834.98	66.23
TIRIGANIAQ	M12-1762	548.40	551.00	1015	1.75	1.75	2.38	2.60	6,988,802.62	538,834.98	66.23
TIRIGANIAQ	M12-1762	551.40	554.00	1000	3.33	3.33	2.39	2.60	6,988,802.62	538,834.98	66.23
TIRIGANIAQ	M12-1763A	492.40	497.00	1360	8.55	8.55	3.97	4.60	6,988,876.39	539,380.21	75.85
TIRIGANIAQ	M12-1763A	635.00	637.80	1015	2.83	2.83	2.57	2.80	6,988,876.39	539,380.21	75.85
TIRIGANIAQ	M12-1763A	640.00	642.50	1000	4.54	4.54	2.30	2.50	6,988,876.39	539,380.21	75.85
TIRIGANIAQ	M12-1763C	464.70	467.40	1260	0.22	0.22	2.62	2.70	6,988,875.02	539,380.17	75.66
TIRIGANIAQ	M12-1763C	472.90	476.10	1253	1.83	1.83	3.11	3.20	6,988,875.02	539,380.17	75.66
TIRIGANIAQ	M12-1763C	497.00	500.60	1255	0.04	0.04	3.52	3.60	6,988,875.02	539,380.17	75.66
TIRIGANIAQ	M12-1763C	507.00	511.90	1252	5.40	5.40	4.80	4.90	6,988,875.02	539,380.17	75.66
TIRIGANIAQ	M12-1763C	522.90	526.00	1251	0.03	0.03	3.05	3.10	6,988,875.02	539,380.17	75.66
TIRIGANIAQ	M12-1763C	546.70	550.00	1100	3.28	3.28	3.27	3.30	6,988,875.02	539,380.17	75.66
TIRIGANIAQ	M12-1763C	554.60	557.60	1075	0.03	0.03	2.98	3.00	6,988,875.02	539,380.17	75.66
TIRIGANIAQ	M12-1763C	559.00	561.40	1050	0.91	0.91	2.39	2.40	6,988,875.02	539,380.17	75.66
TIRIGANIAQ	M12-1763C	569.40	572.40	1025	0.19	0.19	3.00	3.00	6,988,875.02	539,380.17	75.66
TIRIGANIAQ	M12-1763C	574.40	577.00	1015	1.73	1.73	2.60	2.60	6,988,875.02	539,380.17	75.66
TIRIGANIAQ	M12-1763C	588.70	591.40	1000	0.84	0.84	2.71	2.70	6,988,875.02	539,380.17	75.66
TIRIGANIAQ	M12-1764	548.30	551.60	1252	2.18	2.18	2.92	3.30	6,988,877.51	538,611.35	65.36
TIRIGANIAQ	M12-1764	599.60	604.00	1025	9.27	9.27	3.97	4.40	6,988,877.51	538,611.35	65.36
TIRIGANIAQ	M12-1764	604.40	607.60	1015	2.16	2.16	2.89	3.20	6,988,877.51	538,611.35	65.36
TIRIGANIAQ	M12-1765	317.60	320.00	1100	0.80	0.80	2.17	2.40	6,988,608.39	538,925.04	70.68
TIRIGANIAQ	M12-1765	346.50	350.30	1000	0.03	0.03	3.55	3.80	6,988,608.39	538,925.04	70.68
TIRIGANIAQ	M12-1767	351.20	355.20	1153	0.03	0.03	3.66	4.00	6,988,724.65	539,075.06	65.47
TIRIGANIAQ	M12-1767	369.40	373.50	1152	14.05	14.05	3.78	4.10	6,988,724.65	539,075.06	65.47
TIRIGANIAQ	M12-1767	389.10	392.50	1170	0.68	0.68	3.15	3.40	6,988,724.65	539,075.06	65.47
TIRIGANIAQ	M12-1767	411.30	414.50	1160	0.04	0.04	2.98	3.20	6,988,724.65	539,075.06	65.47
TIRIGANIAQ	M12-1767	422.60	425.20	1100	0.03	0.03	2.43	2.60	6,988,724.65	539,075.06	65.47
TIRIGANIAQ	M12-1767	438.60	441.20	1025	0.19	0.19	2.44	2.60	6,988,724.65	539,075.06	65.47
TIRIGANIAQ	M12-1767	450.40	453.60	1015	0.98	0.98	3.00	3.20	6,988,724.65	539,075.06	65.47
TIRIGANIAQ	M12-1767	456.00	459.00	1000	0.03	0.03	2.82	3.00	6,988,724.65	539,075.06	65.47
TIRIGANIAQ	M12-1769	469.00	472.00	1256	1.64	1.64	2.93	3.00	6,988,873.58	539,529.93	71.47
TIRIGANIAQ	M12-1769	493.00	499.10	1255	6.75	6.75	6.06	6.10	6,988,873.58	539,529.93	71.47
TIRIGANIAQ	M12-1769	538.60	541.10	1100	0.17	0.17	2.53	2.50	6,988,873.58	539,529.93	71.47
TIRIGANIAQ	M12-1769	550.60	554.00	1075	19.12	19.12	3.46	3.40	6,988,873.58	539,529.93	71.47
TIRIGANIAQ	M12-1769	556.40	560.00	1050	0.15	0.15	3.67	3.60	6,988,873.58	539,529.93	71.47
TIRIGANIAQ	M12-1769	565.40	568.00	1025	0.14	0.14	2.65	2.60	6,988,873.58	539,529.93	71.47
TIRIGANIAQ	M12-1769	570.40	573.00	1015	0.12	0.12	2.66	2.60	6,988,873.58	539,529.93	71.47
TIRIGANIAQ	M12-1769	578.00	581.40	1000	0.85	0.85	3.48	3.40	6,988,873.58	539,529.93	71.47
TIRIGANIAQ	M12-1770A	512.20	515.30	1252	1.75	1.75	2.92	3.10	6,988,862.72	538,650.04	64.12
TIRIGANIAQ	M12-1770A	516.50	519.50	1251	4.60	4.60	2.83	3.00	6,988,862.72	538,650.04	64.12
TIRIGANIAQ	M12-1770A	555.70	558.60	1100	2.71	2.71	2.77	2.90	6,988,862.72	538,650.04	64.12
TIRIGANIAQ	M12-1770A	571.20	574.50	1050	1.61	1.61	3.16	3.30	6,988,862.72	538,650.04	64.12
TIRIGANIAQ	M12-1770A	579.40	582.00	1025	0.44	0.44	2.50	2.60	6,988,862.72	538,650.04	64.12
TIRIGANIAQ	M12-1770A	588.40	591.00	1015	0.03	0.03	2.51	2.60	6,988,862.72	538,650.04	64.12
TIRIGANIAQ	M12-1770A	595.00	597.70	1000	0.15	0.15	2.61	2.70	6,988,862.72	538,650.04	64.12
TIRIGANIAQ	M12-1772A	500.50	503.10	1255	17.73	17.73	2.37	2.60	6,988,810.58	538,910.06	64.87
TIRIGANIAQ	M12-1772A	525.00	528.40	1153	0.66	0.66	3.14	3.40	6,988,810.58	538,910.06	64.87
TIRIGANIAQ	M12-1772A	533.40	536.50	1100	1.75	1.75	2.88	3.10	6,988,810.58	538,910.06	64.87
TIRIGANIAQ	M12-1772A	544.50	546.80	1050	14.09	14.09	2.15	2.30	6,988,810.58	538,910.06	64.87
TIRIGANIAQ	M12-1772A	557.10	559.90	1025	0.03	0.03	2.62	2.80	6,988,810.58	538,910.06	64.87
TIRIGANIAQ	M12-1772A	566.00	568.60	1015	0.03	0.03	2.44	2.60	6,988,810.58	538,910.06	64.87
TIRIGANIAQ	M12-1772A	572.20	574.50	1000	5.02	5.02	2.16	2.30	6,988,810.58	538,910.06	64.87
TIRIGANIAQ	M12-1774	105.60	109.60	1157	2.54	2.54	3.58	4.00	6,988,486.57	538,924.96	66.48
TIRIGANIAQ	M12-1774	182.50	185.50	1100	0.03	0.03	2.76	3.00	6,988,486.57	538,924.96	66.48
TIRIGANIAQ	M12-1774	192.00	195.00	1025	1.37	1.37	2.77	3.00	6,988,486.57	538,924.96	66.48
TIRIGANIAQ	M12-1774	198.50	201.40	1000	0.03	0.03	2.68	2.90	6,988,486.57	538,924.96	66.48
TIRIGANIAQ	M12-1775	338.10	341.10	1150	3.15	3.15	3.05	3.00	6,988,739.69	539,180.00	68.20
TIRIGANIAQ	M12-1775	396.00	399.00	1100	0.32	0.32	3.11	3.00	6,988,739.69	539,180.00	68.20
TIRIGANIAQ	M12-1775	413.40	416.40	1025	2.73	2.73	3.11	3.00	6,988,739.69	539,180.00	68.20
TIRIGANIAQ	M12-1775	424.50	427.50	1000	0.58	0.58	3.12	3.00	6,988,739.69	539,180.00	68.20
TIRIGANIAQ	M12-1776	530.80	534.00	1100	0.03	0.03	3.26	3.20	6,988,877.15	538,611.30	65.23
TIRIGANIAQ	M12-1776	538.50	541.20	1075	0.03	0.03	2.76	2.70	6,988,877.15	538,611.30	65.23
TIRIGANIAQ	M12-1776	569.30	572.90	1015	3.02	3.02	3.71	3.60	6,988,877.15	538,611.30	65.23
TIRIGANIAQ	M12-1778	79.70	82.80	1102	3.13	3.13	3.12	3.10	6,988,406.96	538,949.94	65.86
TIRIGANIAQ	M12-1778	84.90	87.90	1100	1.44	1.44	3.02	3.00	6,988,406.96	538,949.94	65.86
TIRIGANIAQ	M12-1778	101.50	104.00	1000	4.56	4.56	2.53	2.50	6,988,406.96	538,949.94	65.86
TIRIGANIAQ	M12-1780	561.30	564.90	1350	2.52	2.52	3.11	3.60	6,988,894.52	538,859.91	63.61
TIRIGANIAQ	M12-1780	622.00	626.00	1252	3.70	3.70	3.49	4.00	6,988,894.52	538,859.91	63.61
TIRIGANIAQ	M12-1780	630.80	633.00	1050	0.03	0.03	1.92	2.20	6,988,894.52	538,859.91	63.61
TIRIGANIAQ	M12-1781A	450.50	453.80	1154	4.46	4.46	3.00	3.30	6,988,754.81	539,889.48	66.92
TIRIGANIAQ	M12-1781A	453.80	456.60	1153	1.14	1.14	2.55	2.80	6,988,754.81	539,889.48	66.92
TIRIGANIAQ	M12-1781A	458.40	461.80	1100	0.03	0.03	3.10	3.40	6,988,754.81	539,889.48	66.92
TIRIGANIAQ	M12-1781A	491.00	494.00	1050	0.03	0.03	2.79	3.00	6,988,754.81	539,889.48	66.92
TIRIGANIAQ	M12-1782	350.50	359.70	1153	21.79	23.84	8.73	9.20	6,988,728.26	539,139.96	66.30
TIRIGANIAQ	M12-1782	367.50	371.00	1152	8.01	8.01	3.35	3.50	6,988,728.26	539,139.96	66.30
TIRIGANIAQ	M12-1785	472.50	477.00	1260	5.00	5.00	3.28	4.50	6,988,760.88	539,010.03	64.55
TIRIGANIAQ	M12-1785	485.00	490.00	1256	0.81	0.81	3.66	5.00	6,988,760.88	539,010.03	64.55
TIRIGANIAQ	M12-1785	492.00	497.00	1255	2.15	2.15	3.67	5.00	6,988,760.88	539,010.03	64.55
TIRIGANIAQ	M12-1785	533.30	536.30	1153	0.44	0.44	2.25	3.00	6,988,760.88	539,010.03	64.55
TIRIGANIAQ	M12-1785	559.10	563.10	1050	0.73	0.73	3.04	4.00	6,988,760.88	539,010.03	64.55
TIRIGANIAQ	M12-1785	569.80	573.20	1025	0.03	0.03	2.60	3.40	6,988,760.88	539,010.03	64.55
TIRIGANIAQ	M12-1785	580.90	584.20	1015	0.47	0.47	2.54	3.30	6,988,760.88	539,010.03	64.55
TIRIGANIAQ	M12-1785	587.60	591.10	1000	0.30	0.30	2.70	3.50	6,988,760.88	539,010.03	64.55

TIRIGANIAQ	M12-1786	550.00	553.00	1256	1.47	1.47	2.70	3.00	6,988,867.06	538,725.01	64.24
TIRIGANIAQ	M12-1786	574.40	578.00	1251	1.82	1.82	3.27	3.60	6,988,867.06	538,725.01	64.24
TIRIGANIAQ	M12-1786	581.40	585.00	1153	1.57	1.57	3.27	3.60	6,988,867.06	538,725.01	64.24
TIRIGANIAQ	M12-1786	594.00	597.10	1100	13.69	13.69	2.83	3.10	6,988,867.06	538,725.01	64.24
TIRIGANIAQ	M12-1786	599.00	602.00	1050	7.00	7.00	2.74	3.00	6,988,867.06	538,725.01	64.24
TIRIGANIAQ	M12-1786	609.00	611.80	1025	6.08	6.08	2.56	2.80	6,988,867.06	538,725.01	64.24
TIRIGANIAQ	M12-1786	613.00	619.40	1015	10.15	10.15	5.87	6.40	6,988,867.06	538,725.01	64.24
TIRIGANIAQ	M12-1786	629.00	631.60	1000	4.33	4.33	2.39	2.60	6,988,867.06	538,725.01	64.24
TIRIGANIAQ	M12-1787	372.60	375.50	1255	4.64	4.64	2.65	2.90	6,988,756.75	539,355.14	78.12
TIRIGANIAQ	M12-1787	402.70	406.40	1155	1.52	1.52	3.42	3.70	6,988,756.75	539,355.14	78.12
TIRIGANIAQ	M12-1787	408.20	411.80	1154	2.56	2.56	3.33	3.60	6,988,756.75	539,355.14	78.12
TIRIGANIAQ	M12-1787	420.40	423.40	1153	13.52	13.52	2.79	3.00	6,988,756.75	539,355.14	78.12
TIRIGANIAQ	M12-1787	430.00	433.70	1152	19.71	19.71	3.45	3.70	6,988,756.75	539,355.14	78.12
TIRIGANIAQ	M12-1787	445.00	447.80	1100	0.91	0.91	2.62	2.80	6,988,756.75	539,355.14	78.12
TIRIGANIAQ	M12-1787	455.40	458.20	1075	0.03	0.03	2.63	2.80	6,988,756.75	539,355.14	78.12
TIRIGANIAQ	M12-1787	463.40	466.60	1050	0.65	0.65	3.02	3.20	6,988,756.75	539,355.14	78.12
TIRIGANIAQ	M12-1787	471.20	474.20	1025	0.03	0.03	2.85	3.00	6,988,756.75	539,355.14	78.12
TIRIGANIAQ	M12-1787	484.00	487.10	1015	0.62	0.62	2.98	3.10	6,988,756.75	539,355.14	78.12
TIRIGANIAQ	M12-1787	489.20	492.60	1000	7.74	7.74	3.29	3.40	6,988,756.75	539,355.14	78.12
TIRIGANIAQ	M12-1788	52.80	55.80	1102	0.03	0.03	2.88	3.00	6,988,382.40	538,875.33	67.16
TIRIGANIAQ	M12-1788	57.30	60.40	1100	0.03	0.03	2.98	3.10	6,988,382.40	538,875.33	67.16
TIRIGANIAQ	M12-1789	493.60	496.50	1000	11.38	11.38	2.96	2.90	6,988,744.38	540,360.00	68.44
TIRIGANIAQ	M12-1790	534.10	537.10	1153	6.81	6.81	2.64	3.00	6,988,808.47	538,809.83	66.42
TIRIGANIAQ	M12-1790	542.40	545.30	1100	1.84	1.84	2.57	2.90	6,988,808.47	538,809.83	66.42
TIRIGANIAQ	M12-1790	559.50	562.50	1050	0.30	0.30	2.71	3.00	6,988,808.47	538,809.83	66.42
TIRIGANIAQ	M12-1790	567.00	570.00	1025	0.03	0.03	2.74	3.00	6,988,808.47	538,809.83	66.42
TIRIGANIAQ	M12-1790	574.90	577.60	1015	2.99	2.99	2.48	2.70	6,988,808.47	538,809.83	66.42
TIRIGANIAQ	M12-1790	582.80	585.40	1000	0.03	0.03	2.41	2.60	6,988,808.47	538,809.83	66.42
TIRIGANIAQ	M12-1791	545.00	550.30	1350	13.81	13.81	4.46	5.30	6,988,855.78	538,920.03	63.89
TIRIGANIAQ	M12-1791	618.60	621.60	1153	4.83	4.83	2.66	3.00	6,988,855.78	538,920.03	63.89
TIRIGANIAQ	M12-1791	627.00	629.60	1025	0.52	0.52	2.32	2.60	6,988,855.78	538,920.03	63.89
TIRIGANIAQ	M12-1791	634.40	637.00	1015	0.42	0.42	2.33	2.60	6,988,855.78	538,920.03	63.89
TIRIGANIAQ	M12-1791	637.00	640.00	1000	1.06	1.06	2.69	3.00	6,988,855.78	538,920.03	63.89
TIRIGANIAQ	M12-1795	311.00	313.50	1256	1.51	1.51	2.30	2.50	6,988,715.78	539,840.67	66.95
TIRIGANIAQ	M12-1795	335.00	339.00	1251	0.03	0.03	3.72	4.00	6,988,715.78	539,840.67	66.95
TIRIGANIAQ	M12-1795	357.00	359.70	1155	1.07	1.07	2.53	2.70	6,988,715.78	539,840.67	66.95
TIRIGANIAQ	M12-1795	365.90	369.00	1154	0.61	0.61	2.91	3.10	6,988,715.78	539,840.67	66.95
TIRIGANIAQ	M12-1795	373.00	375.60	1153	1.30	1.30	2.45	2.60	6,988,715.78	539,840.67	66.95
TIRIGANIAQ	M12-1795	378.50	382.10	1152	1.38	1.38	3.39	3.60	6,988,715.78	539,840.67	66.95
TIRIGANIAQ	M12-1795	386.00	389.10	1100	1.59	1.59	2.93	3.10	6,988,715.78	539,840.67	66.95
TIRIGANIAQ	M12-1795	391.00	393.40	1087	2.44	2.44	2.27	2.40	6,988,715.78	539,840.67	66.95
TIRIGANIAQ	M12-1795	397.20	400.00	1075	0.45	0.45	2.66	2.80	6,988,715.78	539,840.67	66.95
TIRIGANIAQ	M12-1795	410.00	413.10	1050	9.75	9.75	2.95	3.10	6,988,715.78	539,840.67	66.95
TIRIGANIAQ	M12-1795	427.00	430.50	1000	0.62	0.62	3.34	3.50	6,988,715.78	539,840.67	66.95
TIRIGANIAQ	M12-1797	285.90	288.70	1100	0.98	0.98	2.46	2.80	6,988,564.08	538,989.77	71.72
TIRIGANIAQ	M12-1797	294.10	297.10	1050	0.42	0.42	2.64	3.00	6,988,564.08	538,989.77	71.72
TIRIGANIAQ	M12-1797	297.30	299.90	1025	0.09	0.09	2.30	2.60	6,988,564.08	538,989.77	71.72
TIRIGANIAQ	M12-1797	300.10	307.60	1000	13.44	13.44	6.61	7.50	6,988,564.08	538,989.77	71.72
TIRIGANIAQ	M12-1799	366.00	369.00	1252	7.10	7.10	2.79	3.00	6,988,745.38	539,130.05	65.70
TIRIGANIAQ	M12-1799	386.00	391.50	1153	5.09	5.09	5.20	5.50	6,988,745.38	539,130.05	65.70
TIRIGANIAQ	M12-1799	397.80	401.40	1150	1.18	1.18	3.42	3.60	6,988,745.38	539,130.05	65.70
TIRIGANIAQ	M12-1799	407.70	411.00	1152	7.38	7.38	3.16	3.30	6,988,745.38	539,130.05	65.70
TIRIGANIAQ	M12-1799	422.40	425.50	1170	3.93	3.93	2.99	3.10	6,988,745.38	539,130.05	65.70
TIRIGANIAQ	M12-1799	427.00	429.60	1160	2.47	2.47	2.52	2.60	6,988,745.38	539,130.05	65.70
TIRIGANIAQ	M12-1799	431.70	435.50	1100	5.94	5.94	3.68	3.80	6,988,745.38	539,130.05	65.70
TIRIGANIAQ	M12-1799	448.50	451.50	1050	0.13	0.13	2.91	3.00	6,988,745.38	539,130.05	65.70
TIRIGANIAQ	M12-1799	459.20	462.40	1025	0.03	0.03	3.12	3.20	6,988,745.38	539,130.05	65.70
TIRIGANIAQ	M12-1799	467.70	470.30	1015	9.50	9.50	2.54	2.60	6,988,745.38	539,130.05	65.70
TIRIGANIAQ	M12-1799	472.50	475.50	1000	0.03	0.03	2.94	3.00	6,988,745.38	539,130.05	65.70
TIRIGANIAQ	M12-1805	31.80	34.60	1100	0.44	0.44	2.81	2.80	6,988,383.84	539,889.30	68.69
TIRIGANIAQ	M12-1805	68.30	72.30	1050	3.24	3.24	4.05	4.00	6,988,383.84	539,889.30	68.69
TIRIGANIAQ	M12-1805	75.60	81.00	1025	3.97	3.97	5.48	5.40	6,988,383.84	539,889.30	68.69
TIRIGANIAQ	M12-1805	83.00	87.70	1000	5.59	5.59	4.78	4.70	6,988,383.84	539,889.30	68.69
TIRIGANIAQ	M12-1806	23.00	27.90	1100	2.89	2.89	4.84	4.90	6,988,352.89	539,648.09	78.56
TIRIGANIAQ	M12-1806	30.00	33.00	1087	0.25	0.25	2.97	3.00	6,988,352.89	539,648.09	78.56
TIRIGANIAQ	M12-1806	36.00	39.30	1075	11.82	11.82	3.27	3.30	6,988,352.89	539,648.09	78.56
TIRIGANIAQ	M12-1806	45.00	48.00	1050	1.47	1.47	2.98	3.00	6,988,352.89	539,648.09	78.56
TIRIGANIAQ	M12-1806	53.00	56.00	1025	1.04	1.04	2.98	3.00	6,988,352.89	539,648.09	78.56
TIRIGANIAQ	M12-1806	58.00	61.80	1000	9.98	9.98	3.78	3.80	6,988,352.89	539,648.09	78.56
TIRIGANIAQ	M12-1809	267.00	271.50	1100	0.03	0.03	3.04	4.50	6,988,514.68	539,168.59	74.51
TIRIGANIAQ	M12-1809	296.40	301.00	1000	0.11	0.11	3.12	4.60	6,988,514.68	539,168.59	74.51
TIRIGANIAQ	M12-1814	87.40	90.10	1000	0.32	0.32	2.71	2.70	6,988,369.81	540,129.20	65.27
TIRIGANIAQ	M12-1817	120.90	123.90	1254	0.44	0.44	2.83	3.00	6,988,521.43	540,635.09	70.56
TIRIGANIAQ	M12-1817	125.90	128.90	1257	0.62	0.62	2.83	3.00	6,988,521.43	540,635.09	70.56
TIRIGANIAQ	M12-1817	135.90	138.90	1251	1.01	1.01	2.84	3.00	6,988,521.43	540,635.09	70.56
TIRIGANIAQ	M12-1817	152.10	155.60	1155	1.20	1.20	3.33	3.50	6,988,521.43	540,635.09	70.56
TIRIGANIAQ	M12-1817	153.60	156.70	1100	1.35	1.35	2.95	3.10	6,988,521.43	540,635.09	70.56
TIRIGANIAQ	M12-1817	170.20	173.50	1087	1.12	1.12	3.17	3.30	6,988,521.43	540,635.09	70.56
TIRIGANIAQ	M12-1817	179.50	182.50	1075	0.24	0.24	2.90	3.00	6,988,521.43	540,635.09	70.56
TIRIGANIAQ	M12-1817	191.50	194.50	1050	0.27	0.27	2.93	3.00	6,988,521.43	540,635.09	70.56
TIRIGANIAQ	M12-1817	235.00	237.80	1000	20.24	20.24	2.80	2.80	6,988,521.43	540,635.09	70.56
TIRIGANIAQ	M12-1822	4.60	8.00	1154	0.24	0.24	3.34	3.40	6,988,372.23	540,429.37	66.50
TIRIGANIAQ	M12-1822	16.30	19.20	1100	0.03	0.03	2.85	2.90	6,988,372.23	540,429.37	66.50
TIRIGANIAQ	M12-1822	38.20	41.00	1075	0.03	0.03	2.81	2.80	6,988,372.23	540,429.37	66.50
TIRIGANIAQ	M12-1822	63.20	65.80	1050	0.03	0.03	2.64	2.60	6,988,372.23	540,429.37	66.50
TIRIGANIAQ	M12-1822	88.60	91.10	1000	3.67	3.67	2.56	2.50	6,988,372.23	540,429.37	66.50
TIRIGANIAQ	M12-1823	137.90	140.80	1100	2.51	2.51	2.78	2.90	6,988,457.94	538,800.02	65.94
TIRIGANIAQ	M12-1823	165.80	169.50	1000	0.72	0.72	3.57	3.70	6,988,457.94	538,800.02	65.94
TIRIGANIAQ	M12-1826	16.00	18.60	1000	3.20	3.20	2.59	2.60	6,988,288.89	540,310.25	66.66
TIRIGANIAQ	M12-1828	251.40	254.50	1100	2.21	2.21	2.88	3.10	6,988,563.55	539,291.78	68.87

TIRIGANIAQ	M12-1828	272.60	275.20	1000	1.83	1.83	2.43	2.60	6,988,563.55	539,291.78	68.87
TIRIGANIAQ	M12-1835	69.70	73.50	1102	4.87	4.87	3.44	3.80	6,988,397.23	539,104.12	70.23
TIRIGANIAQ	M12-1835	71.70	74.70	1100	6.17	6.17	2.72	3.00	6,988,397.23	539,104.12	70.23
TIRIGANIAQ	M12-1835	93.00	96.00	1025	3.40	3.40	2.74	3.00	6,988,397.23	539,104.12	70.23
TIRIGANIAQ	M12-1835	104.00	108.00	1000	2.81	2.81	3.67	4.00	6,988,397.23	539,104.12	70.23
TIRIGANIAQ	M12-1840	29.60	33.00	1025	0.07	0.07	3.02	3.40	6,988,342.04	539,208.11	71.96
TIRIGANIAQ	M12-1840	42.40	45.40	1000	2.88	2.88	2.70	3.00	6,988,342.04	539,208.11	71.96
TIRIGANIAQ	M12-1841	297.00	300.00	1170	0.28	0.28	2.47	3.00	6,988,617.04	539,020.01	72.22
TIRIGANIAQ	M12-1841	355.60	358.80	1100	1.49	1.49	2.69	3.20	6,988,617.04	539,020.01	72.22
TIRIGANIAQ	M12-1841	368.00	371.00	1025	0.03	0.03	2.53	3.00	6,988,617.04	539,020.01	72.22
TIRIGANIAQ	M12-1841	380.60	386.80	1000	4.45	4.45	5.26	6.20	6,988,617.04	539,020.01	72.22
TIRIGANIAQ	M12-1848	227.50	230.30	1254	0.25	0.25	2.82	2.80	6,988,645.88	540,569.95	73.47
TIRIGANIAQ	M12-1848	293.00	296.40	1075	0.06	0.06	3.48	3.40	6,988,645.88	540,569.95	73.47
TIRIGANIAQ	M12-1848	306.00	309.00	1050	0.49	0.49	3.07	3.00	6,988,645.88	540,569.95	73.47
TIRIGANIAQ	M12-1852	94.50	97.50	1156	0.18	0.18	2.57	3.00	6,988,448.48	539,198.16	76.11
TIRIGANIAQ	M12-1852	128.30	132.90	1100	2.85	2.85	3.96	4.60	6,988,448.48	539,198.16	76.11
TIRIGANIAQ	M12-1856	86.10	88.40	1102	24.77	24.77	2.33	2.30	6,988,431.00	539,700.24	73.85
TIRIGANIAQ	M12-1856	88.40	91.20	1100	10.08	10.08	2.84	2.80	6,988,431.00	539,700.24	73.85
TIRIGANIAQ	M12-1856	97.00	100.00	1087	3.61	3.61	3.04	3.00	6,988,431.00	539,700.24	73.85
TIRIGANIAQ	M12-1856	106.00	109.00	1075	1.69	1.69	3.04	3.00	6,988,431.00	539,700.24	73.85
TIRIGANIAQ	M12-1856	109.40	113.00	1050	0.58	0.58	3.65	3.60	6,988,431.00	539,700.24	73.85
TIRIGANIAQ	M12-1856	118.00	124.50	1025	1.11	1.11	6.61	6.50	6,988,431.00	539,700.24	73.85
TIRIGANIAQ	M12-1856	127.40	130.00	1000	2.16	2.16	2.64	2.60	6,988,431.00	539,700.24	73.85
TIRIGANIAQ	M12-1861	359.80	363.10	1100	0.29	0.29	2.62	3.30	6,988,618.94	538,927.05	71.15
TIRIGANIAQ	M12-1861	381.90	385.00	1025	0.97	0.97	2.49	3.10	6,988,618.94	538,927.05	71.15
TIRIGANIAQ	M12-1864	101.70	107.30	1100	10.59	10.59	4.71	5.60	6,988,431.82	539,700.27	73.83
TIRIGANIAQ	M12-1864	108.30	111.50	1087	6.06	6.06	2.70	3.20	6,988,431.82	539,700.27	73.83
TIRIGANIAQ	M12-1864	120.60	124.50	1075	5.70	5.70	3.31	3.90	6,988,431.82	539,700.27	73.83
TIRIGANIAQ	M12-1864	127.50	131.10	1050	0.65	0.65	3.06	3.60	6,988,431.82	539,700.27	73.83
TIRIGANIAQ	M12-1864	134.20	140.50	1025	9.17	9.17	5.37	6.30	6,988,431.82	539,700.27	73.83
TIRIGANIAQ	M12-1864	148.50	152.60	1000	2.96	2.96	3.51	4.10	6,988,431.82	539,700.27	73.83
TIRIGANIAQ	M12-1869	32.30	36.00	1050	0.03	0.03	3.54	3.70	6,988,336.97	539,999.92	65.53
TIRIGANIAQ	M12-1869	39.00	42.30	1025	0.05	0.05	3.17	3.30	6,988,336.97	539,999.92	65.53
TIRIGANIAQ	M12-1869	52.50	55.70	1000	75.60	75.60	3.10	3.20	6,988,336.97	539,999.92	65.53
TIRIGANIAQ	M12-1870	34.40	37.00	1075	0.37	0.37	2.52	2.60	6,988,352.42	539,768.04	72.98
TIRIGANIAQ	M12-1870	41.70	44.50	1050	10.21	10.21	2.72	2.80	6,988,352.42	539,768.04	72.98
TIRIGANIAQ	M12-1870	47.50	50.10	1025	0.44	0.44	2.53	2.60	6,988,352.42	539,768.04	72.98
TIRIGANIAQ	M12-1870	55.10	57.60	1000	6.58	6.58	2.44	2.50	6,988,352.42	539,768.04	72.98
TIRIGANIAQ	M12-1871	123.10	126.00	1102	0.95	0.95	2.86	2.90	6,988,461.60	539,650.01	75.97
TIRIGANIAQ	M12-1871	125.80	129.70	1100	3.42	3.42	3.85	3.90	6,988,461.60	539,650.01	75.97
TIRIGANIAQ	M12-1871	131.00	133.30	1087	5.63	5.63	2.28	2.30	6,988,461.60	539,650.01	75.97
TIRIGANIAQ	M12-1871	136.50	139.00	1075	5.80	5.80	2.48	2.50	6,988,461.60	539,650.01	75.97
TIRIGANIAQ	M12-1871	143.40	146.00	1050	0.03	0.03	2.59	2.60	6,988,461.60	539,650.01	75.97
TIRIGANIAQ	M12-1871	156.00	159.00	1025	0.51	0.51	3.00	3.00	6,988,461.60	539,650.01	75.97
TIRIGANIAQ	M12-1871	162.00	164.60	1000	0.71	0.71	2.61	2.60	6,988,461.60	539,650.01	75.97
TIRIGANIAQ	M12-1873	73.90	76.50	1157	0.62	0.62	2.45	2.60	6,988,445.65	539,332.03	72.49
TIRIGANIAQ	M12-1873	90.00	93.00	1156	8.85	8.85	2.85	3.00	6,988,445.65	539,332.03	72.49
TIRIGANIAQ	M12-1873	111.40	114.60	1102	2.83	2.83	3.07	3.20	6,988,445.65	539,332.03	72.49
TIRIGANIAQ	M12-1873	115.20	118.40	1100	2.22	2.22	3.07	3.20	6,988,445.65	539,332.03	72.49
TIRIGANIAQ	M12-1873	138.80	141.40	1025	0.03	0.03	2.52	2.60	6,988,445.65	539,332.03	72.49
TIRIGANIAQ	M12-1873	144.40	147.00	1000	11.23	11.23	2.53	2.60	6,988,445.65	539,332.03	72.49
TIRIGANIAQ	M12-1875	144.40	148.00	1050	0.66	0.66	3.04	3.60	6,988,480.65	538,608.00	61.18
TIRIGANIAQ	M12-1876	59.20	61.80	1000	0.12	0.12	2.60	2.60	6,988,335.45	540,250.06	66.42
TIRIGANIAQ	M12-1877	125.40	128.70	1100	3.82	3.82	3.33	3.30	6,988,475.00	539,749.90	71.30
TIRIGANIAQ	M12-1877	129.80	132.60	1087	0.82	0.82	2.83	2.80	6,988,475.00	539,749.90	71.30
TIRIGANIAQ	M12-1877	138.00	141.00	1075	0.03	0.03	3.03	3.00	6,988,475.00	539,749.90	71.30
TIRIGANIAQ	M12-1877	145.40	153.20	1050	2.49	2.49	7.90	7.80	6,988,475.00	539,749.90	71.30
TIRIGANIAQ	M12-1877	157.00	159.60	1025	0.15	0.15	2.64	2.60	6,988,475.00	539,749.90	71.30
TIRIGANIAQ	M12-1877	164.40	167.80	1000	1.10	1.10	3.45	3.40	6,988,475.00	539,749.90	71.30
TIRIGANIAQ	M12-1882	39.80	44.00	1100	16.35	16.35	4.12	4.20	6,988,374.41	539,309.95	77.02
TIRIGANIAQ	M12-1882	46.00	49.00	1087	0.42	0.42	2.94	3.00	6,988,374.41	539,309.95	77.02
TIRIGANIAQ	M12-1882	52.40	55.30	1075	1.13	1.13	2.85	2.90	6,988,374.41	539,309.95	77.02
TIRIGANIAQ	M12-1882	55.30	58.00	1050	0.49	0.49	2.65	2.70	6,988,374.41	539,309.95	77.02
TIRIGANIAQ	M12-1882	66.80	69.50	1025	0.30	0.30	2.66	2.70	6,988,374.41	539,309.95	77.02
TIRIGANIAQ	M12-1882	76.40	79.40	1000	0.03	0.03	2.95	3.00	6,988,374.41	539,309.95	77.02
TIRIGANIAQ	M12-1883	64.20	67.00	1102	1.79	1.79	2.80	2.80	6,988,393.51	539,022.00	67.16
TIRIGANIAQ	M12-1883	65.40	68.30	1100	1.69	1.69	2.91	2.90	6,988,393.51	539,022.00	67.16
TIRIGANIAQ	M12-1883	81.00	83.60	1025	0.16	0.16	2.62	2.60	6,988,393.51	539,022.00	67.16
TIRIGANIAQ	M12-1883	88.40	91.60	1000	0.31	0.31	3.24	3.20	6,988,393.51	539,022.00	67.16
TIRIGANIAQ	M12-1885	68.90	71.10	1102	0.54	0.54	2.11	2.20	6,988,399.29	539,469.91	75.71
TIRIGANIAQ	M12-1885	71.10	75.00	1100	13.86	13.86	3.74	3.90	6,988,399.29	539,469.91	75.71
TIRIGANIAQ	M12-1885	76.00	79.00	1087	7.58	7.58	2.88	3.00	6,988,399.29	539,469.91	75.71
TIRIGANIAQ	M12-1885	85.00	88.00	1075	1.65	1.65	2.89	3.00	6,988,399.29	539,469.91	75.71
TIRIGANIAQ	M12-1885	91.00	94.00	1050	2.53	2.53	2.89	3.00	6,988,399.29	539,469.91	75.71
TIRIGANIAQ	M12-1885	100.00	102.60	1025	0.82	0.82	2.51	2.60	6,988,399.29	539,469.91	75.71
TIRIGANIAQ	M12-1885	105.00	111.00	1000	12.78	12.78	5.79	6.00	6,988,399.29	539,469.91	75.71
TIRIGANIAQ	M12-1886	48.30	51.30	1102	7.48	7.48	3.01	3.00	6,988,384.22	539,594.99	78.61
TIRIGANIAQ	M12-1886	53.80	59.30	1100	7.86	7.86	5.52	5.50	6,988,384.22	539,594.99	78.61
TIRIGANIAQ	M12-1886	60.80	65.30	1087	1.43	1.43	4.52	4.50	6,988,384.22	539,594.99	78.61
TIRIGANIAQ	M12-1886	65.30	68.30	1075	2.19	2.19	3.02	3.00	6,988,384.22	539,594.99	78.61
TIRIGANIAQ	M12-1886	75.80	78.80	1050	2.95	2.95	3.02	3.00	6,988,384.22	539,594.99	78.61
TIRIGANIAQ	M12-1886	83.00	86.00	1025	2.72	2.72	3.03	3.00	6,988,384.22	539,594.99	78.61
TIRIGANIAQ	M12-1886	91.90	94.20	1000	0.16	0.16	2.32	2.30	6,988,384.22	539,594.99	78.61
TIRIGANIAQ	M13-1908	28.00	30.90	1025	3.35	3.35	2.79	2.90	6,988,370.02	538,599.78	60.06
TIRIGANIAQ	M13-1908	31.90	34.60	1000	0.91	0.91	2.60	2.70	6,988,370.02	538,599.78	60.06
TIRIGANIAQ	M13-1914	10.80	13.00	1000	-	-	2.20	2.20	6,988,283.87	540,224.88	65.71
TIRIGANIAQ	M13-1917	79.00	81.50	1000	0.16	0.16	2.57	2.50	6,988,363.95	540,209.95	66.17
TIRIGANIAQ	M13-1918	83.30	88.30	1100	9.72	9.72	5.10	5.00	6,988,445.15	538,575.83	60.03
TIRIGANIAQ	M13-1918	89.20	91.60	1050	28.48	28.48	2.45	2.40	6,988,445.15	538,575.83	60.03
TIRIGANIAQ	M13-1918	93.20	96.20	1025	0.03	0.03	3.06	3.00	6,988,445.15	538,575.83	60.03

TIRIGANIAQ	M13-1918	97.80	100.30	1000	0.25	0.25	2.55	2.50	6,988,445.15	538,575.83	60.03
TIRIGANIAQ	M13-1920	55.30	57.90	1000	27.22	30.99	2.63	2.60	6,988,334.75	540,149.50	65.35
TIRIGANIAQ	M13-1924	111.10	114.20	1000	0.57	0.57	2.86	3.10	6,988,384.79	540,249.85	66.21
TIRIGANIAQ	M13-1925	140.00	144.00	1155	2.65	2.65	3.42	4.00	6,988,528.07	540,140.21	66.47
TIRIGANIAQ	M13-1925	160.00	165.00	1154	2.91	2.91	4.30	5.00	6,988,528.07	540,140.21	66.47
TIRIGANIAQ	M13-1925	181.40	185.00	1153	0.03	0.03	3.12	3.60	6,988,528.07	540,140.21	66.47
TIRIGANIAQ	M13-1925	205.00	208.00	1100	2.22	2.22	2.63	3.00	6,988,528.07	540,140.21	66.47
TIRIGANIAQ	M13-1925	241.00	244.00	1050	0.32	0.32	2.67	3.00	6,988,528.07	540,140.21	66.47
TIRIGANIAQ	M13-1925	246.00	249.50	1025	0.03	0.03	3.12	3.50	6,988,528.07	540,140.21	66.47
TIRIGANIAQ	M13-1925	253.50	257.00	1000	0.13	0.13	3.13	3.50	6,988,528.07	540,140.21	66.47
TIRIGANIAQ	M13-1928	144.30	148.30	1102	1.33	1.33	3.64	4.00	6,988,484.96	540,160.05	66.69
TIRIGANIAQ	M13-1928	148.90	151.90	1100	0.41	0.41	2.74	3.00	6,988,484.96	540,160.05	66.69
TIRIGANIAQ	M13-1928	182.40	185.80	1050	2.58	2.58	3.14	3.40	6,988,484.96	540,160.05	66.69
TIRIGANIAQ	M13-1928	191.80	195.00	1025	6.16	6.16	2.96	3.20	6,988,484.96	540,160.05	66.69
TIRIGANIAQ	M13-1928	199.90	204.10	1000	4.08	4.08	3.89	4.20	6,988,484.96	540,160.05	66.69
TIRIGANIAQ	M13-1929	183.70	186.50	1154	-	-	2.77	2.80	6,988,569.80	539,999.80	66.78
TIRIGANIAQ	M13-1929	199.00	202.00	1153	0.24	0.24	3.00	3.00	6,988,569.80	539,999.80	66.78
TIRIGANIAQ	M13-1929	227.80	230.60	1100	0.46	0.46	2.84	2.80	6,988,569.80	539,999.80	66.78
TIRIGANIAQ	M13-1929	232.30	234.70	1087	2.03	2.03	2.43	2.40	6,988,569.80	539,999.80	66.78
TIRIGANIAQ	M13-1929	238.30	240.80	1075	0.58	0.58	2.54	2.50	6,988,569.80	539,999.80	66.78
TIRIGANIAQ	M13-1929	250.40	252.80	1050	0.43	0.43	2.44	2.40	6,988,569.80	539,999.80	66.78
TIRIGANIAQ	M13-1929	254.70	257.30	1025	6.75	6.75	2.65	2.60	6,988,569.80	539,999.80	66.78
TIRIGANIAQ	M13-1929	268.40	271.10	1000	5.02	5.02	2.76	2.70	6,988,569.80	539,999.80	66.78
TIRIGANIAQ	M13-1931	92.30	95.20	1102	3.78	3.78	2.84	2.90	6,988,427.45	539,274.55	75.35
TIRIGANIAQ	M13-1931	94.10	96.60	1100	3.36	3.36	2.45	2.50	6,988,427.45	539,274.55	75.35
TIRIGANIAQ	M13-1931	113.40	115.90	1025	2.74	2.74	2.48	2.50	6,988,427.45	539,274.55	75.35
TIRIGANIAQ	M13-1931	123.00	126.00	1000	0.14	0.14	2.99	3.00	6,988,427.45	539,274.55	75.35
TIRIGANIAQ	M13-1933A	315.90	318.80	1153	0.04	0.04	3.04	2.90	6,988,676.75	540,250.02	65.57
TIRIGANIAQ	M13-1933A	322.70	325.70	1100	5.67	5.67	3.15	3.00	6,988,676.75	540,250.02	65.57
TIRIGANIAQ	M13-1933A	335.20	338.50	1075	0.80	0.80	3.48	3.30	6,988,676.75	540,250.02	65.57
TIRIGANIAQ	M13-1933A	345.00	348.00	1050	0.16	0.16	3.16	3.00	6,988,676.75	540,250.02	65.57
TIRIGANIAQ	M13-1933A	352.50	355.00	1025	0.06	0.06	2.64	2.50	6,988,676.75	540,250.02	65.57
TIRIGANIAQ	M13-1933A	375.30	377.70	1000	0.65	0.65	2.54	2.40	6,988,676.75	540,250.02	65.57
TIRIGANIAQ	M13-1935	192.90	196.10	1151	-	-	2.82	3.20	6,988,523.10	539,944.71	65.89
TIRIGANIAQ	M13-1935	205.30	212.30	1100	17.55	17.55	6.22	7.00	6,988,523.10	539,944.71	65.89
TIRIGANIAQ	M13-1935	212.30	215.20	1087	0.15	0.15	2.58	2.90	6,988,523.10	539,944.71	65.89
TIRIGANIAQ	M13-1935	217.50	220.20	1075	1.06	1.06	2.42	2.70	6,988,523.10	539,944.71	65.89
TIRIGANIAQ	M13-1935	227.20	229.90	1050	5.13	5.13	2.43	2.70	6,988,523.10	539,944.71	65.89
TIRIGANIAQ	M13-1935	233.20	235.80	1025	1.56	1.56	2.35	2.60	6,988,523.10	539,944.71	65.89
TIRIGANIAQ	M13-1935	243.20	245.80	1000	10.39	10.39	2.36	2.60	6,988,523.10	539,944.71	65.89
TIRIGANIAQ	M13-1940	261.20	264.10	1100	23.19	23.19	2.65	2.90	6,988,554.38	539,266.17	68.53
TIRIGANIAQ	M13-1940	281.30	284.00	1000	0.03	0.03	2.48	2.70	6,988,554.38	539,266.17	68.53
TIRIGANIAQ	M13-1943	172.00	175.00	1100	0.37	0.37	2.85	3.00	6,988,510.67	539,924.89	66.21
TIRIGANIAQ	M13-1943	176.00	178.60	1087	0.40	0.40	2.47	2.60	6,988,510.67	539,924.89	66.21
TIRIGANIAQ	M13-1943	187.00	190.00	1075	3.15	3.15	2.86	3.00	6,988,510.67	539,924.89	66.21
TIRIGANIAQ	M13-1943	194.40	197.00	1050	0.45	0.45	2.48	2.60	6,988,510.67	539,924.89	66.21
TIRIGANIAQ	M13-1943	202.50	205.00	1025	1.02	1.02	2.39	2.50	6,988,510.67	539,924.89	66.21
TIRIGANIAQ	M13-1943	211.00	213.20	1000	10.09	10.09	2.11	2.20	6,988,510.67	539,924.89	66.21
TIRIGANIAQ	M13-1945	442.70	445.50	1100	2.30	2.30	2.70	2.80	6,988,771.05	540,149.92	65.58
TIRIGANIAQ	M13-1945	464.20	466.60	1050	1.86	1.86	2.33	2.40	6,988,771.05	540,149.92	65.58
TIRIGANIAQ	M13-1945	474.90	477.60	1025	11.13	11.13	2.63	2.70	6,988,771.05	540,149.92	65.58
TIRIGANIAQ	M13-1945	481.65	484.50	1000	1.09	1.09	2.78	2.85	6,988,771.05	540,149.92	65.58
TIRIGANIAQ	M13-1947	167.40	170.00	1050	1.62	1.62	2.64	2.60	6,988,495.71	538,739.58	65.64
TIRIGANIAQ	M13-1947	181.40	184.00	1000	5.61	5.61	2.65	2.60	6,988,495.71	538,739.58	65.64
TIRIGANIAQ	M13-1949	385.80	389.30	1153	1.26	1.26	2.98	3.50	6,988,730.87	538,675.11	66.26
TIRIGANIAQ	M13-1949	422.20	426.50	1100	8.98	8.98	3.80	4.30	6,988,730.87	538,675.11	66.26
TIRIGANIAQ	M13-1949	427.30	430.30	1075	0.46	0.46	2.66	3.00	6,988,730.87	538,675.11	66.26
TIRIGANIAQ	M13-1951	217.40	222.00	1155	0.33	0.33	3.72	4.60	6,988,583.85	539,869.75	66.63
TIRIGANIAQ	M13-1951	242.00	247.00	1154	6.65	6.65	4.07	5.00	6,988,583.85	539,869.75	66.63
TIRIGANIAQ	M13-1951	251.00	254.80	1153	1.53	1.53	3.10	3.80	6,988,583.85	539,869.75	66.63
TIRIGANIAQ	M13-1951	262.00	266.80	1152	13.19	13.19	3.93	4.80	6,988,583.85	539,869.75	66.63
TIRIGANIAQ	M13-1951	268.20	272.00	1151	5.24	5.24	3.12	3.80	6,988,583.85	539,869.75	66.63
TIRIGANIAQ	M13-1951	281.00	287.90	1100	10.15	10.15	5.69	6.90	6,988,583.85	539,869.75	66.63
TIRIGANIAQ	M13-1951	292.00	295.00	1087	11.22	11.22	2.48	3.00	6,988,583.85	539,869.75	66.63
TIRIGANIAQ	M13-1951	299.50	303.00	1075	13.34	13.34	2.91	3.50	6,988,583.85	539,869.75	66.63
TIRIGANIAQ	M13-1951	310.00	313.00	1050	0.22	0.22	2.50	3.00	6,988,583.85	539,869.75	66.63
TIRIGANIAQ	M13-1951	321.40	324.80	1000	0.24	0.24	2.85	3.40	6,988,583.85	539,869.75	66.63
TIRIGANIAQ	M13-1952	41.00	44.00	1075	0.03	0.03	2.93	3.00	6,988,385.43	540,899.74	67.68
TIRIGANIAQ	M13-1952	54.50	57.00	1050	6.79	6.79	2.46	2.50	6,988,385.43	540,899.74	67.68
TIRIGANIAQ	M13-1954	199.00	202.00	1100	0.28	0.28	2.63	3.00	6,988,495.20	538,839.87	65.48
TIRIGANIAQ	M13-1954	203.40	206.40	1050	2.06	2.06	2.63	3.00	6,988,495.20	538,839.87	65.48
TIRIGANIAQ	M13-1954	210.40	213.40	1025	2.80	2.80	2.64	3.00	6,988,495.20	538,839.87	65.48
TIRIGANIAQ	M13-1954	224.80	227.90	1000	2.20	2.20	2.74	3.10	6,988,495.20	538,839.87	65.48
TIRIGANIAQ	M13-1956	292.00	295.00	1100	0.03	0.03	2.34	3.00	6,988,570.41	539,279.65	68.03
TIRIGANIAQ	M13-1956	327.00	330.10	1000	0.03	0.03	2.47	3.10	6,988,570.41	539,279.65	68.03
TIRIGANIAQ	M13-1961	444.00	446.60	1075	0.14	0.14	2.78	2.60	6,988,771.14	540,224.99	65.72
TIRIGANIAQ	M13-1961	449.00	451.80	1050	2.56	2.56	3.00	2.80	6,988,771.14	540,224.99	65.72
TIRIGANIAQ	M13-1961	460.80	463.00	1025	0.03	0.03	2.36	2.20	6,988,771.14	540,224.99	65.72
TIRIGANIAQ	M13-1961	464.40	468.30	1000	0.50	0.50	4.19	3.90	6,988,771.14	540,224.99	65.72
TIRIGANIAQ	M13-1963	118.60	123.00	1100	6.62	6.62	4.43	4.40	6,988,473.27	539,800.03	69.58
TIRIGANIAQ	M13-1963	131.00	134.00	1087	5.08	5.08	3.03	3.00	6,988,473.27	539,800.03	69.58
TIRIGANIAQ	M13-1963	141.40	144.00	1075	0.13	0.13	2.63	2.60	6,988,473.27	539,800.03	69.58
TIRIGANIAQ	M13-1963	149.00	152.00	1050	22.05	22.05	3.03	3.00	6,988,473.27	539,800.03	69.58
TIRIGANIAQ	M13-1963	154.00	156.60	1025	1.69	1.69	2.63	2.60	6,988,473.27	539,800.03	69.58
TIRIGANIAQ	M13-1963	161.00	163.40	1000	0.03	0.03	2.43	2.40	6,988,473.27	539,800.03	69.58
TIRIGANIAQ	M13-1966	155.10	158.10	1100	0.03	0.03	2.91	3.00	6,988,470.26	538,864.90	65.47
TIRIGANIAQ	M13-1966	170.50	173.35	1000	4.05	4.05	2.78	2.85	6,988,470.26	538,864.90	65.47
TIRIGANIAQ	M13-1967	264.50	268.60	1153	2.20	2.20	3.39	4.10	6,988,621.36	539,364.84	76.07
TIRIGANIAQ	M13-1967	327.40	330.30	1100	0.80	0.80	2.48	2.90	6,988,621.36	539,364.84	76.07
TIRIGANIAQ	M13-1967	340.50	343.40	1075	0.03	0.03	2.49	2.90	6,988,621.36	539,364.84	76.07

TIRIGANIAQ	M13-1967	363.40	366.60	1025	1.30	1.30	2.75	3.20	6,988,621.36	539,364.84	76.07
TIRIGANIAQ	M13-1967	368.00	371.50	1015	17.54	17.54	3.00	3.50	6,988,621.36	539,364.84	76.07
TIRIGANIAQ	M13-1967	373.00	376.10	1000	0.11	0.11	2.66	3.10	6,988,621.36	539,364.84	76.07
TIRIGANIAQ	M13-1972	145.20	148.90	1100	4.33	4.33	3.54	3.70	6,988,490.35	539,749.70	70.71
TIRIGANIAQ	M13-1972	155.00	158.00	1087	5.56	5.56	2.87	3.00	6,988,490.35	539,749.70	70.71
TIRIGANIAQ	M13-1972	160.40	163.50	1075	0.57	0.57	2.97	3.10	6,988,490.35	539,749.70	70.71
TIRIGANIAQ	M13-1972	174.90	178.00	1050	4.88	4.88	2.98	3.10	6,988,490.35	539,749.70	70.71
TIRIGANIAQ	M13-1972	179.00	181.60	1025	4.12	4.12	2.50	2.60	6,988,490.35	539,749.70	70.71
TIRIGANIAQ	M13-1972	185.00	188.00	1000	7.12	7.12	2.89	3.00	6,988,490.35	539,749.70	70.71
TIRIGANIAQ	M13-1975	379.80	382.80	1075	2.36	2.36	2.88	3.00	6,988,704.03	540,330.02	66.21
TIRIGANIAQ	M13-1975	390.00	393.00	1050	0.25	0.25	2.88	3.00	6,988,704.03	540,330.02	66.21
TIRIGANIAQ	M13-1975	424.50	427.40	1000	18.23	18.23	2.81	2.90	6,988,704.03	540,330.02	66.21
TIRIGANIAQ	M13-1976	258.90	261.60	1100	1.49	1.49	2.60	2.70	6,988,540.04	538,889.88	65.89
TIRIGANIAQ	M13-1976	265.00	267.50	1050	0.03	0.03	2.45	2.50	6,988,540.04	538,889.88	65.89
TIRIGANIAQ	M13-1976	282.30	287.00	1000	17.22	19.67	4.78	4.70	6,988,540.04	538,889.88	65.89
TIRIGANIAQ	M13-1981	330.10	333.90	1155	1.31	1.31	3.37	3.80	6,988,691.79	539,320.03	75.88
TIRIGANIAQ	M13-1981	344.40	348.00	1154	3.15	3.15	3.22	3.60	6,988,691.79	539,320.03	75.88
TIRIGANIAQ	M13-1981	349.40	352.80	1153	3.53	3.53	3.05	3.40	6,988,691.79	539,320.03	75.88
TIRIGANIAQ	M13-1981	352.20	355.50	1150	1.05	1.05	2.97	3.30	6,988,691.79	539,320.03	75.88
TIRIGANIAQ	M13-1981	359.10	362.60	1152	2.00	2.00	3.16	3.50	6,988,691.79	539,320.03	75.88
TIRIGANIAQ	M13-1981	363.40	366.80	1170	18.28	18.28	3.08	3.40	6,988,691.79	539,320.03	75.88
TIRIGANIAQ	M13-1981	380.00	383.40	1160	7.11	7.11	3.14	3.40	6,988,691.79	539,320.03	75.88
TIRIGANIAQ	M13-1981	395.30	397.80	1100	0.04	0.04	2.35	2.50	6,988,691.79	539,320.03	75.88
TIRIGANIAQ	M13-1981	401.00	403.50	1075	0.17	0.17	2.37	2.50	6,988,691.79	539,320.03	75.88
TIRIGANIAQ	M13-1981	419.40	422.10	1025	1.05	1.05	2.59	2.70	6,988,691.79	539,320.03	75.88
TIRIGANIAQ	M13-1981	425.20	427.90	1015	9.76	9.76	2.59	2.70	6,988,691.79	539,320.03	75.88
TIRIGANIAQ	M13-1981	439.60	442.60	1000	0.22	0.22	2.90	3.00	6,988,691.79	539,320.03	75.88
TIRIGANIAQ	M13-1985	266.00	268.60	1100	0.68	0.68	2.27	2.60	6,988,547.31	538,969.80	70.57
TIRIGANIAQ	M13-1985	272.00	274.30	1050	0.32	0.32	2.01	2.30	6,988,547.31	538,969.80	70.57
TIRIGANIAQ	M13-1985	274.70	277.40	1025	0.29	0.29	2.36	2.70	6,988,547.31	538,969.80	70.57
TIRIGANIAQ	M13-1985	278.60	281.10	1000	1.41	1.41	2.19	2.50	6,988,547.31	538,969.80	70.57
TIRIGANIAQ	M13-1990	272.90	276.30	1154	0.03	0.03	2.92	3.40	6,988,634.77	539,609.96	73.02
TIRIGANIAQ	M13-1990	286.20	289.50	1153	1.89	1.89	2.86	3.30	6,988,634.77	539,609.96	73.02
TIRIGANIAQ	M13-1990	320.20	323.30	1152	1.56	1.56	2.73	3.10	6,988,634.77	539,609.96	73.02
TIRIGANIAQ	M13-1990	329.80	333.00	1151	0.62	0.62	2.83	3.20	6,988,634.77	539,609.96	73.02
TIRIGANIAQ	M13-1990	340.20	342.80	1100	1.46	1.46	2.30	2.60	6,988,634.77	539,609.96	73.02
TIRIGANIAQ	M13-1999	161.60	165.30	1254	0.06	0.06	3.23	3.70	6,988,550.20	540,700.55	69.44
TIRIGANIAQ	M13-1999	230.80	234.00	1075	1.62	1.62	2.90	3.20	6,988,550.20	540,700.55	69.44
TIRIGANIAQ	M13-1999	255.70	259.50	1025	0.18	0.18	3.52	3.80	6,988,550.20	540,700.55	69.44
TIRIGANIAQ	M13-1999	285.00	288.00	1000	0.57	0.57	2.82	3.00	6,988,550.20	540,700.55	69.44
TIRIGANIAQ	M13-2004	289.60	294.50	1154	9.43	9.43	4.03	4.90	6,988,646.14	539,580.08	73.65
TIRIGANIAQ	M13-2004	297.30	301.20	1153	3.13	3.13	3.21	3.90	6,988,646.14	539,580.08	73.65
TIRIGANIAQ	M13-2004	329.80	333.70	1150	1.60	1.60	3.25	3.90	6,988,646.14	539,580.08	73.65
TIRIGANIAQ	M13-2004	342.10	345.10	1152	0.24	0.24	2.52	3.00	6,988,646.14	539,580.08	73.65
TIRIGANIAQ	M13-2004	354.00	357.30	1151	0.71	0.71	2.78	3.30	6,988,646.14	539,580.08	73.65
TIRIGANIAQ	M13-2004	364.10	366.90	1100	13.70	13.70	2.37	2.80	6,988,646.14	539,580.08	73.65
TIRIGANIAQ	M13-2004	370.70	373.40	1075	0.03	0.03	2.29	2.70	6,988,646.14	539,580.08	73.65
TIRIGANIAQ	M13-2004	389.10	392.30	1025	3.64	3.64	2.75	3.20	6,988,646.14	539,580.08	73.65
TIRIGANIAQ	M13-2004	395.70	398.50	1000	0.05	0.05	2.42	2.80	6,988,646.14	539,580.08	73.65
TIRIGANIAQ	M13-2006	141.90	144.50	1157	0.67	0.67	2.35	2.60	6,988,522.43	539,024.62	71.55
TIRIGANIAQ	M13-2006	223.40	226.50	1100	0.85	0.85	2.87	3.10	6,988,522.43	539,024.62	71.55
TIRIGANIAQ	M13-2006	230.50	233.50	1025	3.87	3.87	2.79	3.00	6,988,522.43	539,024.62	71.55
TIRIGANIAQ	M13-2013	126.50	129.60	1254	0.85	0.85	2.59	3.10	6,988,523.09	540,839.98	65.82
TIRIGANIAQ	M13-2013	186.00	190.00	1075	0.60	0.60	3.38	4.00	6,988,523.09	540,839.98	65.82
TIRIGANIAQ	M13-2013	196.00	200.60	1050	1.81	1.81	3.91	4.60	6,988,523.09	540,839.98	65.82
TIRIGANIAQ	M13-2013	214.00	217.60	1025	0.38	0.38	3.08	3.60	6,988,523.09	540,839.98	65.82
TIRIGANIAQ	M13-2027	427.00	430.50	1153	0.03	0.03	3.35	3.50	6,988,777.86	538,960.02	64.02
TIRIGANIAQ	M13-2027	433.50	437.20	1152	0.34	0.34	3.55	3.70	6,988,777.86	538,960.02	64.02
TIRIGANIAQ	M13-2027	469.00	471.40	1100	1.88	1.88	2.32	2.40	6,988,777.86	538,960.02	64.02
TIRIGANIAQ	M13-2027	482.30	484.50	1050	0.14	0.14	2.13	2.20	6,988,777.86	538,960.02	64.02
TIRIGANIAQ	M13-2027	489.70	492.40	1025	1.16	1.16	2.62	2.70	6,988,777.86	538,960.02	64.02
TIRIGANIAQ	M13-2027	498.20	500.60	1015	19.88	19.88	2.33	2.40	6,988,777.86	538,960.02	64.02
TIRIGANIAQ	M13-2027	501.60	504.60	1000	0.93	0.93	2.92	3.00	6,988,777.86	538,960.02	64.02
TIRIGANIAQ	M13-2030A	289.50	291.80	1100	0.13	0.13	1.88	2.30	6,988,561.59	539,114.94	72.39
TIRIGANIAQ	M13-2030A	304.70	308.00	1025	0.03	0.03	2.72	3.30	6,988,561.59	539,114.94	72.39
TIRIGANIAQ	M13-2030A	317.60	322.20	1000	0.06	0.06	3.82	4.60	6,988,561.59	539,114.94	72.39
TIRIGANIAQ	M13-2050	461.80	465.50	1252	11.08	11.08	3.46	3.70	6,988,822.04	538,959.91	63.24
TIRIGANIAQ	M13-2050	509.20	513.00	1100	1.32	1.32	3.63	3.80	6,988,822.04	538,959.91	63.24
TIRIGANIAQ	M13-2050	530.00	532.40	1050	13.37	13.37	2.31	2.40	6,988,822.04	538,959.91	63.24
TIRIGANIAQ	M13-2050	537.80	541.10	1025	6.21	6.21	3.19	3.30	6,988,822.04	538,959.91	63.24
TIRIGANIAQ	M13-2050	542.40	545.30	1015	7.35	7.35	2.81	2.90	6,988,822.04	538,959.91	63.24
TIRIGANIAQ	M13-2050	548.40	550.50	1000	5.04	5.04	2.04	2.10	6,988,822.04	538,959.91	63.24
TIRIGANIAQ	M13-2059A	433.60	437.20	1153	-	-	3.13	3.60	6,988,755.73	538,620.13	67.20
TIRIGANIAQ	M13-2059A	459.30	462.50	1100	11.58	11.58	2.81	3.20	6,988,755.73	538,620.13	67.20
TIRIGANIAQ	M13-2059A	472.40	475.50	1075	13.24	13.24	2.73	3.10	6,988,755.73	538,620.13	67.20
TIRIGANIAQ	M13-2071B	424.10	427.40	1100	13.89	13.89	2.80	3.30	6,988,754.20	538,480.90	65.54
TIRIGANIAQ	M13-2071B	439.80	443.00	1075	0.40	0.40	2.72	3.20	6,988,754.20	538,480.90	65.54
TIRIGANIAQ	M13-2072	78.00	80.80	1157	0.06	0.06	2.81	2.80	6,988,470.07	539,000.03	69.12
TIRIGANIAQ	M13-2072	143.80	146.40	1100	0.51	0.51	2.68	2.60	6,988,470.07	539,000.03	69.12
TIRIGANIAQ	M13-2078	156.40	159.00	1152	2.97	2.97	2.31	2.60	6,988,513.16	539,400.12	75.71
TIRIGANIAQ	M13-2078	200.50	204.20	1100	1.46	1.46	3.33	3.70	6,988,513.16	539,400.12	75.71
TIRIGANIAQ	M13-2084	430.20	435.00	1153	8.06	8.06	4.22	4.80	6,988,796.46	538,430.08	65.91
TIRIGANIAQ	M13-2084	463.80	466.80	1100	18.38	18.38	2.64	3.00	6,988,796.46	538,430.08	65.91
TIRIGANIAQ	M13-2084	470.00	472.70	1075	0.71	0.71	2.38	2.70	6,988,796.46	538,430.08	65.91
TIRIGANIAQ	M13-2091	164.70	167.70	1254	0.37	0.37	2.74	3.00	6,988,580.78	540,499.98	69.11
TIRIGANIAQ	M13-2091	180.10	183.00	1257	0.31	0.31	2.66	2.90	6,988,580.78	540,499.98	69.11
TIRIGANIAQ	M13-2097A	109.20	111.80	1152	-	-	2.40	2.60	6,988,465.06	539,500.06	76.96
TIRIGANIAQ	M13-2097A	142.90	145.70	1100	0.96	0.96	2.63	2.80	6,988,465.06	539,500.06	76.96
TIRIGANIAQ	M13-2097A	151.90	154.60	1075	5.76	5.76	2.54	2.70	6,988,465.06	539,500.06	76.96
TIRIGANIAQ	M13-2097A	155.50	158.10	1050	0.85	0.85	2.45	2.60	6,988,465.06	539,500.06	76.96

TIRIGANIAQ	M13-2097A	164.50	167.50	1025	0.98	0.98	2.84	3.00	6,988,465.06	539,500.06	76.96
TIRIGANIAQ	M13-2097A	169.00	172.80	1000	0.15	0.15	3.61	3.80	6,988,465.06	539,500.06	76.96
TIRIGANIAQ	M13-2112	95.30	97.80	1102	4.66	4.66	2.27	2.50	6,988,422.69	539,599.89	78.08
TIRIGANIAQ	M13-2112	97.80	102.10	1100	13.17	13.17	3.91	4.30	6,988,422.69	539,599.89	78.08
TIRIGANIAQ	M13-2112	104.50	107.60	1087	4.21	4.21	2.83	3.10	6,988,422.69	539,599.89	78.08
TIRIGANIAQ	M13-2112	107.60	115.70	1075	24.91	24.91	7.39	8.10	6,988,422.69	539,599.89	78.08
TIRIGANIAQ	M13-2112	121.20	124.50	1050	1.09	1.09	3.02	3.30	6,988,422.69	539,599.89	78.08
TIRIGANIAQ	M13-2112	129.00	132.10	1025	0.85	0.85	2.85	3.10	6,988,422.69	539,599.89	78.08
TIRIGANIAQ	M13-2112	136.40	138.70	1000	17.16	17.16	2.12	2.30	6,988,422.69	539,599.89	78.08
TIRIGANIAQ	M13-2125	309.50	312.20	1100	0.18	0.18	2.71	2.70	6,988,645.88	539,465.75	77.34
TIRIGANIAQ	M13-2126	153.00	155.80	1100	0.38	0.38	2.75	2.80	6,988,499.59	539,861.85	68.12
TIRIGANIAQ	M13-2126	168.00	171.00	1087	2.69	2.69	2.96	3.00	6,988,499.59	539,861.85	68.12
TIRIGANIAQ	M13-2126	173.30	176.10	1075	0.43	0.43	2.77	2.80	6,988,499.59	539,861.85	68.12
TIRIGANIAQ	M13-2126	178.70	181.50	1050	0.05	0.05	2.77	2.80	6,988,499.59	539,861.85	68.12
TIRIGANIAQ	M13-2126	184.50	189.00	1025	1.61	1.61	4.47	4.50	6,988,499.59	539,861.85	68.12
TIRIGANIAQ	M13-2126	190.00	193.00	1000	50.93	50.93	2.98	3.00	6,988,499.59	539,861.85	68.12
TIRIGANIAQ	M13-2187	327.20	329.50	1260	4.07	4.07	2.06	2.30	6,988,739.38	539,790.15	67.11
TIRIGANIAQ	M13-2187	338.60	341.30	1263	4.21	4.21	2.42	2.70	6,988,739.38	539,790.15	67.11
TIRIGANIAQ	M13-2187	346.70	349.70	1256	0.33	0.33	2.70	3.00	6,988,739.38	539,790.15	67.11
TIRIGANIAQ	M13-2187	375.80	379.50	1252	0.51	0.51	3.36	3.70	6,988,739.38	539,790.15	67.11
TIRIGANIAQ	M13-2187	390.00	393.20	1251	7.01	7.01	2.92	3.20	6,988,739.38	539,790.15	67.11
TIRIGANIAQ	M13-2187	397.50	400.50	1155	0.80	0.80	2.74	3.00	6,988,739.38	539,790.15	67.11
TIRIGANIAQ	M13-2187	407.80	411.00	1154	2.19	2.19	2.93	3.20	6,988,739.38	539,790.15	67.11
TIRIGANIAQ	M13-2187	416.20	419.10	1153	3.56	3.56	2.67	2.90	6,988,739.38	539,790.15	67.11
TIRIGANIAQ	M13-2187	421.80	424.80	1152	2.76	2.76	2.76	3.00	6,988,739.38	539,790.15	67.11
TIRIGANIAQ	M13-2187	424.80	428.00	1100	13.43	13.43	2.95	3.20	6,988,739.38	539,790.15	67.11
TIRIGANIAQ	M13-2187	438.00	441.00	1075	0.03	0.03	2.79	3.00	6,988,739.38	539,790.15	67.11
TIRIGANIAQ	M13-2187	450.30	453.30	1050	0.46	0.46	2.80	3.00	6,988,739.38	539,790.15	67.11
TIRIGANIAQ	M13-2187	458.30	461.20	1025	0.30	0.30	2.71	2.90	6,988,739.38	539,790.15	67.11
TIRIGANIAQ	M14-2257	228.00	232.00	1153	0.07	0.07	3.52	4.00	6,988,580.93	539,910.18	66.71
TIRIGANIAQ	M14-2257	248.60	251.50	1151	0.50	0.50	2.57	2.90	6,988,580.93	539,910.18	66.71
TIRIGANIAQ	M14-2257	259.60	262.60	1100	0.04	0.04	2.68	3.00	6,988,580.93	539,910.18	66.71
TIRIGANIAQ	M14-2257	266.60	270.00	1087	0.00	0.00	3.05	3.40	6,988,580.93	539,910.18	66.71
TIRIGANIAQ	M14-2257	285.00	288.00	1050	0.01	0.01	2.71	3.00	6,988,580.93	539,910.18	66.71
TIRIGANIAQ	M14-2257	293.40	296.40	1000	0.11	0.11	2.72	3.00	6,988,580.93	539,910.18	66.71
TIRIGANIAQ	M14-2266	34.70	37.10	1000	0.40	0.40	2.36	2.40	6,988,384.88	538,536.31	60.14
TIRIGANIAQ	M14-2269	13.50	16.00	1050	0.72	0.72	2.42	2.50	6,988,386.02	538,496.81	59.58
TIRIGANIAQ	M14-2269	31.20	34.60	1000	0.15	0.15	3.32	3.40	6,988,386.02	538,496.81	59.58
TIRIGANIAQ	M14-2272	99.80	103.30	1100	9.30	9.30	3.40	3.50	6,988,443.80	538,640.00	61.02
TIRIGANIAQ	M14-2272	104.30	109.70	1050	3.09	3.09	5.25	5.40	6,988,443.80	538,640.00	61.02
TIRIGANIAQ	M14-2272	111.50	114.00	1025	3.77	3.77	2.44	2.50	6,988,443.80	538,640.00	61.02
TIRIGANIAQ	M14-2272	118.40	121.50	1000	0.63	0.63	3.03	3.10	6,988,443.80	538,640.00	61.02
TIRIGANIAQ	M14-2296	71.30	74.00	1100	4.05	4.05	2.41	2.70	6,988,438.03	540,885.52	67.01
TIRIGANIAQ	M14-2296	95.30	98.30	1075	0.16	0.16	2.69	3.00	6,988,438.03	540,885.52	67.01
TIRIGANIAQ	M14-2296	105.00	114.00	1050	1.47	1.47	8.10	9.00	6,988,438.03	540,885.52	67.01
TIRIGANIAQ	M14-2296	123.00	126.00	1025	3.35	3.35	2.71	3.00	6,988,438.03	540,885.52	67.01
TIRIGANIAQ	M14-2302	635.80	638.20	1025	0.01	0.01	2.37	2.40	6,988,905.39	539,250.16	75.11
TIRIGANIAQ	M14-2302	641.00	643.80	1015	0.01	0.01	2.77	2.80	6,988,905.39	539,250.16	75.11
TIRIGANIAQ	M14-2302	647.00	649.80	1000	3.80	3.80	2.78	2.80	6,988,905.39	539,250.16	75.11
TIRIGANIAQ	M14-2307	317.70	324.00	1154	3.60	3.60	5.20	6.30	6,988,667.96	539,540.10	74.21
TIRIGANIAQ	M14-2307	329.70	337.70	1153	3.86	3.86	6.62	8.00	6,988,667.96	539,540.10	74.21
TIRIGANIAQ	M14-2307	349.50	352.70	1150	9.94	9.94	2.66	3.20	6,988,667.96	539,540.10	74.21
TIRIGANIAQ	M14-2307	365.90	369.60	1152	0.07	0.07	3.09	3.70	6,988,667.96	539,540.10	74.21
TIRIGANIAQ	M14-2307	375.40	378.80	1100	0.19	0.19	2.85	3.40	6,988,667.96	539,540.10	74.21
TIRIGANIAQ	M14-2307	391.20	393.80	1075	0.06	0.06	2.19	2.60	6,988,667.96	539,540.10	74.21
TIRIGANIAQ	M14-2307	406.20	409.20	1025	0.01	0.01	2.54	3.00	6,988,667.96	539,540.10	74.21
TIRIGANIAQ	M14-2307	407.10	411.90	1015	0.07	0.07	4.07	4.80	6,988,667.96	539,540.10	74.21
TIRIGANIAQ	M14-2307	411.90	420.00	1000	14.07	14.07	6.88	8.10	6,988,667.96	539,540.10	74.21
TIRIGANIAQ	M14-2308	170.40	172.70	1152	4.01	4.01	2.16	2.30	6,988,519.94	539,584.96	76.81
TIRIGANIAQ	M14-2308	194.50	197.20	1100	1.65	1.65	2.58	2.70	6,988,519.94	539,584.96	76.81
TIRIGANIAQ	M14-2308	206.40	208.90	1075	0.04	0.04	2.40	2.50	6,988,519.94	539,584.96	76.81
TIRIGANIAQ	M14-2308	231.50	234.40	1000	0.11	0.11	2.81	2.90	6,988,519.94	539,584.96	76.81
TIRIGANIAQ	M14-2309	217.20	220.30	1153	11.27	11.27	2.64	3.10	6,988,580.72	539,545.19	77.01
TIRIGANIAQ	M14-2309	282.70	285.90	1100	1.91	1.91	2.81	3.20	6,988,580.72	539,545.19	77.01
TIRIGANIAQ	M14-2310	314.30	317.00	1153	0.14	0.14	2.56	2.70	6,988,673.59	539,540.47	74.36
TIRIGANIAQ	M14-2310	334.50	338.10	1150	2.04	2.04	3.45	3.60	6,988,673.59	539,540.47	74.36
TIRIGANIAQ	M14-2310	343.80	349.20	1152	6.64	6.64	5.19	5.40	6,988,673.59	539,540.47	74.36
TIRIGANIAQ	M14-2310	359.10	361.70	1100	0.24	0.24	2.51	2.60	6,988,673.59	539,540.47	74.36
TIRIGANIAQ	M14-2311	278.50	282.20	1153	0.01	0.01	3.13	3.70	6,988,641.08	539,580.07	73.61
TIRIGANIAQ	M14-2311	315.20	318.50	1150	2.03	2.03	2.84	3.30	6,988,641.08	539,580.07	73.61
TIRIGANIAQ	M14-2311	324.10	325.00	1152	0.01	0.01	0.78	0.90	6,988,641.08	539,580.07	73.61
TIRIGANIAQ	M14-2311	325.30	327.20	1152	3.90	3.90	1.64	1.90	6,988,641.08	539,580.07	73.61
TIRIGANIAQ	M14-2311	348.70	351.40	1100	10.23	10.23	2.35	2.70	6,988,641.08	539,580.07	73.61
TIRIGANIAQ	M14-2317	283.00	286.50	1154	3.01	3.01	2.99	3.50	6,988,648.22	539,620.06	72.31
TIRIGANIAQ	M14-2317	295.90	300.00	1153	0.01	0.01	3.52	4.10	6,988,648.22	539,620.06	72.31
TIRIGANIAQ	M14-2317	326.70	330.20	1152	0.04	0.04	3.05	3.50	6,988,648.22	539,620.06	72.31
TIRIGANIAQ	M14-2317	344.50	349.00	1151	3.01	3.01	3.94	4.50	6,988,648.22	539,620.06	72.31
TIRIGANIAQ	M14-2317	353.50	358.00	1100	1.88	1.88	3.95	4.50	6,988,648.22	539,620.06	72.31
TIRIGANIAQ	ML075-001	95.30	98.10	1100	0.53	0.53	3.06	2.80	6,988,481.52	539,739.89	10.95
TIRIGANIAQ	ML075-001	101.50	104.30	1087	0.37	0.37	3.06	2.80	6,988,481.52	539,739.89	10.95
TIRIGANIAQ	ML075-001	107.00	109.30	1075	0.17	0.17	2.52	2.30	6,988,481.52	539,739.89	10.95
TIRIGANIAQ	ML075-001	114.00	119.60	1050	2.49	2.49	6.13	5.60	6,988,481.52	539,739.89	10.95
TIRIGANIAQ	ML075-001	125.50	130.20	1025	1.79	1.79	5.15	4.70	6,988,481.52	539,739.89	10.95
TIRIGANIAQ	ML075-001	131.50	133.70	1000	4.57	4.57	2.41	2.20	6,988,481.52	539,739.89	10.95
TIRIGANIAQ	ML075-002	95.10	97.60	1100	13.14	13.14	2.72	2.50	6,988,481.55	539,739.57	10.78
TIRIGANIAQ	ML075-002	102.10	104.40	1087	3.89	3.89	2.50	2.30	6,988,481.55	539,739.57	10.78
TIRIGANIAQ	ML075-002	105.70	108.60	1075	0.62	0.62	3.15	2.90	6,988,481.55	539,739.57	10.78
TIRIGANIAQ	ML075-002	115.10	119.50	1050	3.92	3.92	4.79	4.40	6,988,481.55	539,739.57	10.78
TIRIGANIAQ	ML075-002	125.60	131.90	1025	8.63	8.63	6.87	6.30	6,988,481.55	539,739.57	10.78
TIRIGANIAQ	ML075-002	136.00	138.70	1000	1.70	1.70	2.94	2.70	6,988,481.55	539,739.57	10.78

TIRIGANIAQ	ML075-003	97.80	100.00	1100	13.93	13.93	2.35	2.20	6,988,481.43	539,739.25	10.01
TIRIGANIAQ	ML075-003	107.40	109.80	1087	9.26	9.26	2.57	2.40	6,988,481.43	539,739.25	10.01
TIRIGANIAQ	ML075-003	111.90	115.10	1075	0.80	0.80	3.43	3.20	6,988,481.43	539,739.25	10.01
TIRIGANIAQ	ML075-003	116.90	124.30	1050	1.70	1.70	7.94	7.40	6,988,481.43	539,739.25	10.01
TIRIGANIAQ	ML075-003	129.00	136.00	1025	2.11	2.11	7.52	7.00	6,988,481.43	539,739.25	10.01
TIRIGANIAQ	ML075-003	140.90	143.70	1000	0.81	0.81	3.01	2.80	6,988,481.43	539,739.25	10.01
TIRIGANIAQ	ML075-004	102.60	106.80	1100	6.99	6.99	4.35	4.20	6,988,481.53	539,738.77	10.02
TIRIGANIAQ	ML075-004	110.60	113.30	1087	1.39	1.39	2.80	2.70	6,988,481.53	539,738.77	10.02
TIRIGANIAQ	ML075-004	118.10	121.80	1075	1.21	1.21	3.84	3.70	6,988,481.53	539,738.77	10.02
TIRIGANIAQ	ML075-004	122.30	126.90	1050	2.44	2.44	4.78	4.60	6,988,481.53	539,738.77	10.02
TIRIGANIAQ	ML075-004	135.70	142.70	1025	0.50	0.50	7.30	7.00	6,988,481.53	539,738.77	10.02
TIRIGANIAQ	ML075-004	144.50	147.50	1000	1.38	1.38	3.13	3.00	6,988,481.53	539,738.77	10.02
TIRIGANIAQ	ML075-005	107.40	112.40	1100	26.79	26.79	5.00	5.00	6,988,481.91	539,738.31	10.06
TIRIGANIAQ	ML075-005	114.00	116.60	1087	0.46	0.46	2.60	2.60	6,988,481.91	539,738.31	10.06
TIRIGANIAQ	ML075-005	123.40	126.50	1075	0.77	0.77	3.11	3.10	6,988,481.91	539,738.31	10.06
TIRIGANIAQ	ML075-005	128.50	136.70	1050	0.97	0.97	8.24	8.20	6,988,481.91	539,738.31	10.06
TIRIGANIAQ	ML075-005	142.50	146.30	1025	6.10	6.10	3.83	3.80	6,988,481.91	539,738.31	10.06
TIRIGANIAQ	ML075-005	151.30	154.50	1000	5.14	5.14	3.24	3.20	6,988,481.91	539,738.31	10.06
TIRIGANIAQ	ML075-006	92.70	97.40	1100	12.36	12.36	5.14	4.70	6,988,481.66	539,739.39	9.74
TIRIGANIAQ	ML075-006	99.00	103.00	1087	0.93	0.93	4.38	4.00	6,988,481.66	539,739.39	9.74
TIRIGANIAQ	ML075-006	105.60	108.20	1075	0.01	0.01	2.85	2.60	6,988,481.66	539,739.39	9.74
TIRIGANIAQ	ML075-006	112.20	119.00	1050	3.20	3.20	7.45	6.80	6,988,481.66	539,739.39	9.74
TIRIGANIAQ	ML075-006	123.90	127.10	1025	0.46	0.46	3.51	3.20	6,988,481.66	539,739.39	9.74
TIRIGANIAQ	ML075-006	130.00	132.60	1000	2.03	2.03	2.85	2.60	6,988,481.66	539,739.39	9.74
TIRIGANIAQ	ML075-007	91.70	95.60	1100	18.96	18.96	4.30	3.90	6,988,481.60	539,739.77	9.79
TIRIGANIAQ	ML075-007	98.50	100.80	1087	1.75	1.75	2.54	2.30	6,988,481.60	539,739.77	9.79
TIRIGANIAQ	ML075-007	103.40	106.00	1075	0.75	0.75	2.87	2.60	6,988,481.60	539,739.77	9.79
TIRIGANIAQ	ML075-007	112.10	116.60	1050	4.60	4.60	4.96	4.50	6,988,481.60	539,739.77	9.79
TIRIGANIAQ	ML075-007	125.00	128.00	1025	5.20	5.20	3.31	3.00	6,988,481.60	539,739.77	9.79
TIRIGANIAQ	ML075-007	130.00	132.30	1000	1.96	1.96	2.54	2.30	6,988,481.60	539,739.77	9.79
TIRIGANIAQ	ML075-008	91.50	95.70	1100	11.57	11.57	4.61	4.20	6,988,481.70	539,739.89	9.48
TIRIGANIAQ	ML075-008	97.20	100.00	1087	0.31	0.31	3.08	2.80	6,988,481.70	539,739.89	9.48
TIRIGANIAQ	ML075-008	103.80	108.20	1075	3.41	3.41	4.83	4.40	6,988,481.70	539,739.89	9.48
TIRIGANIAQ	ML075-008	109.90	116.00	1050	5.79	5.79	6.70	6.10	6,988,481.70	539,739.89	9.48
TIRIGANIAQ	ML075-008	119.80	123.10	1025	0.38	0.38	3.63	3.30	6,988,481.70	539,739.89	9.48
TIRIGANIAQ	ML075-008	129.80	132.00	1000	0.65	0.65	2.42	2.20	6,988,481.70	539,739.89	9.48
TIRIGANIAQ	ML150-001	86.30	87.80	1000	15.83	15.83	1.18	1.50	6,988,291.68	540,044.20	(72.95)
TIRIGANIAQ	ML150-001	88.10	93.10	1000	4.23	4.23	3.95	5.00	6,988,291.68	540,044.20	(72.95)
TIRIGANIAQ	ML150-001	99.00	102.80	1025	3.99	3.99	3.00	3.80	6,988,291.68	540,044.20	(72.95)
TIRIGANIAQ	ML150-001	115.40	118.50	1050	0.04	0.04	2.47	3.10	6,988,291.68	540,044.20	(72.95)
TIRIGANIAQ	ML150-001	155.70	159.20	1100	0.05	0.05	2.84	3.50	6,988,291.68	540,044.20	(72.95)
TIRIGANIAQ	ML150-001	161.50	164.60	1102	1.30	1.30	2.52	3.10	6,988,291.68	540,044.20	(72.95)
TIRIGANIAQ	ML150-001	186.50	189.60	1153	0.27	0.27	2.53	3.10	6,988,291.68	540,044.20	(72.95)
TIRIGANIAQ	ML150-001	212.10	215.70	1154	5.08	5.08	2.95	3.60	6,988,291.68	540,044.20	(72.95)
TIRIGANIAQ	ML150-001	222.20	226.20	1155	1.71	1.71	3.29	4.00	6,988,291.68	540,044.20	(72.95)
TIRIGANIAQ	ML150-002	92.60	93.40	1000	57.00	57.00	0.65	0.80	6,988,292.25	540,043.25	(72.19)
TIRIGANIAQ	ML150-002	93.70	96.50	1000	8.84	8.84	2.27	2.80	6,988,292.25	540,043.25	(72.19)
TIRIGANIAQ	ML150-002	113.60	117.00	1025	1.94	1.94	2.77	3.40	6,988,292.25	540,043.25	(72.19)
TIRIGANIAQ	ML150-002	120.40	122.80	1050	0.03	0.03	1.96	2.40	6,988,292.25	540,043.25	(72.19)
TIRIGANIAQ	ML150-002	123.10	124.60	1050	0.02	0.02	1.23	1.50	6,988,292.25	540,043.25	(72.19)
TIRIGANIAQ	ML150-002	152.00	155.40	1100	0.90	0.90	2.82	3.40	6,988,292.25	540,043.25	(72.19)
TIRIGANIAQ	ML150-002	184.30	187.50	1153	1.77	1.77	2.68	3.20	6,988,292.25	540,043.25	(72.19)
TIRIGANIAQ	ML150-002	197.20	200.30	1154	2.60	2.60	2.61	3.10	6,988,292.25	540,043.25	(72.19)
TIRIGANIAQ	ML150-002	210.00	213.00	1155	0.43	0.43	2.53	3.00	6,988,292.25	540,043.25	(72.19)
TIRIGANIAQ	ML150-002	254.30	266.70	1257	0.71	0.71	10.77	12.40	6,988,292.25	540,043.25	(72.19)
TIRIGANIAQ	ML150-002	277.40	282.50	1254	2.02	2.02	4.44	5.10	6,988,292.25	540,043.25	(72.19)
TIRIGANIAQ	ML150-003	84.00	91.00	1000	24.62	24.62	6.07	7.00	6,988,291.96	540,041.60	(73.34)
TIRIGANIAQ	ML150-003	104.60	108.00	1025	1.09	1.09	2.98	3.40	6,988,291.96	540,041.60	(73.34)
TIRIGANIAQ	ML150-003	110.90	113.70	1050	0.02	0.02	2.47	2.80	6,988,291.96	540,041.60	(73.34)
TIRIGANIAQ	ML150-003	135.00	138.00	1100	0.24	0.24	2.68	3.00	6,988,291.96	540,041.60	(73.34)
TIRIGANIAQ	ML150-003	172.00	175.20	1153	1.54	1.54	2.95	3.20	6,988,291.96	540,041.60	(73.34)
TIRIGANIAQ	ML150-003	204.00	207.10	1155	6.63	6.63	2.88	3.10	6,988,291.96	540,041.60	(73.34)
TIRIGANIAQ	ML150-003	256.90	260.70	1254	0.01	0.01	3.60	3.80	6,988,291.96	540,041.60	(73.34)
TIRIGANIAQ	ML150-004	97.00	101.70	1000	1.06	1.06	3.70	4.70	6,988,291.03	540,039.70	(73.40)
TIRIGANIAQ	ML150-004	115.20	120.00	1025	1.88	1.88	3.83	4.80	6,988,291.03	540,039.70	(73.40)
TIRIGANIAQ	ML150-004	121.00	122.90	1050	0.01	0.01	1.52	1.90	6,988,291.03	540,039.70	(73.40)
TIRIGANIAQ	ML150-004	123.20	125.90	1050	0.00	0.00	2.17	2.70	6,988,291.03	540,039.70	(73.40)
TIRIGANIAQ	ML150-004	137.20	138.00	1075	0.00	0.00	0.65	0.80	6,988,291.03	540,039.70	(73.40)
TIRIGANIAQ	ML150-004	138.30	140.90	1075	0.06	0.06	2.11	2.60	6,988,291.03	540,039.70	(73.40)
TIRIGANIAQ	ML150-004	145.20	148.80	1087	0.24	0.24	2.94	3.60	6,988,291.03	540,039.70	(73.40)
TIRIGANIAQ	ML150-004	156.60	160.00	1100	1.47	1.47	2.79	3.40	6,988,291.03	540,039.70	(73.40)
TIRIGANIAQ	ML150-004	192.00	197.50	1153	4.21	4.21	4.57	5.50	6,988,291.03	540,039.70	(73.40)
TIRIGANIAQ	ML150-004	207.10	210.10	1154	1.25	1.25	2.51	3.00	6,988,291.03	540,039.70	(73.40)
TIRIGANIAQ	ML150-004	226.40	229.60	1155	0.20	0.20	2.69	3.20	6,988,291.03	540,039.70	(73.40)
TIRIGANIAQ	ML150-005A	130.50	135.50	1000	3.06	3.06	3.29	5.00	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-005A	155.10	167.00	1025	0.70	0.70	7.96	11.90	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-005A	175.80	180.30	1050	5.35	5.35	3.09	4.50	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-005A	188.50	192.60	1075	0.64	0.64	2.89	4.10	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-005A	198.30	200.00	1087	0.12	0.12	1.20	1.70	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-005A	200.30	203.70	1087	0.14	0.14	2.40	3.40	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-005A	210.90	218.30	1100	0.39	0.39	5.27	7.40	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-005A	225.30	229.10	1151	1.02	1.02	2.83	3.80	6,988,291.14	540,039.96	(73.50)

TIRIGANIAQ	ML150-005A	251.50	260.50	1153	1.59	1.59	6.89	9.00	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-005A	263.20	266.40	1154	0.18	0.18	2.46	3.20	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-005A	279.50	283.20	1155	0.07	0.07	2.88	3.70	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-005A	291.90	295.20	1251	13.18	13.18	2.59	3.30	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-005A	327.20	331.00	1263	4.55	4.55	3.06	3.80	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-005A	344.50	350.00	1260	1.50	1.50	4.55	5.50	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-005A	350.30	351.50	1260	1.80	1.80	1.01	1.20	6,988,291.14	540,039.96	(73.50)
TIRIGANIAQ	ML150-006	91.10	100.10	1000	3.42	3.42	6.55	9.00	6,988,291.69	540,039.49	(72.54)
TIRIGANIAQ	ML150-006	100.40	101.00	1000	0.22	0.22	0.44	0.60	6,988,291.69	540,039.49	(72.54)
TIRIGANIAQ	ML150-006	101.30	102.50	1000	3.59	3.59	0.88	1.20	6,988,291.69	540,039.49	(72.54)
TIRIGANIAQ	ML150-006	107.00	111.10	1025	3.07	3.07	3.00	4.10	6,988,291.69	540,039.49	(72.54)
TIRIGANIAQ	ML150-006	124.90	128.20	1050	0.01	0.01	2.42	3.30	6,988,291.69	540,039.49	(72.54)
TIRIGANIAQ	ML150-006	164.00	167.90	1100	1.04	1.04	2.90	3.90	6,988,291.69	540,039.49	(72.54)
TIRIGANIAQ	ML150-006	202.20	205.90	1153	1.28	1.28	2.78	3.70	6,988,291.69	540,039.49	(72.54)
TIRIGANIAQ	ML150-006	214.60	218.30	1154	0.47	0.47	2.78	3.70	6,988,291.69	540,039.49	(72.54)
TIRIGANIAQ	ML150-006	231.50	235.30	1155	0.61	0.61	2.86	3.80	6,988,291.69	540,039.49	(72.54)
TIRIGANIAQ	ML150-006	296.00	302.90	1254	0.06	0.06	5.23	6.90	6,988,291.69	540,039.49	(72.54)
DISCOVERY	M13-2136	501.80	504.40	5240	-	-	3.08	2.60	554,829.02	6,982,014.80	87.01
DISCOVERY	M13-2136	521.60	526.50	5210	23.57	24.24	5.85	4.90	554,829.02	6,982,014.80	87.01
DISCOVERY	M13-2137	298.60	302.40	5240	6.78	6.78	4.26	3.80	554,586.99	6,981,824.83	77.73
DISCOVERY	M13-2137	303.00	306.10	5230	1.20	1.20	3.48	3.10	554,586.99	6,981,824.83	77.73
DISCOVERY	M13-2137	312.70	316.10	5220	12.51	12.51	3.82	3.40	554,586.99	6,981,824.83	77.73
DISCOVERY	M13-2137	324.00	327.80	5210	10.96	10.96	4.28	3.80	554,586.99	6,981,824.83	77.73
DISCOVERY	M13-2139	275.30	279.10	5240	0.50	0.50	4.50	3.80	554,445.95	6,981,896.35	74.76
DISCOVERY	M13-2139	284.10	287.00	5230	1.34	1.34	3.43	2.90	554,445.95	6,981,896.35	74.76
DISCOVERY	M13-2140	6.00	9.10	5240	2.29	2.29	3.72	3.10	554,260.77	6,981,639.24	69.45
DISCOVERY	M13-2140	19.50	23.00	5230	0.34	0.34	4.20	3.50	554,260.77	6,981,639.24	69.45
DISCOVERY	M13-2140	50.80	55.30	5210	0.09	0.09	5.42	4.50	554,260.77	6,981,639.24	69.45
DISCOVERY	M13-2141	243.00	245.60	5240	2.86	2.86	3.13	2.60	554,631.00	6,981,777.11	77.52
DISCOVERY	M13-2141	247.00	250.00	5210	0.94	0.94	3.61	3.00	554,631.00	6,981,777.11	77.52
DISCOVERY	M13-2142	6.90	11.50	5240	5.43	5.43	5.54	4.60	554,229.90	6,981,663.53	69.21
DISCOVERY	M13-2142	18.50	21.30	5230	0.12	0.12	3.37	2.80	554,229.90	6,981,663.53	69.21
DISCOVERY	M12-1744	326.00	328.60	5210	0.44	0.44	3.19	2.60	554,819.94	6,981,833.87	86.38
DISCOVERY	M12-1744	397.90	401.00	5140	5.56	5.56	3.82	3.10	554,819.94	6,981,833.87	86.38
DISCOVERY	M12-1744	411.40	414.50	5120	0.22	0.22	3.82	3.10	554,819.94	6,981,833.87	86.38
DISCOVERY	M12-1755	268.40	271.40	5240	18.29	18.29	3.66	3.00	554,616.65	6,981,815.91	78.45
DISCOVERY	M12-1755	279.50	282.30	5210	0.13	0.13	3.42	2.80	554,616.65	6,981,815.91	78.45
DISCOVERY	M12-1760	349.50	352.50	5240	0.03	0.03	3.62	3.00	554,748.84	6,981,873.07	84.79
DISCOVERY	M12-1760	352.70	355.60	5210	6.33	6.33	3.50	2.90	554,748.84	6,981,873.07	84.79
DISCOVERY	M12-1768	108.40	111.00	5210	0.31	0.31	3.18	2.60	554,727.60	6,981,607.92	72.82
DISCOVERY	M12-1768	155.70	156.10	5150	0.08	0.08	0.49	0.40	554,727.60	6,981,607.92	72.82
DISCOVERY	M12-1768	167.70	170.70	5140	4.63	4.63	3.68	3.00	554,727.60	6,981,607.92	72.82
DISCOVERY	M12-1768	181.50	185.50	5120	0.47	0.47	4.91	4.00	554,727.60	6,981,607.92	72.82
DISCOVERY	M12-1768	215.60	216.40	5110	0.06	0.06	0.98	0.80	554,727.60	6,981,607.92	72.82
DISCOVERY	M12-1768	217.40	218.30	5110	3.24	3.24	1.11	0.90	554,727.60	6,981,607.92	72.82
DISCOVERY	M12-1773	273.70	276.50	5240	1.86	1.86	3.40	2.80	554,762.84	6,981,791.44	80.83
DISCOVERY	M12-1773	282.10	285.00	5210	0.53	0.53	3.53	2.90	554,762.84	6,981,791.44	80.83
DISCOVERY	M12-1773	356.90	360.00	5140	2.70	2.70	3.79	3.10	554,762.84	6,981,791.44	80.83
DISCOVERY	M12-1773	365.00	368.00	5120	0.07	0.07	3.66	3.00	554,762.84	6,981,791.44	80.83
DISCOVERY	M12-1777	303.00	305.60	5240	2.13	16.77	3.13	2.60	554,481.71	6,981,936.32	77.71
DISCOVERY	M12-1777	317.10	320.00	5230	27.38	27.38	3.50	2.90	554,481.71	6,981,936.32	77.71
DISCOVERY	M12-1777	354.00	357.00	5210	1.13	1.13	3.63	3.00	554,481.71	6,981,936.32	77.71
DISCOVERY	M12-1784	258.80	261.10	5240	10.74	10.74	2.78	2.30	554,403.99	6,981,928.67	75.89
DISCOVERY	M12-1784	270.50	272.70	5230	0.28	0.28	2.66	2.20	554,403.99	6,981,928.67	75.89
DISCOVERY	M12-1784	337.50	340.40	5210	0.03	0.03	3.53	2.90	554,403.99	6,981,928.67	75.89
DISCOVERY	M12-1792	164.10	166.80	5240	0.43	0.43	3.21	2.70	554,281.08	6,981,871.61	71.61
DISCOVERY	M12-1792	169.00	171.60	5230	0.03	0.03	3.09	2.60	554,281.08	6,981,871.61	71.61
DISCOVERY	M12-1796	227.40	230.00	5240	1.93	1.93	3.01	2.60	554,428.38	6,981,839.80	73.51
DISCOVERY	M12-1796	237.70	240.30	5230	0.42	0.42	3.01	2.60	554,428.38	6,981,839.80	73.51
DISCOVERY	M12-1796	279.00	282.00	5210	0.03	0.03	3.49	3.00	554,428.38	6,981,839.80	73.51
DISCOVERY	M12-1803	343.50	346.10	5240	15.17	15.17	3.03	2.60	554,551.13	6,981,927.58	80.25
DISCOVERY	M12-1803	347.00	350.00	5230	1.29	1.29	3.49	3.00	554,551.13	6,981,927.58	80.25
DISCOVERY	M12-1803	382.30	384.80	5210	1.64	8.58	2.92	2.50	554,551.13	6,981,927.58	80.25
DISCOVERY	M12-1816	394.30	397.00	5240	1.23	1.23	3.23	2.70	554,502.78	6,982,066.99	80.42
DISCOVERY	M12-1816	400.00	402.40	5230	0.31	0.31	2.87	2.40	554,502.78	6,982,066.99	80.42
DISCOVERY	M13-2129	441.70	444.10	5240	-	-	2.74	2.40	554,786.92	6,981,939.25	86.94
DISCOVERY	M13-2129	456.00	459.60	5210	3.42	3.42	4.12	3.60	554,786.92	6,981,939.25	86.94
DISCOVERY	M13-2132	335.90	338.40	5240	0.79	0.79	2.81	2.50	554,620.10	6,981,868.12	79.92
DISCOVERY	M13-2132	355.90	360.90	5220	3.87	3.87	5.62	5.00	554,620.10	6,981,868.12	79.92
DISCOVERY	M13-2132	363.90	369.40	5210	8.39	8.39	6.19	5.50	554,620.10	6,981,868.12	79.92
DISCOVERY	M13-2145	293.00	297.00	5240	3.40	3.40	4.73	4.00	554,489.91	6,981,887.29	75.79
DISCOVERY	M13-2145	298.00	301.80	5230	2.39	2.39	4.50	3.80	554,489.91	6,981,887.29	75.79
DISCOVERY	M13-2145	332.10	335.10	5210	7.19	7.19	3.58	3.00	554,489.91	6,981,887.29	75.79
DISCOVERY	M13-2146	288.40	291.00	5240	0.03	0.03	3.08	2.60	554,520.89	6,981,871.81	75.82
DISCOVERY	M13-2146	295.00	297.60	5230	1.07	1.07	3.08	2.60	554,520.89	6,981,871.81	75.82
DISCOVERY	M13-2146	319.20	321.90	5210	7.11	7.11	3.21	2.70	554,520.89	6,981,871.81	75.82
DISCOVERY	M13-2148	87.50	90.80	5240	2.31	2.31	3.65	3.30	554,161.55	6,981,835.39	69.60
DISCOVERY	M13-2148	99.30	101.90	5230	0.64	0.64	2.89	2.60	554,161.55	6,981,835.39	69.60
DISCOVERY	M13-2149	45.00	47.60	5240	0.91	0.91	3.20	2.60	554,307.67	6,981,668.57	70.03
DISCOVERY	M13-2149	53.00	59.80	5230	6.54	6.54	8.37	6.80	554,307.67	6,981,668.57	70.03
DISCOVERY	M13-2149	87.60	90.40	5210	4.76	9.81	3.46	2.80	554,307.67	6,981,668.57	70.03
DISCOVERY	M13-2151	261.00	264.00	5240	1.94	1.94	3.34	3.00	554,566.84	6,981,797.11	75.68
DISCOVERY	M13-2151	266.00	269.00	5230	0.30	0.30	3.35	3.00	554,566.84	6,981,797.11	75.68

DISCOVERY	M13-2151	276.00	279.00	5220	0.84	0.84	3.36	3.00	554,566.84	6,981,797.11	75.68
DISCOVERY	M13-2151	280.80	284.10	5210	12.56	12.56	3.70	3.30	554,566.84	6,981,797.11	75.68
DISCOVERY	M13-2152	176.40	178.60	5230	0.73	0.73	2.43	2.20	554,182.65	6,981,941.57	70.14
DISCOVERY	M13-2152	176.40	178.60	5240	0.73	0.73	2.43	2.20	554,182.65	6,981,941.57	70.14
DISCOVERY	M13-2153	26.00	28.80	5230	4.88	4.88	3.36	2.80	554,274.64	6,981,636.32	69.51
DISCOVERY	M13-2153	50.10	54.00	5210	0.03	0.03	4.69	3.90	554,274.64	6,981,636.32	69.51
DISCOVERY	M13-2154A	349.00	352.00	5240	3.67	3.67	3.40	3.00	554,575.10	6,981,909.02	80.34
DISCOVERY	M13-2154A	360.10	362.60	5230	7.43	7.43	2.83	2.50	554,575.10	6,981,909.02	80.34
DISCOVERY	M13-2154A	385.60	388.90	5210	16.49	16.49	3.74	3.30	554,575.10	6,981,909.02	80.34
DISCOVERY	M13-2156	17.20	20.00	5240	1.45	4.28	3.38	2.80	554,315.66	6,981,629.40	69.88
DISCOVERY	M13-2156	27.00	32.50	5230	4.44	4.44	6.65	5.50	554,315.66	6,981,629.40	69.88
DISCOVERY	M13-2156	55.80	61.20	5210	4.74	4.74	6.55	5.40	554,315.66	6,981,629.40	69.88
DISCOVERY	M13-2157	4.80	7.60	5230	0.13	0.13	3.42	2.80	554,296.67	6,981,604.95	69.30
DISCOVERY	M13-2157	28.80	33.80	5210	3.68	3.68	6.12	5.00	554,296.67	6,981,604.95	69.30
DISCOVERY	M13-2158	102.40	106.20	5240	5.64	5.64	4.14	3.80	554,147.15	6,981,867.62	70.08
DISCOVERY	M13-2158	107.20	109.50	5230	0.03	0.03	2.51	2.30	554,147.15	6,981,867.62	70.08
DISCOVERY	M13-2159	298.30	300.80	5240	0.62	0.62	2.83	2.50	554,546.01	6,981,857.17	75.99
DISCOVERY	M13-2159	314.00	316.60	5230	6.51	6.51	2.96	2.60	554,546.01	6,981,857.17	75.99
DISCOVERY	M13-2159	330.60	336.30	5210	8.01	8.01	6.49	5.70	554,546.01	6,981,857.17	75.99
DISCOVERY	M13-2161	9.50	12.30	5230	0.85	0.85	3.40	2.80	554,325.90	6,981,600.58	70.19
DISCOVERY	M13-2161	25.00	29.00	5220	3.13	3.13	4.86	4.00	554,325.90	6,981,600.58	70.19
DISCOVERY	M13-2161	30.00	39.00	5210	6.84	6.84	10.94	9.00	554,325.90	6,981,600.58	70.19
DISCOVERY	M13-2162	37.20	40.90	5240	0.52	0.52	4.44	3.70	554,468.91	6,981,589.02	71.10
DISCOVERY	M13-2162	45.00	48.40	5210	2.15	2.15	4.09	3.40	554,468.91	6,981,589.02	71.10
DISCOVERY	M13-2163	156.20	159.30	5240	1.15	7.63	3.51	3.10	554,251.76	6,981,881.30	70.87
DISCOVERY	M13-2163	173.50	179.40	5230	10.15	10.15	6.68	5.90	554,251.76	6,981,881.30	70.87
DISCOVERY	M13-2165	9.40	13.60	5240	0.51	0.51	5.03	4.20	554,466.02	6,981,559.21	70.71
DISCOVERY	M13-2165	17.00	20.00	5210	0.25	0.25	3.59	3.00	554,466.02	6,981,559.21	70.71
DISCOVERY	M13-2166	288.00	293.70	5240	11.11	11.11	6.77	5.70	554,446.60	6,981,952.01	76.94
DISCOVERY	M13-2166	303.30	306.00	5230	22.89	25.74	3.21	2.70	554,446.60	6,981,952.01	76.94
DISCOVERY	M13-2167	21.40	24.80	5240	2.05	2.05	4.17	3.40	554,499.82	6,981,564.35	70.99
DISCOVERY	M13-2167	27.80	30.80	5210	0.39	0.39	3.68	3.00	554,499.82	6,981,564.35	70.99
DISCOVERY	M13-2168	186.80	190.70	5240	0.46	0.46	4.38	3.90	554,273.01	6,981,906.91	71.17
DISCOVERY	M13-2168	207.80	211.10	5230	0.35	0.35	3.72	3.30	554,273.01	6,981,906.91	71.17
DISCOVERY	M13-2170	231.80	234.70	5240	0.28	0.28	3.44	2.90	554,469.87	6,981,821.20	74.63
DISCOVERY	M13-2170	238.40	241.20	5230	4.92	4.92	3.32	2.80	554,469.87	6,981,821.20	74.63
DISCOVERY	M13-2170	243.00	245.50	5220	2.55	2.55	2.97	2.50	554,469.87	6,981,821.20	74.63
DISCOVERY	M13-2170	263.10	266.20	5210	4.53	4.53	3.69	3.10	554,469.87	6,981,821.20	74.63
DISCOVERY	M13-2171	124.20	127.10	5240	0.08	0.08	3.52	2.90	554,582.04	6,981,657.06	73.61
DISCOVERY	M13-2171	128.10	130.80	5210	1.46	1.46	3.28	2.70	554,582.04	6,981,657.06	73.61
DISCOVERY	M13-2172	184.20	189.70	5230	0.08	0.08	6.19	5.50	554,213.76	6,981,944.29	70.44
DISCOVERY	M13-2172	184.20	189.70	5240	0.08	0.08	6.19	5.50	554,213.76	6,981,944.29	70.44
DISCOVERY	M13-2174	253.50	256.30	5240	1.09	4.05	3.33	2.80	554,484.03	6,981,849.99	75.01
DISCOVERY	M13-2174	259.20	262.00	5230	0.12	0.12	3.33	2.80	554,484.03	6,981,849.99	75.01
DISCOVERY	M13-2174	289.90	292.80	5210	14.00	14.00	3.46	2.90	554,484.03	6,981,849.99	75.01
DISCOVERY	M13-2175	373.50	376.10	5240	0.72	0.72	2.96	2.60	554,549.49	6,981,962.90	78.67
DISCOVERY	M13-2175	386.90	390.80	5230	0.62	0.62	4.44	3.90	554,549.49	6,981,962.90	78.67
DISCOVERY	M13-2175	424.00	426.40	5210	0.03	0.03	2.74	2.40	554,549.49	6,981,962.90	78.67
DISCOVERY	M13-2176	328.90	333.90	5240	24.93	24.93	5.77	5.00	554,510.01	6,981,918.22	77.22
DISCOVERY	M13-2176	336.40	339.10	5230	3.34	3.34	3.12	2.70	554,510.01	6,981,918.22	77.22
DISCOVERY	M13-2176	368.80	372.10	5210	0.61	0.61	3.82	3.30	554,510.01	6,981,918.22	77.22
DISCOVERY	M13-2178	140.50	143.60	5240	0.30	0.30	3.70	3.10	554,604.14	6,981,670.63	73.22
DISCOVERY	M13-2178	149.40	152.60	5210	0.50	0.50	3.82	3.20	554,604.14	6,981,670.63	73.22
DISCOVERY	M13-2182	225.20	227.80	5230	0.20	0.20	2.86	2.60	554,222.24	6,981,985.76	71.66
DISCOVERY	M13-2182	225.20	227.80	5240	0.20	0.20	2.86	2.60	554,222.24	6,981,985.76	71.66
DISCOVERY	M13-2184	205.70	208.40	5240	0.42	0.42	3.20	2.70	554,623.13	6,981,734.30	74.77
DISCOVERY	M13-2184	209.50	213.00	5210	3.54	3.54	4.15	3.50	554,623.13	6,981,734.30	74.77
DISCOVERY	M13-2186	143.00	146.00	5240	0.45	0.45	3.51	3.00	554,329.16	6,981,798.78	71.41
DISCOVERY	M13-2186	151.70	154.40	5230	0.77	0.77	3.16	2.70	554,329.16	6,981,798.78	71.41
DISCOVERY	M13-2186	216.20	219.20	5210	-	-	3.53	3.00	554,329.16	6,981,798.78	71.41
DISCOVERY	M13-2188	203.70	206.50	5240	0.59	0.59	3.31	2.80	554,465.15	6,981,789.90	74.45
DISCOVERY	M13-2188	211.50	214.10	5230	2.18	2.18	3.08	2.60	554,465.15	6,981,789.90	74.45
DISCOVERY	M13-2188	218.50	221.20	5220	1.50	1.50	3.20	2.70	554,465.15	6,981,789.90	74.45
DISCOVERY	M13-2188	233.60	241.10	5210	5.64	5.64	8.90	7.50	554,465.15	6,981,789.90	74.45
DISCOVERY	M13-2190	143.50	146.30	5240	0.55	0.55	3.36	2.80	554,345.67	6,981,786.37	71.46
DISCOVERY	M13-2190	147.00	150.80	5230	1.93	1.93	4.57	3.80	554,345.67	6,981,786.37	71.46
DISCOVERY	M13-2191	172.00	174.60	5240	0.03	0.03	3.07	2.60	554,425.79	6,981,769.72	73.68
DISCOVERY	M13-2191	179.80	182.20	5230	0.03	0.03	2.84	2.40	554,425.79	6,981,769.72	73.68
DISCOVERY	M13-2191	210.50	213.70	5210	2.42	2.42	3.79	3.20	554,425.79	6,981,769.72	73.68
DISCOVERY	M14-2325	495.00	498.60	5210	0.66	0.66	4.21	3.60	554,628.00	6,982,021.29	83.22
FZONE	GT13-62	23.70	28.80	4130	2.95	2.95	5.53	5.10	542,787.82	6,986,126.77	57.59
FZONE	GT13-62	26.40	32.70	4120	6.69	6.69	6.83	6.30	542,787.82	6,986,126.77	57.59
FZONE	GT13-62	33.70	38.50	4110	1.63	1.63	5.21	4.80	542,787.82	6,986,126.77	57.59
FZONE	M12-1542	19.80	22.20	4135	-	-	3.01	2.40	542,250.76	6,986,320.37	59.64
FZONE	M12-1542	37.50	39.90	4120	0.03	0.03	3.01	2.40	542,250.76	6,986,320.37	59.64
FZONE	M12-1543	42.00	45.00	4120	0.15	0.15	3.79	3.00	542,223.59	6,986,332.39	59.72
FZONE	M12-1546	99.80	102.60	4120	-	-	3.51	2.80	542,252.00	6,986,404.00	61.00
FZONE	M12-1547	81.50	84.00	4135	0.01	0.01	3.14	2.50	542,279.78	6,986,392.89	61.36
FZONE	M12-1547	96.80	99.25	4120	0.88	0.88	3.08	2.45	542,279.78	6,986,392.89	61.36
FZONE	M12-1551	159.60	162.00	4120	-	-	3.01	2.40	542,282.53	6,986,478.97	60.75
FZONE	M12-1554	145.40	148.00	4135	0.15	0.15	3.26	2.60	542,310.91	6,986,468.97	60.49
FZONE	M12-1554	160.40	163.00	4120	0.03	0.03	3.26	2.60	542,310.91	6,986,468.97	60.49
FZONE	M12-1556	168.40	170.70	4135	0.03	0.03	2.86	2.30	542,294.90	6,986,509.09	58.86
FZONE	M12-1556	183.00	185.30	4120	0.49	0.49	2.87	2.30	542,294.90	6,986,509.09	58.86
FZONE	M12-1559	177.00	183.00	4137	2.85	2.85	7.49	6.00	542,416.29	6,986,464.17	57.16
FZONE	M12-1559	185.00	188.00	4135	7.21	7.21	3.74	3.00	542,416.29	6,986,464.17	57.16
FZONE	M12-1559	191.20	195.00	4130	2.08	2.08	4.74	3.80	542,416.29	6,986,464.17	57.16
FZONE	M12-1559	201.50	205.00	4120	4.46	4.46	4.37	3.50	542,416.29	6,986,464.17	57.16
FZONE	M12-1559	206.75	211.05	4115	7.35	7.35	5.37	4.30	542,416.29	6,986,464.17	57.16
FZONE	M12-1559	216.40	222.00	4110	4.40	4.40	6.99	5.60	542,416.29	6,986,464.17	57.16

FZONE	M12-1565	158.70	161.60	4135	0.30	0.30	3.54	2.90	542,419.13	6,986,414.78	59.37
FZONE	M12-1565	164.00	168.30	4130	17.84	17.84	5.24	4.30	542,419.13	6,986,414.78	59.37
FZONE	M12-1565	175.00	178.00	4120	0.16	0.16	3.66	3.00	542,419.13	6,986,414.78	59.37
FZONE	M12-1565	187.40	190.00	4110	2.00	2.00	3.17	2.60	542,419.13	6,986,414.78	59.37
FZONE	M12-1565	210.00	212.60	4100	3.05	3.05	3.17	2.60	542,419.13	6,986,414.78	59.37
FZONE	M12-1567	148.00	151.80	4135	3.45	3.45	4.67	3.80	542,462.24	6,986,390.06	60.47
FZONE	M12-1567	155.00	157.00	4120	4.75	4.75	2.46	2.00	542,462.24	6,986,390.06	60.47
FZONE	M12-1567	172.00	174.60	4110	2.22	2.22	3.19	2.60	542,462.24	6,986,390.06	60.47
FZONE	M12-1567	202.00	204.60	4100	1.98	1.98	3.20	2.60	542,462.24	6,986,390.06	60.47
FZONE	M12-1575	147.50	149.90	4135	4.81	4.81	2.83	2.40	542,462.32	6,986,390.28	60.55
FZONE	M12-1575	157.30	160.00	4120	3.45	3.45	3.19	2.70	542,462.32	6,986,390.28	60.55
FZONE	M12-1575	178.40	180.90	4110	0.60	0.60	2.96	2.50	542,462.32	6,986,390.28	60.55
FZONE	M12-1575	209.00	211.80	4100	0.22	0.22	3.33	2.80	542,462.32	6,986,390.28	60.55
FZONE	M12-1578	13.00	16.00	4135	2.57	2.57	3.78	3.00	542,462.03	6,986,228.22	59.52
FZONE	M12-1578	18.40	21.00	4130	0.14	0.14	3.27	2.60	542,462.03	6,986,228.22	59.52
FZONE	M12-1578	25.40	28.50	4120	5.00	5.00	3.90	3.10	542,462.03	6,986,228.22	59.52
FZONE	M12-1578	47.40	51.10	4110	0.39	0.39	4.66	3.70	542,462.03	6,986,228.22	59.52
FZONE	M12-1578	72.00	75.00	4100	0.03	0.03	3.78	3.00	542,462.03	6,986,228.22	59.52
FZONE	M12-1581	115.40	118.85	4140	0.25	0.25	4.21	3.45	542,538.96	6,986,341.49	56.07
FZONE	M12-1581	126.00	128.30	4135	0.03	0.03	2.81	2.30	542,538.96	6,986,341.49	56.07
FZONE	M12-1581	133.00	135.15	4130	0.80	0.80	2.63	2.15	542,538.96	6,986,341.49	56.07
FZONE	M12-1581	144.40	147.65	4120	3.26	3.26	3.97	3.25	542,538.96	6,986,341.49	56.07
FZONE	M12-1581	157.90	161.25	4110	0.09	0.09	4.09	3.35	542,538.96	6,986,341.49	56.07
FZONE	M12-1581	181.90	184.40	4100	0.62	0.62	3.06	2.50	542,538.96	6,986,341.49	56.07
FZONE	M12-1585	30.10	33.00	4140	0.03	0.03	3.38	2.90	542,532.80	6,986,233.46	57.25
FZONE	M12-1585	44.20	47.20	4135	1.67	1.67	3.51	3.00	542,532.80	6,986,233.46	57.25
FZONE	M12-1585	48.60	51.20	4130	0.08	0.08	3.04	2.60	542,532.80	6,986,233.46	57.25
FZONE	M12-1585	57.20	60.20	4120	0.36	0.36	3.51	3.00	542,532.80	6,986,233.46	57.25
FZONE	M12-1585	72.50	75.50	4110	0.06	0.06	3.51	3.00	542,532.80	6,986,233.46	57.25
FZONE	M12-1585	105.50	108.40	4100	5.61	11.40	3.40	2.90	542,532.80	6,986,233.46	57.25
FZONE	M12-1587	64.50	67.50	4140	0.12	0.12	3.71	3.00	542,558.01	6,986,277.87	56.27
FZONE	M12-1587	76.00	78.60	4135	0.03	0.03	3.22	2.60	542,558.01	6,986,277.87	56.27
FZONE	M12-1587	83.40	86.60	4130	0.03	0.03	3.96	3.20	542,558.01	6,986,277.87	56.27
FZONE	M12-1587	91.00	94.40	4120	0.03	0.03	4.21	3.40	542,558.01	6,986,277.87	56.27
FZONE	M12-1587	106.50	109.40	4110	0.56	0.56	3.59	2.90	542,558.01	6,986,277.87	56.27
FZONE	M12-1587	137.00	140.00	4100	0.90	0.90	3.72	3.00	542,558.01	6,986,277.87	56.27
FZONE	M12-1591	39.00	41.30	4140	0.03	0.03	2.74	2.30	542,573.23	6,986,235.31	56.89
FZONE	M12-1591	47.00	50.00	4135	0.39	0.39	3.58	3.00	542,573.23	6,986,235.31	56.89
FZONE	M12-1591	57.60	60.60	4130	0.03	0.03	3.59	3.00	542,573.23	6,986,235.31	56.89
FZONE	M12-1591	64.80	68.60	4120	0.03	0.03	4.55	3.80	542,573.23	6,986,235.31	56.89
FZONE	M12-1591	72.80	75.80	4110	0.03	0.03	3.59	3.00	542,573.23	6,986,235.31	56.89
FZONE	M12-1591	112.60	115.00	4100	-	-	2.89	2.40	542,573.23	6,986,235.31	56.89
FZONE	M12-1592	52.00	55.80	4130	0.03	0.03	4.72	3.80	542,604.34	6,986,235.05	56.23
FZONE	M12-1592	73.30	76.30	4120	0.03	0.03	3.73	3.00	542,604.34	6,986,235.05	56.23
FZONE	M12-1592	85.10	88.20	4110	-	-	3.85	3.10	542,604.34	6,986,235.05	56.23
FZONE	M12-1592	116.40	119.00	4100	0.03	0.03	3.23	2.60	542,604.34	6,986,235.05	56.23
FZONE	M12-1596	54.60	59.60	4130	8.39	8.39	6.12	5.00	542,633.14	6,986,224.74	56.42
FZONE	M12-1596	70.30	73.30	4120	1.82	1.82	3.68	3.00	542,633.14	6,986,224.74	56.42
FZONE	M12-1596	78.00	81.00	4110	0.13	0.13	3.68	3.00	542,633.14	6,986,224.74	56.42
FZONE	M12-1596	118.50	121.40	4100	0.01	0.01	3.57	2.90	542,633.14	6,986,224.74	56.42
FZONE	M12-1598	12.00	14.90	4140	2.90	2.90	3.61	2.90	542,560.44	6,986,203.54	57.17
FZONE	M12-1598	18.10	20.80	4135	3.62	3.62	3.36	2.70	542,560.44	6,986,203.54	57.17
FZONE	M12-1598	26.60	29.80	4130	1.56	1.56	3.98	3.20	542,560.44	6,986,203.54	57.17
FZONE	M12-1598	32.20	35.00	4120	0.03	0.03	3.48	2.80	542,560.44	6,986,203.54	57.17
FZONE	M12-1598	42.10	45.40	4110	0.03	0.03	4.11	3.30	542,560.44	6,986,203.54	57.17
FZONE	M12-1598	84.80	87.40	4100	0.40	0.40	3.24	2.60	542,560.44	6,986,203.54	57.17
FZONE	M12-1601	18.75	21.60	4130	0.06	0.06	3.50	2.85	542,616.43	6,986,183.97	56.88
FZONE	M12-1601	30.40	33.55	4120	0.83	0.83	3.87	3.15	542,616.43	6,986,183.97	56.88
FZONE	M12-1601	37.50	40.50	4110	0.03	0.03	3.69	3.00	542,616.43	6,986,183.97	56.88
FZONE	M12-1601	83.90	86.30	4100	-	-	2.96	2.40	542,616.43	6,986,183.97	56.88
FZONE	M12-1602	97.55	100.50	4130	4.88	4.88	3.51	2.95	542,704.91	6,986,241.03	55.45
FZONE	M12-1602	100.50	103.10	4120	4.74	4.74	3.09	2.60	542,704.91	6,986,241.03	55.45
FZONE	M12-1602	115.00	118.00	4110	-	-	3.58	3.00	542,704.91	6,986,241.03	55.45
FZONE	M12-1603	9.80	13.30	4130	7.79	7.79	4.40	3.50	542,644.04	6,986,172.32	57.02
FZONE	M12-1603	17.00	20.00	4120	0.03	0.03	3.77	3.00	542,644.04	6,986,172.32	57.02
FZONE	M12-1603	28.70	31.60	4110	0.12	0.12	3.65	2.90	542,644.04	6,986,172.32	57.02
FZONE	M12-1604	97.10	100.00	4130	14.49	14.49	3.54	2.90	542,679.89	6,986,259.87	55.88
FZONE	M12-1604	102.00	107.00	4120	3.08	3.08	6.11	5.00	542,679.89	6,986,259.87	55.88
FZONE	M12-1604	117.40	120.00	4110	1.77	1.77	3.18	2.60	542,679.89	6,986,259.87	55.88
FZONE	M12-1604	159.00	161.90	4100	0.03	0.03	3.57	2.90	542,679.89	6,986,259.87	55.88
FZONE	M12-1608	6.50	9.00	4130	2.17	2.17	3.14	2.50	542,667.00	6,986,148.00	57.02
FZONE	M12-1608	12.00	14.60	4120	0.10	0.10	3.26	2.60	542,667.00	6,986,148.00	57.02
FZONE	M12-1608	28.00	31.00	4110	2.44	2.44	3.76	3.00	542,667.00	6,986,148.00	57.02
FZONE	M12-1610	119.30	122.40	4130	1.70	1.70	3.85	3.10	542,661.38	6,986,296.17	55.77
FZONE	M12-1610	127.85	130.70	4120	1.05	1.05	3.54	2.85	542,661.38	6,986,296.17	55.77
FZONE	M12-1610	142.10	144.80	4110	1.12	1.12	3.36	2.70	542,661.38	6,986,296.17	55.77
FZONE	M12-1610	179.40	182.00	4100	-	-	3.24	2.60	542,661.38	6,986,296.17	55.77
FZONE	M12-1611	5.00	7.65	4130	2.05	2.05	3.34	2.65	542,698.83	6,986,136.85	59.03
FZONE	M12-1611	14.00	16.60	4120	1.16	1.16	3.28	2.60	542,698.83	6,986,136.85	59.03
FZONE	M12-1611	23.00	25.50	4110	0.03	0.03	3.15	2.50	542,698.83	6,986,136.85	59.03
FZONE	M12-1614	5.00	8.00	4130	0.95	0.95	3.76	3.00	542,737.30	6,986,122.75	58.27
FZONE	M12-1614	13.00	15.00	4120	0.70	0.70	2.51	2.00	542,737.30	6,986,122.75	58.27
FZONE	M12-1614	18.40	20.65	4110	1.88	1.88	2.82	2.25	542,737.30	6,986,122.75	58.27
FZONE	M12-1615	119.00	121.50	4130	1.47	1.47	3.11	2.50	542,632.60	6,986,305.60	55.78
FZONE	M12-1615	134.80	137.60	4120	0.17	0.17	3.49	2.80	542,632.60	6,986,305.60	55.78
FZONE	M12-1615	146.50	149.10	4110	0.11	0.11	3.24	2.60	542,632.60	6,986,305.60	55.78
FZONE	M12-1615	177.50	180.10	4100	-	-	3.25	2.60	542,632.60	6,986,305.60	55.78
FZONE	M12-1618	23.05	25.25	4130	9.02	9.02	2.77	2.20	542,876.73	6,986,106.74	58.97
FZONE	M12-1618	33.00	35.25	4120	2.75	2.75	2.84	2.25	542,876.73	6,986,106.74	58.97
FZONE	M12-1618	45.00	47.05	4110	0.39	0.39	2.59	2.05	542,876.73	6,986,106.74	58.97

FZONE	M12-1620	60.90	63.50	4130	0.08	0.08	3.12	2.60	542,952.02	6,986,132.31	56.43
FZONE	M12-1620	75.10	78.00	4120	1.67	1.67	3.49	2.90	542,952.02	6,986,132.31	56.43
FZONE	M12-1620	81.75	84.30	4110	0.39	0.39	3.07	2.55	542,952.02	6,986,132.31	56.43
FZONE	M12-1624	90.00	93.00	4130	0.03	0.03	3.53	3.00	542,881.86	6,986,200.64	54.82
FZONE	M12-1624	101.00	104.00	4120	0.19	0.19	3.54	3.00	542,881.86	6,986,200.64	54.82
FZONE	M12-1624	121.00	125.00	4110	0.17	0.17	4.72	4.00	542,881.86	6,986,200.64	54.82
FZONE	M12-1627	68.40	70.80	4130	-	-	2.93	2.40	542,980.94	6,986,124.74	56.55
FZONE	M12-1627	74.30	76.70	4120	0.03	0.03	2.93	2.40	542,980.94	6,986,124.74	56.55
FZONE	M12-1627	81.70	84.80	4110	0.56	0.56	3.79	3.10	542,980.94	6,986,124.74	56.55
FZONE	M12-1629	86.20	88.80	4130	4.13	4.13	3.24	2.60	543,024.61	6,986,126.95	56.18
FZONE	M12-1629	90.00	91.00	4120	5.35	5.35	1.25	1.00	543,024.61	6,986,126.95	56.18
FZONE	M12-1629	91.15	93.80	4120	6.88	6.88	3.30	2.65	543,024.61	6,986,126.95	56.18
FZONE	M12-1629	98.10	100.40	4110	0.21	0.21	2.87	2.30	543,024.61	6,986,126.95	56.18
FZONE	M12-1633	59.00	62.00	4130	0.10	0.10	3.67	3.00	543,083.60	6,986,058.43	59.53
FZONE	M12-1633	68.00	70.60	4120	0.07	0.07	3.18	2.60	543,083.60	6,986,058.43	59.53
FZONE	M12-1633	83.40	85.80	4110	1.86	1.86	2.94	2.40	543,083.60	6,986,058.43	59.53
FZONE	M12-1634	83.80	87.00	4130	2.44	2.44	4.02	3.20	542,881.74	6,986,200.17	54.90
FZONE	M12-1634	94.00	97.00	4120	1.14	1.14	3.77	3.00	542,881.74	6,986,200.17	54.90
FZONE	M12-1634	114.80	117.60	4110	0.05	0.05	3.51	2.80	542,881.74	6,986,200.17	54.90
FZONE	M12-1636	160.80	165.00	4130	20.60	22.08	5.20	4.20	542,940.05	6,986,264.08	54.28
FZONE	M12-1636	172.40	175.00	4120	0.03	0.03	3.22	2.60	542,940.05	6,986,264.08	54.28
FZONE	M12-1636	182.50	186.00	4110	0.03	0.03	4.34	3.50	542,940.05	6,986,264.08	54.28
FZONE	M12-1637	58.30	61.00	4130	0.49	0.49	3.17	2.70	543,108.68	6,986,042.17	60.10
FZONE	M12-1637	65.40	68.60	4120	0.03	0.03	3.75	3.20	543,108.68	6,986,042.17	60.10
FZONE	M12-1637	76.50	79.30	4110	0.70	0.70	3.28	2.80	543,108.68	6,986,042.17	60.10
FZONE	M12-1640	33.25	35.65	4130	0.15	0.15	2.93	2.40	543,110.36	6,986,017.66	62.13
FZONE	M12-1640	44.15	47.00	4120	1.70	1.70	3.48	2.85	543,110.36	6,986,017.66	62.13
FZONE	M12-1640	53.60	56.35	4110	0.12	0.12	3.36	2.75	543,110.36	6,986,017.66	62.13
FZONE	M12-1642	46.90	49.50	4130	0.32	0.32	3.22	2.60	542,684.94	6,986,194.27	56.44
FZONE	M12-1642	53.20	56.00	4120	0.57	0.57	3.46	2.80	542,684.94	6,986,194.27	56.44
FZONE	M12-1642	65.00	67.70	4110	1.01	1.01	3.34	2.70	542,684.94	6,986,194.27	56.44
FZONE	M12-1643	132.00	136.00	4130	0.48	0.48	5.01	4.00	543,205.81	6,986,120.64	53.85
FZONE	M12-1643	141.00	144.30	4120	0.15	0.15	4.13	3.30	543,205.81	6,986,120.64	53.85
FZONE	M12-1643	147.40	150.00	4115	0.32	0.32	3.25	2.60	543,205.81	6,986,120.64	53.85
FZONE	M12-1645	87.00	89.60	4130	0.14	0.14	3.15	2.60	543,139.01	6,986,077.32	55.90
FZONE	M12-1645	97.00	100.00	4120	0.23	0.23	3.64	3.00	543,139.01	6,986,077.32	55.90
FZONE	M12-1645	100.00	103.20	4115	6.23	6.23	3.88	3.20	543,139.01	6,986,077.32	55.90
FZONE	M12-1645	108.10	110.70	4110	0.03	0.03	3.15	2.60	543,139.01	6,986,077.32	55.90
FZONE	M12-1648	61.40	64.30	4130	0.43	0.43	3.55	2.90	543,140.83	6,986,039.36	60.18
FZONE	M12-1648	68.00	70.80	4120	0.77	0.77	3.43	2.80	543,140.83	6,986,039.36	60.18
FZONE	M12-1649	137.50	141.50	4130	2.07	2.07	4.96	4.00	543,242.81	6,986,105.71	53.26
FZONE	M12-1649	144.90	147.50	4120	0.29	0.29	3.22	2.60	543,242.81	6,986,105.71	53.26
FZONE	M12-1653	40.70	43.30	4130	0.03	0.03	3.26	2.60	543,160.05	6,986,008.29	62.45
FZONE	M12-1653	50.70	53.70	4120	0.03	0.03	3.77	3.00	543,160.05	6,986,008.29	62.45
FZONE	M12-1655	98.00	103.00	4130	4.30	4.30	6.25	5.00	543,321.74	6,986,034.71	56.72
FZONE	M12-1655	106.00	108.60	4120	3.59	3.59	3.25	2.60	543,321.74	6,986,034.71	56.72
FZONE	M12-1656	80.35	83.00	4130	2.91	2.91	3.30	2.65	543,264.73	6,986,025.39	58.56
FZONE	M12-1656	91.60	94.00	4120	0.19	0.19	2.99	2.40	543,264.73	6,986,025.39	58.56
FZONE	M12-1660	108.40	111.60	4130	0.19	0.19	3.64	3.20	543,322.00	6,986,035.28	56.65
FZONE	M12-1660	113.40	116.20	4120	0.48	0.48	3.19	2.80	543,322.00	6,986,035.28	56.65
FZONE	M12-1662	79.80	83.00	4130	1.98	1.98	4.03	3.20	543,321.24	6,986,006.51	59.45
FZONE	M12-1662	90.00	92.40	4120	0.65	0.65	3.03	2.40	543,321.24	6,986,006.51	59.45
FZONE	M12-1663	101.70	104.30	4130	0.58	0.58	3.21	2.60	543,362.31	6,986,028.22	56.07
FZONE	M12-1663	108.70	111.40	4120	0.23	0.23	3.33	2.70	543,362.31	6,986,028.22	56.07
FZONE	M12-1666	60.40	63.00	4130	3.04	3.04	3.15	2.60	543,341.32	6,985,975.74	61.24
FZONE	M12-1666	64.50	67.00	4120	0.03	0.03	3.03	2.50	543,341.32	6,985,975.74	61.24
FZONE	M12-1667	103.00	105.80	4130	4.10	4.10	3.44	2.80	543,432.24	6,986,014.88	55.39
FZONE	M12-1667	109.90	112.80	4120	0.95	0.95	3.56	2.90	543,432.24	6,986,014.88	55.39
FZONE	M12-1669	88.10	91.70	4130	0.88	0.88	4.45	3.60	543,396.48	6,986,004.52	56.19
FZONE	M12-1669	93.70	96.10	4120	0.62	0.62	2.97	2.40	543,396.48	6,986,004.52	56.19
FZONE	M12-1670	85.90	88.50	4130	0.15	0.15	3.17	2.60	543,467.14	6,985,993.59	55.26
FZONE	M12-1670	94.90	97.50	4120	0.13	0.13	3.17	2.60	543,467.14	6,985,993.59	55.26
FZONE	M12-1671	81.80	84.75	4130	1.76	1.76	3.47	2.95	543,502.96	6,985,976.23	55.20
FZONE	M12-1671	89.20	93.50	4120	5.53	5.53	5.07	4.30	543,502.96	6,985,976.23	55.20
FZONE	M12-1674	9.00	10.60	4160	0.03	0.03	1.94	1.60	543,547.72	6,985,979.74	54.60
FZONE	M12-1674	96.00	99.00	4130	11.03	11.03	3.67	3.00	543,547.72	6,985,979.74	54.60
FZONE	M12-1675	40.00	43.00	4160	0.17	0.17	3.72	3.00	543,524.00	6,986,028.44	54.54
FZONE	M12-1676	60.00	63.70	4160	2.84	2.84	4.52	3.70	543,497.08	6,986,067.00	54.42
FZONE	M12-1677	13.60	16.50	4160	1.71	1.71	3.49	2.90	543,585.41	6,985,965.69	54.95
FZONE	M12-1677	90.00	92.60	4130	3.13	3.13	3.15	2.60	543,585.41	6,985,965.69	54.95
FZONE	M12-1678	63.50	66.50	4160	1.37	1.37	3.67	3.00	543,535.01	6,986,056.88	54.08
FZONE	M12-1678	149.00	151.60	4130	2.49	2.49	3.20	2.60	543,535.01	6,986,056.88	54.08
FZONE	M12-1678	154.80	157.20	4120	0.03	0.03	2.96	2.40	543,535.01	6,986,056.88	54.08
FZONE	M12-1680	78.50	81.50	4130	0.80	0.80	3.65	3.00	543,616.27	6,985,935.04	56.40
FZONE	M12-1680	82.20	84.10	4120	0.03	0.03	2.31	1.90	543,616.27	6,985,935.04	56.40
FZONE	M12-1685	35.30	38.00	4160	8.82	8.82	3.27	2.70	543,560.24	6,986,011.69	54.39
FZONE	M12-1686	49.00	52.00	4130	0.46	0.46	3.68	3.00	543,640.90	6,985,890.26	59.73
FZONE	M12-1686	55.00	57.60	4120	4.66	4.66	3.19	2.60	543,640.90	6,985,890.26	59.73
FZONE	M12-1687	34.50	37.00	4160	0.08	0.08	3.04	2.50	543,597.78	6,985,997.58	54.49
FZONE	M12-1690	23.00	26.50	4160	3.07	3.07	4.20	3.50	543,664.95	6,985,951.16	55.51
FZONE	M12-1690	96.00	99.00	4130	0.03	0.03	3.63	3.00	543,664.95	6,985,951.16	55.51
FZONE	M12-1690	100.40	103.00	4120	0.03	0.03	3.15	2.60	543,664.95	6,985,951.16	55.51
FZONE	M12-1693	63.20	66.20	4160	-	-	3.64	3.00	543,572.93	6,986,043.55	54.28
FZONE	M12-1696	61.40	64.80	4160	0.21	0.21	4.11	3.40	543,609.74	6,986,026.93	54.24
FZONE	M12-1697	22.70	27.10	4160	0.05	0.05	5.28	4.40	543,703.04	6,985,936.47	55.07
FZONE	M12-1697	94.60	98.40	4130	-	-	4.59	3.80	543,703.04	6,985,936.47	55.07
FZONE	M12-1699	19.50	24.00	4160	0.44	0.44	5.43	4.50	543,739.55	6,985,919.96	53.33
FZONE	M12-1732	48.00	53.00	4130	6.01	6.01	6.07	5.00	543,677.87	6,985,875.05	61.60
FZONE	M12-1732	56.40	60.00	4120	0.16	0.16	4.37	3.60	543,677.87	6,985,875.05	61.60
FZONE	M12-1734	26.80	29.40	4130	0.58	0.58	3.19	2.60	543,325.79	6,985,936.99	64.84

FZONE	M12-1734	34.80	38.00	4120	1.01	1.01	3.93	3.20	543,325.79	6,985,936.99	64.84
FZONE	M12-1735	20.50	23.60	4130	2.99	2.99	3.84	3.10	543,510.34	6,985,887.33	62.09
FZONE	M12-1735	25.60	27.70	4120	0.18	0.18	2.60	2.10	543,510.34	6,985,887.33	62.09
FZONE	M12-1758	617.40	620.00	4130	9.84	9.84	3.16	2.60	542,936.81	6,986,823.37	66.13
FZONE	M12-1758	622.00	624.60	4120	1.85	1.85	3.16	2.60	542,936.81	6,986,823.37	66.13
FZONE	M12-1758	636.00	638.80	4110	0.03	0.03	3.40	2.80	542,936.81	6,986,823.37	66.13
FZONE	M12-1771	555.10	559.10	4130	13.39	13.39	4.91	4.00	542,836.05	6,986,807.96	65.01
FZONE	M12-1771	580.00	582.80	4120	4.89	4.89	3.45	2.80	542,836.05	6,986,807.96	65.01
FZONE	M12-1771	595.40	598.20	4110	1.34	1.34	3.46	2.80	542,836.05	6,986,807.96	65.01
FZONE	M12-1779	397.30	401.00	4135	4.83	4.83	4.35	3.70	542,649.11	6,986,655.35	64.11
FZONE	M12-1779	404.00	407.00	4130	10.25	10.25	3.53	3.00	542,649.11	6,986,655.35	64.11
FZONE	M12-1779	411.00	413.60	4120	0.29	0.29	3.06	2.60	542,649.11	6,986,655.35	64.11
FZONE	M12-1779	418.00	420.60	4110	0.04	0.04	3.06	2.60	542,649.11	6,986,655.35	64.11
FZONE	M12-1802	22.00	27.00	4130	6.50	6.50	6.18	5.00	543,474.20	6,985,903.22	61.99
FZONE	M12-1802	28.00	30.20	4120	2.34	2.34	2.72	2.20	543,474.20	6,985,903.22	61.99
FZONE	M12-1819	450.00	452.60	4130	0.54	0.54	3.24	2.60	543,240.84	6,986,526.48	58.00
FZONE	M12-1819	457.40	460.00	4120	0.32	0.32	3.23	2.60	543,240.84	6,986,526.48	58.00
FZONE	M12-1833	376.10	378.50	4130	2.29	2.29	2.98	2.40	543,435.82	6,986,407.62	56.67
FZONE	M12-1833	383.10	386.00	4120	0.13	0.13	3.60	2.90	543,435.82	6,986,407.62	56.67
FZONE	M13-1991	157.00	161.00	4130	3.62	3.62	4.88	4.00	542,883.28	6,986,277.41	54.65
FZONE	M13-1991	164.00	169.30	4120	9.79	10.09	6.47	5.30	542,883.28	6,986,277.41	54.65
FZONE	M13-1991	175.10	178.10	4110	0.03	0.03	3.66	3.00	542,883.28	6,986,277.41	54.65
FZONE	M13-2000	173.90	176.30	4130	1.32	1.32	2.95	2.40	542,845.72	6,986,312.36	54.43
FZONE	M13-2000	191.70	194.30	4120	0.03	0.03	3.20	2.60	542,845.72	6,986,312.36	54.43
FZONE	M13-2000	199.80	202.70	4110	0.03	0.03	3.57	2.90	542,845.72	6,986,312.36	54.43
FZONE	M13-2011	152.90	155.50	4150	0.27	0.27	3.20	2.60	542,795.36	6,986,372.01	55.82
FZONE	M13-2011	214.50	217.70	4130	2.17	2.17	3.96	3.20	542,795.36	6,986,372.01	55.82
FZONE	M13-2011	220.00	223.30	4120	7.00	7.00	4.08	3.30	542,795.36	6,986,372.01	55.82
FZONE	M13-2011	235.80	238.40	4110	0.03	0.03	3.22	2.60	542,795.36	6,986,372.01	55.82
FZONE	M13-2016	147.20	150.20	4180	0.35	0.35	3.71	3.00	544,160.71	6,985,867.59	52.33
FZONE	M13-2016	153.50	156.30	4170	0.03	0.03	3.46	2.80	544,160.71	6,985,867.59	52.33
FZONE	M13-2021	100.00	102.60	4180	2.66	2.66	3.23	2.60	544,195.19	6,985,794.44	52.84
FZONE	M13-2021	104.00	107.00	4170	1.55	1.55	3.73	3.00	544,195.19	6,985,794.44	52.84
FZONE	M13-2025	421.40	424.90	4130	0.03	0.03	4.05	3.50	542,866.29	6,986,587.87	60.53
FZONE	M13-2025	441.60	444.50	4120	1.30	1.30	3.36	2.90	542,866.29	6,986,587.87	60.53
FZONE	M13-2025	455.60	458.20	4110	0.03	0.03	3.02	2.60	542,866.29	6,986,587.87	60.53
FZONE	M13-2029	82.40	85.00	4180	0.24	0.24	3.23	2.60	543,998.25	6,985,840.84	53.66
FZONE	M13-2029	86.00	89.50	4170	1.14	1.14	4.34	3.50	543,998.25	6,985,840.84	53.66
FZONE	M13-2036	180.00	183.00	4180	0.27	0.27	3.72	3.00	544,116.16	6,985,925.23	52.71
FZONE	M13-2036	183.00	185.93	4170	0.21	0.21	3.64	2.93	544,116.16	6,985,925.23	52.71
FZONE	M13-2045	162.50	169.50	4130	6.43	6.43	8.62	7.00	543,312.60	6,986,133.09	53.16
FZONE	M13-2045	172.90	175.50	4120	1.90	1.90	3.20	2.60	543,312.60	6,986,133.09	53.16
FZONE	M13-2055	195.90	198.40	4130	1.44	1.44	3.05	2.50	543,186.29	6,986,206.68	53.29
FZONE	M13-2055	200.40	204.70	4120	8.08	8.08	5.25	4.30	543,186.29	6,986,206.68	53.29
FZONE	M13-2055	204.70	206.95	4115	1.89	1.89	2.75	2.25	543,186.29	6,986,206.68	53.29
FZONE	M13-2055	219.20	221.40	4110	-	-	2.69	2.20	543,186.29	6,986,206.68	53.29
FZONE	M13-2057	302.60	305.00	4135	8.66	8.66	2.92	2.40	542,665.75	6,986,534.13	58.00
FZONE	M13-2057	306.40	312.00	4130	3.54	3.54	6.80	5.60	542,665.75	6,986,534.13	58.00
FZONE	M13-2057	314.60	317.50	4120	1.60	1.60	3.52	2.90	542,665.75	6,986,534.13	58.00
FZONE	M13-2057	327.00	330.10	4110	1.98	1.98	3.77	3.10	542,665.75	6,986,534.13	58.00
FZONE	M13-2063	193.50	196.20	4130	0.03	0.03	3.30	2.70	543,085.84	6,986,241.68	53.48
FZONE	M13-2063	199.10	201.60	4120	0.03	0.03	3.06	2.50	543,085.84	6,986,241.68	53.48
FZONE	M13-2063	207.00	209.50	4110	0.24	0.24	3.06	2.50	543,085.84	6,986,241.68	53.48
FZONE	M13-2069	130.70	133.50	4130	2.39	2.39	3.27	2.80	543,140.20	6,986,132.21	53.61
FZONE	M13-2069	137.60	140.10	4120	2.29	2.29	2.92	2.50	543,140.20	6,986,132.21	53.61
FZONE	M13-2069	143.70	148.60	4115	10.44	10.44	5.72	4.90	543,140.20	6,986,132.21	53.61
FZONE	M13-2069	148.60	151.50	4110	0.79	0.79	3.39	2.90	543,140.20	6,986,132.21	53.61
FZONE	M13-2070	325.00	327.00	4135	3.68	3.68	2.40	2.00	542,628.33	6,986,572.24	59.50
FZONE	M13-2070	330.00	333.90	4120	7.22	7.22	4.68	3.90	542,628.33	6,986,572.24	59.50
FZONE	M13-2070	330.00	333.90	4130	7.22	7.22	4.68	3.90	542,628.33	6,986,572.24	59.50
FZONE	M13-2070	353.30	355.80	4110	0.56	0.56	3.01	2.50	542,628.33	6,986,572.24	59.50
FZONE	M13-2076	275.60	279.60	4120	6.87	6.87	4.90	4.00	543,299.06	6,986,285.19	54.12
FZONE	M13-2076	275.60	279.60	4130	6.87	6.87	4.90	4.00	543,299.06	6,986,285.19	54.12
FZONE	M13-2081	354.50	360.00	4135	8.70	8.70	6.72	5.50	542,662.26	6,986,611.19	62.11
FZONE	M13-2081	360.00	364.00	4130	5.37	5.37	4.89	4.00	542,662.26	6,986,611.19	62.11
FZONE	M13-2081	368.80	371.50	4120	7.09	7.09	3.30	2.70	542,662.26	6,986,611.19	62.11
FZONE	M13-2081	393.50	396.70	4110	2.27	2.27	3.92	3.20	542,662.26	6,986,611.19	62.11
FZONE	M13-2087	240.50	243.10	4130	4.42	4.42	3.15	2.60	543,077.19	6,986,296.89	54.63
FZONE	M13-2087	244.50	247.30	4120	1.20	1.20	3.39	2.80	543,077.19	6,986,296.89	54.63
FZONE	M13-2087	251.30	254.30	4110	0.03	0.03	3.64	3.00	543,077.19	6,986,296.89	54.63
FZONE	M13-2093	577.70	580.50	4130	4.08	4.08	3.35	2.80	542,871.69	6,986,776.86	63.98
FZONE	M13-2093	590.50	593.30	4120	0.03	0.03	3.37	2.80	542,871.69	6,986,776.86	63.98
FZONE	M13-2093	604.70	607.40	4110	0.03	0.03	3.26	2.70	542,871.69	6,986,776.86	63.98
FZONE	M13-2102	366.70	372.70	4135	6.40	6.40	7.28	6.00	542,605.76	6,986,637.50	63.30
FZONE	M13-2102	373.70	376.70	4130	2.97	2.97	3.64	3.00	542,605.76	6,986,637.50	63.30
FZONE	M13-2102	376.70	379.20	4120	0.84	0.84	3.04	2.50	542,605.76	6,986,637.50	63.30
FZONE	M13-2102	404.00	406.60	4110	1.80	1.80	3.16	2.60	542,605.76	6,986,637.50	63.30
FZONE	M13-2107	461.40	469.80	4135	5.11	5.11	10.23	8.40	542,500.33	6,986,764.01	64.13
FZONE	M13-2107	477.10	480.00	4120	0.05	0.05	3.54	2.90	542,500.33	6,986,764.01	64.13
FZONE	M13-2107	496.10	498.60	4110	5.31	5.31	3.06	2.50	542,500.33	6,986,764.01	64.13
FZONE	M13-2119A	491.40	494.10	4130	0.45	0.45	3.25	2.70	542,901.26	6,986,649.79	60.86
FZONE	M13-2119A	501.40	504.00	4120	8.46	8.46	3.13	2.60	542,901.26	6,986,649.79	60.86
FZONE	M13-2119A	515.00	517.50	4110	0.03	0.03	3.01	2.50	542,901.26	6,986,649.79	60.86
FZONE	M13-2124	391.70	396.00	4135	5.38	5.38	5.16	4.30	542,596.76	6,986,669.53	64.20
FZONE	M13-2124	400.40	403.30	4130	3.40	3.40	3.48	2.90	542,596.76	6,986,669.53	64.20
FZONE	M13-2124	405.00	410.90	4120	5.31	5.31	7.08	5.90	542,596.76	6,986,669.53	64.20
FZONE	M13-2124	427.00	429.40	4110	2.31	2.31	2.88	2.40	542,596.76	6,986,669.53	64.20
FZONE	M13-2128A	309.70	310.70	4135	4.90	4.90	1.20	1.00	542,337.92	6,986,671.97	59.48
FZONE	M13-2128A	313.70	314.70	4135	4.16	4.16	1.20	1.00	542,337.92	6,986,671.97	59.48
FZONE	M13-2128A	325.20	327.90	4120	2.47	2.47	3.24	2.70	542,337.92	6,986,671.97	59.48

FZONE	M13-2131	389.30	392.50	4130	0.03	0.03	3.77	3.20	542,979.62	6,986,495.12	58.78
FZONE	M13-2131	397.50	400.50	4120	0.08	0.08	3.54	3.00	542,979.62	6,986,495.12	58.78
FZONE	M13-2131	411.90	414.00	4110	0.03	0.03	2.48	2.10	542,979.62	6,986,495.12	58.78
FZONE	M13-2134	455.20	458.90	4135	7.58	7.58	4.41	3.70	542,663.64	6,986,726.18	64.14
FZONE	M13-2134	459.60	463.00	4130	6.82	6.82	4.05	3.40	542,663.64	6,986,726.18	64.14
FZONE	M13-2134	463.00	466.90	4120	6.61	6.61	4.64	3.90	542,663.64	6,986,726.18	64.14
FZONE	M13-2134	479.00	481.50	4110	0.05	0.05	2.98	2.50	542,663.64	6,986,726.18	64.14
FZONE	M13-2135	366.40	369.30	4120	0.03	0.03	3.40	2.90	542,313.89	6,986,717.63	59.93
FZONE	M13-2138	341.50	344.50	4130	3.79	3.79	3.72	3.00	543,031.65	6,986,436.13	57.86
FZONE	M13-2138	346.50	349.50	4120	0.46	0.46	3.72	3.00	543,031.65	6,986,436.13	57.86
FZONE	M13-2138	358.80	361.60	4110	0.09	0.09	3.47	2.80	543,031.65	6,986,436.13	57.86
FZONE	M13-2143	533.30	536.30	4130	3.89	3.89	3.56	3.00	542,768.85	6,986,775.32	65.72
FZONE	M13-2143	560.80	563.80	4120	0.24	0.24	3.57	3.00	542,768.85	6,986,775.32	65.72
FZONE	M13-2143	574.10	577.40	4110	0.74	0.74	3.93	3.30	542,768.85	6,986,775.32	65.72
FZONE	M13-2144	298.00	301.00	4130	0.16	0.16	3.56	3.00	543,256.43	6,986,301.50	54.54
FZONE	M13-2144	303.00	306.00	4120	1.37	1.37	3.57	3.00	543,256.43	6,986,301.50	54.54
FZONE	M13-2195	452.20	456.00	4135	4.00	4.00	4.36	3.80	542,590.49	6,986,706.06	63.77
FZONE	M13-2195	459.00	462.00	4120	1.18	1.18	3.45	3.00	542,590.49	6,986,706.06	63.77
FZONE	M13-2195	471.20	473.60	4110	0.03	0.03	2.77	2.40	542,590.49	6,986,706.06	63.77
NORMEG	GT13-39	4.40	9.00	923	10.76	10.76	4.14	4.60	538,474.00	6,988,236.79	57.88
NORMEG	GT13-39	21.90	25.80	922	7.27	7.27	3.52	3.90	538,474.00	6,988,236.79	57.88
NORMEG	GT13-39	29.50	33.70	921	10.17	10.17	3.79	4.20	538,474.00	6,988,236.79	57.88
NORMEG	GT13-39	49.00	52.70	920	1.14	1.14	3.36	3.70	538,474.00	6,988,236.79	57.88
NORMEG	GT13-39	62.50	71.60	911	1.67	1.67	8.29	9.10	538,474.00	6,988,236.79	57.88
NORMEG	M11-1010	22.00	25.00	901	3.96	3.96	3.21	3.00	540,308.26	6,988,021.30	64.11
NORMEG	M11-1013	12.60	15.60	910	-	-	3.20	3.00	540,427.23	6,988,133.65	67.11
NORMEG	M11-1013	114.00	117.00	901	0.20	0.20	3.29	3.00	540,427.23	6,988,133.65	67.11
NORMEG	M11-1015	10.70	13.50	901	1.32	1.32	3.03	2.80	540,547.59	6,987,994.22	65.58
NORMEG	M11-1019	27.00	30.00	905	0.71	0.71	3.23	3.00	540,368.04	6,988,084.60	65.15
NORMEG	M11-1019	50.00	53.00	902	0.49	0.49	3.24	3.00	540,368.04	6,988,084.60	65.15
NORMEG	M11-1019	71.00	74.00	901	5.23	5.23	3.25	3.00	540,368.04	6,988,084.60	65.15
NORMEG	M11-1020	22.10	25.00	901	0.73	0.73	3.14	2.90	540,667.36	6,988,003.65	64.49
NORMEG	M11-1022	53.00	56.00	902	1.08	1.08	3.25	3.00	540,488.16	6,988,084.38	65.55
NORMEG	M11-1022	93.00	98.00	901	0.86	0.86	5.44	5.00	540,488.16	6,988,084.38	65.55
NORMEG	M11-1023	87.90	91.00	901	0.43	0.43	3.29	3.10	540,668.24	6,988,082.66	65.32
NORMEG	M11-1025	63.00	68.00	902	1.30	1.30	5.41	5.00	540,548.20	6,988,083.36	65.48
NORMEG	M11-1025	92.00	95.00	901	3.42	3.42	3.25	3.00	540,548.20	6,988,083.36	65.48
NORMEG	M11-1026	115.30	119.00	902	1.23	1.23	4.01	3.70	540,607.00	6,988,132.77	65.51
NORMEG	M11-1026	135.00	143.00	901	3.49	3.49	8.68	8.00	540,607.00	6,988,132.77	65.51
NORMEG	M11-1029	7.70	10.60	901	6.89	6.89	3.09	2.90	540,487.94	6,987,984.47	65.05
NORMEG	M11-1030	42.00	48.00	901	1.48	1.48	6.43	6.00	540,727.15	6,988,033.77	65.37
NORMEG	M11-1033	70.60	74.00	902	2.28	2.28	3.70	3.40	540,847.86	6,988,083.54	69.03
NORMEG	M11-1033	79.00	84.30	901	19.77	24.07	5.76	5.30	540,847.86	6,988,083.54	69.03
NORMEG	M11-1038	135.00	138.00	902	0.45	0.45	3.25	3.00	540,909.89	6,988,164.61	68.28
NORMEG	M11-1038	160.00	163.00	901	4.05	4.05	3.26	3.00	540,909.89	6,988,164.61	68.28
NORMEG	M11-1051	23.30	27.00	901	1.26	1.26	3.99	3.70	540,248.85	6,988,034.34	63.92
NORMEG	M11-1063	153.00	156.00	988	5.33	5.33	3.19	3.00	540,090.76	6,988,437.55	64.72
NORMEG	M11-1066	150.40	153.40	988	0.15	0.15	3.12	3.00	540,105.30	6,988,430.77	65.98
NORMEG	M11-1104	114.00	117.00	902	0.78	0.78	3.26	3.00	540,997.53	6,988,133.04	68.17
NORMEG	M11-1104	130.40	133.60	901	0.04	0.04	3.48	3.20	540,997.53	6,988,133.04	68.17
NORMEG	M11-1105	27.00	30.00	907	-	-	3.21	3.00	538,837.45	6,988,183.68	60.95
NORMEG	M11-1110	147.00	150.00	988	0.06	0.06	3.19	3.00	538,410.07	6,988,521.29	58.65
NORMEG	M11-1111	84.30	87.50	902	1.17	1.17	3.25	3.20	540,941.04	6,988,092.21	68.33
NORMEG	M11-1111	102.50	108.50	901	6.86	6.86	6.08	6.00	540,941.04	6,988,092.21	68.33
NORMEG	M11-1113	16.50	20.30	930	0.80	0.80	4.02	3.80	539,136.98	6,988,233.58	65.85
NORMEG	M11-1113	43.80	46.70	920	5.01	5.01	3.09	2.90	539,136.98	6,988,233.58	65.85
NORMEG	M11-1113	62.00	65.80	911	0.06	0.06	4.06	3.80	539,136.98	6,988,233.58	65.85
NORMEG	M11-1113	79.30	83.00	910	0.19	0.19	3.96	3.70	539,136.98	6,988,233.58	65.85
NORMEG	M11-1113	84.50	87.50	907	0.49	0.49	3.22	3.00	539,136.98	6,988,233.58	65.85
NORMEG	M11-1113	103.40	106.90	906	0.64	0.64	3.77	3.50	539,136.98	6,988,233.58	65.85
NORMEG	M11-1113	115.70	119.50	904	1.22	1.22	4.10	3.80	539,136.98	6,988,233.58	65.85
NORMEG	M11-1118	40.10	43.00	901	6.48	6.48	3.14	2.90	540,997.95	6,988,033.51	68.42
NORMEG	M11-1123	60.00	63.00	911	12.99	12.99	3.22	3.00	538,897.04	6,988,233.22	68.91
NORMEG	M11-1123	65.50	68.50	910	0.43	0.43	3.22	3.00	538,897.04	6,988,233.22	68.91
NORMEG	M11-1123	74.40	77.60	907	1.85	1.85	3.44	3.20	538,897.04	6,988,233.22	68.91
NORMEG	M11-1124	94.00	97.00	901	4.02	4.02	3.27	3.00	541,056.99	6,988,087.56	69.22
NORMEG	M11-1134	155.20	158.00	988	-	-	3.00	2.80	540,089.89	6,988,438.61	65.93
NORMEG	M11-1161	449.00	452.00	987	0.64	0.64	2.97	3.00	540,115.02	6,988,691.97	66.32
NORMEG	M11-1183	62.60	66.10	910	5.64	5.64	2.99	3.50	540,367.96	6,988,164.42	66.16
NORMEG	M11-1183	154.50	158.30	902	0.21	0.21	3.43	3.80	540,367.96	6,988,164.42	66.16
NORMEG	M11-1183	192.00	195.60	901	0.03	0.03	3.30	3.60	540,367.96	6,988,164.42	66.16
NORMEG	M11-1186	360.00	363.60	987	0.12	0.12	3.41	3.60	539,990.08	6,988,615.34	67.44
NORMEG	M11-1196	50.90	54.20	910	0.03	0.03	3.41	3.30	540,367.85	6,988,163.51	65.97
NORMEG	M11-1196	153.00	156.20	901	23.69	23.69	3.40	3.20	540,367.85	6,988,163.51	65.97
NORMEG	M11-1207	265.00	269.00	901	2.64	2.64	3.78	4.00	540,607.08	6,988,214.16	66.21
NORMEG	M11-1214	227.00	230.00	988	0.45	0.45	3.29	3.00	538,250.03	6,988,629.06	59.16
NORMEG	M11-1217	224.00	227.00	901	0.60	0.60	3.23	3.00	540,607.14	6,988,212.74	65.91
NORMEG	M11-1227	179.80	182.80	988	0.05	0.05	3.38	3.00	538,597.08	6,988,531.31	61.49
NORMEG	M11-1230	232.60	235.40	901	0.94	0.94	2.87	2.80	540,607.14	6,988,213.25	65.94
NORMEG	M11-1236	514.30	518.00	988	0.50	0.50	3.34	3.70	539,585.19	6,988,749.27	71.73
NORMEG	M11-1245	21.80	24.80	901	6.53	6.53	3.25	3.00	541,178.46	6,987,982.93	70.49
NORMEG	M11-1252	43.00	45.70	901	0.41	0.41	2.91	2.70	541,118.01	6,988,033.72	69.89
NORMEG	M11-1266	257.30	258.80	987	0.03	0.03	1.50	1.50	540,039.92	6,988,529.43	66.79
NORMEG	M11-1279	109.00	112.00	902	1.96	1.96	3.22	3.00	540,847.04	6,988,127.88	69.14
NORMEG	M11-1279	118.40	124.45	901	4.24	4.24	6.50	6.05	540,847.04	6,988,127.88	69.14
NORMEG	M11-1288	102.90	105.80	902	0.63	0.63	3.17	2.90	540,727.00	6,988,134.00	67.70
NORMEG	M11-1288	138.00	142.20	901	1.06	1.06	4.61	4.20	540,727.00	6,988,134.00	67.70
NORMEG	M11-1300	66.00	69.00	911	0.11	0.11	3.19	3.00	538,957.07	6,988,230.53	71.27
NORMEG	M11-1300	70.00	73.00	910	0.21	0.21	3.19	3.00	538,957.07	6,988,230.53	71.27
NORMEG	M11-1300	76.00	79.00	907	0.19	0.19	3.20	3.00	538,957.07	6,988,230.53	71.27

NORMEG	M11-1306	69.00	72.00	911	9.08	9.08	3.04	3.00	538,957.04	6,988,230.80	70.99
NORMEG	M11-1306	74.00	77.10	910	0.68	0.68	3.15	3.10	538,957.04	6,988,230.80	70.99
NORMEG	M11-1306	81.40	84.80	907	0.55	0.55	3.46	3.40	538,957.04	6,988,230.80	70.99
NORMEG	M11-1312	30.40	33.60	910	1.10	1.10	3.43	3.20	540,423.78	6,988,154.33	66.40
NORMEG	M11-1312	131.00	134.00	901	0.59	0.59	3.28	3.00	540,423.78	6,988,154.33	66.40
NORMEG	M11-1314	443.00	446.60	920	0.83	0.83	3.97	3.60	539,094.15	6,988,638.34	68.35
NORMEG	M11-1314	473.00	477.00	910	2.17	2.17	4.42	4.00	539,094.15	6,988,638.34	68.35
NORMEG	M11-1314	480.00	487.00	907	5.14	5.14	7.75	7.00	539,094.15	6,988,638.34	68.35
NORMEG	M11-1317	123.55	130.80	902	3.56	3.56	7.63	7.25	540,570.25	6,988,139.23	65.31
NORMEG	M11-1317	149.00	153.00	901	0.33	0.33	4.21	4.00	540,570.25	6,988,139.23	65.31
NORMEG	M11-1323	12.80	23.00	902	2.93	2.93	10.84	10.20	540,450.10	6,988,044.00	64.30
NORMEG	M11-1323	50.30	54.00	901	0.74	0.74	3.96	3.70	540,450.10	6,988,044.00	64.30
NORMEG	M11-1330	24.00	27.00	902	1.23	1.23	3.24	3.00	540,559.92	6,988,035.40	64.61
NORMEG	M11-1330	46.90	50.00	901	0.34	0.34	3.38	3.10	540,559.92	6,988,035.40	64.61
NORMEG	M11-1337	429.50	433.00	920	0.04	0.04	3.83	3.50	539,094.16	6,988,637.81	68.53
NORMEG	M11-1337	459.50	463.30	910	0.04	0.04	4.17	3.80	539,094.16	6,988,637.81	68.53
NORMEG	M11-1337	469.00	472.80	907	0.12	0.12	4.18	3.80	539,094.16	6,988,637.81	68.53
NORMEG	M11-1344	15.00	19.50	901	1.32	1.32	4.69	4.50	540,394.98	6,988,019.17	64.16
NORMEG	M11-1346	15.00	18.80	902	2.01	2.01	3.98	3.80	540,335.01	6,988,049.11	63.60
NORMEG	M11-1346	42.00	45.00	901	0.72	0.72	3.17	3.00	540,335.01	6,988,049.11	63.60
NORMEG	M11-1356	37.00	40.00	905	5.42	5.42	3.20	3.00	540,275.10	6,988,107.85	63.83
NORMEG	M11-1356	96.00	99.00	901	0.14	0.14	3.23	3.00	540,275.10	6,988,107.85	63.83
NORMEG	M11-1358	309.70	312.30	987	0.03	0.03	2.61	2.60	540,090.14	6,988,595.60	66.91
NORMEG	M11-1359	349.50	353.30	930	1.45	1.45	3.78	3.80	539,169.91	6,988,560.60	71.72
NORMEG	M12-1475	14.80	18.00	923	25.62	25.62	3.42	3.20	538,526.87	6,988,247.83	58.05
NORMEG	M12-1475	42.00	46.50	920	0.16	0.16	4.83	4.50	538,526.87	6,988,247.83	58.05
NORMEG	M12-1475	62.00	65.00	911	0.45	0.45	3.22	3.00	538,526.87	6,988,247.83	58.05
NORMEG	M12-1476	225.00	228.00	988	1.48	1.48	3.08	3.00	538,169.73	6,988,620.46	58.12
NORMEG	M12-1478	31.00	33.60	902	20.16	20.16	2.81	2.60	540,936.75	6,988,032.86	69.33
NORMEG	M12-1478	37.80	41.10	901	0.08	0.08	3.56	3.30	540,936.75	6,988,032.86	69.33
NORMEG	M12-1480	15.00	18.60	923	1.83	1.83	3.62	3.60	538,526.86	6,988,248.17	58.14
NORMEG	M12-1480	45.00	49.00	920	1.40	1.40	4.06	4.00	538,526.86	6,988,248.17	58.14
NORMEG	M12-1480	62.00	68.00	911	1.77	1.77	6.11	6.00	538,526.86	6,988,248.17	58.14
NORMEG	M12-1483	192.00	195.00	988	3.90	3.90	3.30	3.00	538,200.22	6,988,591.48	58.25
NORMEG	M12-1486	17.80	20.80	901	-	-	3.21	3.00	540,966.73	6,988,009.55	69.60
NORMEG	M12-1487	76.50	79.50	923	0.79	0.79	3.17	3.00	538,577.94	6,988,315.73	59.40
NORMEG	M12-1487	89.00	92.00	922	3.21	3.21	3.18	3.00	538,577.94	6,988,315.73	59.40
NORMEG	M12-1487	117.00	120.80	920	1.06	1.06	4.04	3.80	538,577.94	6,988,315.73	59.40
NORMEG	M12-1487	133.40	137.00	911	1.06	1.06	3.84	3.60	538,577.94	6,988,315.73	59.40
NORMEG	M12-1488	178.60	182.20	988	-	-	3.74	3.60	538,224.97	6,988,566.29	59.21
NORMEG	M12-1489	109.50	112.70	923	2.41	2.41	3.25	3.20	538,526.76	6,988,336.58	60.28
NORMEG	M12-1489	118.00	121.00	922	1.96	1.96	3.05	3.00	538,526.76	6,988,336.58	60.28
NORMEG	M12-1489	144.00	151.80	920	28.93	35.60	7.93	7.80	538,526.76	6,988,336.58	60.28
NORMEG	M12-1489	153.00	158.00	911	8.96	8.96	5.08	5.00	538,526.76	6,988,336.58	60.28
NORMEG	M12-1493	13.00	16.00	901	1.89	1.89	3.18	3.00	541,027.16	6,988,009.03	70.22
NORMEG	M12-1496	144.00	147.00	988	-	-	3.28	3.00	538,224.87	6,988,546.00	58.45
NORMEG	M12-1498	14.50	17.50	988	3.00	3.00	3.07	3.00	538,466.88	6,988,364.93	59.74
NORMEG	M12-1498	134.40	137.80	923	0.03	0.03	3.54	3.40	538,466.88	6,988,364.93	59.74
NORMEG	M12-1499	11.50	14.00	901	0.83	0.83	2.66	2.50	541,087.23	6,988,007.48	68.67
NORMEG	M12-1504	84.80	87.85	988	9.78	9.78	3.12	3.05	538,526.92	6,988,424.93	59.79
NORMEG	M12-1504	197.00	200.00	923	0.16	0.16	3.10	3.00	538,526.92	6,988,424.93	59.79
NORMEG	M12-1504	225.20	228.40	920	1.31	1.31	3.33	3.20	538,526.92	6,988,424.93	59.79
NORMEG	M12-1514	31.90	36.00	930	0.58	0.58	4.26	4.10	538,466.84	6,988,299.45	58.00
NORMEG	M12-1514	47.90	51.90	925	-	-	4.17	4.00	538,466.84	6,988,299.45	58.00
NORMEG	M12-1514	69.40	73.00	923	1.58	1.58	3.78	3.60	538,466.84	6,988,299.45	58.00
NORMEG	M12-1514	78.00	80.85	922	0.95	0.95	3.00	2.85	538,466.84	6,988,299.45	58.00
NORMEG	M12-1514	89.30	93.00	921	0.03	0.03	3.90	3.70	538,466.84	6,988,299.45	58.00
NORMEG	M12-1514	104.00	114.20	920	17.61	28.46	10.80	10.20	538,466.84	6,988,299.45	58.00
NORMEG	M12-1514	121.50	124.60	911	0.56	0.56	3.29	3.10	538,466.84	6,988,299.45	58.00
NORMEG	M12-1518	62.30	65.30	930	0.07	0.07	3.10	3.00	538,406.98	6,988,334.31	58.05
NORMEG	M12-1518	84.00	87.00	925	2.99	2.99	3.11	3.00	538,406.98	6,988,334.31	58.05
NORMEG	M12-1518	94.50	104.00	924	8.59	8.59	9.84	9.50	538,406.98	6,988,334.31	58.05
NORMEG	M12-1518	105.50	109.90	923	1.99	1.99	4.56	4.40	538,406.98	6,988,334.31	58.05
NORMEG	M12-1518	113.40	116.60	922	1.03	1.03	3.32	3.20	538,406.98	6,988,334.31	58.05
NORMEG	M12-1518	122.20	128.20	921	2.00	2.00	6.22	6.00	538,406.98	6,988,334.31	58.05
NORMEG	M12-1524	84.80	87.80	907	0.05	0.05	3.19	3.00	538,627.61	6,988,234.90	58.45
NORMEG	M12-1530	359.00	362.00	920	0.96	0.96	3.10	3.00	540,205.02	6,988,593.41	65.52
NORMEG	M12-1534	51.80	55.00	907	0.38	0.38	3.43	3.20	538,678.08	6,988,203.75	58.53
NORMEG	M12-1552	115.90	119.00	920	3.48	3.48	3.30	3.10	538,257.29	6,988,326.31	58.18
NORMEG	M12-1569	111.40	114.00	988	6.57	6.57	2.82	2.60	538,524.96	6,988,463.61	59.71
NORMEG	M12-1576	247.00	250.00	921	8.65	8.65	3.29	3.00	538,625.01	6,988,464.02	60.94
NORMEG	M12-1576	253.00	256.60	920	22.85	22.85	3.95	3.60	538,625.01	6,988,464.02	60.94
NORMEG	M12-1576	270.80	273.80	911	0.03	0.03	3.29	3.00	538,625.01	6,988,464.02	60.94
NORMEG	M12-1576	293.50	296.50	907	2.82	2.82	3.30	3.00	538,625.01	6,988,464.02	60.94
NORMEG	M12-1582	120.00	125.00	902	1.49	1.49	5.44	5.00	540,696.88	6,988,143.55	66.61
NORMEG	M12-1582	137.40	140.50	901	6.26	6.26	3.38	3.10	540,696.88	6,988,143.55	66.61
NORMEG	M12-1594	203.40	207.00	902	1.16	1.16	3.89	3.60	540,731.32	6,988,231.32	69.22
NORMEG	M12-1594	221.20	228.40	901	8.11	8.11	7.79	7.20	540,731.32	6,988,231.32	69.22
NORMEG	M12-1597	364.00	368.00	920	2.36	2.36	4.16	4.00	538,799.88	6,988,525.77	65.09
NORMEG	M12-1597	386.10	390.10	907	0.11	0.11	4.17	4.00	538,799.88	6,988,525.77	65.09
NORMEG	M12-1605	36.00	39.00	925	3.13	3.13	3.04	3.00	538,359.53	6,988,274.18	57.95
NORMEG	M12-1605	44.00	47.00	924	1.09	1.09	3.05	3.00	538,359.53	6,988,274.18	57.95
NORMEG	M12-1605	49.00	56.00	923	7.84	7.84	7.14	7.00	538,359.53	6,988,274.18	57.95
NORMEG	M12-1605	58.00	61.00	921	1.56	1.56	3.07	3.00	538,359.53	6,988,274.18	57.95
NORMEG	M12-1605	71.00	76.20	920	12.89	12.89	5.34	5.20	538,359.53	6,988,274.18	57.95
NORMEG	M12-1605	89.70	92.90	911	0.03	0.03	3.30	3.20	538,359.53	6,988,274.18	57.95
NORMEG	M12-1606	247.00	250.00	902	0.66	0.66	3.27	3.00	540,792.25	6,988,287.14	67.95
NORMEG	M12-1606	267.00	270.00	901	1.32	1.32	3.28	3.00	540,792.25	6,988,287.14	67.95
NORMEG	M12-1616	177.00	180.00	923	0.04	0.04	3.20	3.00	538,360.22	6,988,409.31	58.27
NORMEG	M12-1617	499.00	502.00	987	4.77	4.77	3.14	3.00	539,768.08	6,988,773.94	67.85

NORMEG	M12-1621	391.00	394.00	920	15.52	15.52	3.09	3.00	538,924.60	6,988,550.23	68.05
NORMEG	M12-1621	397.20	400.00	911	0.21	0.21	2.89	2.80	538,924.60	6,988,550.23	68.05
NORMEG	M12-1621	402.00	405.60	910	30.28	30.28	3.72	3.60	538,924.60	6,988,550.23	68.05
NORMEG	M12-1632	295.00	298.00	902	9.41	9.41	3.27	3.00	540,731.05	6,988,332.72	67.99
NORMEG	M12-1632	303.00	309.00	901	0.77	0.77	6.54	6.00	540,731.05	6,988,332.72	67.99
NORMEG	M12-1651	19.10	24.30	930	1.74	1.74	5.38	5.20	538,424.98	6,988,289.92	57.99
NORMEG	M12-1651	37.00	40.00	925	0.03	0.03	3.13	3.00	538,424.98	6,988,289.92	57.99
NORMEG	M12-1651	46.00	50.60	924	5.40	5.40	4.83	4.60	538,424.98	6,988,289.92	57.99
NORMEG	M12-1651	60.00	64.00	923	1.09	1.09	4.22	4.00	538,424.98	6,988,289.92	57.99
NORMEG	M12-1651	68.00	71.00	922	1.09	1.09	3.18	3.00	538,424.98	6,988,289.92	57.99
NORMEG	M12-1651	82.00	86.00	921	1.93	1.93	4.25	4.00	538,424.98	6,988,289.92	57.99
NORMEG	M12-1651	95.80	98.80	920	0.53	0.53	3.20	3.00	538,424.98	6,988,289.92	57.99
NORMEG	M12-1651	101.00	104.00	911	0.82	0.82	3.20	3.00	538,424.98	6,988,289.92	57.99
NORMEG	M12-1657	52.00	55.30	925	3.80	3.80	3.46	3.30	538,299.80	6,988,294.00	57.85
NORMEG	M12-1657	87.40	90.60	920	2.30	2.30	3.41	3.20	538,299.80	6,988,294.00	57.85
NORMEG	M12-1657	97.00	100.00	911	1.57	1.57	3.20	3.00	538,299.80	6,988,294.00	57.85
NORMEG	M12-1672	91.00	95.00	988	0.18	0.18	3.66	4.00	538,599.92	6,988,408.06	59.97
NORMEG	M12-1679	95.00	98.60	988	0.48	0.48	3.16	3.60	538,599.93	6,988,408.10	59.92
NORMEG	M12-1679	241.35	244.90	921	1.46	1.46	3.45	3.55	538,599.93	6,988,408.10	59.92
NORMEG	M12-1679	255.80	259.50	920	6.93	6.93	3.61	3.70	538,599.93	6,988,408.10	59.92
NORMEG	M12-1679	273.80	278.30	911	0.71	0.71	4.42	4.50	538,599.93	6,988,408.10	59.92
NORMEG	M12-1679	287.30	290.10	907	0.03	0.03	2.76	2.80	538,599.93	6,988,408.10	59.92
NORMEG	M12-1684	88.00	92.00	988	0.59	0.59	4.00	4.00	538,449.75	6,988,450.29	59.31
NORMEG	M12-1684	222.00	225.00	923	0.03	0.03	3.07	3.00	538,449.75	6,988,450.29	59.31
NORMEG	M12-1688	450.50	455.00	987	1.03	1.03	4.14	4.50	540,115.09	6,988,663.16	65.70
NORMEG	M12-1694	161.00	165.00	920	0.12	0.12	4.31	4.00	538,700.08	6,988,358.66	60.85
NORMEG	M12-1694	198.80	202.50	907	0.03	0.03	4.01	3.70	538,700.08	6,988,358.66	60.85
NORMEG	M12-1701	357.30	361.00	920	0.03	0.03	3.72	3.70	538,700.22	6,988,528.76	64.97
NORMEG	M12-1701	384.00	388.00	907	0.36	0.36	4.04	4.00	538,700.22	6,988,528.76	64.97
NORMEG	M12-1704A	507.00	511.00	988	1.19	1.19	3.72	4.00	539,385.35	6,988,731.48	77.73
NORMEG	M12-1705	499.30	503.00	987	0.95	0.95	3.76	3.70	540,040.33	6,988,740.08	66.64
NORMEG	M12-1708	61.50	66.00	902	1.19	1.19	4.91	4.50	540,457.08	6,988,099.25	65.51
NORMEG	M12-1708	90.40	93.80	901	1.58	1.58	3.72	3.40	540,457.08	6,988,099.25	65.51
NORMEG	M12-1709	199.00	202.60	920	0.47	0.47	3.85	3.60	538,774.96	6,988,385.23	67.87
NORMEG	M12-1709A	204.20	207.80	920	0.03	0.03	3.80	3.60	538,774.96	6,988,385.23	67.87
NORMEG	M12-1709A	235.00	238.00	907	0.03	0.03	3.18	3.00	538,774.96	6,988,385.23	67.87
NORMEG	M12-1711	253.00	257.00	920	0.89	0.89	4.09	4.00	538,700.13	6,988,428.69	63.87
NORMEG	M12-1711	277.40	281.00	907	1.68	1.68	3.70	3.60	538,700.13	6,988,428.69	63.87
NORMEG	M12-1725	473.70	480.00	920	0.94	0.94	6.31	6.30	539,025.02	6,988,614.65	73.98
NORMEG	M12-1725	500.90	504.00	910	0.06	0.06	3.13	3.10	539,025.02	6,988,614.65	73.98
NORMEG	M12-1730	276.80	279.40	987	0.03	0.03	2.63	2.60	540,095.39	6,988,546.07	67.69
NORMEG	M12-1730	343.00	345.80	920	0.13	0.13	2.87	2.80	540,095.39	6,988,546.07	67.69
NORMEG	M12-1737B	444.00	448.50	988	0.09	0.09	2.94	4.50	539,165.09	6,988,576.74	70.27
NORMEG	M12-1742	474.00	478.50	987	1.28	1.28	4.23	4.50	540,105.86	6,988,688.05	66.27
NORMEG	M12-1748	508.80	512.30	988	3.43	3.43	3.46	3.50	538,940.02	6,988,759.51	65.28
NORMEG	M12-1748	519.80	522.80	987	0.03	0.03	2.97	3.00	538,940.02	6,988,759.51	65.28
NORMEG	M12-1756	281.30	284.30	920	1.98	1.98	3.21	3.00	540,175.19	6,988,512.32	66.34
NORMEG	M12-1756	384.90	387.60	910	2.34	2.34	2.95	2.70	540,175.19	6,988,512.32	66.34
NORMEG	M12-1759	473.00	475.60	988	2.73	2.73	2.72	2.60	539,180.06	6,988,740.08	68.15
NORMEG	M12-1759	573.00	576.00	920	0.88	0.88	3.21	3.00	539,180.06	6,988,740.08	68.15
NORMEG	M12-1759	593.30	596.30	910	2.12	2.12	3.23	3.00	539,180.06	6,988,740.08	68.15
NORMEG	M12-1763C	597.00	600.00	988	5.33	5.33	3.16	3.00	539,380.17	6,988,875.02	75.66
NORMEG	M12-1765	473.50	477.10	920	33.58	57.46	3.67	3.60	538,925.04	6,988,608.39	70.68
NORMEG	M12-1765	481.00	484.40	911	0.80	0.80	3.47	3.40	538,925.04	6,988,608.39	70.68
NORMEG	M12-1765	485.00	488.00	910	3.47	3.47	3.06	3.00	538,925.04	6,988,608.39	70.68
NORMEG	M12-1767	463.40	466.80	988	0.50	0.50	3.38	3.40	539,075.06	6,988,724.65	65.47
NORMEG	M12-1767	508.00	511.00	930	14.98	14.98	3.01	3.00	539,075.06	6,988,724.65	65.47
NORMEG	M12-1767	573.20	577.20	920	0.06	0.06	4.06	4.00	539,075.06	6,988,724.65	65.47
NORMEG	M12-1767	604.20	607.10	907	2.67	2.67	2.96	2.90	539,075.06	6,988,724.65	65.47
NORMEG	M12-1769	581.70	584.00	988	0.14	0.14	2.46	2.30	539,529.93	6,988,873.58	71.47
NORMEG	M12-1769	637.80	641.00	930	3.36	3.36	3.45	3.20	539,529.93	6,988,873.58	71.47
NORMEG	M12-1769	688.10	691.10	911	3.93	3.93	3.26	3.00	539,529.93	6,988,873.58	71.47
NORMEG	M12-1774	318.80	322.10	920	2.10	2.10	3.35	3.30	538,924.96	6,988,486.57	66.48
NORMEG	M12-1774	330.90	335.00	911	0.04	0.04	4.17	4.10	538,924.96	6,988,486.57	66.48
NORMEG	M12-1774	337.40	341.20	910	0.93	0.93	3.87	3.80	538,924.96	6,988,486.57	66.48
NORMEG	M12-1774	345.40	348.20	907	0.80	0.80	2.86	2.80	538,924.96	6,988,486.57	66.48
NORMEG	M12-1775	540.00	543.30	920	36.38	87.29	3.64	3.30	539,180.00	6,988,739.69	68.20
NORMEG	M12-1775	559.20	562.20	910	39.79	54.38	3.31	3.00	539,180.00	6,988,739.69	68.20
NORMEG	M12-1778	209.00	213.50	920	1.24	1.24	4.86	4.50	538,949.94	6,988,406.96	65.86
NORMEG	M12-1778	228.50	232.30	911	0.08	0.08	4.11	3.80	538,949.94	6,988,406.96	65.86
NORMEG	M12-1778	243.60	246.50	907	0.21	0.21	3.15	2.90	538,949.94	6,988,406.96	65.86
NORMEG	M12-1781A	516.50	520.00	988	8.49	8.49	3.48	3.50	539,889.48	6,988,754.81	66.92
NORMEG	M12-1781A	533.00	538.50	987	1.89	1.89	5.48	5.50	539,889.48	6,988,754.81	66.92
NORMEG	M12-1783	99.50	103.30	930	0.64	0.64	4.08	3.80	539,092.08	6,988,316.35	66.79
NORMEG	M12-1783	155.00	158.00	910	0.03	0.03	3.25	3.00	539,092.08	6,988,316.35	66.79
NORMEG	M12-1783	168.50	172.10	907	0.03	0.03	3.91	3.60	539,092.08	6,988,316.35	66.79
NORMEG	M12-1787	555.80	558.80	930	22.51	22.51	3.12	3.00	539,355.14	6,988,756.75	78.12
NORMEG	M12-1787	595.00	598.00	911	4.50	4.50	3.14	3.00	539,355.14	6,988,756.75	78.12
NORMEG	M12-1788	192.00	195.10	920	5.17	5.17	3.29	3.10	538,875.33	6,988,382.40	67.16
NORMEG	M12-1788	205.30	208.30	911	2.96	2.96	3.19	3.00	538,875.33	6,988,382.40	67.16
NORMEG	M12-1788	222.50	225.60	907	0.03	0.03	3.31	3.10	538,875.33	6,988,382.40	67.16
NORMEG	M12-1793	90.70	93.90	910	0.48	0.48	3.27	3.20	539,000.23	6,988,249.02	70.92
NORMEG	M12-1793	101.50	104.50	907	0.03	0.03	3.07	3.00	539,000.23	6,988,249.02	70.92
NORMEG	M12-1794	89.00	92.00	930	3.32	3.32	3.22	3.00	539,227.25	6,988,304.79	71.33
NORMEG	M12-1794	120.30	124.00	920	0.75	0.75	3.99	3.70	539,227.25	6,988,304.79	71.33
NORMEG	M12-1794	133.80	138.20	911	12.66	12.66	4.76	4.40	539,227.25	6,988,304.79	71.33
NORMEG	M12-1794	145.30	149.00	910	0.22	0.22	4.01	3.70	539,227.25	6,988,304.79	71.33
NORMEG	M12-1794	166.70	170.00	906	0.39	0.39	3.59	3.30	539,227.25	6,988,304.79	71.33
NORMEG	M12-1794	177.50	180.50	904	0.35	0.35	3.26	3.00	539,227.25	6,988,304.79	71.33
NORMEG	M12-1794	191.00	194.00	903	0.97	0.97	3.27	3.00	539,227.25	6,988,304.79	71.33

NORMEG	M12-1794	204.40	209.70	902	1.52	1.52	5.79	5.30	539,227.25	6,988,304.79	71.33
NORMEG	M12-1797	440.80	444.40	920	0.77	0.77	3.53	3.60	538,989.77	6,988,564.08	71.72
NORMEG	M12-1797	448.70	452.10	911	0.31	0.31	3.36	3.40	538,989.77	6,988,564.08	71.72
NORMEG	M12-1797	454.10	457.80	910	0.36	0.36	3.67	3.70	538,989.77	6,988,564.08	71.72
NORMEG	M12-1799	481.90	485.30	988	0.03	0.03	3.51	3.40	539,130.05	6,988,745.38	65.70
NORMEG	M12-1799	544.50	548.30	930	9.13	9.13	3.96	3.80	539,130.05	6,988,745.38	65.70
NORMEG	M12-1799	597.00	600.00	920	0.43	0.43	3.15	3.00	539,130.05	6,988,745.38	65.70
NORMEG	M12-1800	483.00	490.00	907	5.42	5.42	7.45	7.00	538,650.08	6,988,649.30	65.44
NORMEG	M12-1805	89.40	92.80	988	0.87	0.87	3.62	3.40	539,889.30	6,988,383.84	68.69
NORMEG	M12-1805	94.30	97.30	987	0.93	0.93	3.20	3.00	539,889.30	6,988,383.84	68.69
NORMEG	M12-1805	180.40	183.80	920	0.39	0.39	3.67	3.40	539,889.30	6,988,383.84	68.69
NORMEG	M12-1805	216.40	219.40	911	1.34	1.34	3.26	3.00	539,889.30	6,988,383.84	68.69
NORMEG	M12-1806	70.00	73.20	988	1.23	1.23	3.35	3.20	539,648.09	6,988,352.89	78.56
NORMEG	M12-1806	128.00	131.00	930	0.36	0.36	3.18	3.00	539,648.09	6,988,352.89	78.56
NORMEG	M12-1806	176.40	188.40	911	14.01	18.10	12.84	12.00	539,648.09	6,988,352.89	78.56
NORMEG	M12-1806	197.00	200.20	910	2.33	2.33	3.43	3.20	539,648.09	6,988,352.89	78.56
NORMEG	M12-1809	443.90	448.00	920	20.50	20.50	3.32	4.10	539,168.59	6,988,514.68	74.51
NORMEG	M12-1809	484.50	487.50	910	0.12	0.12	2.48	3.00	539,168.59	6,988,514.68	74.51
NORMEG	M12-1809	492.60	496.50	907	0.16	0.16	3.24	3.90	539,168.59	6,988,514.68	74.51
NORMEG	M12-1813	92.30	95.30	920	1.29	1.29	3.18	3.00	539,829.35	6,988,292.99	72.01
NORMEG	M12-1813	137.00	140.00	911	3.16	3.16	3.20	3.00	539,829.35	6,988,292.99	72.01
NORMEG	M12-1813	159.00	162.00	910	0.63	0.63	3.21	3.00	539,829.35	6,988,292.99	72.01
NORMEG	M12-1813	233.40	236.30	901	0.78	0.78	3.13	2.90	539,829.35	6,988,292.99	72.01
NORMEG	M12-1814	152.00	154.60	920	0.36	0.36	2.78	2.60	540,129.20	6,988,369.81	65.27
NORMEG	M12-1814	172.00	175.00	909	1.00	1.00	3.21	3.00	540,129.20	6,988,369.81	65.27
NORMEG	M12-1814	239.00	242.00	910	2.46	2.46	3.26	3.00	540,129.20	6,988,369.81	65.27
NORMEG	M12-1817	349.50	353.30	909	1.05	1.05	4.12	3.80	540,635.09	6,988,521.43	70.56
NORMEG	M12-1817	476.30	479.30	902	0.72	0.72	3.31	3.00	540,635.09	6,988,521.43	70.56
NORMEG	M12-1818	41.00	44.00	920	4.35	4.35	3.16	3.00	540,009.21	6,988,238.26	66.58
NORMEG	M12-1821	71.00	74.00	920	4.67	4.67	3.30	3.00	540,129.29	6,988,276.14	64.50
NORMEG	M12-1821	84.00	87.00	909	1.25	1.25	3.31	3.00	540,129.29	6,988,276.14	64.50
NORMEG	M12-1821	139.20	141.80	910	5.83	5.83	2.89	2.60	540,129.29	6,988,276.14	64.50
NORMEG	M12-1822	207.00	210.00	909	0.21	0.21	3.27	3.00	540,429.37	6,988,372.23	66.50
NORMEG	M12-1822	254.40	257.60	910	0.37	0.37	3.51	3.20	540,429.37	6,988,372.23	66.50
NORMEG	M12-1822	317.00	320.00	902	0.36	0.36	3.31	3.00	540,429.37	6,988,372.23	66.50
NORMEG	M12-1822	344.00	347.00	901	0.03	0.03	3.32	3.00	540,429.37	6,988,372.23	66.50
NORMEG	M12-1823	285.00	288.00	920	0.60	0.60	3.11	3.00	538,800.02	6,988,457.94	65.94
NORMEG	M12-1823	313.50	316.70	907	6.31	6.31	3.35	3.20	538,800.02	6,988,457.94	65.94
NORMEG	M12-1826	124.00	127.00	909	0.92	0.92	3.21	3.00	540,310.25	6,988,288.89	66.66
NORMEG	M12-1826	278.30	281.30	901	4.45	4.45	3.29	3.00	540,310.25	6,988,288.89	66.66
NORMEG	M12-1828	359.70	362.80	930	0.23	0.23	3.12	3.10	539,291.78	6,988,563.55	68.87
NORMEG	M12-1828	424.10	427.00	906	0.03	0.03	3.00	2.90	539,291.78	6,988,563.55	68.87
NORMEG	M12-1828	480.90	484.30	902	0.37	0.37	3.56	3.40	539,291.78	6,988,563.55	68.87
NORMEG	M12-1831	464.80	468.00	920	0.70	0.70	3.30	3.20	538,804.93	6,988,599.62	65.65
NORMEG	M12-1834	169.10	173.00	909	0.74	0.74	3.50	3.90	540,611.22	6,988,306.17	68.18
NORMEG	M12-1834	318.60	322.50	902	0.77	0.77	3.70	3.90	540,611.22	6,988,306.17	68.18
NORMEG	M12-1834	366.50	370.10	901	5.86	5.86	3.47	3.60	540,611.22	6,988,306.17	68.18
NORMEG	M12-1835	267.40	271.00	907	0.05	0.05	3.65	3.60	539,104.12	6,988,397.23	70.23
NORMEG	M12-1840	136.00	139.00	930	0.60	0.60	2.94	3.00	539,208.11	6,988,342.04	71.96
NORMEG	M12-1840	163.80	171.00	920	2.44	2.44	7.12	7.20	539,208.11	6,988,342.04	71.96
NORMEG	M12-1840	181.00	185.00	911	0.15	0.15	3.96	4.00	539,208.11	6,988,342.04	71.96
NORMEG	M12-1840	196.00	199.50	910	14.25	14.25	3.48	3.50	539,208.11	6,988,342.04	71.96
NORMEG	M12-1840	221.00	224.00	906	0.55	0.55	3.01	3.00	539,208.11	6,988,342.04	71.96
NORMEG	M12-1840	245.00	248.00	903	4.78	4.78	3.03	3.00	539,208.11	6,988,342.04	71.96
NORMEG	M12-1840	256.50	260.00	902	0.03	0.03	3.55	3.50	539,208.11	6,988,342.04	71.96
NORMEG	M12-1841	521.40	525.00	920	1.07	1.07	3.38	3.60	539,020.01	6,988,617.04	72.22
NORMEG	M12-1841	532.40	536.00	911	0.51	0.51	3.40	3.60	539,020.01	6,988,617.04	72.22
NORMEG	M12-1841	541.40	544.80	910	2.44	2.44	3.23	3.40	539,020.01	6,988,617.04	72.22
NORMEG	M12-1843	104.00	107.00	909	1.91	1.91	2.72	3.00	540,357.07	6,988,241.23	66.46
NORMEG	M12-1843	147.00	151.00	910	4.22	4.22	3.67	4.00	540,357.07	6,988,241.23	66.46
NORMEG	M12-1843	222.10	225.50	902	4.74	4.74	3.18	3.40	540,357.07	6,988,241.23	66.46
NORMEG	M12-1843	275.90	280.20	901	1.64	1.64	4.09	4.30	540,357.07	6,988,241.23	66.46
NORMEG	M12-1846	486.00	489.80	907	4.79	4.79	3.73	3.80	538,705.04	6,988,585.15	65.02
NORMEG	M12-1852	238.00	241.50	930	1.23	1.23	3.29	3.50	539,198.16	6,988,448.48	76.11
NORMEG	M12-1856	135.40	138.60	988	0.03	0.03	3.41	3.20	539,700.24	6,988,431.00	73.85
NORMEG	M12-1856	146.00	150.00	987	0.86	0.86	4.27	4.00	539,700.24	6,988,431.00	73.85
NORMEG	M12-1856	213.00	216.00	930	1.28	1.28	3.24	3.00	539,700.24	6,988,431.00	73.85
NORMEG	M12-1856	242.00	245.00	911	3.93	3.93	3.25	3.00	539,700.24	6,988,431.00	73.85
NORMEG	M12-1856	254.00	258.00	910	10.90	10.90	4.34	4.00	539,700.24	6,988,431.00	73.85
NORMEG	M12-1856	365.30	368.00	901	0.76	0.76	2.95	2.70	539,700.24	6,988,431.00	73.85
NORMEG	M12-1861	552.00	555.30	911	1.94	1.94	3.09	3.30	538,927.05	6,988,618.94	71.15
NORMEG	M12-1864	274.30	278.00	911	0.40	0.40	3.47	3.70	539,700.27	6,988,431.82	73.83
NORMEG	M12-1864	297.70	301.30	910	1.03	1.03	3.40	3.60	539,700.27	6,988,431.82	73.83
NORMEG	M12-1864	361.40	364.80	902	2.86	2.86	3.27	3.40	539,700.27	6,988,431.82	73.83
NORMEG	M12-1865	157.80	160.80	904	1.00	1.00	3.23	3.00	539,708.06	6,988,283.07	80.16
NORMEG	M12-1865	230.90	234.00	901	3.84	3.84	3.38	3.10	539,708.06	6,988,283.07	80.16
NORMEG	M12-1867	180.40	184.00	988	2.48	2.48	3.52	3.60	538,521.76	6,988,512.85	60.06
NORMEG	M12-1867	305.00	311.80	923	3.14	3.14	6.77	6.80	538,521.76	6,988,512.85	60.06
NORMEG	M12-1868	25.00	28.00	930	16.11	16.11	2.93	3.00	539,587.96	6,988,231.89	73.64
NORMEG	M12-1868	59.10	62.60	911	0.77	0.77	3.46	3.50	539,587.96	6,988,231.89	73.64
NORMEG	M12-1869	137.10	140.50	920	0.03	0.03	3.55	3.40	539,999.92	6,988,336.97	65.53
NORMEG	M12-1870	71.40	75.00	987	0.79	0.79	3.71	3.60	539,768.04	6,988,352.42	72.98
NORMEG	M12-1870	188.20	190.90	911	1.07	1.07	2.88	2.70	539,768.04	6,988,352.42	72.98
NORMEG	M12-1870	208.40	211.40	910	8.27	8.27	3.21	3.00	539,768.04	6,988,352.42	72.98
NORMEG	M12-1870	221.00	224.00	904	1.54	1.54	3.22	3.00	539,768.04	6,988,352.42	72.98
NORMEG	M12-1870	299.40	302.40	901	3.81	3.81	3.27	3.00	539,768.04	6,988,352.42	72.98
NORMEG	M12-1871	280.00	283.00	911	0.03	0.03	3.25	3.00	539,650.01	6,988,461.60	75.97
NORMEG	M12-1871	296.90	299.80	910	0.78	0.78	3.15	2.90	539,650.01	6,988,461.60	75.97
NORMEG	M12-1873	232.00	238.70	930	10.81	10.81	7.02	6.70	539,332.03	6,988,445.65	72.49
NORMEG	M12-1873	246.70	257.20	920	22.52	22.52	11.03	10.50	539,332.03	6,988,445.65	72.49

NORMEG	M12-1873	261.20	267.00	911	1.21	1.21	6.10	5.80	539,332.03	6,988,445.65	72.49
NORMEG	M12-1873	276.00	279.00	910	6.06	6.06	3.16	3.00	539,332.03	6,988,445.65	72.49
NORMEG	M12-1873	294.00	297.00	906	0.10	0.10	3.17	3.00	539,332.03	6,988,445.65	72.49
NORMEG	M12-1873	333.00	336.00	903	1.45	1.45	3.19	3.00	539,332.03	6,988,445.65	72.49
NORMEG	M12-1875	328.50	332.30	920	18.02	18.02	3.56	3.80	538,608.00	6,988,480.65	61.18
NORMEG	M12-1875	359.30	363.00	907	0.34	0.34	3.48	3.70	538,608.00	6,988,480.65	61.18
NORMEG	M12-1876	156.60	159.70	909	2.61	2.61	3.28	3.10	540,250.06	6,988,335.45	66.42
NORMEG	M12-1877	283.00	293.00	911	28.80	30.02	10.83	10.00	539,749.90	6,988,475.00	71.30
NORMEG	M12-1877	306.80	309.60	910	0.80	0.80	3.04	2.80	539,749.90	6,988,475.00	71.30
NORMEG	M12-1877	339.00	342.00	904	0.83	0.83	3.27	3.00	539,749.90	6,988,475.00	71.30
NORMEG	M12-1877	350.90	353.70	902	1.03	1.03	3.05	2.80	539,749.90	6,988,475.00	71.30
NORMEG	M12-1877	408.40	411.40	901	8.43	8.43	3.29	3.00	539,749.90	6,988,475.00	71.30
NORMEG	M12-1880	101.30	104.70	930	0.68	0.68	3.22	3.40	539,149.92	6,988,309.85	67.35
NORMEG	M12-1880	122.30	126.00	920	4.07	4.07	3.54	3.70	539,149.92	6,988,309.85	67.35
NORMEG	M12-1880	177.00	181.20	910	0.08	0.08	4.14	4.20	539,149.92	6,988,309.85	67.35
NORMEG	M12-1880	183.10	186.20	907	2.63	2.63	3.07	3.10	539,149.92	6,988,309.85	67.35
NORMEG	M12-1882	172.00	175.00	930	0.65	0.65	3.14	3.00	539,309.95	6,988,374.41	77.02
NORMEG	M12-1882	180.80	185.30	920	0.19	0.19	4.72	4.50	539,309.95	6,988,374.41	77.02
NORMEG	M12-1882	198.00	202.60	911	0.03	0.03	4.83	4.60	539,309.95	6,988,374.41	77.02
NORMEG	M12-1882	217.40	220.50	910	0.61	0.61	3.27	3.10	539,309.95	6,988,374.41	77.02
NORMEG	M12-1882	222.40	226.00	906	0.57	0.57	3.80	3.60	539,309.95	6,988,374.41	77.02
NORMEG	M12-1882	255.70	258.70	904	1.45	1.45	3.18	3.00	539,309.95	6,988,374.41	77.02
NORMEG	M12-1882	261.00	264.00	903	26.90	72.90	3.18	3.00	539,309.95	6,988,374.41	77.02
NORMEG	M12-1883	231.00	234.00	907	0.13	0.13	3.27	3.00	539,022.00	6,988,393.51	67.16
NORMEG	M12-1884	52.00	55.00	930	5.30	5.30	3.18	3.00	539,310.00	6,988,246.67	72.19
NORMEG	M12-1884	65.00	68.60	920	2.36	2.36	3.83	3.60	539,310.00	6,988,246.67	72.19
NORMEG	M12-1884	73.40	77.00	911	1.69	1.69	3.83	3.60	539,310.00	6,988,246.67	72.19
NORMEG	M12-1884	106.00	109.00	906	0.35	0.35	3.20	3.00	539,310.00	6,988,246.67	72.19
NORMEG	M12-1884	117.40	120.80	904	2.68	2.68	3.63	3.40	539,310.00	6,988,246.67	72.19
NORMEG	M12-1884	140.00	142.90	903	2.73	2.73	3.10	2.90	539,310.00	6,988,246.67	72.19
NORMEG	M12-1886	98.70	101.70	988	1.19	1.19	3.18	3.00	539,594.99	6,988,384.22	78.61
NORMEG	M12-1886	174.80	177.50	930	3.13	3.13	2.91	2.70	539,594.99	6,988,384.22	78.61
NORMEG	M12-1886	204.50	207.80	911	0.18	0.18	3.57	3.30	539,594.99	6,988,384.22	78.61
NORMEG	M13-1893	13.00	16.80	925	1.88	1.88	3.87	3.80	538,400.01	6,988,255.32	57.94
NORMEG	M13-1893	18.00	24.00	924	5.27	5.27	6.14	6.00	538,400.01	6,988,255.32	57.94
NORMEG	M13-1893	27.00	35.20	923	17.06	17.06	8.41	8.20	538,400.01	6,988,255.32	57.94
NORMEG	M13-1893	35.50	39.00	922	0.67	0.67	3.59	3.50	538,400.01	6,988,255.32	57.94
NORMEG	M13-1893	47.00	50.00	921	4.26	4.26	3.08	3.00	538,400.01	6,988,255.32	57.94
NORMEG	M13-1893	55.50	60.30	920	3.11	3.11	4.94	4.80	538,400.01	6,988,255.32	57.94
NORMEG	M13-1893	66.00	70.00	911	3.30	3.30	4.12	4.00	538,400.01	6,988,255.32	57.94
NORMEG	M13-1901	18.40	21.60	920	3.86	3.86	3.46	3.20	538,480.13	6,988,210.54	57.97
NORMEG	M13-1901	40.00	43.50	911	1.08	1.08	3.79	3.50	538,480.13	6,988,210.54	57.97
NORMEG	M13-1906	17.80	20.60	925	1.08	1.08	2.86	2.80	538,499.92	6,988,264.69	57.89
NORMEG	M13-1906	33.40	36.90	923	3.96	3.96	3.58	3.50	538,499.92	6,988,264.69	57.89
NORMEG	M13-1906	40.80	43.80	922	3.47	3.47	3.07	3.00	538,499.92	6,988,264.69	57.89
NORMEG	M13-1906	51.00	54.30	921	0.08	0.08	3.39	3.30	538,499.92	6,988,264.69	57.89
NORMEG	M13-1906	73.50	79.40	920	4.56	4.56	6.08	5.90	538,499.92	6,988,264.69	57.89
NORMEG	M13-1906	85.40	88.30	911	29.34	29.34	2.99	2.90	538,499.92	6,988,264.69	57.89
NORMEG	M13-1908	173.10	176.60	920	3.09	3.09	3.67	3.50	538,599.78	6,988,370.02	60.06
NORMEG	M13-1908	186.00	190.00	911	0.96	0.96	4.21	4.00	538,599.78	6,988,370.02	60.06
NORMEG	M13-1909	19.00	22.50	905	0.13	0.13	3.58	3.50	540,360.06	6,988,074.14	64.18
NORMEG	M13-1909	41.50	44.70	902	-	-	3.29	3.20	540,360.06	6,988,074.14	64.18
NORMEG	M13-1909	64.80	68.60	901	0.65	0.65	3.92	3.80	540,360.06	6,988,074.14	64.18
NORMEG	M13-1914	109.10	112.20	909	1.12	1.12	3.30	3.10	540,224.88	6,988,283.87	65.71
NORMEG	M13-1915	29.30	32.30	930	0.12	0.12	3.25	3.00	539,199.58	6,988,240.95	65.82
NORMEG	M13-1915	55.50	58.60	920	0.17	0.17	3.37	3.10	539,199.58	6,988,240.95	65.82
NORMEG	M13-1915	65.90	68.30	911	-	-	2.61	2.40	539,199.58	6,988,240.95	65.82
NORMEG	M13-1915	107.00	110.60	906	0.08	0.08	3.93	3.60	539,199.58	6,988,240.95	65.82
NORMEG	M13-1915	121.00	124.50	904	0.28	0.28	3.83	3.50	539,199.58	6,988,240.95	65.82
NORMEG	M13-1915	138.00	141.60	903	2.34	2.34	3.95	3.60	539,199.58	6,988,240.95	65.82
NORMEG	M13-1915	145.00	148.30	902	0.03	0.03	3.62	3.30	539,199.58	6,988,240.95	65.82
NORMEG	M13-1917	153.00	156.60	920	0.96	0.96	3.89	3.60	540,209.95	6,988,363.95	66.17
NORMEG	M13-1917	173.30	176.20	909	1.13	1.13	3.14	2.90	540,209.95	6,988,363.95	66.17
NORMEG	M13-1918	107.30	110.30	988	1.08	1.08	3.21	3.00	538,575.83	6,988,445.15	60.03
NORMEG	M13-1918	216.30	219.90	923	0.44	0.44	3.91	3.60	538,575.83	6,988,445.15	60.03
NORMEG	M13-1918	237.00	240.00	920	0.84	0.84	3.26	3.00	538,575.83	6,988,445.15	60.03
NORMEG	M13-1918	257.50	260.50	911	13.11	13.11	3.27	3.00	538,575.83	6,988,445.15	60.03
NORMEG	M13-1919	33.40	36.40	930	5.28	5.28	3.23	3.00	539,249.67	6,988,245.34	66.36
NORMEG	M13-1919	61.90	64.60	920	0.15	0.15	2.91	2.70	539,249.67	6,988,245.34	66.36
NORMEG	M13-1919	79.60	82.70	911	1.69	1.69	3.35	3.10	539,249.67	6,988,245.34	66.36
NORMEG	M13-1919	99.30	102.70	906	0.14	0.14	3.68	3.40	539,249.67	6,988,245.34	66.36
NORMEG	M13-1919	117.90	120.20	904	0.98	0.98	2.50	2.30	539,249.67	6,988,245.34	66.36
NORMEG	M13-1919	136.70	141.20	903	2.25	2.25	4.89	4.50	539,249.67	6,988,245.34	66.36
NORMEG	M13-1919	154.60	159.10	902	2.88	2.88	4.89	4.50	539,249.67	6,988,245.34	66.36
NORMEG	M13-1920	117.30	120.10	920	1.20	1.20	2.99	2.80	540,149.50	6,988,334.75	65.35
NORMEG	M13-1920	139.00	142.00	909	0.38	0.38	3.21	3.00	540,149.50	6,988,334.75	65.35
NORMEG	M13-1922	174.80	178.00	902	0.18	0.18	3.49	3.20	540,674.95	6,988,208.66	68.03
NORMEG	M13-1922	202.00	204.80	901	3.51	3.51	3.07	2.80	540,674.95	6,988,208.66	68.03
NORMEG	M13-1923	103.00	106.00	930	0.99	0.99	3.09	3.00	539,274.91	6,988,312.17	72.90
NORMEG	M13-1923	115.40	119.70	920	0.22	0.22	4.45	4.30	539,274.91	6,988,312.17	72.90
NORMEG	M13-1923	136.20	140.60	911	0.17	0.17	4.58	4.40	539,274.91	6,988,312.17	72.90
NORMEG	M13-1923	156.00	160.00	910	0.34	0.34	4.18	4.00	539,274.91	6,988,312.17	72.90
NORMEG	M13-1923	172.50	176.60	906	6.07	6.07	4.30	4.10	539,274.91	6,988,312.17	72.90
NORMEG	M13-1923	189.00	192.00	904	0.08	0.08	3.15	3.00	539,274.91	6,988,312.17	72.90
NORMEG	M13-1923	206.00	209.00	903	1.79	1.79	3.17	3.00	539,274.91	6,988,312.17	72.90
NORMEG	M13-1923	220.40	224.00	902	1.51	1.51	3.81	3.60	539,274.91	6,988,312.17	72.90
NORMEG	M13-1925	269.50	273.30	987	1.30	1.30	3.62	3.80	540,140.21	6,988,528.07	66.47
NORMEG	M13-1930	168.20	171.20	902	0.11	0.11	3.19	3.00	540,855.11	6,988,192.40	67.87
NORMEG	M13-1930	184.50	188.90	901	1.42	1.42	4.70	4.40	540,855.11	6,988,192.40	67.87
NORMEG	M13-1931	207.30	210.30	930	2.72	2.72	3.17	3.00	539,274.55	6,988,427.45	75.35

NORMEG	M13-1931	221.60	226.60	920	5.65	5.65	5.29	5.00	539,274.55	6,988,427.45	75.35
NORMEG	M13-1931	233.20	237.70	911	7.03	7.03	4.76	4.50	539,274.55	6,988,427.45	75.35
NORMEG	M13-1931	248.50	254.20	910	4.35	4.35	6.03	5.70	539,274.55	6,988,427.45	75.35
NORMEG	M13-1931	274.10	277.50	906	0.10	0.10	3.60	3.40	539,274.55	6,988,427.45	75.35
NORMEG	M13-1931	309.00	312.10	903	0.38	0.38	3.29	3.10	539,274.55	6,988,427.45	75.35
NORMEG	M13-1931	322.70	326.40	902	1.59	1.59	3.93	3.70	539,274.55	6,988,427.45	75.35
NORMEG	M13-1936	426.50	429.50	923	0.53	0.53	2.92	3.00	538,589.86	6,988,598.43	62.52
NORMEG	M13-1938	212.00	215.00	902	4.73	4.73	3.13	3.00	540,909.86	6,988,230.90	67.89
NORMEG	M13-1940	366.80	369.80	930	0.03	0.03	2.97	3.00	539,266.17	6,988,554.38	68.53
NORMEG	M13-1940	453.40	456.50	906	11.77	11.77	3.15	3.10	539,266.17	6,988,554.38	68.53
NORMEG	M13-1940	495.00	498.60	902	8.70	8.70	3.70	3.60	539,266.17	6,988,554.38	68.53
NORMEG	M13-1941	181.30	184.30	902	0.85	0.85	3.26	3.00	540,949.90	6,988,204.77	67.89
NORMEG	M13-1942	105.40	109.20	920	-	-	3.85	3.80	538,899.50	6,988,285.74	69.93
NORMEG	M13-1942	124.00	127.00	911	0.21	0.21	3.05	3.00	538,899.50	6,988,285.74	69.93
NORMEG	M13-1942	138.00	142.50	907	4.53	4.53	4.59	4.50	538,899.50	6,988,285.74	69.93
NORMEG	M13-1943	307.50	310.50	920	0.30	0.30	3.08	3.00	539,924.89	6,988,510.67	66.21
NORMEG	M13-1943	349.00	352.00	911	0.92	0.92	3.10	3.00	539,924.89	6,988,510.67	66.21
NORMEG	M13-1945	516.00	519.80	987	0.31	0.31	3.93	3.80	540,149.92	6,988,771.05	65.58
NORMEG	M13-1946	185.50	189.50	909	0.58	0.58	3.64	4.00	540,861.13	6,988,305.32	67.76
NORMEG	M13-1946	309.00	312.10	902	0.42	0.42	2.95	3.10	540,861.13	6,988,305.32	67.76
NORMEG	M13-1947	304.00	307.00	920	1.52	1.52	3.27	3.00	538,739.58	6,988,495.71	65.64
NORMEG	M13-1947	327.00	330.00	907	0.65	0.65	3.28	3.00	538,739.58	6,988,495.71	65.64
NORMEG	M13-1954	355.20	358.60	920	3.21	3.21	3.34	3.40	538,839.87	6,988,495.20	65.48
NORMEG	M13-1954	381.50	385.00	907	-	-	3.47	3.50	538,839.87	6,988,495.20	65.48
NORMEG	M13-1956	422.30	425.30	930	0.18	0.18	2.66	3.00	539,279.65	6,988,570.41	68.03
NORMEG	M13-1956	448.80	452.00	920	0.78	0.78	2.92	3.20	539,279.65	6,988,570.41	68.03
NORMEG	M13-1958	78.30	81.30	930	0.10	0.10	3.09	3.00	539,600.22	6,988,290.03	77.78
NORMEG	M13-1958	113.30	117.00	911	2.87	2.87	3.83	3.70	539,600.22	6,988,290.03	77.78
NORMEG	M13-1963	288.40	291.80	911	0.39	0.39	3.65	3.40	539,800.03	6,988,473.27	69.58
NORMEG	M13-1963	313.40	317.00	910	0.24	0.24	3.87	3.60	539,800.03	6,988,473.27	69.58
NORMEG	M13-1963	331.40	334.50	904	25.66	25.66	3.34	3.10	539,800.03	6,988,473.27	69.58
NORMEG	M13-1963	343.00	346.20	902	1.43	1.43	3.45	3.20	539,800.03	6,988,473.27	69.58
NORMEG	M13-1966	280.50	284.00	920	0.77	0.77	3.72	3.50	538,864.90	6,988,470.26	65.47
NORMEG	M13-1966	301.00	305.00	911	1.29	1.29	4.26	4.00	538,864.90	6,988,470.26	65.47
NORMEG	M13-1966	309.00	312.00	910	15.87	15.87	3.20	3.00	538,864.90	6,988,470.26	65.47
NORMEG	M13-1966	314.00	317.00	907	1.45	1.45	3.20	3.00	538,864.90	6,988,470.26	65.47
NORMEG	M13-1969	58.00	61.60	920	0.90	0.90	3.74	3.60	538,268.09	6,988,263.31	57.82
NORMEG	M13-1972	305.00	310.20	911	2.30	2.30	5.40	5.20	539,749.70	6,988,490.35	70.71
NORMEG	M13-1972	330.30	333.30	910	0.60	0.60	3.13	3.00	539,749.70	6,988,490.35	70.71
NORMEG	M13-1972	368.40	371.00	904	0.36	0.36	2.73	2.60	539,749.70	6,988,490.35	70.71
NORMEG	M13-1972	383.00	386.00	902	6.27	6.27	3.16	3.00	539,749.70	6,988,490.35	70.71
NORMEG	M13-1979	65.40	68.70	930	3.21	3.21	3.47	3.30	538,357.90	6,988,349.53	58.10
NORMEG	M13-1979	120.00	123.00	923	0.03	0.03	3.19	3.00	538,357.90	6,988,349.53	58.10
NORMEG	M13-1984	61.00	64.00	930	0.03	0.03	3.17	3.00	538,380.97	6,988,334.70	58.16
NORMEG	M13-1984	82.40	85.60	925	0.37	0.37	3.40	3.20	538,380.97	6,988,334.70	58.16
NORMEG	M13-1984	95.00	97.80	924	0.29	0.29	2.98	2.80	538,380.97	6,988,334.70	58.16
NORMEG	M13-1984	106.00	109.60	923	0.59	0.59	3.84	3.60	538,380.97	6,988,334.70	58.16
NORMEG	M13-1984	118.00	120.80	921	3.96	3.96	2.99	2.80	538,380.97	6,988,334.70	58.16
NORMEG	M13-1984	136.40	138.00	911	-	-	1.71	1.60	538,380.97	6,988,334.70	58.16
NORMEG	M13-1985	413.00	417.00	920	0.27	0.27	3.88	4.00	538,969.80	6,988,547.31	70.57
NORMEG	M13-1985	423.00	426.60	911	5.37	5.37	3.51	3.60	538,969.80	6,988,547.31	70.57
NORMEG	M13-1985	428.00	431.80	910	0.49	0.49	3.71	3.80	538,969.80	6,988,547.31	70.57
NORMEG	M13-1988	126.20	128.90	911	2.08	2.08	2.94	2.70	538,330.01	6,988,326.47	57.93
NORMEG	M13-1993	55.60	58.80	925	3.02	3.02	3.42	3.20	538,274.84	6,988,299.11	57.98
NORMEG	M13-1993	94.40	97.50	920	39.89	54.57	3.32	3.10	538,274.84	6,988,299.11	57.98
NORMEG	M13-1996	22.00	25.60	925	0.05	0.05	3.81	3.60	538,299.91	6,988,266.49	57.97
NORMEG	M13-1996	62.20	65.20	920	0.11	0.11	3.16	3.00	538,299.91	6,988,266.49	57.97
NORMEG	M13-1996	75.30	78.00	911	0.12	0.12	2.85	2.70	538,299.91	6,988,266.49	57.97
NORMEG	M13-1998	20.20	23.30	925	32.72	32.72	3.26	3.10	538,324.86	6,988,261.67	57.96
NORMEG	M13-1998	43.30	47.00	921	0.23	0.23	3.90	3.70	538,324.86	6,988,261.67	57.96
NORMEG	M13-1998	56.40	59.80	920	1.57	1.57	3.59	3.40	538,324.86	6,988,261.67	57.96
NORMEG	M13-1998	70.90	74.30	911	0.06	0.06	3.59	3.40	538,324.86	6,988,261.67	57.96
NORMEG	M13-2003	48.80	51.80	930	0.17	0.17	3.17	3.00	538,428.88	6,988,324.93	58.12
NORMEG	M13-2003	66.00	69.20	925	3.68	3.68	3.39	3.20	538,428.88	6,988,324.93	58.12
NORMEG	M13-2003	78.90	82.00	924	0.03	0.03	3.29	3.10	538,428.88	6,988,324.93	58.12
NORMEG	M13-2003	89.00	92.50	923	0.33	0.33	3.72	3.50	538,428.88	6,988,324.93	58.12
NORMEG	M13-2003	101.30	104.60	922	0.52	0.52	3.51	3.30	538,428.88	6,988,324.93	58.12
NORMEG	M13-2003	116.30	119.60	921	1.83	1.83	3.51	3.30	538,428.88	6,988,324.93	58.12
NORMEG	M13-2003	126.70	129.90	920	1.28	1.28	3.41	3.20	538,428.88	6,988,324.93	58.12
NORMEG	M13-2005	97.30	100.30	907	0.16	0.16	3.22	3.00	538,781.93	6,988,253.60	61.50
NORMEG	M13-2006	357.70	361.00	920	0.35	0.35	3.39	3.30	539,024.62	6,988,522.43	71.55
NORMEG	M13-2006	379.40	382.30	910	3.78	3.78	2.99	2.90	539,024.62	6,988,522.43	71.55
NORMEG	M13-2006	399.00	402.00	907	3.21	3.21	3.12	3.00	539,024.62	6,988,522.43	71.55
NORMEG	M13-2008	13.50	18.00	930	2.38	2.38	4.61	4.50	538,447.90	6,988,284.51	58.05
NORMEG	M13-2008	37.30	41.60	925	0.56	0.56	4.42	4.30	538,447.90	6,988,284.51	58.05
NORMEG	M13-2008	44.40	50.60	924	0.86	0.86	6.37	6.20	538,447.90	6,988,284.51	58.05
NORMEG	M13-2008	56.60	60.00	923	0.99	0.99	3.50	3.40	538,447.90	6,988,284.51	58.05
NORMEG	M13-2008	63.00	67.00	922	1.70	1.70	4.11	4.00	538,447.90	6,988,284.51	58.05
NORMEG	M13-2008	76.40	79.40	921	1.07	1.07	3.09	3.00	538,447.90	6,988,284.51	58.05
NORMEG	M13-2008	91.50	99.50	920	4.12	4.12	8.25	8.00	538,447.90	6,988,284.51	58.05
NORMEG	M13-2008	107.80	110.60	911	2.55	2.55	2.89	2.80	538,447.90	6,988,284.51	58.05
NORMEG	M13-2010	39.00	43.40	907	0.22	0.22	4.67	4.40	538,807.72	6,988,197.83	59.87
NORMEG	M13-2012	37.60	41.30	911	0.10	0.10	3.94	3.70	538,878.83	6,988,207.00	64.67
NORMEG	M13-2012	43.40	46.10	910	1.91	1.91	2.88	2.70	538,878.83	6,988,207.00	64.67
NORMEG	M13-2012	54.50	59.60	907	22.00	22.00	5.44	5.10	538,878.83	6,988,207.00	64.67
NORMEG	M13-2014	14.50	22.10	924	6.26	6.26	8.00	7.60	538,422.98	6,988,257.40	58.02
NORMEG	M13-2014	24.10	31.10	923	4.98	4.98	7.37	7.00	538,422.98	6,988,257.40	58.02
NORMEG	M13-2014	33.00	36.40	922	2.92	2.92	3.58	3.40	538,422.98	6,988,257.40	58.02
NORMEG	M13-2014	43.00	50.00	921	9.32	9.32	7.38	7.00	538,422.98	6,988,257.40	58.02
NORMEG	M13-2014	65.00	71.00	920	5.94	5.94	6.34	6.00	538,422.98	6,988,257.40	58.02

NORMEG	M13-2014	73.00	77.00	911	5.77	5.77	4.23	4.00	538,422.98	6,988,257.40	58.02
NORMEG	M13-2017	53.50	58.00	920	0.13	0.13	4.78	4.50	538,858.29	6,988,240.81	66.19
NORMEG	M13-2017	67.80	71.60	911	0.03	0.03	4.05	3.80	538,858.29	6,988,240.81	66.19
NORMEG	M13-2017	78.50	82.30	907	0.18	0.18	4.05	3.80	538,858.29	6,988,240.81	66.19
NORMEG	M13-2018	74.40	78.00	920	1.01	1.01	3.87	3.60	538,831.83	6,988,263.57	65.48
NORMEG	M13-2018	107.70	111.00	907	-	-	3.56	3.30	538,831.83	6,988,263.57	65.48
NORMEG	M13-2019	15.00	17.40	925	0.94	0.94	2.52	2.40	538,360.81	6,988,251.97	57.91
NORMEG	M13-2019	20.00	23.00	924	4.11	4.11	3.15	3.00	538,360.81	6,988,251.97	57.91
NORMEG	M13-2019	28.00	31.50	923	1.80	1.80	3.67	3.50	538,360.81	6,988,251.97	57.91
NORMEG	M13-2019	34.50	37.50	921	40.25	40.25	3.15	3.00	538,360.81	6,988,251.97	57.91
NORMEG	M13-2019	41.50	47.00	920	17.45	17.45	5.77	5.50	538,360.81	6,988,251.97	57.91
NORMEG	M13-2019	68.00	71.40	911	4.11	4.11	3.57	3.40	538,360.81	6,988,251.97	57.91
NORMEG	M13-2023	80.40	84.50	920	0.38	0.38	4.41	4.10	538,878.85	6,988,266.33	68.75
NORMEG	M13-2023	95.00	97.70	911	0.20	0.20	2.91	2.70	538,878.85	6,988,266.33	68.75
NORMEG	M13-2023	108.10	111.00	907	0.95	0.95	3.13	2.90	538,878.85	6,988,266.33	68.75
NORMEG	M13-2026	56.80	60.00	925	0.03	0.03	3.40	3.20	538,330.02	6,988,296.38	58.02
NORMEG	M13-2026	91.50	94.50	920	0.03	0.03	3.19	3.00	538,330.02	6,988,296.38	58.02
NORMEG	M13-2026	98.00	101.00	911	0.54	0.54	3.20	3.00	538,330.02	6,988,296.38	58.02
NORMEG	M13-2027	508.40	511.00	988	1.51	1.51	2.67	2.60	538,960.02	6,988,777.86	64.02
NORMEG	M13-2027	520.90	522.00	987	0.03	0.03	1.13	1.10	538,960.02	6,988,777.86	64.02
NORMEG	M13-2028	84.00	87.30	911	1.15	1.15	3.52	3.30	538,916.90	6,988,254.91	70.12
NORMEG	M13-2028	92.90	96.00	910	0.09	0.09	3.31	3.10	538,916.90	6,988,254.91	70.12
NORMEG	M13-2028	98.40	101.60	907	1.26	1.26	3.42	3.20	538,916.90	6,988,254.91	70.12
NORMEG	M13-2030A	454.00	457.30	920	0.56	0.56	3.08	3.30	539,114.94	6,988,561.59	72.39
NORMEG	M13-2030A	475.90	478.90	910	2.90	2.90	2.80	3.00	539,114.94	6,988,561.59	72.39
NORMEG	M13-2030A	483.20	486.30	907	0.54	0.54	2.90	3.10	539,114.94	6,988,561.59	72.39
NORMEG	M13-2031	59.30	62.30	911	0.03	0.03	3.22	3.00	538,936.87	6,988,229.41	70.06
NORMEG	M13-2031	66.90	69.90	910	10.37	10.37	3.22	3.00	538,936.87	6,988,229.41	70.06
NORMEG	M13-2031	71.90	75.00	907	0.03	0.03	3.33	3.10	538,936.87	6,988,229.41	70.06
NORMEG	M13-2033	22.00	24.90	930	0.12	0.12	3.07	2.90	538,385.89	6,988,288.96	58.07
NORMEG	M13-2033	41.30	45.00	925	0.03	0.03	3.93	3.70	538,385.89	6,988,288.96	58.07
NORMEG	M13-2033	52.00	55.70	924	0.07	0.07	3.94	3.70	538,385.89	6,988,288.96	58.07
NORMEG	M13-2033	64.00	67.00	923	5.36	5.36	3.20	3.00	538,385.89	6,988,288.96	58.07
NORMEG	M13-2033	72.70	75.60	921	0.76	0.76	3.09	2.90	538,385.89	6,988,288.96	58.07
NORMEG	M13-2033	84.00	87.00	920	8.72	8.72	3.20	3.00	538,385.89	6,988,288.96	58.07
NORMEG	M13-2033	95.00	97.60	911	0.28	0.28	2.78	2.60	538,385.89	6,988,288.96	58.07
NORMEG	M13-2034	30.70	33.80	925	0.25	0.25	3.32	3.10	538,526.25	6,988,283.70	57.98
NORMEG	M13-2034	48.20	51.60	923	8.75	8.75	3.66	3.40	538,526.25	6,988,283.70	57.98
NORMEG	M13-2034	57.80	60.80	922	0.03	0.03	3.23	3.00	538,526.25	6,988,283.70	57.98
NORMEG	M13-2034	79.40	83.00	920	4.21	4.21	3.88	3.60	538,526.25	6,988,283.70	57.98
NORMEG	M13-2034	92.30	95.10	911	1.11	1.11	3.02	2.80	538,526.25	6,988,283.70	57.98
NORMEG	M13-2037	44.20	47.20	925	1.35	1.35	3.08	3.00	538,489.89	6,988,296.89	57.95
NORMEG	M13-2037	63.70	66.70	923	0.31	0.31	3.12	3.00	538,489.89	6,988,296.89	57.95
NORMEG	M13-2037	71.70	74.90	922	3.20	3.20	3.34	3.20	538,489.89	6,988,296.89	57.95
NORMEG	M13-2037	84.20	87.20	921	1.22	1.22	3.14	3.00	538,489.89	6,988,296.89	57.95
NORMEG	M13-2037	104.60	107.80	920	8.56	8.56	3.36	3.20	538,489.89	6,988,296.89	57.95
NORMEG	M13-2037	114.40	117.40	911	3.36	3.36	3.15	3.00	538,489.89	6,988,296.89	57.95
NORMEG	M13-2039	26.90	30.10	925	0.33	0.33	3.38	3.20	538,550.28	6,988,278.44	57.98
NORMEG	M13-2039	44.20	47.40	923	1.01	1.01	3.39	3.20	538,550.28	6,988,278.44	57.98
NORMEG	M13-2039	51.10	54.80	922	2.63	2.63	3.92	3.70	538,550.28	6,988,278.44	57.98
NORMEG	M13-2039	76.30	79.40	920	0.33	0.33	3.29	3.10	538,550.28	6,988,278.44	57.98
NORMEG	M13-2039	94.80	98.30	911	2.27	2.27	3.72	3.50	538,550.28	6,988,278.44	57.98
NORMEG	M13-2041	20.10	23.10	923	0.91	0.91	2.75	3.00	538,573.95	6,988,256.98	57.48
NORMEG	M13-2041	37.70	41.90	922	7.89	7.89	3.88	4.20	538,573.95	6,988,256.98	57.48
NORMEG	M13-2041	59.70	63.90	920	0.83	0.83	3.93	4.20	538,573.95	6,988,256.98	57.48
NORMEG	M13-2041	81.80	86.40	911	5.41	5.41	4.36	4.60	538,573.95	6,988,256.98	57.48
NORMEG	M13-2043	71.40	74.60	925	1.12	1.12	3.42	3.20	538,523.77	6,988,324.63	58.64
NORMEG	M13-2043	91.70	95.00	923	15.69	15.69	3.53	3.30	538,523.77	6,988,324.63	58.64
NORMEG	M13-2043	98.80	101.80	922	0.08	0.08	3.22	3.00	538,523.77	6,988,324.63	58.64
NORMEG	M13-2043	119.60	123.30	920	0.80	0.80	3.97	3.70	538,523.77	6,988,324.63	58.64
NORMEG	M13-2043	133.60	136.80	911	0.72	0.72	3.45	3.20	538,523.77	6,988,324.63	58.64
NORMEG	M13-2046	51.30	55.70	922	3.67	3.67	4.78	4.40	538,597.96	6,988,275.89	58.30
NORMEG	M13-2046	72.60	75.60	920	0.24	0.24	3.27	3.00	538,597.96	6,988,275.89	58.30
NORMEG	M13-2047	85.40	88.70	925	3.57	3.57	3.53	3.30	538,499.67	6,988,343.41	59.09
NORMEG	M13-2047	103.50	106.50	923	0.88	0.88	3.22	3.00	538,499.67	6,988,343.41	59.09
NORMEG	M13-2047	114.20	117.20	922	1.00	1.00	3.23	3.00	538,499.67	6,988,343.41	59.09
NORMEG	M13-2047	146.50	153.20	920	16.13	16.13	7.24	6.70	538,499.67	6,988,343.41	59.09
NORMEG	M13-2047	153.20	156.20	911	2.51	2.51	3.24	3.00	538,499.67	6,988,343.41	59.09
NORMEG	M13-2049	72.40	76.00	922	1.33	1.33	3.76	3.60	538,598.71	6,988,292.99	58.18
NORMEG	M13-2049	93.00	96.00	920	0.03	0.03	3.14	3.00	538,598.71	6,988,292.99	58.18
NORMEG	M13-2050	555.00	558.00	988	0.16	0.16	3.07	3.00	538,959.91	6,988,822.04	63.24
NORMEG	M13-2050	565.50	568.50	987	1.47	1.47	3.08	3.00	538,959.91	6,988,822.04	63.24
NORMEG	M13-2054	86.40	90.00	925	0.63	0.63	3.82	3.60	538,479.82	6,988,345.01	58.72
NORMEG	M13-2054	104.80	107.60	923	2.08	2.08	2.98	2.80	538,479.82	6,988,345.01	58.72
NORMEG	M13-2054	113.90	117.00	922	0.97	0.97	3.30	3.10	538,479.82	6,988,345.01	58.72
NORMEG	M13-2054	143.20	146.30	920	4.02	4.02	3.32	3.10	538,479.82	6,988,345.01	58.72
NORMEG	M13-2054	157.50	160.70	911	0.38	0.38	3.43	3.20	538,479.82	6,988,345.01	58.72
NORMEG	M13-2061	67.00	70.00	925	1.46	1.46	3.20	3.00	538,548.59	6,988,322.95	59.22
NORMEG	M13-2061	90.00	93.00	923	0.03	0.03	3.22	3.00	538,548.59	6,988,322.95	59.22
NORMEG	M13-2061	96.00	99.00	922	3.06	3.06	3.22	3.00	538,548.59	6,988,322.95	59.22
NORMEG	M13-2061	122.00	125.00	920	2.14	2.14	3.24	3.00	538,548.59	6,988,322.95	59.22
NORMEG	M13-2061	141.00	144.60	911	0.12	0.12	3.89	3.60	538,548.59	6,988,322.95	59.22
NORMEG	M13-2064	102.00	104.70	930	0.06	0.06	2.92	2.70	538,406.18	6,988,382.35	59.47
NORMEG	M13-2064	148.00	151.00	923	1.72	1.72	3.27	3.00	538,406.18	6,988,382.35	59.47
NORMEG	M13-2064	164.90	168.90	921	3.53	3.53	4.37	4.00	538,406.18	6,988,382.35	59.47
NORMEG	M13-2078	317.40	321.00	930	-	-	3.58	3.60	539,400.12	6,988,513.16	75.71
NORMEG	M13-2078	329.20	332.40	920	0.72	0.72	3.20	3.20	539,400.12	6,988,513.16	75.71
NORMEG	M13-2078	341.40	344.70	911	1.59	1.59	3.31	3.30	539,400.12	6,988,513.16	75.71
NORMEG	M13-2078	349.50	352.50	910	3.22	3.22	3.02	3.00	539,400.12	6,988,513.16	75.71
NORMEG	M13-2078	383.00	386.30	906	0.23	0.23	3.36	3.30	539,400.12	6,988,513.16	75.71

NORMEG	M13-2098	10.50	12.80	911	0.03	0.03	2.37	2.30	539,166.53	6,988,168.01	65.43
NORMEG	M13-2098	26.10	29.40	907	0.18	0.18	3.41	3.30	539,166.53	6,988,168.01	65.43
NORMEG	M13-2098	42.80	46.00	906	0.88	0.88	3.32	3.20	539,166.53	6,988,168.01	65.43
NORMEG	M13-2098	54.80	58.50	904	0.08	0.08	3.85	3.70	539,166.53	6,988,168.01	65.43
NORMEG	M13-2098	77.00	80.00	903	0.56	0.56	3.13	3.00	539,166.53	6,988,168.01	65.43
NORMEG	M13-2101	45.70	48.20	906	4.71	4.71	2.67	2.50	539,209.95	6,988,172.04	65.60
NORMEG	M13-2101	56.40	59.50	904	0.20	0.20	3.32	3.10	539,209.95	6,988,172.04	65.60
NORMEG	M13-2101	79.00	82.00	903	2.02	2.02	3.22	3.00	539,209.95	6,988,172.04	65.60
NORMEG	M13-2103	24.80	27.80	906	0.11	0.11	3.09	3.00	539,263.03	6,988,160.23	65.70
NORMEG	M13-2103	43.50	47.20	904	0.34	0.34	3.82	3.70	539,263.03	6,988,160.23	65.70
NORMEG	M13-2103	62.00	65.00	903	1.87	1.87	3.11	3.00	539,263.03	6,988,160.23	65.70
NORMEG	M13-2103	74.30	77.30	902	1.63	1.63	3.11	3.00	539,263.03	6,988,160.23	65.70
NORMEG	M13-2105	16.00	19.00	902	2.61	2.61	3.18	3.00	539,276.89	6,988,100.03	64.34
NORMEG	M13-2109	16.80	22.20	907	0.03	0.03	4.09	5.40	539,050.04	6,988,149.62	71.79
NORMEG	M13-2112	256.30	259.30	911	2.48	2.48	3.02	3.00	539,599.89	6,988,422.69	78.08
NORMEG	M13-2113	18.00	19.70	907	3.78	3.78	1.69	1.70	539,103.05	6,988,146.01	72.80
NORMEG	M13-2113	25.00	28.00	906	4.35	4.35	2.98	3.00	539,103.05	6,988,146.01	72.80
NORMEG	M13-2117	210.40	214.40	909	14.81	14.81	4.20	4.00	540,824.95	6,988,349.81	67.73
NORMEG	M13-2117	314.00	317.00	902	17.07	17.07	3.25	3.00	540,824.95	6,988,349.81	67.73
NORMEG	M13-2117	337.00	340.00	901	3.13	3.13	3.26	3.00	540,824.95	6,988,349.81	67.73
NORMEG	M13-2120	22.70	24.40	903	3.01	3.01	1.78	1.70	539,165.05	6,988,104.99	73.89
NORMEG	M13-2125	411.00	414.00	930	0.53	0.53	3.22	3.00	539,465.75	6,988,645.88	77.34
NORMEG	M13-2125	445.50	448.40	911	7.85	7.85	3.14	2.90	539,465.75	6,988,645.88	77.34
NORMEG	M13-2125	460.90	463.60	906	5.31	5.31	2.93	2.70	539,465.75	6,988,645.88	77.34
NORMEG	M13-2126	289.50	292.50	920	9.00	9.00	3.18	3.00	539,861.85	6,988,499.59	68.12
NORMEG	M13-2126	330.80	333.80	911	4.87	4.87	3.20	3.00	539,861.85	6,988,499.59	68.12
NORMEG	M13-2187	493.10	495.70	987	17.00	17.00	2.58	2.60	539,790.15	6,988,739.38	67.11
NORMEG	M14-2221	13.40	16.60	906	1.45	1.45	3.33	3.20	539,325.06	6,988,143.46	65.91
NORMEG	M14-2221	20.00	25.00	904	15.33	15.33	5.21	5.00	539,325.06	6,988,143.46	65.91
NORMEG	M14-2221	40.00	43.50	903	2.72	2.72	3.67	3.50	539,325.06	6,988,143.46	65.91
NORMEG	M14-2223	18.15	21.00	904	0.64	0.64	3.01	2.85	539,289.82	6,988,133.23	64.64
NORMEG	M14-2223	34.80	38.40	903	0.23	0.23	3.82	3.60	539,289.82	6,988,133.23	64.64
NORMEG	M14-2223	41.30	44.40	902	0.72	0.72	3.29	3.10	539,289.82	6,988,133.23	64.64
NORMEG	M14-2225	25.00	28.90	904	0.02	0.02	3.54	3.90	539,234.64	6,988,133.52	64.17
NORMEG	M14-2225	40.90	44.40	903	0.79	0.79	3.20	3.50	539,234.64	6,988,133.52	64.17
NORMEG	M14-2226	12.00	12.60	906	0.00	0.00	0.63	0.60	539,194.84	6,988,132.82	66.22
NORMEG	M14-2226	21.80	24.80	904	0.08	0.08	3.17	3.00	539,194.84	6,988,132.82	66.22
NORMEG	M14-2226	42.30	45.50	903	1.79	1.79	3.40	3.20	539,194.84	6,988,132.82	66.22
NORMEG	M14-2227A	23.20	26.10	920	4.24	4.24	3.00	2.90	539,245.76	6,988,195.00	65.60
NORMEG	M14-2227A	30.00	33.80	911	0.11	0.11	3.95	3.80	539,245.76	6,988,195.00	65.60
NORMEG	M14-2227A	58.00	61.00	906	0.12	0.12	3.14	3.00	539,245.76	6,988,195.00	65.60
NORMEG	M14-2227A	73.60	77.00	904	2.55	2.55	3.57	3.40	539,245.76	6,988,195.00	65.60
NORMEG	M14-2227A	99.50	102.50	903	1.13	1.13	3.16	3.00	539,245.76	6,988,195.00	65.60
NORMEG	M14-2227A	112.30	116.00	902	0.09	0.09	3.90	3.70	539,245.76	6,988,195.00	65.60
NORMEG	M14-2231	22.30	25.70	920	-	-	3.47	3.40	539,213.71	6,988,200.21	65.49
NORMEG	M14-2231	35.10	38.80	911	-	-	3.79	3.70	539,213.71	6,988,200.21	65.49
NORMEG	M14-2231	74.50	77.50	906	0.13	0.13	3.11	3.00	539,213.71	6,988,200.21	65.49
NORMEG	M14-2231	81.30	84.50	904	0.79	0.79	3.32	3.20	539,213.71	6,988,200.21	65.49
NORMEG	M14-2231	98.30	101.30	903	0.36	0.36	3.13	3.00	539,213.71	6,988,200.21	65.49
NORMEG	M14-2231	113.30	116.80	902	0.86	0.86	3.66	3.50	539,213.71	6,988,200.21	65.49
NORMEG	M14-2233	33.80	37.50	930	0.65	0.65	3.82	3.70	539,162.78	6,988,242.05	65.78
NORMEG	M14-2233	56.50	60.10	920	0.27	0.27	3.73	3.60	539,162.78	6,988,242.05	65.78
NORMEG	M14-2233	72.60	76.40	911	5.12	5.12	3.94	3.80	539,162.78	6,988,242.05	65.78
NORMEG	M14-2233	90.50	93.60	910	0.93	0.93	3.22	3.10	539,162.78	6,988,242.05	65.78
NORMEG	M14-2233	94.10	97.80	907	1.36	1.36	3.85	3.70	539,162.78	6,988,242.05	65.78
NORMEG	M14-2233	116.90	120.30	906	3.96	3.96	3.55	3.40	539,162.78	6,988,242.05	65.78
NORMEG	M14-2233	128.30	131.00	904	0.13	0.13	2.83	2.70	539,162.78	6,988,242.05	65.78
NORMEG	M14-2233	142.00	145.00	903	1.17	1.17	3.15	3.00	539,162.78	6,988,242.05	65.78
NORMEG	M14-2233	154.50	157.70	902	0.10	0.10	3.37	3.20	539,162.78	6,988,242.05	65.78
NORMEG	M14-2235	20.40	23.05	920	0.02	0.02	2.77	2.65	539,163.75	6,988,197.33	65.76
NORMEG	M14-2235	33.00	36.10	911	0.89	0.89	3.25	3.10	539,163.75	6,988,197.33	65.76
NORMEG	M14-2235	52.50	55.90	907	0.14	0.14	3.58	3.40	539,163.75	6,988,197.33	65.76
NORMEG	M14-2235	74.80	78.60	906	0.15	0.15	4.02	3.80	539,163.75	6,988,197.33	65.76
NORMEG	M14-2235	84.00	87.00	904	0.19	0.19	3.17	3.00	539,163.75	6,988,197.33	65.76
NORMEG	M14-2235	105.10	108.50	903	2.42	2.42	3.60	3.40	539,163.75	6,988,197.33	65.76
NORMEG	M14-2235	111.00	114.00	902	0.75	0.75	3.18	3.00	539,163.75	6,988,197.33	65.76
NORMEG	M14-2237	84.20	87.30	930	4.51	4.51	3.26	3.10	539,164.10	6,988,293.22	66.94
NORMEG	M14-2237	108.20	111.40	920	20.72	20.72	3.42	3.20	539,164.10	6,988,293.22	66.94
NORMEG	M14-2237	132.80	135.70	911	0.05	0.05	3.13	2.90	539,164.10	6,988,293.22	66.94
NORMEG	M14-2237	138.30	141.20	910	0.66	0.66	3.14	2.90	539,164.10	6,988,293.22	66.94
NORMEG	M14-2237	142.90	146.30	907	0.10	0.10	3.69	3.40	539,164.10	6,988,293.22	66.94
NORMEG	M14-2237	156.10	159.00	906	7.27	7.27	3.15	2.90	539,164.10	6,988,293.22	66.94
NORMEG	M14-2237	185.20	188.20	903	0.17	0.17	3.27	3.00	539,164.10	6,988,293.22	66.94
NORMEG	M14-2237	192.80	195.80	902	2.30	2.30	3.27	3.00	539,164.10	6,988,293.22	66.94
NORMEG	M14-2245	59.30	63.00	930	4.60	4.60	3.87	3.70	539,203.18	6,988,264.04	66.63
NORMEG	M14-2245	78.00	81.00	920	0.16	0.16	3.15	3.00	539,203.18	6,988,264.04	66.63
NORMEG	M14-2245	93.90	97.00	911	0.01	0.01	3.27	3.10	539,203.18	6,988,264.04	66.63
NORMEG	M14-2245	105.00	108.00	910	9.31	9.31	3.17	3.00	539,203.18	6,988,264.04	66.63
NORMEG	M14-2245	129.00	132.00	906	28.30	28.30	3.18	3.00	539,203.18	6,988,264.04	66.63
NORMEG	M14-2245	142.00	145.60	904	1.40	1.40	3.83	3.60	539,203.18	6,988,264.04	66.63
NORMEG	M14-2245	160.00	163.00	903	0.05	0.05	3.20	3.00	539,203.18	6,988,264.04	66.63
NORMEG	M14-2245	167.00	170.00	902	19.01	19.01	3.20	3.00	539,203.18	6,988,264.04	66.63
NORMEG	M14-2247	33.80	36.80	930	7.31	7.31	2.96	3.00	539,244.48	6,988,248.01	66.21
NORMEG	M14-2247	69.00	72.00	920	0.06	0.06	2.98	3.00	539,244.48	6,988,248.01	66.21
NORMEG	M14-2247	85.50	88.50	911	5.17	5.17	3.00	3.00	539,244.48	6,988,248.01	66.21
NORMEG	M14-2247	109.50	113.00	906	0.62	0.62	3.54	3.50	539,244.48	6,988,248.01	66.21
NORMEG	M14-2249	68.30	71.60	930	7.96	7.96	3.43	3.30	539,284.24	6,988,279.81	72.09
NORMEG	M14-2249	85.40	88.30	920	20.87	43.63	3.02	2.90	539,284.24	6,988,279.81	72.09
NORMEG	M14-2249	103.10	106.10	911	0.98	0.98	3.15	3.00	539,284.24	6,988,279.81	72.09
NORMEG	M14-2249	138.00	141.00	906	0.05	0.05	3.17	3.00	539,284.24	6,988,279.81	72.09

NORMEG	M14-2249	159.50	162.40	904	2.73	2.73	3.07	2.90	539,284.24	6,988,279.81	72.09
NORMEG	M14-2249	173.00	176.00	903	0.39	0.39	3.18	3.00	539,284.24	6,988,279.81	72.09
NORMEG	M14-2249	184.80	187.60	902	0.37	0.37	2.97	2.80	539,284.24	6,988,279.81	72.09
NORMEG	M14-2252	31.70	34.80	930	0.44	0.44	3.30	3.10	539,324.12	6,988,225.95	71.41
NORMEG	M14-2252	49.00	52.00	911	1.20	1.20	3.20	3.00	539,324.12	6,988,225.95	71.41
NORMEG	M14-2252	87.40	91.00	906	0.96	0.96	3.87	3.60	539,324.12	6,988,225.95	71.41
NORMEG	M14-2252	97.00	100.00	904	0.29	0.29	3.23	3.00	539,324.12	6,988,225.95	71.41
NORMEG	M14-2252	119.00	122.00	903	0.03	0.03	3.23	3.00	539,324.12	6,988,225.95	71.41
NORMEG	M14-2253	18.90	21.90	930	-	-	3.08	3.00	539,284.19	6,988,223.07	67.70
NORMEG	M14-2253	34.10	37.60	920	0.98	0.98	3.60	3.50	539,284.19	6,988,223.07	67.70
NORMEG	M14-2253	50.90	54.70	911	-	-	3.92	3.80	539,284.19	6,988,223.07	67.70
NORMEG	M14-2253	86.40	90.50	906	0.28	0.28	4.25	4.10	539,284.19	6,988,223.07	67.70
NORMEG	M14-2253	105.40	108.80	904	0.37	0.37	3.53	3.40	539,284.19	6,988,223.07	67.70
NORMEG	M14-2253	124.80	127.40	903	4.91	4.91	2.71	2.60	539,284.19	6,988,223.07	67.70
NORMEG	M14-2253	132.60	135.70	902	0.66	0.66	3.24	3.10	539,284.19	6,988,223.07	67.70
NORMEG	M14-2254	15.20	18.00	921	3.78	3.78	2.96	2.80	538,340.23	6,988,229.54	57.79
NORMEG	M14-2254	21.00	24.60	920	3.60	3.60	3.81	3.60	538,340.23	6,988,229.54	57.79
NORMEG	M14-2254	43.00	46.50	911	4.60	4.60	3.71	3.50	538,340.23	6,988,229.54	57.79
NORMEG	M14-2255	25.50	28.30	920	2.85	2.85	2.92	2.80	539,290.67	6,988,201.84	67.13
NORMEG	M14-2255	29.30	32.00	911	1.20	1.20	2.82	2.70	539,290.67	6,988,201.84	67.13
NORMEG	M14-2255	65.40	68.60	906	0.20	0.20	3.36	3.20	539,290.67	6,988,201.84	67.13
NORMEG	M14-2255	83.30	86.80	904	0.14	0.14	3.69	3.50	539,290.67	6,988,201.84	67.13
NORMEG	M14-2255	105.00	108.00	903	3.48	3.48	3.17	3.00	539,290.67	6,988,201.84	67.13
NORMEG	M14-2255	111.00	114.00	902	0.83	0.83	3.17	3.00	539,290.67	6,988,201.84	67.13
NORMEG	M14-2256	21.00	23.40	920	0.66	0.66	2.53	2.40	538,380.23	6,988,223.16	57.62
NORMEG	M14-2256	30.80	33.70	911	5.30	5.30	3.06	2.90	538,380.23	6,988,223.16	57.62
NORMEG	M14-2257	327.00	330.00	987	0.47	0.47	2.92	3.00	539,910.18	6,988,580.93	66.71
NORMEG	M14-2258	15.80	17.60	921	0.02	0.02	1.89	1.80	538,419.80	6,988,226.08	57.86
NORMEG	M14-2258	27.00	30.40	920	0.24	0.24	3.57	3.40	538,419.80	6,988,226.08	57.86
NORMEG	M14-2258	39.00	42.80	911	0.04	0.04	4.00	3.80	538,419.80	6,988,226.08	57.86
NORMEG	M14-2259	17.80	22.80	904	0.40	0.40	3.56	5.00	539,125.80	6,988,118.86	72.80
NORMEG	M14-2262	15.00	18.00	930	0.57	0.57	3.15	3.00	539,095.13	6,988,222.60	66.05
NORMEG	M14-2262	33.00	36.00	920	0.59	0.59	3.16	3.00	539,095.13	6,988,222.60	66.05
NORMEG	M14-2262	58.00	61.50	910	1.38	1.38	3.70	3.50	539,095.13	6,988,222.60	66.05
NORMEG	M14-2262	83.00	85.90	907	0.25	0.25	3.08	2.90	539,095.13	6,988,222.60	66.05
NORMEG	M14-2263	59.40	62.80	922	1.40	1.40	3.60	3.40	538,619.92	6,988,279.48	58.45
NORMEG	M14-2263	81.00	84.00	920	17.34	17.34	3.19	3.00	538,619.92	6,988,279.48	58.45
NORMEG	M14-2263	131.40	134.50	907	2.50	2.50	3.32	3.10	538,619.92	6,988,279.48	58.45
NORMEG	M14-2265	101.00	104.80	923	0.35	0.35	3.94	3.80	538,575.62	6,988,337.20	59.28
NORMEG	M14-2265	117.10	120.30	922	1.38	1.38	3.34	3.20	538,575.62	6,988,337.20	59.28
NORMEG	M14-2265	142.00	145.00	920	0.03	0.03	3.14	3.00	538,575.62	6,988,337.20	59.28
NORMEG	M14-2265	155.70	159.10	911	0.32	0.32	3.57	3.40	538,575.62	6,988,337.20	59.28
NORMEG	M14-2266	44.00	46.20	988	0.12	0.12	2.28	2.20	538,536.31	6,988,384.88	60.14
NORMEG	M14-2266	154.60	157.90	923	0.69	0.69	3.52	3.30	538,536.31	6,988,384.88	60.14
NORMEG	M14-2266	180.40	184.00	920	1.02	1.02	3.85	3.60	538,536.31	6,988,384.88	60.14
NORMEG	M14-2266	194.80	199.00	911	3.62	3.62	4.49	4.20	538,536.31	6,988,384.88	60.14
NORMEG	M14-2269	45.50	47.90	988	0.08	0.08	2.48	2.40	538,496.81	6,988,386.02	59.58
NORMEG	M14-2269	146.80	150.60	923	0.01	0.01	4.06	3.80	538,496.81	6,988,386.02	59.58
NORMEG	M14-2269	179.90	182.80	920	0.04	0.04	3.13	2.90	538,496.81	6,988,386.02	59.58
NORMEG	M14-2272	239.70	245.00	921	3.38	3.38	5.60	5.30	538,640.00	6,988,443.80	61.02
NORMEG	M14-2272	252.30	256.40	920	0.12	0.12	4.34	4.10	538,640.00	6,988,443.80	61.02
NORMEG	M14-2272	273.60	280.20	911	3.42	3.42	7.00	6.60	538,640.00	6,988,443.80	61.02
NORMEG	M14-2272	288.50	291.90	907	0.03	0.03	3.61	3.40	538,640.00	6,988,443.80	61.02
NORMEG	M14-2296	305.50	309.80	909	0.94	0.94	4.32	4.30	540,885.52	6,988,438.03	67.01
NORMEG	M14-2309	386.90	390.00	930	0.13	0.13	2.97	3.10	539,545.19	6,988,580.72	77.01
NORMEG	M14-2309	466.20	469.60	906	15.04	15.04	3.44	3.40	539,545.19	6,988,580.72	77.01
NORMEG	ML075-004	152.60	155.70	988	0.04	0.04	3.30	3.10	539,738.77	6,988,481.53	10.02
NORMEG	ML075-004	161.10	163.80	987	0.02	0.02	2.88	2.70	539,738.77	6,988,481.53	10.02
NORMEG	ML075-005	158.00	161.00	988	0.15	0.15	3.09	3.00	539,738.31	6,988,481.91	10.06
NORMEG	ML075-005	171.00	174.10	987	0.09	0.09	3.20	3.10	539,738.31	6,988,481.91	10.06
NORMEG	ML150-001	75.00	78.00	988	1.06	1.06	2.36	3.00	540,044.20	6,988,291.68	(72.95)
NORMEG	ML150-002	68.00	76.00	987	2.44	2.44	6.36	8.00	540,043.25	6,988,292.25	(72.19)
NORMEG	ML150-003	66.00	69.80	987	0.91	0.91	3.19	3.80	540,041.60	6,988,291.96	(73.34)
NORMEG	ML150-004	77.20	81.40	987	0.12	0.12	3.20	4.20	540,039.70	6,988,291.03	(73.40)
NORMEG	ML150-006	80.70	85.10	988	1.81	1.81	3.18	4.40	540,039.49	6,988,291.69	(72.54)
PUMP	GT13-50	20.60	23.50	3330	1.21	1.21	3.60	2.90	540,313.48	6,986,850.85	61.64
PUMP	GT13-52	15.70	19.00	3320	0.03	0.03	3.77	3.30	540,397.73	6,986,798.84	61.78
PUMP	GT13-56	46.00	51.00	3130	1.58	1.58	5.66	5.00	539,408.51	6,986,853.58	57.53
PUMP	GT13-70	41.40	44.00	3101	7.57	7.57	3.42	2.60	540,440.02	6,986,434.63	63.96
PUMP	GT13-70	51.25	56.10	3100	3.01	3.01	6.38	4.85	540,440.02	6,986,434.63	63.96
PUMP	M12-1375	38.50	41.10	3340	10.18	10.18	3.49	2.60	540,313.62	6,986,884.86	61.88
PUMP	M12-1375	45.40	48.00	3330	0.03	0.03	3.49	2.60	540,313.62	6,986,884.86	61.88
PUMP	M12-1378	68.00	71.00	3340	3.23	3.23	4.03	3.00	540,328.84	6,986,922.32	61.85
PUMP	M12-1378	79.00	81.50	3330	1.03	1.03	3.36	2.50	540,328.84	6,986,922.32	61.85
PUMP	M12-1380	101.70	104.70	3340	5.72	5.72	4.03	3.00	540,343.26	6,986,957.61	61.84
PUMP	M12-1380	105.70	108.40	3330	2.20	2.20	3.63	2.70	540,343.26	6,986,957.61	61.84
PUMP	M12-1382	113.30	116.30	3130	0.03	0.03	4.02	3.00	539,634.19	6,986,891.37	58.73
PUMP	M12-1382	162.80	165.80	3110	0.03	0.03	4.01	3.00	539,634.19	6,986,891.37	58.73
PUMP	M12-1382	168.80	172.00	3109	8.05	8.05	4.28	3.20	539,634.19	6,986,891.37	58.73
PUMP	M12-1384	66.40	69.00	3340	1.68	1.68	3.50	2.60	540,356.42	6,986,909.66	62.06
PUMP	M12-1384	75.00	81.00	3330	1.84	1.84	8.07	6.00	540,356.42	6,986,909.66	62.06
PUMP	M12-1387	98.80	103.80	3340	4.18	4.18	6.69	5.00	540,372.09	6,986,947.92	61.81
PUMP	M12-1387	104.80	107.90	3330	4.13	4.13	4.15	3.10	540,372.09	6,986,947.92	61.81
PUMP	M12-1387	126.20	129.80	3320	2.20	2.20	4.82	3.60	540,372.09	6,986,947.92	61.81
PUMP	M12-1387	154.30	159.20	3301	6.62	6.62	6.56	4.90	540,372.09	6,986,947.92	61.81
PUMP	M12-1388	82.60	85.20	3130	1.34	1.34	3.47	2.60	539,618.35	6,986,852.47	58.22
PUMP	M12-1388	132.20	135.20	3110	0.03	0.03	4.01	3.00	539,618.35	6,986,852.47	58.22
PUMP	M12-1388	146.20	148.80	3109	8.41	8.41	3.47	2.60	539,618.35	6,986,852.47	58.22
PUMP	M12-1392	20.00	28.00	3130	6.37	6.37	10.57	8.00	539,570.93	6,986,779.88	57.90
PUMP	M12-1392	70.00	72.60	3110	0.03	0.03	3.44	2.60	539,570.93	6,986,779.88	57.90

PUMP	M12-1392	76.00	78.40	3109	0.03	0.03	3.17	2.40	539,570.93	6,986,779.88	57.90
PUMP	M12-1395	126.00	130.50	3340	1.65	1.65	6.02	4.50	540,386.68	6,986,985.23	61.90
PUMP	M12-1395	133.50	136.50	3330	1.76	1.76	4.02	3.00	540,386.68	6,986,985.23	61.90
PUMP	M12-1395	153.60	158.60	3320	2.83	2.83	6.70	5.00	540,386.68	6,986,985.23	61.90
PUMP	M12-1395	189.00	195.00	3301	1.78	1.78	8.04	6.00	540,386.68	6,986,985.23	61.90
PUMP	M12-1397	39.60	42.60	3130	0.34	0.34	4.02	3.00	539,658.95	6,986,747.08	59.21
PUMP	M12-1397	47.80	51.00	3100	2.32	2.32	4.28	3.20	539,658.95	6,986,747.08	59.21
PUMP	M12-1397	82.70	85.30	3109	0.13	0.13	3.48	2.60	539,658.95	6,986,747.08	59.21
PUMP	M12-1400	64.50	67.50	3340	3.68	3.68	4.02	3.00	540,387.58	6,986,888.04	61.76
PUMP	M12-1400	69.00	75.00	3330	2.03	2.03	8.04	6.00	540,387.58	6,986,888.04	61.76
PUMP	M12-1400	85.50	88.50	3320	2.30	2.30	4.02	3.00	540,387.58	6,986,888.04	61.76
PUMP	M12-1401	39.80	42.00	3110	0.03	0.03	2.94	2.20	539,572.52	6,986,735.79	57.62
PUMP	M12-1401	50.00	52.50	3109	6.04	6.04	3.35	2.50	539,572.52	6,986,735.79	57.62
PUMP	M12-1404	23.50	26.00	3165	5.69	5.69	3.34	2.50	539,536.70	6,986,848.55	57.77
PUMP	M12-1407	92.90	95.50	3340	2.94	2.94	3.50	2.60	540,402.85	6,986,926.21	61.90
PUMP	M12-1407	100.50	103.00	3330	0.03	0.03	3.36	2.50	540,402.85	6,986,926.21	61.90
PUMP	M12-1407	115.00	118.00	3320	14.30	14.30	4.03	3.00	540,402.85	6,986,926.21	61.90
PUMP	M12-1407	123.00	126.00	3310	2.34	2.34	4.03	3.00	540,402.85	6,986,926.21	61.90
PUMP	M12-1408	18.30	20.50	3165	1.59	1.59	2.96	2.20	539,498.81	6,986,863.18	57.75
PUMP	M12-1409	45.20	50.10	3165	8.78	8.78	6.56	4.90	539,467.43	6,986,879.30	57.81
PUMP	M12-1409	90.50	93.00	3100	0.03	0.03	3.35	2.50	539,467.43	6,986,879.30	57.81
PUMP	M12-1410	123.20	126.00	3340	4.13	4.13	3.76	2.80	540,417.50	6,986,962.77	61.59
PUMP	M12-1410	129.00	132.10	3330	1.24	1.24	4.17	3.10	540,417.50	6,986,962.77	61.59
PUMP	M12-1410	149.80	157.00	3320	6.46	6.46	9.68	7.20	540,417.50	6,986,962.77	61.59
PUMP	M12-1410	161.80	172.10	3310	7.01	7.01	13.85	10.30	540,417.50	6,986,962.77	61.59
PUMP	M12-1410	182.30	185.40	3301	2.01	2.01	4.17	3.10	540,417.50	6,986,962.77	61.59
PUMP	M12-1410	189.80	192.80	3180	0.17	0.17	4.04	3.00	540,417.50	6,986,962.77	61.59
PUMP	M12-1411	50.30	52.50	3165	0.38	0.38	2.95	2.20	539,519.32	6,986,897.33	57.63
PUMP	M12-1420	70.10	73.00	3165	0.97	0.97	3.89	2.90	539,483.22	6,986,917.50	57.75
PUMP	M12-1420	122.30	125.10	3100	4.53	13.03	3.76	2.80	539,483.22	6,986,917.50	57.75
PUMP	M12-1423	37.90	40.30	3130	0.03	0.03	3.23	2.40	539,413.71	6,986,853.09	57.76
PUMP	M12-1423	52.50	55.10	3100	3.74	3.74	3.50	2.60	539,413.71	6,986,853.09	57.76
PUMP	M12-1426	14.00	16.20	3195	1.01	1.01	2.95	2.20	539,445.50	6,986,931.58	57.79
PUMP	M12-1426	94.40	96.90	3130	0.25	0.25	3.35	2.50	539,445.50	6,986,931.58	57.79
PUMP	M12-1429	40.40	42.90	3195	22.09	22.09	3.35	2.50	539,460.03	6,986,968.57	58.57
PUMP	M12-1432	97.60	100.00	3190	1.64	1.64	3.22	2.40	539,438.51	6,987,023.22	57.83
PUMP	M12-1435	60.60	63.00	3195	2.58	2.58	3.22	2.40	539,423.44	6,986,985.60	57.66
PUMP	M12-1435	68.30	70.60	3190	0.59	0.59	3.08	2.30	539,423.44	6,986,985.60	57.66
PUMP	M12-1437	89.00	95.00	3340	6.07	6.07	8.05	6.00	540,436.56	6,986,909.19	61.95
PUMP	M12-1437	97.00	101.00	3330	3.40	3.40	5.37	4.00	540,436.56	6,986,909.19	61.95
PUMP	M12-1437	103.00	106.00	3320	3.55	3.55	4.03	3.00	540,436.56	6,986,909.19	61.95
PUMP	M12-1437	122.00	124.70	3310	2.04	2.04	3.62	2.70	540,436.56	6,986,909.19	61.95
PUMP	M12-1441	53.50	55.50	3195	0.25	0.25	2.64	2.00	539,389.79	6,986,983.75	57.77
PUMP	M12-1441	60.50	63.30	3190	0.04	0.04	3.70	2.80	539,389.79	6,986,983.75	57.77
PUMP	M12-1441	70.90	75.30	3180	5.40	5.40	5.82	4.40	539,389.79	6,986,983.75	57.77
PUMP	M12-1442	125.20	128.00	3340	4.03	4.03	3.76	2.80	540,451.31	6,986,945.19	61.93
PUMP	M12-1442	129.40	132.00	3330	1.99	1.99	3.49	2.60	540,451.31	6,986,945.19	61.93
PUMP	M12-1442	135.00	138.00	3320	7.58	7.58	4.03	3.00	540,451.31	6,986,945.19	61.93
PUMP	M12-1442	156.60	159.60	3310	0.31	0.31	4.03	3.00	540,451.31	6,986,945.19	61.93
PUMP	M12-1442	165.00	168.00	3301	5.00	5.00	4.03	3.00	540,451.31	6,986,945.19	61.93
PUMP	M12-1442	187.50	190.50	3180	0.18	0.18	4.02	3.00	540,451.31	6,986,945.19	61.93
PUMP	M12-1444	78.80	83.00	3195	6.29	6.29	5.65	4.20	539,399.29	6,987,023.62	57.66
PUMP	M12-1444	90.00	93.00	3190	4.88	4.88	4.03	3.00	539,399.29	6,987,023.62	57.66
PUMP	M12-1444	99.80	102.20	3180	5.25	5.25	3.23	2.40	539,399.29	6,987,023.62	57.66
PUMP	M12-1447	97.60	100.00	3195	3.21	3.21	3.22	2.40	539,358.00	6,987,039.00	58.00
PUMP	M12-1447	101.00	104.20	3190	1.43	1.43	4.30	3.20	539,358.00	6,987,039.00	58.00
PUMP	M12-1449	173.90	176.50	3340	1.39	1.39	3.48	2.60	540,474.89	6,987,001.96	62.27
PUMP	M12-1449	177.50	180.50	3330	5.53	5.53	4.01	3.00	540,474.89	6,987,001.96	62.27
PUMP	M12-1449	181.50	184.50	3320	2.43	2.43	4.01	3.00	540,474.89	6,987,001.96	62.27
PUMP	M12-1449	202.00	207.30	3310	4.07	4.07	7.08	5.30	540,474.89	6,987,001.96	62.27
PUMP	M12-1449	211.00	217.10	3301	6.47	6.47	8.15	6.10	540,474.89	6,987,001.96	62.27
PUMP	M12-1449	236.30	239.30	3180	0.32	0.32	4.01	3.00	540,474.89	6,987,001.96	62.27
PUMP	M12-1450	69.20	73.00	3195	2.28	2.28	5.09	3.80	539,345.79	6,986,999.70	58.41
PUMP	M12-1450	74.00	78.00	3190	6.50	6.50	5.36	4.00	539,345.79	6,986,999.70	58.41
PUMP	M12-1452	40.40	45.00	3195	5.40	5.40	5.71	4.60	539,322.98	6,986,967.55	58.45
PUMP	M12-1452	46.00	51.00	3190	4.09	4.09	6.21	5.00	539,322.98	6,986,967.55	58.45
PUMP	M12-1452	52.40	54.70	3180	0.03	0.03	2.86	2.30	539,322.98	6,986,967.55	58.45
PUMP	M12-1452	81.50	84.00	3130	0.44	0.44	3.11	2.50	539,322.98	6,986,967.55	58.45
PUMP	M12-1458	212.00	215.40	3340	2.17	2.17	4.28	3.40	540,474.97	6,987,002.22	61.86
PUMP	M12-1458	216.50	220.50	3320	15.03	15.03	5.04	4.00	540,474.97	6,987,002.22	61.86
PUMP	M12-1466	191.60	194.50	3340	0.67	0.67	3.88	2.90	540,445.39	6,987,032.89	61.64
PUMP	M12-1466	202.00	204.80	3330	1.36	1.36	3.75	2.80	540,445.39	6,987,032.89	61.64
PUMP	M12-1466	212.20	215.60	3320	0.08	0.08	4.55	3.40	540,445.39	6,987,032.89	61.64
PUMP	M12-1466	218.00	221.00	3310	0.67	0.67	4.01	3.00	540,445.39	6,987,032.89	61.64
PUMP	M12-1466	231.50	234.60	3301	6.80	6.80	4.15	3.10	540,445.39	6,987,032.89	61.64
PUMP	M12-1471	189.00	196.00	3330	2.13	2.13	9.36	7.00	540,407.96	6,987,036.11	61.94
PUMP	M12-1471	207.00	210.50	3320	4.47	4.47	4.68	3.50	540,407.96	6,987,036.11	61.94
PUMP	M12-1471	222.40	225.00	3310	3.18	3.18	3.48	2.60	540,407.96	6,987,036.11	61.94
PUMP	M12-1471	233.50	236.00	3301	12.28	12.28	3.35	2.50	540,407.96	6,987,036.11	61.94
PUMP	M12-1485	234.90	237.60	3310	6.52	6.52	3.38	2.70	540,408.30	6,987,036.95	62.76
PUMP	M12-1485	253.80	257.00	3301	2.83	2.83	4.02	3.20	540,408.30	6,987,036.95	62.76
PUMP	M12-1494	64.40	67.50	3340	2.76	2.76	4.11	3.10	540,493.05	6,986,851.21	62.89
PUMP	M12-1494	77.45	80.70	3320	2.94	2.94	4.31	3.25	540,493.05	6,986,851.21	62.89
PUMP	M12-1494	82.00	85.00	3310	2.41	2.41	3.98	3.00	540,493.05	6,986,851.21	62.89
PUMP	M12-1501	125.20	128.00	3340	2.76	2.76	3.75	2.80	540,485.80	6,986,930.94	61.90
PUMP	M12-1501	131.40	134.20	3330	4.84	4.84	3.75	2.80	540,485.80	6,986,930.94	61.90
PUMP	M12-1501	144.00	147.00	3320	4.62	4.62	4.02	3.00	540,485.80	6,986,930.94	61.90
PUMP	M12-1501	154.00	158.00	3310	6.42	6.42	5.36	4.00	540,485.80	6,986,930.94	61.90
PUMP	M12-1508	41.90	44.70	3320	4.86	4.86	3.76	2.80	540,514.26	6,986,799.32	61.94
PUMP	M12-1508	57.40	60.20	3301	-	-	3.76	2.80	540,514.26	6,986,799.32	61.94

PUMP	M12-1508	94.80	99.00	3300	4.41	4.41	5.65	4.20	540,514.26	6,986,799.32	61.94
PUMP	M12-1515	11.70	14.20	3320	0.99	0.99	3.35	2.50	540,500.49	6,986,765.76	61.97
PUMP	M12-1515A	13.00	15.70	3320	2.81	2.81	3.63	2.70	540,501.04	6,986,767.18	62.08
PUMP	M12-1515A	28.40	31.00	3301	1.07	1.07	3.50	2.60	540,501.04	6,986,767.18	62.08
PUMP	M12-1521	21.00	23.50	3320	0.72	0.72	3.35	2.50	540,465.26	6,986,782.63	62.18
PUMP	M12-1521	25.50	28.00	3310	9.03	9.03	3.35	2.50	540,465.26	6,986,782.63	62.18
PUMP	M12-1521	31.00	40.00	3301	5.47	5.47	12.08	9.00	540,465.26	6,986,782.63	62.18
PUMP	M12-1527	31.00	33.25	3320	0.41	0.41	3.01	2.25	540,437.85	6,986,810.57	61.98
PUMP	M12-1529	19.60	22.50	3320	1.06	1.06	3.89	2.90	540,395.47	6,986,807.17	62.15
PUMP	M12-1548	106.30	109.10	3340	1.58	1.58	3.76	2.80	540,500.11	6,986,901.88	62.20
PUMP	M12-1548	117.00	120.00	3320	1.31	1.31	4.03	3.00	540,500.11	6,986,901.88	62.20
PUMP	M12-1555	71.50	74.50	3340	3.38	3.38	4.01	3.00	540,587.45	6,986,828.42	61.74
PUMP	M12-1566	146.00	153.00	3340	3.07	3.07	9.39	7.00	540,371.57	6,987,026.08	61.92
PUMP	M12-1566	160.40	163.00	3330	0.03	0.03	3.49	2.60	540,371.57	6,987,026.08	61.92
PUMP	M12-1566	176.60	179.40	3320	0.27	0.27	3.75	2.80	540,371.57	6,987,026.08	61.92
PUMP	M12-1566	218.40	221.70	3301	0.97	0.97	4.43	3.30	540,371.57	6,987,026.08	61.92
PUMP	M12-1572	175.70	178.50	3330	5.02	5.02	3.64	2.80	540,371.80	6,987,026.61	61.84
PUMP	M12-1572	192.00	195.00	3320	0.08	0.08	3.90	3.00	540,371.80	6,987,026.61	61.84
PUMP	M12-1572	223.50	227.50	3301	2.83	2.83	5.20	4.00	540,371.80	6,987,026.61	61.84
PUMP	M12-1580	149.00	151.70	3330	1.01	1.01	3.59	2.70	540,276.28	6,987,037.87	61.86
PUMP	M12-1584	45.55	48.35	3460	4.11	4.11	3.73	2.80	540,164.91	6,987,044.86	62.03
PUMP	M12-1584	164.90	167.90	3402	2.87	2.87	4.02	3.00	540,164.91	6,987,044.86	62.03
PUMP	M12-1584	170.50	172.95	3341	2.11	2.11	3.28	2.45	540,164.91	6,987,044.86	62.03
PUMP	M12-1593	43.40	46.60	3460	0.89	0.89	4.28	3.20	540,110.04	6,987,065.21	62.03
PUMP	M12-1593	172.90	175.60	3402	6.08	6.08	3.62	2.70	540,110.04	6,987,065.21	62.03
PUMP	M12-1593	178.20	180.40	3341	8.40	8.40	2.95	2.20	540,110.04	6,987,065.21	62.03
PUMP	M12-1593	183.00	185.60	3400	9.82	9.82	3.48	2.60	540,110.04	6,987,065.21	62.03
PUMP	M12-1593	191.40	195.00	3299	6.54	6.54	4.82	3.60	540,110.04	6,987,065.21	62.03
PUMP	M12-1599	92.30	95.00	3460	11.05	11.05	3.61	2.70	540,082.17	6,987,143.99	61.94
PUMP	M12-1599	130.20	132.70	3440	1.23	1.23	3.34	2.50	540,082.17	6,987,143.99	61.94
PUMP	M12-1599	203.00	206.00	3405	7.98	7.98	4.02	3.00	540,082.17	6,987,143.99	61.94
PUMP	M12-1599	217.50	223.00	3402	4.73	4.73	7.37	5.50	540,082.17	6,987,143.99	61.94
PUMP	M12-1599	226.00	229.40	3400	3.26	3.26	4.55	3.40	540,082.17	6,987,143.99	61.94
PUMP	M12-1599	243.90	246.60	3299	4.08	4.08	3.62	2.70	540,082.17	6,987,143.99	61.94
PUMP	M12-1607	43.45	47.00	3460	2.58	2.58	4.76	3.55	540,006.81	6,987,122.34	62.05
PUMP	M12-1607	102.45	105.00	3440	3.21	3.21	3.43	2.55	540,006.81	6,987,122.34	62.05
PUMP	M12-1607	133.50	136.35	3412	0.18	0.18	3.83	2.85	540,006.81	6,987,122.34	62.05
PUMP	M12-1607	172.25	175.25	3400	1.40	1.40	4.03	3.00	540,006.81	6,987,122.34	62.05
PUMP	M12-1613	134.30	137.60	3412	0.71	0.71	4.43	3.30	539,939.88	6,987,133.38	62.04
PUMP	M12-1626	157.60	160.20	3413	3.43	3.43	3.42	2.60	539,890.84	6,987,192.30	61.81
PUMP	M12-1626	179.30	182.30	3411	9.51	9.51	3.95	3.00	539,890.84	6,987,192.30	61.81
PUMP	M12-1630	251.30	254.30	3340	3.57	3.57	3.75	3.00	540,498.35	6,987,053.79	61.92
PUMP	M12-1635	203.40	207.40	3412	2.48	2.48	5.35	4.00	539,972.89	6,987,217.87	61.86
PUMP	M12-1639	125.60	128.30	3460	1.62	1.62	3.62	2.70	540,039.90	6,987,204.70	61.85
PUMP	M12-1639	170.80	173.40	3440	0.69	0.69	3.49	2.60	540,039.90	6,987,204.70	61.85
PUMP	M12-1639	218.00	221.00	3412	3.00	3.00	4.03	3.00	540,039.90	6,987,204.70	61.85
PUMP	M12-1639	231.00	236.00	3405	8.62	8.62	6.72	5.00	540,039.90	6,987,204.70	61.85
PUMP	M12-1639	251.00	254.60	3400	8.07	8.07	4.84	3.60	540,039.90	6,987,204.70	61.85
PUMP	M12-1650	193.30	196.80	3340	5.63	5.63	4.41	3.50	540,568.17	6,986,960.50	61.58
PUMP	M12-1659	168.00	171.00	3460	2.03	2.03	4.02	3.00	540,114.63	6,987,229.77	61.64
PUMP	M12-1659	201.00	203.60	3440	1.26	1.26	3.48	2.60	540,114.63	6,987,229.77	61.64
PUMP	M12-1659	274.00	278.90	3405	3.30	3.30	6.57	4.90	540,114.63	6,987,229.77	61.64
PUMP	M12-1659	298.00	301.00	3400	1.33	1.33	4.02	3.00	540,114.63	6,987,229.77	61.64
PUMP	M12-1664	129.60	132.70	3320	0.82	0.82	3.90	3.10	540,502.17	6,986,907.63	61.83
PUMP	M12-1673	115.30	118.00	3402	1.00	1.00	3.60	2.70	540,141.16	6,986,980.03	62.15
PUMP	M12-1673	118.60	120.90	3341	0.14	0.14	3.07	2.30	540,141.16	6,986,980.03	62.15
PUMP	M12-1689	156.50	159.50	3340	3.61	3.61	3.89	3.00	540,496.66	6,986,957.14	61.88
PUMP	M12-1689	171.00	174.00	3320	1.33	1.33	3.89	3.00	540,496.66	6,986,957.14	61.88
PUMP	M12-1695	105.90	108.50	3300	1.30	1.30	3.36	2.60	540,523.48	6,986,824.61	60.59
PUMP	M12-1700	197.10	201.00	3340	5.47	5.47	5.08	3.90	540,514.94	6,987,001.37	61.95
PUMP	M12-1700	209.50	212.50	3320	3.74	3.74	3.91	3.00	540,514.94	6,987,001.37	61.95
PUMP	M12-1702	74.00	76.40	3330	0.03	0.03	3.21	2.40	540,211.94	6,986,949.81	61.82
PUMP	M12-1702	88.60	91.20	3341	2.07	2.07	3.48	2.60	540,211.94	6,986,949.81	61.82
PUMP	M12-1707	109.90	112.45	3460	0.37	0.37	3.43	2.55	540,195.33	6,987,123.26	61.72
PUMP	M12-1707	223.65	226.30	3402	2.94	2.94	3.56	2.65	540,195.33	6,987,123.26	61.72
PUMP	M12-1707	228.40	230.85	3341	2.10	2.10	3.30	2.45	540,195.33	6,987,123.26	61.72
PUMP	M12-1712	122.60	125.30	3460	1.65	1.65	3.61	2.70	540,141.56	6,987,147.69	61.84
PUMP	M12-1712	233.50	236.50	3402	2.76	2.76	4.00	3.00	540,141.56	6,987,147.69	61.84
PUMP	M12-1712	263.50	266.50	3299	1.31	1.31	4.00	3.00	540,141.56	6,987,147.69	61.84
PUMP	M12-1714	207.00	215.00	3413	3.59	3.59	10.68	8.00	539,923.49	6,987,274.53	61.85
PUMP	M12-1714	235.60	239.00	3412	0.64	0.64	4.54	3.40	539,923.49	6,987,274.53	61.85
PUMP	M12-1714	248.80	251.80	3411	3.03	3.03	4.01	3.00	539,923.49	6,987,274.53	61.85
PUMP	M12-1719	119.20	123.80	3101	7.83	7.83	6.18	4.60	540,412.49	6,986,527.73	68.29
PUMP	M12-1719	133.40	135.80	3100	0.39	0.39	3.22	2.40	540,412.49	6,986,527.73	68.29
PUMP	M12-1724	66.20	69.00	3101	1.12	1.12	3.76	2.80	540,570.63	6,986,468.06	73.36
PUMP	M12-1724	77.00	80.00	3100	0.22	0.22	4.03	3.00	540,570.63	6,986,468.06	73.36
PUMP	M12-1804	118.50	121.50	3100	0.48	0.48	3.73	3.00	540,784.99	6,986,490.61	67.81
PUMP	M12-1808	92.00	94.80	3100	2.73	2.73	3.41	2.80	540,655.01	6,986,490.21	73.64
PUMP	M12-1811	55.20	58.00	3195	0.71	0.71	3.67	2.80	539,273.94	6,987,010.85	60.17
PUMP	M12-1811	67.20	69.80	3190	3.28	3.28	3.41	2.60	539,273.94	6,987,010.85	60.17
PUMP	M12-1812	117.50	121.20	3101	0.86	0.86	4.94	3.70	540,507.72	6,986,535.29	72.46
PUMP	M12-1812	131.50	133.90	3100	0.28	0.28	3.20	2.40	540,507.72	6,986,535.29	72.46
PUMP	M12-1820	116.60	120.00	3101	2.55	2.55	4.51	3.40	540,348.67	6,986,599.05	65.68
PUMP	M12-1820	122.00	125.60	3100	0.10	0.10	4.78	3.60	540,348.67	6,986,599.05	65.68
PUMP	M12-1824	108.00	110.70	3195	5.09	5.09	3.62	2.70	539,318.43	6,987,083.71	58.50
PUMP	M12-1824	117.80	120.60	3190	0.03	0.03	3.76	2.80	539,318.43	6,987,083.71	58.50
PUMP	M12-1825	133.00	136.00	3101	0.61	0.61	4.00	3.00	540,227.64	6,986,667.12	62.01
PUMP	M12-1825	146.40	149.20	3100	0.03	0.03	3.74	2.80	540,227.64	6,986,667.12	62.01
PUMP	M12-1825	183.00	185.00	3109	7.61	7.61	2.66	2.00	540,227.64	6,986,667.12	62.01
PUMP	M12-1827	106.90	110.00	3402	0.23	0.23	4.12	3.10	540,088.06	6,986,980.18	62.70

PUMP	M12-1827	112.00	114.60	3341	0.05	0.05	3.46	2.60	540,088.06	6,986,980.18	62.70
PUMP	M12-1827	120.00	123.00	3400	0.08	0.08	3.99	3.00	540,088.06	6,986,980.18	62.70
PUMP	M12-1827	127.00	129.90	3299	5.72	5.72	3.86	2.90	540,088.06	6,986,980.18	62.70
PUMP	M12-1829	97.70	103.90	3101	8.58	8.58	8.28	6.20	540,126.14	6,986,644.45	62.39
PUMP	M12-1830	100.40	103.00	3299	7.45	7.45	3.43	2.60	540,016.51	6,986,978.69	62.69
PUMP	M12-1832	191.00	194.20	3195	1.34	1.34	4.26	3.20	539,350.18	6,987,164.02	58.41
PUMP	M12-1832	198.00	201.00	3190	3.83	3.83	4.00	3.00	539,350.18	6,987,164.02	58.41
PUMP	M12-1837	35.70	38.50	3402	0.14	0.14	3.73	2.80	540,054.73	6,986,896.11	61.74
PUMP	M12-1837	39.50	44.60	3341	11.45	11.45	6.80	5.10	540,054.73	6,986,896.11	61.74
PUMP	M12-1837	45.80	49.00	3400	5.40	5.40	4.27	3.20	540,054.73	6,986,896.11	61.74
PUMP	M12-1837	53.50	56.80	3299	6.84	6.84	4.40	3.30	540,054.73	6,986,896.11	61.74
PUMP	M12-1842	203.00	208.00	3101	2.23	2.23	6.71	5.00	539,976.00	6,986,834.63	60.84
PUMP	M12-1844	79.00	81.70	3195	0.52	0.52	3.52	2.70	539,607.89	6,986,996.22	58.32
PUMP	M12-1844	174.50	176.50	3130	0.03	0.03	2.63	2.00	539,607.89	6,986,996.22	58.32
PUMP	M12-1844	212.60	214.80	3110	1.05	1.05	2.90	2.20	539,607.89	6,986,996.22	58.32
PUMP	M12-1850	9.50	12.10	3400	0.66	0.66	3.45	2.60	539,969.69	6,986,900.93	61.49
PUMP	M12-1850	232.50	238.20	3101	11.77	24.57	7.60	5.70	539,969.69	6,986,900.93	61.49
PUMP	M12-1854	140.00	143.80	3130	0.03	0.03	4.32	3.80	539,625.12	6,986,906.28	58.61
PUMP	M12-1854	194.00	196.60	3110	0.03	0.03	2.98	2.60	539,625.12	6,986,906.28	58.61
PUMP	M12-1854	204.00	207.00	3109	0.03	0.03	3.45	3.00	539,625.12	6,986,906.28	58.61
PUMP	M12-1859	253.40	256.50	3101	3.61	3.61	4.14	3.10	539,940.87	6,986,955.74	62.84
PUMP	M12-1862	186.00	188.50	3101	0.92	0.92	3.36	2.50	539,826.40	6,986,931.26	61.80
PUMP	M12-1862	215.60	217.90	3100	4.28	4.28	3.08	2.30	539,826.40	6,986,931.26	61.80
PUMP	M13-1887	293.40	296.40	3413	11.01	11.01	3.87	3.00	539,933.20	6,987,337.75	61.76
PUMP	M13-1887	310.00	312.60	3412	0.05	0.05	3.36	2.60	539,933.20	6,987,337.75	61.76
PUMP	M13-1888	205.70	210.20	3440	1.72	1.72	5.97	4.50	540,005.75	6,987,249.84	61.75
PUMP	M13-1888	242.40	261.60	3412	7.98	7.98	25.51	19.20	540,005.75	6,987,249.84	61.75
PUMP	M13-1889	261.60	264.20	3330	1.91	1.91	3.49	2.60	540,342.97	6,987,149.79	61.94
PUMP	M13-1889	304.60	309.40	3301	7.53	7.53	6.44	4.80	540,342.97	6,987,149.79	61.94
PUMP	M13-1890	26.40	31.10	3341	1.39	1.39	5.73	4.70	539,982.28	6,986,923.36	61.57
PUMP	M13-1890	33.40	40.20	3400	2.50	2.50	8.30	6.80	539,982.28	6,986,923.36	61.57
PUMP	M13-1890	272.90	276.00	3101	6.46	6.46	3.91	3.10	539,982.28	6,986,923.36	61.57
PUMP	M13-1891	398.80	401.00	3110	17.11	17.11	2.86	2.20	539,629.17	6,987,252.89	62.83
PUMP	M13-1891	407.50	410.60	3109	15.61	16.64	4.03	3.10	539,629.17	6,987,252.89	62.83
PUMP	M13-1892	227.40	230.00	3101	9.76	27.80	3.40	2.60	540,048.96	6,986,822.87	59.98
PUMP	M13-1895	198.00	206.50	3101	6.44	6.44	11.23	8.50	539,910.59	6,986,880.74	60.90
PUMP	M13-1898	285.00	288.10	3310	11.31	18.37	4.08	3.10	540,376.98	6,987,101.71	61.70
PUMP	M13-1899	197.40	199.90	3101	0.73	0.73	3.27	2.50	540,131.56	6,986,761.07	61.16
PUMP	M13-1902	263.10	265.30	3100	0.03	0.03	2.92	2.20	539,799.29	6,987,004.35	62.49
PUMP	M13-1904	235.90	238.30	3195	3.44	3.44	3.00	2.40	539,384.71	6,987,182.11	58.41
PUMP	M13-1905	63.60	66.30	3101	0.09	0.09	3.59	2.70	540,214.51	6,986,565.93	61.37
PUMP	M13-1905	67.90	70.00	3100	0.03	0.03	2.79	2.10	540,214.51	6,986,565.93	61.37
PUMP	M13-1910	172.70	175.80	3101	1.38	1.38	4.12	3.10	540,406.95	6,986,642.59	67.92
PUMP	M13-1910	184.00	189.00	3100	12.76	12.76	6.65	5.00	540,406.95	6,986,642.59	67.92
PUMP	M13-1916	169.00	171.70	3195	2.22	2.22	3.45	2.70	539,316.85	6,987,145.40	57.81
PUMP	M13-1916	180.40	186.30	3190	5.82	5.82	7.56	5.90	539,316.85	6,987,145.40	57.81
PUMP	M13-1921	51.80	54.60	3101	0.11	0.11	3.74	2.80	540,354.54	6,986,495.33	59.74
PUMP	M13-1921	62.60	65.60	3100	10.34	10.34	4.01	3.00	540,354.54	6,986,495.33	59.74
PUMP	M13-1927	47.80	50.80	3101	0.22	0.22	4.00	3.00	540,363.42	6,986,459.19	60.67
PUMP	M13-1927	55.60	59.60	3100	2.63	2.63	5.33	4.00	540,363.42	6,986,459.19	60.67
PUMP	M13-1932	40.40	44.00	3101	1.23	1.23	4.80	3.60	540,431.47	6,986,434.72	63.92
PUMP	M13-1932	51.60	54.20	3100	0.18	0.18	3.47	2.60	540,431.47	6,986,434.72	63.92
PUMP	M13-1934	75.70	78.20	3101	3.32	3.32	3.35	2.50	540,421.10	6,986,475.30	65.78
PUMP	M13-1934	89.40	92.10	3100	0.05	0.05	3.62	2.70	540,421.10	6,986,475.30	65.78
PUMP	M13-1937	334.10	339.10	3412	1.48	1.48	6.49	5.00	539,973.98	6,987,352.86	61.72
PUMP	M13-1939	87.90	90.40	3101	2.28	2.28	3.33	2.50	540,456.05	6,986,495.52	70.16
PUMP	M13-1939	103.50	106.00	3100	0.10	0.10	3.33	2.50	540,456.05	6,986,495.52	70.16
PUMP	M13-1944	68.50	71.30	3101	1.46	1.46	3.76	2.80	540,518.77	6,986,477.41	70.69
PUMP	M13-1944	81.00	83.60	3100	0.03	0.03	3.49	2.60	540,518.77	6,986,477.41	70.69
PUMP	M13-1948	18.90	21.60	3101	0.03	0.03	3.61	2.70	540,492.45	6,986,413.31	67.20
PUMP	M13-1948	25.80	28.60	3100	1.17	1.17	3.74	2.80	540,492.45	6,986,413.31	67.20
PUMP	M13-1950	182.50	186.50	3101	9.69	9.69	5.14	4.00	540,345.23	6,986,686.22	64.94
PUMP	M13-1950	188.50	191.50	3100	0.53	0.53	3.86	3.00	540,345.23	6,986,686.22	64.94
PUMP	M13-1953	230.00	232.80	3101	10.40	10.40	3.70	2.80	540,295.86	6,986,775.55	61.68
PUMP	M13-1955	40.50	43.10	3165	0.03	0.03	3.48	2.60	539,487.39	6,986,882.94	57.58
PUMP	M13-1960	57.10	59.30	3130	-	-	2.94	2.20	539,446.79	6,986,870.75	57.64
PUMP	M13-1962	258.10	261.60	3101	0.11	0.11	4.50	3.50	540,379.06	6,986,772.89	61.76
PUMP	M13-1962	269.30	273.60	3100	2.13	2.13	5.53	4.30	540,379.06	6,986,772.89	61.76
PUMP	M13-1964	13.70	16.00	3130	1.24	1.24	3.08	2.30	539,414.90	6,986,820.09	57.45
PUMP	M13-1964	24.90	29.70	3100	2.23	2.23	6.43	4.80	539,414.90	6,986,820.09	57.45
PUMP	M13-1968A	49.10	51.80	3130	0.07	0.07	3.61	2.70	539,389.93	6,986,874.17	57.62
PUMP	M13-1968A	64.40	67.00	3100	0.03	0.03	3.48	2.60	539,389.93	6,986,874.17	57.62
PUMP	M13-1970	14.00	16.00	3320	0.15	0.15	2.68	2.00	540,427.53	6,986,788.26	61.83
PUMP	M13-1974	32.00	35.00	3320	0.91	0.91	4.01	3.00	540,490.88	6,986,792.56	61.93
PUMP	M13-1974	45.80	50.90	3301	20.46	20.46	6.83	5.10	540,490.88	6,986,792.56	61.93
PUMP	M13-1977	18.90	21.50	3340	4.58	4.58	3.47	2.60	540,385.54	6,986,835.01	61.95
PUMP	M13-1977	27.50	30.00	3330	1.28	1.28	3.33	2.50	540,385.54	6,986,835.01	61.95
PUMP	M13-1977	31.60	34.60	3320	2.87	2.87	4.00	3.00	540,385.54	6,986,835.01	61.95
PUMP	M13-1978	16.00	23.50	3195	8.86	8.86	9.90	7.50	539,403.39	6,986,926.76	57.69
PUMP	M13-1978	26.00	36.50	3190	1.68	1.68	13.86	10.50	539,403.39	6,986,926.76	57.69
PUMP	M13-1978	93.70	96.30	3130	0.03	0.03	3.45	2.60	539,403.39	6,986,926.76	57.69
PUMP	M13-1978	107.30	109.80	3100	2.17	2.17	3.32	2.50	539,403.39	6,986,926.76	57.69
PUMP	M13-1982	25.10	28.40	3330	4.09	4.09	4.42	3.30	540,342.14	6,986,848.49	61.93
PUMP	M13-1983	6.00	8.60	3195	1.03	1.03	3.45	2.60	539,298.74	6,986,923.27	57.74
PUMP	M13-1983	16.00	22.70	3190	6.49	6.49	8.89	6.70	539,298.74	6,986,923.27	57.74
PUMP	M13-1983	28.00	30.50	3180	0.03	0.03	3.32	2.50	539,298.74	6,986,923.27	57.74
PUMP	M13-1983	50.00	52.80	3130	4.04	4.04	3.72	2.80	539,298.74	6,986,923.27	57.74
PUMP	M13-1987	40.30	44.30	3330	8.11	8.11	5.32	4.00	540,282.56	6,986,879.52	61.83
PUMP	M13-1989	17.10	20.10	3165	0.51	0.51	4.01	3.00	539,512.98	6,986,841.92	57.68
PUMP	M13-1992	74.50	79.60	3330	5.64	5.64	6.54	5.10	540,315.90	6,986,922.59	61.88

PUMP	M13-1992	343.10	346.20	3101	9.64	9.64	4.06	3.10	540,315.90	6,986,922.59	61.88
PUMP	M13-1994	33.00	35.20	3130	4.92	4.92	2.93	2.20	539,536.97	6,986,809.41	57.53
PUMP	M13-1997	43.80	46.00	3130	0.03	0.03	2.93	2.20	539,565.02	6,986,799.22	57.67
PUMP	M13-1997	67.10	69.50	3110	4.60	4.60	3.20	2.40	539,565.02	6,986,799.22	57.67
PUMP	M13-1997	79.40	81.50	3109	1.13	1.13	2.80	2.10	539,565.02	6,986,799.22	57.67
PUMP	M13-2001	48.00	50.60	3110	1.26	1.26	3.48	2.60	539,597.68	6,986,737.15	58.23
PUMP	M13-2001	60.00	62.60	3109	1.15	1.15	3.48	2.60	539,597.68	6,986,737.15	58.23
PUMP	M13-2015	15.80	18.00	3130	3.22	3.22	2.94	2.20	539,619.61	6,986,731.13	58.65
PUMP	M13-2015	51.40	59.00	3110	7.35	7.35	10.16	7.60	539,619.61	6,986,731.13	58.65
PUMP	M13-2015	68.80	71.00	3109	0.05	0.05	2.94	2.20	539,619.61	6,986,731.13	58.65
PUMP	M13-2020	131.30	136.00	3340	6.41	6.41	5.85	4.70	540,289.89	6,987,018.56	61.69
PUMP	M13-2020	144.50	149.20	3330	2.61	2.61	5.86	4.70	540,289.89	6,987,018.56	61.69
PUMP	M13-2020	215.30	218.80	3301	3.90	3.90	4.37	3.50	540,289.89	6,987,018.56	61.69
PUMP	M13-2020	417.10	419.30	3101	21.02	21.02	2.80	2.20	540,289.89	6,987,018.56	61.69
PUMP	M13-2022A	55.30	57.30	3130	-	-	2.65	2.00	539,630.63	6,986,792.02	58.32
PUMP	M13-2022A	98.10	100.70	3110	0.36	0.36	3.45	2.60	539,630.63	6,986,792.02	58.32
PUMP	M13-2022A	107.80	110.50	3109	2.03	2.03	3.58	2.70	539,630.63	6,986,792.02	58.32
PUMP	M13-2024	26.20	28.80	3101	4.53	4.53	3.39	2.60	540,333.22	6,986,460.28	60.50
PUMP	M13-2024	32.80	35.50	3100	2.32	2.32	3.52	2.70	540,333.22	6,986,460.28	60.50
PUMP	M13-2032	36.60	39.80	3101	6.80	6.80	4.26	3.20	540,368.85	6,986,433.08	60.81
PUMP	M13-2032	45.90	48.40	3100	0.37	0.37	3.32	2.50	540,368.85	6,986,433.08	60.81
PUMP	M13-2035	38.40	41.00	3101	1.10	1.10	3.48	2.60	540,395.60	6,986,424.87	62.37
PUMP	M13-2035	47.10	49.70	3100	3.15	3.15	3.48	2.60	540,395.60	6,986,424.87	62.37
PUMP	M13-2038	46.00	48.60	3101	1.66	1.66	3.46	2.60	540,416.84	6,986,438.22	64.06
PUMP	M13-2038	58.70	61.30	3100	0.11	0.11	3.46	2.60	540,416.84	6,986,438.22	64.06
PUMP	M13-2040	34.10	37.00	3130	2.05	2.05	3.83	2.90	539,686.84	6,986,733.46	58.99
PUMP	M13-2040	44.00	46.25	3100	0.03	0.03	2.97	2.25	539,686.84	6,986,733.46	58.99
PUMP	M13-2042	31.70	34.50	3101	0.79	0.79	3.70	2.80	540,461.84	6,986,421.63	65.76
PUMP	M13-2042	42.90	45.70	3100	0.25	0.25	3.70	2.80	540,461.84	6,986,421.63	65.76
PUMP	M13-2044	65.00	67.60	3130	0.44	0.44	3.46	2.60	539,405.58	6,986,884.75	57.21
PUMP	M13-2044	71.00	74.00	3100	2.46	2.46	4.00	3.00	539,405.58	6,986,884.75	57.21
PUMP	M13-2048	63.20	65.40	3101	1.34	1.34	2.93	2.20	540,450.34	6,986,459.83	68.50
PUMP	M13-2048	77.90	80.50	3100	0.20	0.20	3.46	2.60	540,450.34	6,986,459.83	68.50
PUMP	M13-2051	76.20	79.30	3101	1.58	1.58	4.13	3.10	540,469.08	6,986,479.87	70.17
PUMP	M13-2051	91.10	93.80	3100	0.03	0.03	3.59	2.70	540,469.08	6,986,479.87	70.17
PUMP	M13-2056	368.00	371.10	3413	16.69	27.98	4.02	3.10	539,930.93	6,987,430.76	61.71
PUMP	M13-2056	383.10	385.50	3412	3.15	3.15	3.12	2.40	539,930.93	6,987,430.76	61.71
PUMP	M13-2058	129.00	132.00	3412	0.25	0.25	3.97	3.00	539,956.43	6,987,128.68	61.65
PUMP	M13-2058	368.80	371.30	3101	2.77	2.77	3.33	2.50	539,956.43	6,987,128.68	61.65
PUMP	M13-2060	73.00	77.70	3101	5.81	5.81	6.26	4.70	540,495.97	6,986,479.95	70.87
PUMP	M13-2060	87.00	90.60	3100	0.57	0.57	4.80	3.60	540,495.97	6,986,479.95	70.87
PUMP	M13-2062	69.70	72.40	3101	0.66	0.66	3.62	2.70	540,543.91	6,986,474.39	71.79
PUMP	M13-2062	81.00	83.80	3100	0.12	0.12	3.76	2.80	540,543.91	6,986,474.39	71.79
PUMP	M13-2065	44.40	47.10	3101	3.50	3.50	3.63	2.70	540,529.79	6,986,437.62	70.79
PUMP	M13-2065	53.40	56.10	3100	14.76	14.76	3.63	2.70	540,529.79	6,986,437.62	70.79
PUMP	M13-2068	156.50	160.30	3101	0.55	0.55	4.98	3.80	540,087.47	6,986,716.38	59.90
PUMP	M13-2073	146.90	149.70	3101	2.74	2.74	3.59	2.80	540,008.36	6,986,723.95	59.80
PUMP	M13-2074	96.00	99.00	3340	4.91	4.91	3.68	3.00	540,339.72	6,986,955.68	61.64
PUMP	M13-2074	110.80	113.40	3330	0.03	0.03	3.20	2.60	540,339.72	6,986,955.68	61.64
PUMP	M13-2074	175.40	178.90	3301	1.10	1.10	4.32	3.50	540,339.72	6,986,955.68	61.64
PUMP	M13-2074	378.00	382.00	3101	13.37	13.77	5.08	4.00	540,339.72	6,986,955.68	61.64
PUMP	M13-2075	94.60	97.30	3330	0.02	0.02	3.40	2.70	540,197.94	6,986,977.46	61.90
PUMP	M13-2075	367.60	371.00	3101	8.96	8.96	4.20	3.40	540,197.94	6,986,977.46	61.90
PUMP	M13-2077	242.70	247.10	3101	7.30	7.30	5.67	4.40	540,003.31	6,986,860.17	60.68
PUMP	M13-2079	297.40	300.10	3413	0.61	0.61	3.53	2.70	539,884.25	6,987,348.80	61.78
PUMP	M13-2079	304.40	307.00	3412	3.35	3.35	3.40	2.60	539,884.25	6,987,348.80	61.78
PUMP	M13-2083	260.60	264.70	3101	1.57	1.57	5.42	4.10	539,881.00	6,987,009.87	64.59
PUMP	M13-2085	224.20	227.00	3413	0.17	0.17	3.60	2.80	539,930.96	6,987,264.32	61.74
PUMP	M13-2085	241.70	245.00	3412	0.16	0.16	4.25	3.30	539,930.96	6,987,264.32	61.74
PUMP	M13-2086	276.90	279.50	3101	3.06	3.06	3.26	2.60	540,329.97	6,986,810.77	61.64
PUMP	M13-2088	59.30	61.80	3330	4.12	4.12	3.16	2.50	540,236.33	6,986,914.48	61.73
PUMP	M13-2088	324.60	327.70	3101	10.06	10.06	3.96	3.10	540,236.33	6,986,914.48	61.73
PUMP	M13-2089	45.00	49.00	3341	4.38	4.38	5.30	4.00	539,970.31	6,986,961.67	62.08
PUMP	M13-2089	57.20	60.00	3400	3.41	3.41	3.71	2.80	539,970.31	6,986,961.67	62.08
PUMP	M13-2092	15.00	18.10	3341	0.31	0.31	4.10	3.10	539,960.51	6,986,936.70	61.69
PUMP	M13-2092	28.00	31.00	3400	0.15	0.15	3.97	3.00	539,960.51	6,986,936.70	61.69
PUMP	M13-2094	21.20	24.60	3402	1.72	1.72	4.39	3.40	540,013.51	6,986,907.19	61.25
PUMP	M13-2094	33.80	36.70	3341	3.88	3.88	3.75	2.90	540,013.51	6,986,907.19	61.25
PUMP	M13-2095	47.00	50.00	3402	3.33	3.33	3.90	3.00	540,021.69	6,986,930.59	61.67
PUMP	M13-2095	52.00	58.00	3341	4.42	4.42	7.80	6.00	540,021.69	6,986,930.59	61.67
PUMP	M13-2095	70.00	74.00	3299	2.02	2.02	5.20	4.00	540,021.69	6,986,930.59	61.67
PUMP	M13-2096	41.50	44.90	3402	7.13	7.13	4.28	3.40	540,041.58	6,986,911.25	61.36
PUMP	M13-2096	46.40	50.50	3341	6.70	6.70	5.16	4.10	540,041.58	6,986,911.25	61.36
PUMP	M13-2096	52.20	55.30	3400	5.81	5.81	3.91	3.10	540,041.58	6,986,911.25	61.36
PUMP	M13-2096	60.50	63.30	3299	5.13	5.13	3.53	2.80	540,041.58	6,986,911.25	61.36
PUMP	M13-2096	293.30	295.70	3101	0.63	0.63	3.12	2.40	540,041.58	6,986,911.25	61.36
PUMP	M13-2100	206.10	210.40	3101	5.92	5.92	5.45	4.30	540,329.20	6,986,715.39	62.78
PUMP	M13-2100	215.20	218.20	3100	0.02	0.02	3.80	3.00	540,329.20	6,986,715.39	62.78
PUMP	M13-2104	56.80	60.00	3402	11.33	11.33	4.27	3.20	540,064.06	6,986,923.32	61.62
PUMP	M13-2104	61.00	64.50	3341	6.18	6.18	4.67	3.50	540,064.06	6,986,923.32	61.62
PUMP	M13-2104	64.50	69.00	3400	2.52	2.52	6.00	4.50	540,064.06	6,986,923.32	61.62
PUMP	M13-2104	71.10	74.10	3299	2.30	2.30	4.00	3.00	540,064.06	6,986,923.32	61.62
PUMP	M13-2106A	163.10	166.40	3101	0.67	0.67	4.13	3.30	540,281.06	6,986,662.43	62.32
PUMP	M13-2106A	169.80	171.60	3100	0.03	0.03	2.25	1.80	540,281.06	6,986,662.43	62.32
PUMP	M13-2106A	184.50	186.80	3109	16.31	25.18	2.89	2.30	540,281.06	6,986,662.43	62.32
PUMP	M13-2108A	242.20	244.70	3101	2.13	2.13	3.13	2.50	540,228.56	6,986,800.93	61.97
PUMP	M13-2110	48.90	52.00	3402	0.57	0.57	3.76	3.10	540,085.10	6,986,898.11	61.71
PUMP	M13-2110	54.00	61.00	3341	3.53	3.53	8.49	7.00	540,085.10	6,986,898.11	61.71
PUMP	M13-2110	73.50	76.50	3299	0.18	0.18	3.65	3.00	540,085.10	6,986,898.11	61.71
PUMP	M13-2110	298.90	302.00	3101	2.32	2.32	3.89	3.10	540,085.10	6,986,898.11	61.71

PUMP	M13-2115	146.60	149.40	3101	0.04	0.04	3.54	2.80	540,448.43	6,986,557.59	70.74
PUMP	M13-2115	159.40	161.50	3100	0.11	0.11	2.66	2.10	540,448.43	6,986,557.59	70.74
PUMP	M13-2116	44.80	48.00	3402	0.80	0.80	4.24	3.20	540,084.91	6,986,897.65	61.70
PUMP	M13-2116	48.60	54.10	3341	3.49	3.49	7.29	5.50	540,084.91	6,986,897.65	61.70
PUMP	M13-2116	63.10	66.00	3299	6.80	6.80	3.85	2.90	540,084.91	6,986,897.65	61.70
PUMP	M13-2121	192.00	198.30	3101	5.23	5.23	7.53	6.30	540,395.56	6,986,639.85	68.11
PUMP	M13-2121	202.00	206.00	3100	9.36	9.36	4.78	4.00	540,395.56	6,986,639.85	68.11
PUMP	M13-2122	11.20	14.10	3402	4.15	4.15	3.45	2.90	540,143.21	6,986,867.91	61.95
PUMP	M13-2122	17.90	22.00	3341	3.00	3.00	4.89	4.10	540,143.21	6,986,867.91	61.95
PUMP	M13-2122	287.40	290.20	3101	5.71	5.71	3.43	2.80	540,143.21	6,986,867.91	61.95
PUMP	M13-2180	289.00	294.30	3195	2.84	2.84	6.78	5.30	539,716.58	6,987,241.59	63.46
PUMP	M13-2185	230.20	232.80	3195	6.89	6.89	3.27	2.60	539,654.76	6,987,168.49	62.81
PUMP	M13-2185	343.90	346.10	3110	4.47	4.47	2.80	2.20	539,654.76	6,987,168.49	62.81
PUMP	M14-2216	415.70	418.50	3440	2.55	2.55	3.61	2.80	539,903.84	6,987,531.80	61.47
PUMP	M14-2217	121.40	126.20	3340	1.80	1.80	5.95	4.80	540,408.14	6,986,937.22	61.78
PUMP	M14-2217	134.80	138.80	3330	2.27	2.27	4.97	4.00	540,408.14	6,986,937.22	61.78
PUMP	M14-2217	141.20	146.30	3320	0.01	0.01	6.35	5.10	540,408.14	6,986,937.22	61.78
PUMP	M14-2217	151.70	155.10	3310	0.06	0.06	4.24	3.40	540,408.14	6,986,937.22	61.78
PUMP	M14-2217	173.60	176.50	3301	6.36	6.36	3.62	2.90	540,408.14	6,986,937.22	61.78
PUMP	M14-2217	185.80	190.50	3180	0.00	0.00	5.88	4.70	540,408.14	6,986,937.22	61.78
PUMP	M14-2217	388.20	391.60	3101	7.36	7.36	4.38	3.40	540,408.14	6,986,937.22	61.78
PUMP	M14-2219	363.00	366.20	3440	1.76	1.76	4.15	3.20	539,847.14	6,987,471.79	61.67
PUMP	M14-2220	11.10	13.00	3320	9.19	9.19	2.31	1.90	540,457.93	6,986,767.69	61.71
PUMP	M14-2220	13.00	17.00	3310	27.29	28.66	4.86	4.00	540,457.93	6,986,767.69	61.71
PUMP	M14-2220	20.00	30.50	3301	5.44	5.44	12.80	10.50	540,457.93	6,986,767.69	61.71
PUMP	M14-2220	271.70	274.30	3101	10.52	10.52	3.32	2.60	540,457.93	6,986,767.69	61.71
PUMP	M14-2220	291.00	293.40	3100	0.24	0.24	3.07	2.40	540,457.93	6,986,767.69	61.71
PUMP	M14-2222	475.00	477.60	3109	3.12	3.12	3.27	2.60	539,643.54	6,987,314.37	63.04
PUMP	M14-2224	237.70	240.60	3101	4.59	4.59	3.69	2.90	540,493.35	6,986,695.85	61.86
PUMP	M14-2224	243.30	245.60	3100	0.16	0.16	2.93	2.30	540,493.35	6,986,695.85	61.86
PUMP	M14-2228	150.00	153.00	3101	2.50	2.50	3.90	3.00	540,176.88	6,986,699.26	62.27
PUMP	M14-2228	157.00	161.00	3100	4.27	4.27	5.20	4.00	540,176.88	6,986,699.26	62.27
PUMP	M14-2229	60.00	65.70	3101	25.26	25.26	7.60	5.70	540,078.97	6,986,590.43	60.43
PUMP	M14-2232	141.40	143.90	3101	0.15	0.15	3.32	2.50	539,929.62	6,986,754.77	60.00
PUMP	M14-2234	174.10	177.20	3330	0.13	0.13	3.89	3.10	540,229.26	6,987,054.39	61.81
PUMP	M14-2234	439.20	442.20	3101	0.30	0.30	3.79	3.00	540,229.26	6,987,054.39	61.81
PUMP	M14-2236	259.20	262.00	3180	-	-	3.71	2.80	539,261.01	6,987,234.07	59.01
PUMP	M14-2238	195.40	198.40	3180	3.76	3.76	3.96	3.00	539,194.05	6,987,176.36	58.58
PUMP	M14-2238	216.90	219.60	3130	2.24	2.24	3.57	2.70	539,194.05	6,987,176.36	58.58
PUMP	M14-2239	225.20	228.80	3330	2.00	2.00	4.48	3.60	540,277.30	6,987,095.09	61.72
PUMP	M14-2239	277.00	280.00	3301	2.40	2.40	3.76	3.00	540,277.30	6,987,095.09	61.72
PUMP	M14-2240	173.40	176.20	3180	0.11	0.11	3.74	2.80	539,246.13	6,987,132.24	58.21
PUMP	M14-2241	121.00	124.00	3180	1.46	1.46	3.96	3.00	539,149.79	6,987,107.02	57.93
PUMP	M14-2242	218.10	221.30	3180	2.40	2.40	4.21	3.20	539,137.96	6,987,221.03	59.98
PUMP	M14-2242	231.00	233.60	3130	0.17	0.17	3.42	2.60	539,137.96	6,987,221.03	59.98
PUMP	M14-2243	251.00	253.80	3180	1.37	1.37	3.70	2.80	539,187.13	6,987,253.39	59.24
PUMP	M14-2243	273.10	275.60	3130	0.04	0.04	3.31	2.50	539,187.13	6,987,253.39	59.24
PUMP	M14-2244	127.00	130.00	3460	1.68	1.68	3.65	3.00	540,171.03	6,987,126.28	61.68
PUMP	M14-2244	239.70	241.70	3402	0.31	0.31	2.48	2.00	540,171.03	6,987,126.28	61.68
PUMP	M14-2244	251.30	254.70	3341	6.55	6.55	4.21	3.40	540,171.03	6,987,126.28	61.68
PUMP	M14-2244	476.90	478.90	3101	17.83	17.83	2.47	2.00	540,171.03	6,987,126.28	61.68
PUMP	M14-2246	272.80	275.40	3130	0.39	0.39	3.39	2.60	539,122.42	6,987,280.02	60.34
PUMP	M14-2297	120.60	124.40	3101	4.58	4.58	5.05	3.80	540,063.74	6,986,660.53	59.87
PUMP	M14-2300	44.30	48.00	3101	0.88	0.88	4.92	3.70	540,121.74	6,986,571.00	61.27
PUMP	M14-2300	50.10	53.80	3100	19.52	19.52	4.92	3.70	540,121.74	6,986,571.00	61.27
PUMP	M14-2301	30.40	35.90	3101	2.45	2.45	7.32	5.50	540,069.68	6,986,551.58	60.02
PUMP	M14-2303	37.40	40.70	3101	3.58	3.58	4.39	3.30	540,009.73	6,986,571.32	59.80
PUMP	M14-2305	27.30	29.80	3340	1.32	1.32	3.12	2.50	540,426.15	6,986,835.53	61.38
PUMP	M14-2305	31.90	36.00	3330	4.04	4.04	5.12	4.10	540,426.15	6,986,835.53	61.38
PUMP	M14-2305	53.80	56.80	3320	0.00	0.00	3.76	3.00	540,426.15	6,986,835.53	61.38
PUMP	M14-2305	69.30	72.30	3310	0.02	0.02	3.77	3.00	540,426.15	6,986,835.53	61.38
PUMP	M14-2305	314.80	318.90	3101	8.98	9.50	5.30	4.10	540,426.15	6,986,835.53	61.38
PUMP	M14-2313	88.60	97.80	3101	5.94	5.94	12.31	9.20	540,175.01	6,986,625.49	63.49
PUMP	M14-2313	102.00	105.80	3100	0.01	0.01	5.08	3.80	540,175.01	6,986,625.49	63.49
WESMEG	GT13-39	109.40	112.60	650	0.25	0.25	3.08	3.20	538,474.00	6,988,236.79	57.88
WESMEG	M11-1004	38.20	51.00	480	5.00	5.00	14.36	12.80	540,097.16	6,987,783.06	62.26
WESMEG	M11-1004	72.60	75.30	460	0.48	0.48	3.05	2.70	540,097.16	6,987,783.06	62.26
WESMEG	M11-1004	124.00	129.60	450	0.62	0.62	6.36	5.60	540,097.16	6,987,783.06	62.26
WESMEG	M11-1004	162.50	167.00	440	2.01	2.01	5.09	4.50	540,097.16	6,987,783.06	62.26
WESMEG	M11-1007	58.00	61.00	660	0.76	0.76	3.38	3.00	540,187.65	6,988,031.28	64.45
WESMEG	M11-1007	72.00	75.00	650	2.42	2.42	3.38	3.00	540,187.65	6,988,031.28	64.45
WESMEG	M11-1007	102.00	105.00	625	0.85	0.85	3.40	3.00	540,187.65	6,988,031.28	64.45
WESMEG	M11-1007	115.00	118.00	600	1.23	1.23	3.40	3.00	540,187.65	6,988,031.28	64.45
WESMEG	M11-1007	125.00	128.00	520	1.21	1.21	3.41	3.00	540,187.65	6,988,031.28	64.45
WESMEG	M11-1008	36.00	39.00	490	2.08	2.08	3.39	3.00	540,217.24	6,987,797.06	62.90
WESMEG	M11-1008	92.40	95.40	470	1.36	1.36	3.40	3.00	540,217.24	6,987,797.06	62.90
WESMEG	M11-1008	104.30	107.20	460	0.31	0.31	3.28	2.90	540,217.24	6,987,797.06	62.90
WESMEG	M11-1010	48.00	51.00	670	1.17	1.17	3.32	3.00	540,308.26	6,988,021.30	64.11
WESMEG	M11-1010	80.00	85.70	650	1.04	1.04	6.34	5.70	540,308.26	6,988,021.30	64.11
WESMEG	M11-1010	99.00	102.00	625	0.41	0.41	3.35	3.00	540,308.26	6,988,021.30	64.11
WESMEG	M11-1010	115.00	118.20	600	7.07	7.07	3.58	3.20	540,308.26	6,988,021.30	64.11
WESMEG	M11-1010	256.40	259.60	490	0.79	0.79	3.58	3.20	540,308.26	6,988,021.30	64.11
WESMEG	M11-1012	80.00	82.90	490	1.02	1.02	3.21	2.90	540,277.28	6,987,831.87	63.88
WESMEG	M11-1012	136.00	143.00	470	1.84	1.84	7.80	7.00	540,277.28	6,987,831.87	63.88
WESMEG	M11-1012	150.30	154.00	460	1.28	1.28	4.13	3.70	540,277.28	6,987,831.87	63.88
WESMEG	M11-1013	151.00	154.00	670	0.10	0.10	3.41	3.00	540,427.23	6,988,133.65	67.11
WESMEG	M11-1013	172.30	179.00	650	3.07	3.07	7.65	6.70	540,427.23	6,988,133.65	67.11
WESMEG	M11-1013	197.00	206.50	625	2.08	2.08	10.88	9.50	540,427.23	6,988,133.65	67.11
WESMEG	M11-1013	218.00	225.00	600	1.82	1.82	8.02	7.00	540,427.23	6,988,133.65	67.11
WESMEG	M11-1014	59.00	62.00	490	0.98	0.98	3.33	3.00	540,156.93	6,987,834.25	63.26

WESMEG	M11-1014	132.60	138.00	460	8.17	8.17	6.04	5.40	540,156.93	6,987,834.25	63.26
WESMEG	M11-1015	78.00	80.80	650	7.92	7.92	3.12	2.80	540,547.59	6,987,994.22	65.58
WESMEG	M11-1015	87.00	101.10	625	1.01	1.01	15.74	14.10	540,547.59	6,987,994.22	65.58
WESMEG	M11-1015	113.00	118.00	600	2.68	2.68	5.59	5.00	540,547.59	6,987,994.22	65.58
WESMEG	M11-1015	145.50	149.50	520	0.62	0.62	4.48	4.00	540,547.59	6,987,994.22	65.58
WESMEG	M11-1016	12.00	14.80	500	0.21	0.21	3.10	2.80	540,037.04	6,987,835.37	64.02
WESMEG	M11-1016	51.00	54.00	480	1.35	1.35	3.33	3.00	540,037.04	6,987,835.37	64.02
WESMEG	M11-1016	82.00	86.00	480	0.71	0.71	4.49	4.00	540,037.04	6,987,835.37	64.02
WESMEG	M11-1016	108.00	114.30	460	1.53	1.53	7.09	6.30	540,037.04	6,987,835.37	64.02
WESMEG	M11-1016	153.70	173.80	450	1.19	1.19	22.70	20.10	540,037.04	6,987,835.37	64.02
WESMEG	M11-1016	197.00	200.00	440	0.07	0.07	3.39	3.00	540,037.04	6,987,835.37	64.02
WESMEG	M11-1017	21.50	35.50	650	1.26	1.26	15.56	14.00	540,607.38	6,987,933.96	65.05
WESMEG	M11-1017	44.50	52.50	625	2.56	2.56	8.92	8.00	540,607.38	6,987,933.96	65.05
WESMEG	M11-1017	67.50	81.50	600	1.50	1.50	15.66	14.00	540,607.38	6,987,933.96	65.05
WESMEG	M11-1017	96.80	100.50	520	0.61	0.61	4.15	3.70	540,607.38	6,987,933.96	65.05
WESMEG	M11-1019	117.00	120.00	670	0.26	0.26	3.33	3.00	540,368.04	6,988,084.60	65.15
WESMEG	M11-1019	128.90	133.70	650	1.94	1.94	5.36	4.80	540,368.04	6,988,084.60	65.15
WESMEG	M11-1019	162.40	165.50	625	0.20	0.20	3.49	3.10	540,368.04	6,988,084.60	65.15
WESMEG	M11-1019	167.50	179.50	600	3.47	3.47	13.52	12.00	540,368.04	6,988,084.60	65.15
WESMEG	M11-1020	47.00	50.00	660	13.99	13.99	3.35	3.00	540,667.36	6,988,003.65	64.49
WESMEG	M11-1020	77.80	80.50	710	7.34	7.34	3.00	2.70	540,667.36	6,988,003.65	64.49
WESMEG	M11-1020	108.00	115.60	650	1.77	1.77	8.48	7.60	540,667.36	6,988,003.65	64.49
WESMEG	M11-1020	135.00	138.00	625	0.82	0.82	3.36	3.00	540,667.36	6,988,003.65	64.49
WESMEG	M11-1020	155.50	158.40	600	0.94	0.94	3.26	2.90	540,667.36	6,988,003.65	64.49
WESMEG	M11-1021	47.00	51.00	500	1.49	1.49	4.43	4.00	539,976.90	6,987,883.87	64.31
WESMEG	M11-1021	83.40	86.10	480	0.33	0.33	3.01	2.70	539,976.90	6,987,883.87	64.31
WESMEG	M11-1021	100.00	109.00	480	3.18	3.18	10.07	9.00	539,976.90	6,987,883.87	64.31
WESMEG	M11-1021	151.00	154.30	460	0.42	0.42	3.71	3.30	539,976.90	6,987,883.87	64.31
WESMEG	M11-1021	194.80	207.20	450	2.58	2.58	14.01	12.40	539,976.90	6,987,883.87	64.31
WESMEG	M11-1022	110.00	113.00	670	0.82	0.82	3.36	3.00	540,488.16	6,988,084.38	65.55
WESMEG	M11-1022	158.00	161.50	650	0.96	0.96	3.94	3.50	540,488.16	6,988,084.38	65.55
WESMEG	M11-1022	166.90	183.50	625	1.56	1.56	18.71	16.60	540,488.16	6,988,084.38	65.55
WESMEG	M11-1022	196.50	214.30	600	1.80	1.80	20.10	17.80	540,488.16	6,988,084.38	65.55
WESMEG	M11-1022	231.00	235.70	520	2.04	2.04	5.31	4.70	540,488.16	6,988,084.38	65.55
WESMEG	M11-1023	127.50	131.00	660	0.35	0.35	3.89	3.50	540,668.24	6,988,082.66	65.32
WESMEG	M11-1023	143.00	146.00	710	1.97	1.97	3.34	3.00	540,668.24	6,988,082.66	65.32
WESMEG	M11-1023	191.00	194.00	650	0.06	0.06	3.33	3.00	540,668.24	6,988,082.66	65.32
WESMEG	M11-1023	230.40	235.30	600	2.72	2.72	5.44	4.90	540,668.24	6,988,082.66	65.32
WESMEG	M11-1024	21.50	24.80	600	0.07	0.07	3.67	3.30	540,037.15	6,987,933.62	64.45
WESMEG	M11-1024	33.00	35.80	520	0.64	0.64	3.12	2.80	540,037.15	6,987,933.62	64.45
WESMEG	M11-1024	102.00	104.90	500	0.39	0.39	3.26	2.90	540,037.15	6,987,933.62	64.45
WESMEG	M11-1024	142.50	146.50	480	0.78	0.78	4.51	4.00	540,037.15	6,987,933.62	64.45
WESMEG	M11-1024	180.00	187.00	480	1.71	1.71	7.91	7.00	540,037.15	6,987,933.62	64.45
WESMEG	M11-1024	199.50	202.60	460	0.03	0.03	3.51	3.10	540,037.15	6,987,933.62	64.45
WESMEG	M11-1024	244.10	258.00	450	1.82	1.82	15.76	13.90	540,037.15	6,987,933.62	64.45
WESMEG	M11-1024	288.50	293.80	440	1.54	1.54	6.02	5.30	540,037.15	6,987,933.62	64.45
WESMEG	M11-1025	105.00	110.00	670	0.96	0.96	5.58	5.00	540,548.20	6,988,083.36	65.48
WESMEG	M11-1025	148.00	157.00	710	1.06	1.06	10.08	9.00	540,548.20	6,988,083.36	65.48
WESMEG	M11-1025	160.00	171.50	650	2.23	2.23	12.89	11.50	540,548.20	6,988,083.36	65.48
WESMEG	M11-1025	178.00	182.00	625	1.77	1.77	4.49	4.00	540,548.20	6,988,083.36	65.48
WESMEG	M11-1025	203.60	209.00	600	1.05	1.05	6.07	5.40	540,548.20	6,988,083.36	65.48
WESMEG	M11-1025	228.80	234.00	520	1.21	1.21	5.86	5.20	540,548.20	6,988,083.36	65.48
WESMEG	M11-1026	155.00	158.00	670	0.48	0.48	3.36	3.00	540,607.00	6,988,132.77	65.51
WESMEG	M11-1026	194.00	195.00	710	3.71	3.71	1.12	1.00	540,607.00	6,988,132.77	65.51
WESMEG	M11-1026	196.00	197.00	710	0.21	0.21	1.12	1.00	540,607.00	6,988,132.77	65.51
WESMEG	M11-1026	224.00	234.00	650	6.46	6.46	11.26	10.00	540,607.00	6,988,132.77	65.51
WESMEG	M11-1026	243.40	247.00	625	0.39	0.39	4.06	3.60	540,607.00	6,988,132.77	65.51
WESMEG	M11-1026	272.00	281.00	600	2.75	2.75	10.16	9.00	540,607.00	6,988,132.77	65.51
WESMEG	M11-1026	282.00	285.30	520	0.45	0.45	3.73	3.30	540,607.00	6,988,132.77	65.51
WESMEG	M11-1027	9.60	13.00	650	1.40	1.40	3.75	3.40	540,098.29	6,987,982.86	63.48
WESMEG	M11-1027	65.00	69.50	600	1.56	1.56	5.00	4.50	540,098.29	6,987,982.86	63.48
WESMEG	M11-1027	82.00	85.00	520	0.18	0.18	3.34	3.00	540,098.29	6,987,982.86	63.48
WESMEG	M11-1027	89.50	92.50	510	0.59	0.59	3.34	3.00	540,098.29	6,987,982.86	63.48
WESMEG	M11-1027	137.40	140.50	500	0.28	0.28	3.47	3.10	540,098.29	6,987,982.86	63.48
WESMEG	M11-1027	180.40	184.60	490	0.92	0.92	4.71	4.20	540,098.29	6,987,982.86	63.48
WESMEG	M11-1027	230.00	235.00	480	7.01	7.01	5.63	5.00	540,098.29	6,987,982.86	63.48
WESMEG	M11-1027	238.00	241.00	480	0.86	0.86	3.38	3.00	540,098.29	6,987,982.86	63.48
WESMEG	M11-1027	251.00	254.00	460	0.15	0.15	3.39	3.00	540,098.29	6,987,982.86	63.48
WESMEG	M11-1027	293.50	296.50	450	2.02	2.02	3.39	3.00	540,098.29	6,987,982.86	63.48
WESMEG	M11-1029	21.00	24.00	670	0.10	0.10	3.30	3.00	540,487.94	6,987,984.47	65.05
WESMEG	M11-1029	60.00	69.20	650	1.06	1.06	10.20	9.20	540,487.94	6,987,984.47	65.05
WESMEG	M11-1029	77.00	97.00	625	1.33	1.33	22.24	20.00	540,487.94	6,987,984.47	65.05
WESMEG	M11-1029	101.90	106.00	600	2.92	2.92	4.57	4.10	540,487.94	6,987,984.47	65.05
WESMEG	M11-1029	138.20	142.10	520	5.65	5.65	4.36	3.90	540,487.94	6,987,984.47	65.05
WESMEG	M11-1030	83.40	86.60	660	1.91	1.91	3.55	3.20	540,727.15	6,988,033.77	65.37
WESMEG	M11-1030	92.90	95.90	710	4.79	4.79	3.33	3.00	540,727.15	6,988,033.77	65.37
WESMEG	M11-1031	20.00	23.00	670	1.46	1.46	3.32	3.00	540,426.95	6,987,984.55	64.03
WESMEG	M11-1031	41.70	45.00	650	1.81	1.81	3.66	3.30	540,426.95	6,987,984.55	64.03
WESMEG	M11-1031	68.70	72.20	625	2.97	2.97	3.90	3.50	540,426.95	6,987,984.55	64.03
WESMEG	M11-1031	86.00	95.70	600	2.57	2.57	10.84	9.70	540,426.95	6,987,984.55	64.03
WESMEG	M11-1031	123.00	125.60	520	0.64	0.64	2.92	2.60	540,426.95	6,987,984.55	64.03
WESMEG	M11-1031	225.00	233.80	490	3.38	3.38	9.99	8.80	540,426.95	6,987,984.55	64.03
WESMEG	M11-1033	109.00	112.00	730	1.58	1.58	3.35	3.00	540,847.86	6,988,083.54	69.03
WESMEG	M11-1033	149.30	155.00	710	1.58	1.58	6.36	5.70	540,847.86	6,988,083.54	69.03
WESMEG	M11-1034	8.50	13.00	625	3.83	3.83	4.97	4.50	540,157.83	6,987,933.65	63.06
WESMEG	M11-1034	15.00	21.50	600	2.98	2.98	7.20	6.50	540,157.83	6,987,933.65	63.06
WESMEG	M11-1034	155.50	158.50	490	0.74	0.74	3.35	3.00	540,157.83	6,987,933.65	63.06
WESMEG	M11-1034	210.00	213.20	480	0.76	0.76	3.58	3.20	540,157.83	6,987,933.65	63.06
WESMEG	M11-1034	219.80	225.00	460	1.05	1.05	5.82	5.20	540,157.83	6,987,933.65	63.06
WESMEG	M11-1037	75.00	78.00	460	1.39	1.39	3.34	3.00	540,157.29	6,987,768.26	62.32

WESMEG	M11-1038	167.00	170.00	740	5.06	5.06	3.36	3.00	540,909.89	6,988,164.61	68.28
WESMEG	M11-1039	7.50	12.50	600	1.29	1.29	5.47	5.00	540,424.92	6,987,894.98	64.13
WESMEG	M11-1039	47.00	50.00	520	2.16	2.16	3.29	3.00	540,424.92	6,987,894.98	64.13
WESMEG	M11-1039	146.00	151.00	490	4.27	4.27	5.53	5.00	540,424.92	6,987,894.98	64.13
WESMEG	M11-1039	197.00	200.00	475	1.37	1.37	3.37	3.00	540,424.92	6,987,894.98	64.13
WESMEG	M11-1039	216.00	219.00	470	1.89	1.89	3.37	3.00	540,424.92	6,987,894.98	64.13
WESMEG	M11-1040	40.00	50.00	470	6.43	6.43	11.10	10.00	540,277.14	6,987,733.71	62.37
WESMEG	M11-1040	74.00	80.00	460	0.91	0.91	6.69	6.00	540,277.14	6,987,733.71	62.37
WESMEG	M11-1040	120.17	124.80	440	1.92	1.92	5.19	4.63	540,277.14	6,987,733.71	62.37
WESMEG	M11-1042	25.40	28.50	670	2.03	2.03	3.41	3.10	540,368.53	6,987,984.77	63.72
WESMEG	M11-1042	39.90	48.30	650	2.01	2.01	9.26	8.40	540,368.53	6,987,984.77	63.72
WESMEG	M11-1042	70.00	73.00	625	0.67	0.67	3.32	3.00	540,368.53	6,987,984.77	63.72
WESMEG	M11-1042	75.60	83.00	600	3.09	3.09	8.19	7.40	540,368.53	6,987,984.77	63.72
WESMEG	M11-1042	108.90	112.60	520	1.13	1.13	4.10	3.70	540,368.53	6,987,984.77	63.72
WESMEG	M11-1042	138.40	143.50	510	3.89	3.89	5.66	5.10	540,368.53	6,987,984.77	63.72
WESMEG	M11-1042	220.00	224.00	490	1.43	1.43	4.45	4.00	540,368.53	6,987,984.77	63.72
WESMEG	M11-1043	98.20	101.20	360	3.91	3.91	3.36	3.00	542,497.00	6,987,683.02	65.72
WESMEG	M11-1044	37.00	43.00	490	2.06	2.06	6.62	6.00	540,336.99	6,987,781.68	62.50
WESMEG	M11-1044	100.00	103.00	470	0.49	0.49	3.34	3.00	540,336.99	6,987,781.68	62.50
WESMEG	M11-1044	127.00	131.00	460	2.35	2.35	4.46	4.00	540,336.99	6,987,781.68	62.50
WESMEG	M11-1044	162.90	166.00	440	1.00	1.00	3.47	3.10	540,336.99	6,987,781.68	62.50
WESMEG	M11-1048	35.50	42.00	320	1.60	1.60	7.21	6.50	542,257.04	6,987,682.31	68.16
WESMEG	M11-1048	112.50	115.50	280	0.06	0.06	3.34	3.00	542,257.04	6,987,682.31	68.16
WESMEG	M11-1048	167.40	170.00	240	0.05	0.05	2.90	2.60	542,257.04	6,987,682.31	68.16
WESMEG	M11-1048	189.00	197.00	230	4.09	4.09	8.92	8.00	542,257.04	6,987,682.31	68.16
WESMEG	M11-1050	20.00	23.00	475	2.30	2.30	3.32	3.00	540,457.04	6,987,685.05	63.44
WESMEG	M11-1050	29.00	34.30	470	4.01	4.01	5.87	5.30	540,457.04	6,987,685.05	63.44
WESMEG	M11-1050	42.00	45.00	460	1.25	1.25	3.32	3.00	540,457.04	6,987,685.05	63.44
WESMEG	M11-1050	136.00	143.70	430	3.31	3.31	8.66	7.70	540,457.04	6,987,685.05	63.44
WESMEG	M11-1051	53.00	56.00	670	0.99	0.99	3.34	3.00	540,248.85	6,988,034.34	63.92
WESMEG	M11-1051	62.00	65.00	660	0.35	0.35	3.35	3.00	540,248.85	6,988,034.34	63.92
WESMEG	M11-1051	77.50	81.00	650	2.96	2.96	3.91	3.50	540,248.85	6,988,034.34	63.92
WESMEG	M11-1051	96.50	99.70	625	0.05	0.05	3.58	3.20	540,248.85	6,988,034.34	63.92
WESMEG	M11-1051	114.20	117.50	600	1.78	1.78	3.69	3.30	540,248.85	6,988,034.34	63.92
WESMEG	M11-1051	249.80	253.80	490	2.50	2.50	4.51	4.00	540,248.85	6,988,034.34	63.92
WESMEG	M11-1054	8.30	11.70	490	3.60	3.60	3.76	3.40	540,518.27	6,987,731.99	63.01
WESMEG	M11-1054	75.00	78.00	470	1.64	1.64	3.35	3.00	540,518.27	6,987,731.99	63.01
WESMEG	M11-1054	99.00	105.00	460	2.31	2.31	6.72	6.00	540,518.27	6,987,731.99	63.01
WESMEG	M11-1054	170.60	173.20	430	10.82	10.82	2.93	2.60	540,518.27	6,987,731.99	63.01
WESMEG	M11-1054	180.40	183.00	420	3.80	3.80	2.94	2.60	540,518.27	6,987,731.99	63.01
WESMEG	M11-1057	159.00	162.50	250	1.66	1.66	3.95	3.50	542,016.84	6,987,732.62	63.69
WESMEG	M11-1057	213.50	217.80	230	2.38	2.38	4.86	4.30	542,016.84	6,987,732.62	63.69
WESMEG	M11-1058	125.00	128.00	670	2.19	2.19	3.28	3.00	540,160.16	6,988,129.22	63.71
WESMEG	M11-1058	138.30	141.30	660	0.07	0.07	3.28	3.00	540,160.16	6,988,129.22	63.71
WESMEG	M11-1058	146.80	149.40	650	0.26	0.26	2.85	2.60	540,160.16	6,988,129.22	63.71
WESMEG	M11-1058A	123.80	126.70	670	0.11	0.11	3.15	2.90	540,160.09	6,988,127.26	63.72
WESMEG	M11-1058A	136.00	139.00	660	0.06	0.06	3.26	3.00	540,160.09	6,988,127.26	63.72
WESMEG	M11-1058A	143.40	146.00	650	1.03	1.03	2.83	2.60	540,160.09	6,988,127.26	63.72
WESMEG	M11-1058A	184.00	187.00	625	0.26	0.26	3.29	3.00	540,160.09	6,988,127.26	63.72
WESMEG	M11-1058A	211.00	214.00	600	0.86	0.86	3.31	3.00	540,160.09	6,988,127.26	63.72
WESMEG	M11-1058A	324.00	327.00	490	2.15	2.15	3.33	3.00	540,160.09	6,988,127.26	63.72
WESMEG	M11-1058A	381.50	388.00	480	2.24	2.24	7.25	6.50	540,160.09	6,988,127.26	63.72
WESMEG	M11-1060B	67.50	71.10	460	3.63	3.63	4.00	3.60	540,577.18	6,987,681.97	62.13
WESMEG	M11-1060B	123.20	126.10	430	1.58	1.58	3.24	2.90	540,577.18	6,987,681.97	62.13
WESMEG	M11-1060B	143.40	148.60	420	1.31	1.31	5.83	5.20	540,577.18	6,987,681.97	62.13
WESMEG	M11-1065	71.00	73.80	320	0.38	0.38	3.12	2.80	541,837.04	6,987,733.11	65.04
WESMEG	M11-1065	90.50	93.80	310	0.03	0.03	3.68	3.30	541,837.04	6,987,733.11	65.04
WESMEG	M11-1065	111.00	114.00	300	0.90	0.90	3.36	3.00	541,837.04	6,987,733.11	65.04
WESMEG	M11-1068	61.90	67.80	270	0.73	0.73	6.43	5.90	541,057.07	6,987,682.70	68.76
WESMEG	M11-1073	38.50	42.50	330	4.94	4.94	4.45	4.00	541,776.98	6,987,782.21	64.70
WESMEG	M11-1073	105.50	108.50	320	0.58	0.58	3.38	3.00	541,776.98	6,987,782.21	64.70
WESMEG	M11-1073	114.50	117.50	310	1.32	1.32	3.38	3.00	541,776.98	6,987,782.21	64.70
WESMEG	M11-1073	157.00	160.00	290	7.54	7.54	3.40	3.00	541,776.98	6,987,782.21	64.70
WESMEG	M11-1074	134.00	137.30	270	2.15	2.15	3.67	3.30	541,117.91	6,987,736.57	74.72
WESMEG	M11-1080	49.40	52.80	320	0.03	0.03	3.78	3.40	541,717.03	6,987,733.52	65.52
WESMEG	M11-1080	103.00	106.00	290	0.94	0.94	3.36	3.00	541,717.03	6,987,733.52	65.52
WESMEG	M11-1085	45.40	49.00	650	1.27	1.27	3.99	3.60	538,777.03	6,988,132.23	59.12
WESMEG	M11-1095	7.00	10.00	650	2.34	2.34	3.32	3.00	538,836.91	6,988,083.39	59.96
WESMEG	M11-1097	124.00	127.90	740	2.77	2.77	4.41	3.90	541,416.98	6,988,033.70	65.65
WESMEG	M11-1099	93.40	96.60	300	0.10	0.10	3.52	3.20	541,297.93	6,987,832.77	69.27
WESMEG	M11-1104	143.60	146.60	740	4.27	4.27	3.37	3.00	540,997.53	6,988,133.04	68.17
WESMEG	M11-1104	152.40	155.60	730	1.53	1.53	3.60	3.20	540,997.53	6,988,133.04	68.17
WESMEG	M11-1104	197.00	200.40	720	0.05	0.05	3.86	3.40	540,997.53	6,988,133.04	68.17
WESMEG	M11-1105	99.50	102.60	650	4.65	4.65	3.45	3.10	538,837.45	6,988,183.68	60.95
WESMEG	M11-1105	215.00	219.00	510	2.86	2.86	4.51	4.00	538,837.45	6,988,183.68	60.95
WESMEG	M11-1106	28.70	32.00	720	0.82	0.82	3.64	3.30	541,117.86	6,987,933.16	69.29
WESMEG	M11-1106	51.10	65.20	710	3.28	3.28	15.65	14.10	541,117.86	6,987,933.16	69.29
WESMEG	M11-1111	110.00	114.50	740	4.65	4.65	4.73	4.50	540,941.04	6,988,092.21	68.33
WESMEG	M11-1111	124.30	127.60	730	0.63	0.63	3.47	3.30	540,941.04	6,988,092.21	68.33
WESMEG	M11-1111	155.80	158.80	720	3.60	3.60	3.21	3.00	540,941.04	6,988,092.21	68.33
WESMEG	M11-1113	144.50	148.00	650	2.34	2.34	3.90	3.50	539,136.98	6,988,233.58	65.85
WESMEG	M11-1113	252.30	255.30	510	0.57	0.57	3.38	3.00	539,136.98	6,988,233.58	65.85
WESMEG	M11-1113	292.80	296.80	460	4.33	4.33	4.52	4.00	539,136.98	6,988,233.58	65.85
WESMEG	M11-1114	33.00	36.50	300	3.60	3.60	3.89	3.50	541,357.84	6,987,777.02	69.41
WESMEG	M11-1114	195.00	198.30	270	1.89	1.89	3.71	3.30	541,357.84	6,987,777.02	69.41
WESMEG	M11-1118	51.00	55.80	740	3.27	3.27	5.36	4.80	540,997.95	6,988,033.51	68.42
WESMEG	M11-1118	97.10	100.20	720	1.71	1.71	3.47	3.10	540,997.95	6,988,033.51	68.42
WESMEG	M11-1118	123.50	126.70	710	0.18	0.18	3.59	3.20	540,997.95	6,988,033.51	68.42
WESMEG	M11-1123	156.40	159.40	650	0.50	0.50	3.35	3.00	538,897.04	6,988,233.22	68.91
WESMEG	M11-1123	249.60	253.00	510	2.96	2.96	3.84	3.40	538,897.04	6,988,233.22	68.91

WESMEG	M11-1124	99.40	102.60	740	2.27	2.27	3.59	3.20	541,056.99	6,988,087.56	69.22
WESMEG	M11-1124	110.00	116.00	730	2.18	2.18	6.74	6.00	541,056.99	6,988,087.56	69.22
WESMEG	M11-1124	168.00	171.60	720	5.07	5.07	4.06	3.60	541,056.99	6,988,087.56	69.22
WESMEG	M11-1126	48.50	52.00	460	2.54	2.54	3.86	3.50	540,757.67	6,987,633.18	61.84
WESMEG	M11-1126	80.40	84.50	430	0.13	0.13	4.53	4.10	540,757.67	6,987,633.18	61.84
WESMEG	M11-1128	70.00	74.50	720	1.57	1.57	4.99	4.50	541,057.53	6,987,983.15	68.80
WESMEG	M11-1128	94.70	98.10	710	0.40	0.40	3.78	3.40	541,057.53	6,987,983.15	68.80
WESMEG	M11-1130	64.00	70.50	650	4.95	4.95	7.24	6.50	538,956.97	6,988,133.25	66.55
WESMEG	M11-1130	164.70	167.50	510	2.27	2.27	3.16	2.80	538,956.97	6,988,133.25	66.55
WESMEG	M11-1136	119.00	122.00	520	1.06	1.06	3.35	3.00	539,467.03	6,988,082.97	67.18
WESMEG	M11-1136	126.10	129.00	510	2.07	2.07	3.24	2.90	539,467.03	6,988,082.97	67.18
WESMEG	M11-1136	209.00	211.60	460	1.60	1.60	2.92	2.60	539,467.03	6,988,082.97	67.18
WESMEG	M11-1143	52.80	55.80	510	6.99	6.99	3.31	3.00	539,737.08	6,987,984.02	67.37
WESMEG	M11-1143	83.00	86.00	500	0.97	0.97	3.33	3.00	539,737.08	6,987,984.02	67.37
WESMEG	M11-1148	49.50	52.40	475	2.24	2.24	3.22	2.90	540,397.84	6,987,733.59	63.02
WESMEG	M11-1148	75.50	78.70	470	0.13	0.13	3.56	3.20	540,397.84	6,987,733.59	63.02
WESMEG	M11-1148	91.00	94.00	460	0.94	0.94	3.34	3.00	540,397.84	6,987,733.59	63.02
WESMEG	M11-1148	118.30	121.20	440	0.05	0.05	3.24	2.90	540,397.84	6,987,733.59	63.02
WESMEG	M11-1170	22.40	25.30	660	0.76	0.76	3.17	2.90	540,007.21	6,988,032.65	66.05
WESMEG	M11-1170	39.90	42.90	650	2.94	2.94	3.29	3.00	540,007.21	6,988,032.65	66.05
WESMEG	M11-1170	85.30	88.10	600	2.10	2.10	3.07	2.80	540,007.21	6,988,032.65	66.05
WESMEG	M11-1170	145.60	148.10	510	0.47	0.47	2.78	2.50	540,007.21	6,988,032.65	66.05
WESMEG	M11-1170	189.80	192.50	500	5.04	5.04	3.01	2.70	540,007.21	6,988,032.65	66.05
WESMEG	M11-1170	250.00	255.50	480	2.26	2.26	6.15	5.50	540,007.21	6,988,032.65	66.05
WESMEG	M11-1170	330.20	342.20	450	3.22	3.22	13.44	12.00	540,007.21	6,988,032.65	66.05
WESMEG	M11-1170	367.00	373.00	440	2.67	2.67	6.72	6.00	540,007.21	6,988,032.65	66.05
WESMEG	M11-1170	375.80	378.90	435	1.55	1.55	3.47	3.10	540,007.21	6,988,032.65	66.05
WESMEG	M11-1183	246.20	249.70	650	5.30	5.30	3.42	3.50	540,367.96	6,988,164.42	66.16
WESMEG	M11-1183	288.60	291.70	625	2.63	2.63	3.08	3.10	540,367.96	6,988,164.42	66.16
WESMEG	M11-1183	298.60	308.30	600	1.93	1.93	9.68	9.70	540,367.96	6,988,164.42	66.16
WESMEG	M11-1196	191.00	194.00	670	0.58	0.58	3.31	3.00	540,367.85	6,988,163.51	65.97
WESMEG	M11-1196	207.40	211.40	650	3.35	3.35	4.42	4.00	540,367.85	6,988,163.51	65.97
WESMEG	M11-1196	240.70	244.10	625	0.35	0.35	3.77	3.40	540,367.85	6,988,163.51	65.97
WESMEG	M11-1196	246.40	251.90	600	3.23	3.23	6.11	5.50	540,367.85	6,988,163.51	65.97
WESMEG	M11-1196	316.30	319.20	510	1.28	1.28	3.24	2.90	540,367.85	6,988,163.51	65.97
WESMEG	M11-1197	88.20	90.80	320	1.30	1.30	2.73	2.60	542,257.04	6,987,734.61	68.06
WESMEG	M11-1197	211.70	214.00	240	6.75	6.75	2.49	2.30	542,257.04	6,987,734.61	68.06
WESMEG	M11-1197	243.00	245.70	230	3.29	3.29	2.95	2.70	542,257.04	6,987,734.61	68.06
WESMEG	M11-1206	60.80	63.80	280	3.24	3.24	3.36	3.00	542,257.15	6,987,625.77	65.42
WESMEG	M11-1206	117.00	120.00	240	0.91	0.91	3.38	3.00	542,257.15	6,987,625.77	65.42
WESMEG	M11-1206	138.90	145.50	230	14.36	14.36	7.44	6.60	542,257.15	6,987,625.77	65.42
WESMEG	M11-1206	188.40	191.30	225	0.64	0.64	3.28	2.90	542,257.15	6,987,625.77	65.42
WESMEG	M11-1207	298.00	305.40	670	2.64	2.64	7.41	7.40	540,607.08	6,988,214.16	66.21
WESMEG	M11-1207	322.00	327.00	710	1.07	1.07	5.07	5.00	540,607.08	6,988,214.16	66.21
WESMEG	M11-1212	60.30	64.60	320	0.48	0.48	4.50	4.30	542,319.99	6,987,709.02	67.11
WESMEG	M11-1212	147.00	150.10	280	1.99	1.99	3.31	3.10	542,319.99	6,987,709.02	67.11
WESMEG	M11-1212	183.80	187.00	240	1.25	1.25	3.45	3.20	542,319.99	6,987,709.02	67.11
WESMEG	M11-1212	235.80	240.10	230	2.41	2.41	4.70	4.30	542,319.99	6,987,709.02	67.11
WESMEG	M11-1215	55.10	58.30	320	0.41	0.41	3.48	3.20	542,199.99	6,987,709.10	67.75
WESMEG	M11-1215	187.00	189.50	240	0.04	0.04	2.81	2.50	542,199.99	6,987,709.10	67.75
WESMEG	M11-1215	252.30	256.20	225	1.47	1.47	4.41	3.90	542,199.99	6,987,709.10	67.75
WESMEG	M11-1217	236.40	239.50	670	0.03	0.03	3.44	3.10	540,607.14	6,988,212.74	65.91
WESMEG	M11-1217	272.80	276.00	710	0.19	0.19	3.56	3.20	540,607.14	6,988,212.74	65.91
WESMEG	M11-1217	309.30	312.30	650	15.41	15.41	3.35	3.00	540,607.14	6,988,212.74	65.91
WESMEG	M11-1217	321.60	325.00	650	0.70	0.70	3.80	3.40	540,607.14	6,988,212.74	65.91
WESMEG	M11-1217	337.70	342.00	625	1.77	1.77	4.81	4.30	540,607.14	6,988,212.74	65.91
WESMEG	M11-1217	362.00	370.90	600	2.39	2.39	10.02	8.90	540,607.14	6,988,212.74	65.91
WESMEG	M11-1222	114.00	120.40	320	3.79	3.79	7.24	6.40	541,896.57	6,987,783.02	64.23
WESMEG	M11-1222	126.00	129.00	310	2.07	2.07	3.39	3.00	541,896.57	6,987,783.02	64.23
WESMEG	M11-1222	152.50	155.50	300	1.04	1.04	3.40	3.00	541,896.57	6,987,783.02	64.23
WESMEG	M11-1228	157.00	161.00	320	0.90	0.90	4.54	4.00	541,836.89	6,987,832.89	64.91
WESMEG	M11-1228	179.60	182.80	310	1.52	1.52	3.64	3.20	541,836.89	6,987,832.89	64.91
WESMEG	M11-1228	199.50	203.00	300	1.46	1.46	3.99	3.50	541,836.89	6,987,832.89	64.91
WESMEG	M11-1230	249.30	252.30	670	0.03	0.03	3.19	3.00	540,607.14	6,988,213.25	65.94
WESMEG	M11-1230	286.00	289.00	710	4.26	4.26	3.20	3.00	540,607.14	6,988,213.25	65.94
WESMEG	M11-1230	383.40	390.20	600	1.47	1.47	7.34	6.80	540,607.14	6,988,213.25	65.94
WESMEG	M11-1237	32.00	35.00	330	0.70	0.70	3.34	3.00	541,715.72	6,987,782.18	64.70
WESMEG	M11-1237	97.50	100.50	320	0.10	0.10	3.37	3.00	541,715.72	6,987,782.18	64.70
WESMEG	M11-1237	148.20	151.50	290	6.36	6.36	3.73	3.30	541,715.72	6,987,782.18	64.70
WESMEG	M11-1240	168.30	171.00	320	13.73	27.51	3.06	2.70	541,597.02	6,987,883.85	65.31
WESMEG	M11-1242	64.50	67.50	490	14.21	14.21	3.25	3.00	540,577.03	6,987,775.70	62.76
WESMEG	M11-1242	126.00	129.00	470	2.76	2.76	3.26	3.00	540,577.03	6,987,775.70	62.76
WESMEG	M11-1242	216.00	218.70	430	1.01	1.01	2.96	2.70	540,577.03	6,987,775.70	62.76
WESMEG	M11-1245	28.80	31.90	740	0.60	0.60	3.47	3.10	541,178.46	6,987,982.93	70.49
WESMEG	M11-1245	67.50	70.90	720	4.00	4.00	3.82	3.40	541,178.46	6,987,982.93	70.49
WESMEG	M11-1245	126.00	129.00	710	1.97	1.97	3.39	3.00	541,178.46	6,987,982.93	70.49
WESMEG	M11-1245	226.00	229.00	300	3.01	3.01	3.42	3.00	541,178.46	6,987,982.93	70.49
WESMEG	M11-1252	57.70	61.00	740	5.03	5.03	3.67	3.30	541,118.01	6,988,033.72	69.89
WESMEG	M11-1252	121.00	124.10	720	0.04	0.04	3.48	3.10	541,118.01	6,988,033.72	69.89
WESMEG	M11-1252	169.00	172.20	710	2.03	2.03	3.60	3.20	541,118.01	6,988,033.72	69.89
WESMEG	M11-1255	112.50	115.50	490	0.89	0.89	3.32	3.00	540,218.81	6,987,879.20	62.87
WESMEG	M11-1255	163.00	167.00	470	1.32	1.32	4.44	4.00	540,218.81	6,987,879.20	62.87
WESMEG	M11-1255	176.20	179.20	460	0.04	0.04	3.33	3.00	540,218.81	6,987,879.20	62.87
WESMEG	M11-1265	188.00	193.20	740	2.81	2.81	5.81	5.20	541,058.02	6,988,180.00	70.80
WESMEG	M11-1267	70.40	73.60	710	1.44	1.44	3.60	3.20	540,937.08	6,987,983.71	69.96
WESMEG	M11-1267A	74.30	77.60	710	7.94	7.94	3.61	3.30	540,936.99	6,987,983.91	69.98
WESMEG	M11-1271	43.50	47.40	490	2.36	2.36	4.27	3.90	540,457.68	6,987,780.70	63.44
WESMEG	M11-1271	108.00	116.00	475	1.74	1.74	8.79	8.00	540,457.68	6,987,780.70	63.44
WESMEG	M11-1271	123.00	127.00	470	6.91	6.91	4.40	4.00	540,457.68	6,987,780.70	63.44
WESMEG	M11-1271	133.10	136.30	460	3.37	3.37	3.53	3.20	540,457.68	6,987,780.70	63.44

WESMEG	M11-1271	223.00	225.90	430	1.38	1.38	3.23	2.90	540,457.68	6,987,780.70	63.44
WESMEG	M11-1279	198.50	203.50	710	7.24	7.41	5.59	5.00	540,847.04	6,988,127.88	69.14
WESMEG	M11-1280	11.50	14.50	500	1.24	1.24	3.31	3.00	539,857.00	6,987,883.19	63.31
WESMEG	M11-1280	49.00	52.00	480	0.82	0.82	3.32	3.00	539,857.00	6,987,883.19	63.31
WESMEG	M11-1280	99.00	103.50	455	3.11	3.11	5.00	4.50	539,857.00	6,987,883.19	63.31
WESMEG	M11-1280	188.00	192.00	450	2.32	2.32	4.47	4.00	539,857.00	6,987,883.19	63.31
WESMEG	M11-1280	247.00	250.00	440	0.36	0.36	3.36	3.00	539,857.00	6,987,883.19	63.31
WESMEG	M11-1280	254.90	259.10	435	1.38	1.38	4.70	4.20	539,857.00	6,987,883.19	63.31
WESMEG	M11-1286	58.10	61.00	660	2.03	2.03	3.17	2.90	539,826.95	6,988,078.26	70.29
WESMEG	M11-1286	64.80	68.10	650	0.54	0.54	3.61	3.30	539,826.95	6,988,078.26	70.29
WESMEG	M11-1286	191.00	196.50	500	2.03	2.03	6.07	5.50	539,826.95	6,988,078.26	70.29
WESMEG	M11-1286	359.00	367.00	450	3.43	3.43	8.93	8.00	539,826.95	6,988,078.26	70.29
WESMEG	M11-1288	175.50	178.60	660	0.06	0.06	3.50	3.10	540,727.00	6,988,134.00	67.70
WESMEG	M11-1288	186.00	189.70	710	2.88	2.88	4.19	3.70	540,727.00	6,988,134.00	67.70
WESMEG	M11-1297	71.90	75.00	625	0.86	0.86	3.47	3.10	540,726.93	6,987,931.02	64.13
WESMEG	M11-1298	27.00	30.10	600	0.47	0.47	3.38	3.10	539,982.06	6,987,977.56	66.89
WESMEG	M11-1298	67.20	70.10	520	1.02	1.02	3.17	2.90	539,982.06	6,987,977.56	66.89
WESMEG	M11-1298	131.10	134.60	500	0.84	0.84	3.85	3.50	539,982.06	6,987,977.56	66.89
WESMEG	M11-1298	162.00	165.60	480	1.20	1.20	3.97	3.60	539,982.06	6,987,977.56	66.89
WESMEG	M11-1298	183.00	192.00	480	1.25	1.25	9.95	9.00	539,982.06	6,987,977.56	66.89
WESMEG	M11-1298	225.10	230.00	460	0.78	0.78	5.43	4.90	539,982.06	6,987,977.56	66.89
WESMEG	M11-1298	278.00	286.70	450	3.27	3.27	9.67	8.70	539,982.06	6,987,977.56	66.89
WESMEG	M11-1298	322.00	325.00	440	0.56	0.56	3.35	3.00	539,982.06	6,987,977.56	66.89
WESMEG	M11-1298	326.00	331.20	435	3.72	3.72	5.80	5.20	539,982.06	6,987,977.56	66.89
WESMEG	M11-1300	158.40	161.30	650	2.20	2.20	3.20	2.90	538,957.07	6,988,230.53	71.27
WESMEG	M11-1300	248.70	251.30	510	2.84	2.84	2.89	2.60	538,957.07	6,988,230.53	71.27
WESMEG	M11-1305	170.30	174.00	430	1.32	1.32	4.09	3.70	540,637.14	6,987,729.01	62.01
WESMEG	M11-1306	166.70	169.80	650	1.69	1.69	3.32	3.10	538,957.04	6,988,230.80	70.99
WESMEG	M11-1306	256.20	258.80	510	3.96	3.96	2.83	2.60	538,957.04	6,988,230.80	70.99
WESMEG	M11-1310	121.00	124.00	740	4.26	4.26	3.35	3.00	541,177.22	6,988,082.65	71.31
WESMEG	M11-1310	174.40	178.00	720	2.15	2.15	4.04	3.60	541,177.22	6,988,082.65	71.31
WESMEG	M11-1312	172.40	176.00	670	0.74	0.74	4.07	3.60	540,423.78	6,988,154.33	66.40
WESMEG	M11-1312	197.40	203.60	650	1.95	1.95	7.03	6.20	540,423.78	6,988,154.33	66.40
WESMEG	M11-1312	221.30	227.00	625	1.36	1.36	6.47	5.70	540,423.78	6,988,154.33	66.40
WESMEG	M11-1312	247.00	256.00	600	2.05	2.05	10.22	9.00	540,423.78	6,988,154.33	66.40
WESMEG	M11-1314	532.00	535.70	650	2.55	2.55	4.21	3.70	539,094.15	6,988,638.34	68.35
WESMEG	M11-1317	166.50	169.50	670	1.06	1.06	3.26	3.00	540,570.25	6,988,139.23	65.31
WESMEG	M11-1317	212.00	215.00	710	2.19	2.19	3.26	3.00	540,570.25	6,988,139.23	65.31
WESMEG	M11-1317	218.00	223.00	650	1.36	1.36	5.44	5.00	540,570.25	6,988,139.23	65.31
WESMEG	M11-1317	227.00	234.00	650	1.33	1.33	7.61	7.00	540,570.25	6,988,139.23	65.31
WESMEG	M11-1317	251.40	254.90	625	2.12	2.12	3.80	3.50	540,570.25	6,988,139.23	65.31
WESMEG	M11-1317	278.50	283.00	600	3.64	3.64	4.89	4.50	540,570.25	6,988,139.23	65.31
WESMEG	M11-1317	285.40	288.70	520	1.48	1.48	3.59	3.30	540,570.25	6,988,139.23	65.31
WESMEG	M11-1318	33.00	36.00	710	1.36	1.36	3.32	3.00	540,691.26	6,987,957.03	64.81
WESMEG	M11-1318	95.00	99.50	625	1.60	1.60	5.03	4.50	540,691.26	6,987,957.03	64.81
WESMEG	M11-1318	111.00	114.00	600	0.70	0.70	3.36	3.00	540,691.26	6,987,957.03	64.81
WESMEG	M11-1322	25.90	32.70	480	2.01	2.01	7.53	6.80	539,737.28	6,987,882.58	62.83
WESMEG	M11-1322	98.00	101.30	455	1.22	1.22	3.69	3.30	539,737.28	6,987,882.58	62.83
WESMEG	M11-1322	240.80	243.60	440	0.88	0.88	3.18	2.80	539,737.28	6,987,882.58	62.83
WESMEG	M11-1323	75.00	78.10	670	0.30	0.30	3.43	3.10	540,450.10	6,988,044.00	64.30
WESMEG	M11-1323	109.60	112.80	650	1.04	1.04	3.56	3.20	540,450.10	6,988,044.00	64.30
WESMEG	M11-1323	120.00	133.00	625	2.04	2.04	14.48	13.00	540,450.10	6,988,044.00	64.30
WESMEG	M11-1323	155.00	162.00	600	2.16	2.16	7.82	7.00	540,450.10	6,988,044.00	64.30
WESMEG	M11-1323	189.90	193.50	520	2.92	2.92	4.04	3.60	540,450.10	6,988,044.00	64.30
WESMEG	M11-1323	286.00	289.10	490	1.75	1.75	3.51	3.10	540,450.10	6,988,044.00	64.30
WESMEG	M11-1327	33.20	37.30	650	1.16	1.16	4.50	4.10	540,450.06	6,987,958.21	63.75
WESMEG	M11-1327	50.00	64.00	625	1.44	1.44	15.37	14.00	540,450.06	6,987,958.21	63.75
WESMEG	M11-1327	70.00	80.50	600	1.48	1.48	11.54	10.50	540,450.06	6,987,958.21	63.75
WESMEG	M11-1327	107.80	112.00	520	2.05	2.05	4.62	4.20	540,450.06	6,987,958.21	63.75
WESMEG	M11-1327	209.00	214.00	490	3.68	3.68	5.56	5.00	540,450.06	6,987,958.21	63.75
WESMEG	M11-1330	113.60	117.00	650	0.57	0.57	3.88	3.40	540,559.92	6,988,035.40	64.61
WESMEG	M11-1330	130.00	138.00	625	4.91	5.11	9.14	8.00	540,559.92	6,988,035.40	64.61
WESMEG	M11-1330	156.20	160.10	600	5.21	5.21	4.47	3.90	540,559.92	6,988,035.40	64.61
WESMEG	M11-1330	165.00	170.00	520	1.26	1.26	5.74	5.00	540,559.92	6,988,035.40	64.61
WESMEG	M11-1334	17.00	23.00	625	0.76	0.76	6.69	6.00	540,630.02	6,987,883.93	64.48
WESMEG	M11-1334	28.00	37.00	600	1.04	1.04	10.04	9.00	540,630.02	6,987,883.93	64.48
WESMEG	M11-1334	49.50	55.00	520	2.04	2.04	6.15	5.50	540,630.02	6,987,883.93	64.48
WESMEG	M11-1334	219.00	222.00	470	5.46	5.46	3.42	3.00	540,630.02	6,987,883.93	64.48
WESMEG	M11-1336	20.50	21.30	650	16.00	16.00	0.89	0.80	539,106.95	6,988,082.39	71.24
WESMEG	M11-1336	118.30	121.00	510	2.13	2.13	3.04	2.70	539,106.95	6,988,082.39	71.24
WESMEG	M11-1336	164.20	167.00	460	2.40	2.40	3.16	2.80	539,106.95	6,988,082.39	71.24
WESMEG	M11-1339	10.00	18.00	625	1.71	1.71	8.87	8.00	540,480.13	6,987,917.24	64.47
WESMEG	M11-1339	34.00	50.40	600	2.26	2.26	18.22	16.40	540,480.13	6,987,917.24	64.47
WESMEG	M11-1339	70.50	74.50	520	1.70	1.70	4.46	4.00	540,480.13	6,987,917.24	64.47
WESMEG	M11-1341	20.00	23.80	650	1.23	1.23	4.21	3.80	540,510.21	6,987,931.63	64.50
WESMEG	M11-1341	27.00	33.00	625	1.55	1.55	6.65	6.00	540,510.21	6,987,931.63	64.50
WESMEG	M11-1341	51.00	65.00	600	1.38	1.38	15.56	14.00	540,510.21	6,987,931.63	64.50
WESMEG	M11-1341	88.00	92.40	520	6.08	6.08	4.90	4.40	540,510.21	6,987,931.63	64.50
WESMEG	M11-1344	48.00	51.00	670	0.42	0.42	3.26	3.00	540,394.98	6,988,019.17	64.16
WESMEG	M11-1344	70.50	87.80	650	2.15	2.15	18.85	17.30	540,394.98	6,988,019.17	64.16
WESMEG	M11-1344	93.40	102.00	625	1.20	1.20	9.39	8.60	540,394.98	6,988,019.17	64.16
WESMEG	M11-1344	112.90	129.40	600	3.05	3.05	18.05	16.50	540,394.98	6,988,019.17	64.16
WESMEG	M11-1344	148.00	151.00	520	1.95	1.95	3.29	3.00	540,394.98	6,988,019.17	64.16
WESMEG	M11-1344	268.70	272.00	490	0.43	0.43	3.68	3.30	540,394.98	6,988,019.17	64.16
WESMEG	M11-1345	19.00	21.80	520	1.96	1.96	3.09	2.80	539,467.17	6,987,982.82	62.99
WESMEG	M11-1345	34.00	36.80	510	0.92	0.92	3.10	2.80	539,467.17	6,987,982.82	62.99
WESMEG	M11-1345	88.60	91.30	500	1.02	1.02	3.01	2.70	539,467.17	6,987,982.82	62.99
WESMEG	M11-1345	123.80	126.80	460	0.16	0.16	3.36	3.00	539,467.17	6,987,982.82	62.99
WESMEG	M11-1346	74.30	77.30	670	0.03	0.03	3.30	3.00	540,335.01	6,988,049.11	63.60
WESMEG	M11-1346	96.80	99.60	650	1.88	1.88	3.09	2.80	540,335.01	6,988,049.11	63.60

WESMEG	M11-1346	127.10	131.00	625	1.96	1.96	4.33	3.90	540,335.01	6,988,049.11	63.60
WESMEG	M11-1346	133.00	143.00	600	4.17	4.17	11.10	10.00	540,335.01	6,988,049.11	63.60
WESMEG	M11-1346	210.80	213.90	510	1.26	1.26	3.47	3.10	540,335.01	6,988,049.11	63.60
WESMEG	M11-1351	74.90	77.70	500	0.53	0.53	3.11	2.80	539,916.99	6,987,933.62	66.04
WESMEG	M11-1351	121.00	124.00	480	1.38	1.38	3.35	3.00	539,916.99	6,987,933.62	66.04
WESMEG	M11-1351	127.00	132.00	480	0.74	0.74	5.59	5.00	539,916.99	6,987,933.62	66.04
WESMEG	M11-1351	160.00	165.00	460	3.82	3.82	5.61	5.00	539,916.99	6,987,933.62	66.04
WESMEG	M11-1351	241.00	244.00	450	2.79	2.79	3.39	3.00	539,916.99	6,987,933.62	66.04
WESMEG	M11-1351	288.00	291.60	440	2.16	2.16	4.07	3.60	539,916.99	6,987,933.62	66.04
WESMEG	M11-1351	305.40	308.40	435	1.97	1.97	3.40	3.00	539,916.99	6,987,933.62	66.04
WESMEG	M11-1352	179.00	182.00	225	3.48	3.48	3.35	3.00	542,317.23	6,987,597.14	66.30
WESMEG	M11-1353	16.50	19.50	660	1.63	1.63	3.28	3.00	540,220.01	6,987,979.22	63.60
WESMEG	M11-1353	28.00	32.20	650	3.26	3.26	4.61	4.20	540,220.01	6,987,979.22	63.60
WESMEG	M11-1353	50.40	53.30	625	2.08	2.08	3.20	2.90	540,220.01	6,987,979.22	63.60
WESMEG	M11-1353	63.80	67.00	600	0.66	0.66	3.54	3.20	540,220.01	6,987,979.22	63.60
WESMEG	M11-1353	88.30	95.00	520	1.47	1.47	7.44	6.70	540,220.01	6,987,979.22	63.60
WESMEG	M11-1353	205.40	208.40	490	0.30	0.30	3.37	3.00	540,220.01	6,987,979.22	63.60
WESMEG	M11-1354	15.00	19.30	625	2.17	2.17	4.71	4.30	540,380.18	6,987,922.07	63.71
WESMEG	M11-1354	23.00	30.00	600	1.40	1.40	7.68	7.00	540,380.18	6,987,922.07	63.71
WESMEG	M11-1354	55.90	58.60	520	0.10	0.10	2.97	2.70	540,380.18	6,987,922.07	63.71
WESMEG	M11-1354	169.00	173.00	490	4.59	4.59	4.47	4.00	540,380.18	6,987,922.07	63.71
WESMEG	M11-1355	42.00	45.00	280	3.53	3.53	3.33	3.00	542,197.07	6,987,603.31	64.24
WESMEG	M11-1355	72.00	75.00	250	1.15	1.15	3.34	3.00	542,197.07	6,987,603.31	64.24
WESMEG	M11-1355	99.40	102.00	240	0.47	0.47	2.90	2.60	542,197.07	6,987,603.31	64.24
WESMEG	M11-1355	117.00	129.00	230	5.99	16.66	13.39	12.00	542,197.07	6,987,603.31	64.24
WESMEG	M11-1355	157.50	160.50	225	0.53	0.53	3.35	3.00	542,197.07	6,987,603.31	64.24
WESMEG	M11-1356	121.00	124.00	670	0.74	0.74	3.34	3.00	540,275.10	6,988,107.85	63.83
WESMEG	M11-1356	149.10	152.50	650	8.73	8.73	3.81	3.40	540,275.10	6,988,107.85	63.83
WESMEG	M11-1356	179.50	182.70	625	0.12	0.12	3.60	3.20	540,275.10	6,988,107.85	63.83
WESMEG	M11-1356	185.40	188.60	600	0.75	0.75	3.60	3.20	540,275.10	6,988,107.85	63.83
WESMEG	M11-1359	487.60	492.60	650	1.70	1.70	5.21	5.00	539,169.91	6,988,560.60	71.72
WESMEG	M11-1362	203.50	207.00	225	4.93	4.93	3.90	3.50	542,376.94	6,987,624.74	67.86
WESMEG	M11-1367	88.00	91.00	250	2.76	2.76	3.33	3.00	542,136.95	6,987,622.52	64.51
WESMEG	M11-1367	100.50	103.50	235	1.69	1.69	3.33	3.00	542,136.95	6,987,622.52	64.51
WESMEG	M11-1367	119.00	122.60	240	0.74	0.74	4.00	3.60	542,136.95	6,987,622.52	64.51
WESMEG	M11-1367	186.00	189.00	225	0.51	0.51	3.35	3.00	542,136.95	6,987,622.52	64.51
WESMEG	M11-1369	93.00	96.00	250	0.03	0.03	3.00	3.00	542,136.93	6,987,623.12	64.50
WESMEG	M11-1369	201.00	204.00	225	0.03	0.03	3.05	3.00	542,136.93	6,987,623.12	64.50
WESMEG	M12-1381	45.20	53.20	440	1.22	1.22	8.77	8.00	539,955.61	6,987,659.21	61.90
WESMEG	M12-1381	68.50	71.50	435	2.92	2.92	3.30	3.00	539,955.61	6,987,659.21	61.90
WESMEG	M12-1383	47.50	50.20	450	1.51	1.51	2.97	2.70	539,856.93	6,987,725.51	62.01
WESMEG	M12-1383	116.40	121.00	440	1.11	1.11	5.09	4.60	539,856.93	6,987,725.51	62.01
WESMEG	M12-1383	121.00	126.90	435	2.69	2.69	6.53	5.90	539,856.93	6,987,725.51	62.01
WESMEG	M12-1386	17.40	21.10	440	2.89	2.89	4.00	3.70	540,129.95	6,987,615.27	62.28
WESMEG	M12-1389	60.50	63.50	450	2.03	2.03	3.31	3.00	539,917.06	6,987,727.25	61.97
WESMEG	M12-1389	113.40	116.50	440	0.43	0.43	3.43	3.10	539,917.06	6,987,727.25	61.97
WESMEG	M12-1389	128.40	131.40	435	0.96	0.96	3.32	3.00	539,917.06	6,987,727.25	61.97
WESMEG	M12-1391	71.00	77.00	450	2.23	2.23	6.67	6.00	540,067.17	6,987,723.87	62.27
WESMEG	M12-1391	103.80	107.00	440	2.54	2.54	3.57	3.20	540,067.17	6,987,723.87	62.27
WESMEG	M12-1393	16.00	22.00	460	2.24	2.24	6.57	6.00	539,947.07	6,987,768.32	61.92
WESMEG	M12-1393	29.40	32.40	455	0.55	0.55	3.29	3.00	539,947.07	6,987,768.32	61.92
WESMEG	M12-1393	92.00	99.00	450	1.94	1.94	7.72	7.00	539,947.07	6,987,768.32	61.92
WESMEG	M12-1393	143.10	146.00	440	0.54	0.54	3.20	2.90	539,947.07	6,987,768.32	61.92
WESMEG	M12-1393	161.10	163.80	435	0.03	0.03	2.98	2.70	539,947.07	6,987,768.32	61.92
WESMEG	M12-1394	46.90	50.00	430	7.07	7.07	3.32	3.10	540,486.45	6,987,584.66	62.17
WESMEG	M12-1396	15.00	21.00	480	2.88	2.88	6.54	6.00	539,886.61	6,987,804.89	62.06
WESMEG	M12-1396	120.00	123.00	450	7.02	7.02	3.30	3.00	539,886.61	6,987,804.89	62.06
WESMEG	M12-1396	182.00	189.50	440	2.44	2.44	8.25	7.50	539,886.61	6,987,804.89	62.06
WESMEG	M12-1396	198.00	202.50	435	3.35	3.35	4.96	4.50	539,886.61	6,987,804.89	62.06
WESMEG	M12-1398	66.00	69.20	450	3.45	3.45	3.55	3.20	540,007.02	6,987,724.01	61.76
WESMEG	M12-1398	110.70	113.40	440	0.42	0.42	3.00	2.70	540,007.02	6,987,724.01	61.76
WESMEG	M12-1399	14.20	17.20	470	0.64	0.64	3.31	3.00	540,367.07	6,987,675.02	62.02
WESMEG	M12-1399	36.00	38.70	460	2.32	2.32	2.98	2.70	540,367.07	6,987,675.02	62.02
WESMEG	M12-1402	18.40	22.00	470	4.27	4.27	3.97	3.60	540,426.88	6,987,670.15	62.37
WESMEG	M12-1402	33.90	37.00	460	0.46	0.46	3.42	3.10	540,426.88	6,987,670.15	62.37
WESMEG	M12-1403	75.20	78.00	440	0.13	0.13	3.18	2.80	539,857.17	6,987,681.75	61.87
WESMEG	M12-1403	82.80	87.00	435	2.94	2.94	4.77	4.20	539,857.17	6,987,681.75	61.87
WESMEG	M12-1405	9.70	14.00	490	9.58	9.75	4.79	4.30	540,456.83	6,987,743.66	63.22
WESMEG	M12-1405	71.90	75.00	475	0.29	0.29	3.47	3.10	540,456.83	6,987,743.66	63.22
WESMEG	M12-1405	83.00	86.70	470	2.16	2.16	4.14	3.70	540,456.83	6,987,743.66	63.22
WESMEG	M12-1405	93.00	96.00	460	2.48	2.48	3.36	3.00	540,456.83	6,987,743.66	63.22
WESMEG	M12-1405	184.30	189.80	430	4.84	4.84	6.17	5.50	540,456.83	6,987,743.66	63.22
WESMEG	M12-1405	205.00	208.00	420	1.54	1.54	3.37	3.00	540,456.83	6,987,743.66	63.22
WESMEG	M12-1406	16.30	19.00	480	0.69	0.69	2.96	2.70	540,066.91	6,987,775.42	62.67
WESMEG	M12-1406	30.00	42.00	480	1.92	1.92	13.19	12.00	540,066.91	6,987,775.42	62.67
WESMEG	M12-1406	62.00	65.00	460	0.87	0.87	3.31	3.00	540,066.91	6,987,775.42	62.67
WESMEG	M12-1406	121.00	124.00	450	1.18	1.18	3.34	3.00	540,066.91	6,987,775.42	62.67
WESMEG	M12-1406	151.50	154.50	440	1.30	1.30	3.34	3.00	540,066.91	6,987,775.42	62.67
WESMEG	M12-1412	35.50	40.50	490	2.18	2.18	5.43	5.00	540,127.01	6,987,818.77	62.48
WESMEG	M12-1412	115.00	122.00	460	7.34	7.34	7.70	7.00	540,127.01	6,987,818.77	62.48
WESMEG	M12-1412	163.00	167.00	450	2.04	2.04	4.42	4.00	540,127.01	6,987,818.77	62.48
WESMEG	M12-1413	11.20	14.20	460	1.67	1.67	3.30	3.00	540,541.55	6,987,624.92	62.28
WESMEG	M12-1413	72.60	75.20	430	2.69	2.69	2.89	2.60	540,541.55	6,987,624.92	62.28
WESMEG	M12-1414	33.00	36.00	450	2.44	2.44	3.37	3.00	539,813.14	6,987,711.91	61.59
WESMEG	M12-1416	34.10	41.00	460	1.68	1.68	7.60	6.90	540,607.48	6,987,646.29	62.20
WESMEG	M12-1416	90.40	93.50	430	0.54	0.54	3.50	3.10	540,607.48	6,987,646.29	62.20
WESMEG	M12-1418	78.00	84.00	450	1.23	1.23	6.59	6.00	540,126.98	6,987,725.27	61.71
WESMEG	M12-1418	118.50	121.90	440	1.28	1.28	3.75	3.40	540,126.98	6,987,725.27	61.71
WESMEG	M12-1419	86.00	95.40	450	1.21	1.21	10.52	9.40	539,813.08	6,987,774.20	61.83
WESMEG	M12-1419	152.00	157.20	440	5.31	5.31	5.84	5.20	539,813.08	6,987,774.20	61.83

WESMEG	M12-1419	157.20	163.50	435	1.53	1.53	7.08	6.30	539,813.08	6,987,774.20	61.83
WESMEG	M12-1421	36.50	40.00	460	2.07	2.07	3.86	3.50	540,667.15	6,987,645.00	62.01
WESMEG	M12-1421	87.50	90.50	430	2.16	2.16	3.32	3.00	540,667.15	6,987,645.00	62.01
WESMEG	M12-1421	111.50	114.70	420	1.93	1.93	3.54	3.20	540,667.15	6,987,645.00	62.01
WESMEG	M12-1422	101.00	104.80	450	3.39	3.39	4.28	3.80	539,856.89	6,987,785.20	61.75
WESMEG	M12-1422	158.30	161.60	440	2.37	2.37	3.73	3.30	539,856.89	6,987,785.20	61.75
WESMEG	M12-1422	170.00	178.60	435	2.34	2.34	9.73	8.60	539,856.89	6,987,785.20	61.75
WESMEG	M12-1424	58.30	61.30	460	0.05	0.05	3.24	3.00	540,698.53	6,987,665.84	61.95
WESMEG	M12-1424	108.00	110.80	430	0.03	0.03	3.04	2.80	540,698.53	6,987,665.84	61.95
WESMEG	M12-1425	13.00	16.00	470	10.17	10.17	3.28	3.00	540,187.09	6,987,725.37	61.86
WESMEG	M12-1425	110.00	113.00	440	1.34	1.34	3.33	3.00	540,187.09	6,987,725.37	61.86
WESMEG	M12-1427	135.50	141.30	450	1.84	1.84	6.54	5.80	539,812.96	6,987,832.18	61.95
WESMEG	M12-1427	202.00	204.80	440	1.34	1.34	3.17	2.80	539,812.96	6,987,832.18	61.95
WESMEG	M12-1427	206.00	209.00	435	1.89	1.89	3.39	3.00	539,812.96	6,987,832.18	61.95
WESMEG	M12-1428	76.40	79.20	460	1.25	1.25	3.08	2.80	540,636.91	6,987,687.83	62.31
WESMEG	M12-1428	129.00	132.00	430	1.12	1.12	3.31	3.00	540,636.91	6,987,687.83	62.31
WESMEG	M12-1428	151.00	154.00	420	0.92	0.92	3.31	3.00	540,636.91	6,987,687.83	62.31
WESMEG	M12-1430	13.00	16.10	470	0.52	0.52	3.45	3.10	540,254.00	6,987,712.00	62.00
WESMEG	M12-1430	47.40	50.80	460	2.63	2.63	3.80	3.40	540,254.00	6,987,712.00	62.00
WESMEG	M12-1431	17.00	19.60	470	6.44	6.44	2.87	2.60	540,306.86	6,987,698.52	62.49
WESMEG	M12-1431	49.50	56.80	460	3.54	3.54	8.11	7.30	540,306.86	6,987,698.52	62.49
WESMEG	M12-1431	88.20	93.00	440	1.50	1.50	5.34	4.80	540,306.86	6,987,698.52	62.49
WESMEG	M12-1433	132.60	135.40	450	1.66	1.66	3.14	2.80	539,770.61	6,987,833.82	60.90
WESMEG	M12-1433	199.70	202.70	440	0.49	0.49	3.36	3.00	539,770.61	6,987,833.82	60.90
WESMEG	M12-1433	213.00	216.00	435	10.77	10.77	3.36	3.00	539,770.61	6,987,833.82	60.90
WESMEG	M12-1434	59.40	62.00	490	1.37	1.37	2.91	2.60	540,606.98	6,987,761.49	63.04
WESMEG	M12-1436	28.70	31.60	490	0.03	0.03	3.20	2.90	540,577.09	6,987,736.50	62.60
WESMEG	M12-1436	173.00	178.20	430	7.13	7.13	5.76	5.20	540,577.09	6,987,736.50	62.60
WESMEG	M12-1436	184.00	187.00	420	0.42	0.42	3.33	3.00	540,577.09	6,987,736.50	62.60
WESMEG	M12-1438	169.20	172.10	430	1.48	1.48	3.26	2.90	540,757.31	6,987,732.17	63.91
WESMEG	M12-1439	9.00	12.00	470	5.75	5.75	3.25	3.00	540,247.30	6,987,707.08	62.57
WESMEG	M12-1439	43.40	47.00	460	0.38	0.38	3.92	3.60	540,247.30	6,987,707.08	62.57
WESMEG	M12-1439	102.40	105.60	440	0.38	0.38	3.50	3.20	540,247.30	6,987,707.08	62.57
WESMEG	M12-1440	77.80	81.00	450	0.70	0.70	3.57	3.20	539,770.10	6,987,769.53	62.47
WESMEG	M12-1440	141.50	145.50	440	1.23	1.23	4.47	4.00	539,770.10	6,987,769.53	62.47
WESMEG	M12-1440	152.40	155.60	435	0.05	0.05	3.58	3.20	539,770.10	6,987,769.53	62.47
WESMEG	M12-1443	80.30	83.30	490	0.49	0.49	3.27	3.00	540,367.09	6,987,828.38	63.22
WESMEG	M12-1443	152.10	155.00	470	1.16	1.16	3.19	2.90	540,367.09	6,987,828.38	63.22
WESMEG	M12-1445	39.00	42.00	490	0.67	0.67	3.33	3.00	540,547.18	6,987,758.60	63.19
WESMEG	M12-1446	26.60	29.80	625	0.31	0.31	3.57	3.20	540,751.95	6,987,878.23	64.60
WESMEG	M12-1448	123.00	126.00	440	1.25	1.25	3.37	3.00	539,730.10	6,987,746.99	61.93
WESMEG	M12-1448	136.00	139.00	435	0.82	0.82	3.37	3.00	539,730.10	6,987,746.99	61.93
WESMEG	M12-1451	24.30	29.00	625	1.45	1.45	5.22	4.70	540,697.06	6,987,891.51	64.51
WESMEG	M12-1451	49.20	54.20	600	0.80	0.80	5.56	5.00	540,697.06	6,987,891.51	64.51
WESMEG	M12-1453	23.00	26.00	520	15.51	15.51	3.33	3.00	540,427.37	6,987,862.69	63.48
WESMEG	M12-1453	116.00	121.00	490	2.21	2.21	5.60	5.00	540,427.37	6,987,862.69	63.48
WESMEG	M12-1454	17.00	24.50	660	2.14	2.14	8.23	7.50	540,757.40	6,987,959.33	64.94
WESMEG	M12-1454	27.80	31.00	710	0.46	0.46	3.52	3.20	540,757.40	6,987,959.33	64.94
WESMEG	M12-1454	104.80	107.90	625	3.11	3.11	3.44	3.10	540,757.40	6,987,959.33	64.94
WESMEG	M12-1456	74.70	78.00	440	2.87	2.87	3.69	3.30	539,730.16	6,987,685.43	61.93
WESMEG	M12-1456	84.50	87.50	435	1.95	1.95	3.35	3.00	539,730.16	6,987,685.43	61.93
WESMEG	M12-1457	12.70	22.60	650	3.31	3.31	10.93	9.90	538,577.88	6,988,131.55	58.06
WESMEG	M12-1459	6.50	17.00	625	3.09	3.09	11.59	10.50	540,577.22	6,987,904.88	64.04
WESMEG	M12-1459	35.80	43.80	600	2.75	2.75	8.85	8.00	540,577.22	6,987,904.88	64.04
WESMEG	M12-1459	47.80	54.80	520	2.45	2.45	7.75	7.00	540,577.22	6,987,904.88	64.04
WESMEG	M12-1460	6.40	9.60	650	0.53	0.53	3.55	3.20	540,457.00	6,987,931.10	64.61
WESMEG	M12-1460	17.00	28.80	625	1.10	1.10	13.12	11.80	540,457.00	6,987,931.10	64.61
WESMEG	M12-1460	44.00	54.00	600	2.54	2.54	11.14	10.00	540,457.00	6,987,931.10	64.61
WESMEG	M12-1460	80.50	84.30	520	2.95	2.95	4.24	3.80	540,457.00	6,987,931.10	64.61
WESMEG	M12-1462	70.40	74.40	650	2.69	2.69	4.47	4.00	538,576.58	6,988,195.38	58.14
WESMEG	M12-1463	13.40	15.00	450	0.03	0.03	1.78	1.60	539,790.00	6,987,690.00	62.00
WESMEG	M12-1463B	10.70	12.50	450	0.82	0.82	1.97	1.80	539,790.13	6,987,687.04	61.75
WESMEG	M12-1463B	79.30	82.00	440	0.08	0.08	2.98	2.70	539,790.13	6,987,687.04	61.75
WESMEG	M12-1463B	87.00	90.80	435	1.42	1.42	4.20	3.80	539,790.13	6,987,687.04	61.75
WESMEG	M12-1465	36.00	39.00	650	4.13	4.13	3.35	3.00	538,328.67	6,988,195.74	58.12
WESMEG	M12-1467	32.00	35.00	710	5.79	5.79	3.30	3.00	540,816.96	6,987,960.23	66.72
WESMEG	M12-1468	32.00	36.00	510	2.41	2.41	4.43	4.00	540,306.96	6,987,885.30	63.45
WESMEG	M12-1468	132.90	135.90	490	2.10	2.10	3.34	3.00	540,306.96	6,987,885.30	63.45
WESMEG	M12-1468	187.30	190.70	470	1.45	1.45	3.81	3.40	540,306.96	6,987,885.30	63.45
WESMEG	M12-1468	214.60	219.60	460	3.72	3.72	5.62	5.00	540,306.96	6,987,885.30	63.45
WESMEG	M12-1469	42.50	51.00	650	4.27	4.27	9.50	8.50	538,526.58	6,988,180.46	58.01
WESMEG	M12-1472	95.00	98.00	440	0.18	0.18	3.35	3.00	539,669.94	6,987,702.63	62.33
WESMEG	M12-1474	33.00	40.00	710	5.89	5.89	7.83	7.00	540,876.53	6,987,956.43	69.19
WESMEG	M12-1475	105.00	112.30	650	1.45	1.45	8.12	7.30	538,526.87	6,988,247.83	58.05
WESMEG	M12-1478	50.00	55.40	740	1.19	1.19	6.02	5.40	540,936.75	6,988,032.86	69.33
WESMEG	M12-1478	59.50	62.50	730	0.53	0.53	3.34	3.00	540,936.75	6,988,032.86	69.33
WESMEG	M12-1478	119.30	122.20	710	3.07	3.07	3.25	2.90	540,936.75	6,988,032.86	69.33
WESMEG	M12-1480	110.00	118.40	650	2.69	2.69	8.97	8.40	538,526.86	6,988,248.17	58.14
WESMEG	M12-1482	8.60	12.00	625	2.32	2.32	3.73	3.40	540,337.42	6,987,921.68	64.75
WESMEG	M12-1482	15.00	22.90	600	0.72	0.72	8.66	7.90	540,337.42	6,987,921.68	64.75
WESMEG	M12-1482	63.50	66.50	520	1.79	1.79	3.31	3.00	540,337.42	6,987,921.68	64.75
WESMEG	M12-1482	77.80	81.00	510	0.03	0.03	3.54	3.20	540,337.42	6,987,921.68	64.75
WESMEG	M12-1482	163.10	166.30	490	0.36	0.36	3.58	3.20	540,337.42	6,987,921.68	64.75
WESMEG	M12-1482	219.20	223.20	470	4.44	4.44	4.52	4.00	540,337.42	6,987,921.68	64.75
WESMEG	M12-1484A	192.00	194.80	440	0.44	0.44	3.13	2.80	539,689.85	6,987,820.60	62.80
WESMEG	M12-1486	30.10	33.50	740	4.86	4.86	3.77	3.40	540,966.73	6,988,009.55	69.60
WESMEG	M12-1486	98.60	102.20	710	7.78	7.78	4.04	3.60	540,966.73	6,988,009.55	69.60
WESMEG	M12-1487	191.70	195.10	650	1.01	1.01	3.75	3.40	538,577.94	6,988,315.73	59.40
WESMEG	M12-1489	203.90	212.00	650	0.85	0.85	8.58	8.10	538,526.76	6,988,336.58	60.28
WESMEG	M12-1493	32.00	35.00	740	0.16	0.16	3.29	3.00	541,027.16	6,988,009.03	70.22

WESMEG	M12-1493	85.50	88.60	720	1.57	1.57	3.40	3.10	541,027.16	6,988,009.03	70.22
WESMEG	M12-1493	110.00	113.50	710	3.32	3.32	3.87	3.50	541,027.16	6,988,009.03	70.22
WESMEG	M12-1495	155.42	158.75	440	0.03	0.03	3.69	3.33	539,670.44	6,987,770.24	62.00
WESMEG	M12-1498	212.50	215.60	650	0.94	0.94	3.34	3.10	538,466.88	6,988,364.93	59.74
WESMEG	M12-1499	21.80	29.00	740	1.60	1.60	7.93	7.20	541,087.23	6,988,007.48	68.67
WESMEG	M12-1499	95.00	97.90	720	0.28	0.28	3.22	2.90	541,087.23	6,988,007.48	68.67
WESMEG	M12-1499	134.60	138.40	710	1.91	1.91	4.24	3.80	541,087.23	6,988,007.48	68.67
WESMEG	M12-1500	14.50	17.50	670	-	-	3.33	3.00	540,337.63	6,987,986.91	63.46
WESMEG	M12-1500	39.90	44.00	650	3.06	3.06	4.57	4.10	540,337.63	6,987,986.91	63.46
WESMEG	M12-1500	63.50	66.80	625	0.25	0.25	3.69	3.30	540,337.63	6,987,986.91	63.46
WESMEG	M12-1500	70.00	84.00	600	6.07	11.10	15.68	14.00	540,337.63	6,987,986.91	63.46
WESMEG	M12-1500	141.20	144.20	510	-	-	3.39	3.00	540,337.63	6,987,986.91	63.46
WESMEG	M12-1504	285.30	288.50	650	0.64	0.64	3.46	3.20	538,526.92	6,988,424.93	59.79
WESMEG	M12-1505	17.10	20.20	650	0.55	0.55	3.44	3.10	540,306.79	6,987,952.03	63.39
WESMEG	M12-1505	30.00	33.80	625	0.32	0.32	4.22	3.80	540,306.79	6,987,952.03	63.39
WESMEG	M12-1505	41.70	50.30	600	4.00	4.00	9.56	8.60	540,306.79	6,987,952.03	63.39
WESMEG	M12-1505	102.80	106.50	510	1.39	1.39	4.14	3.70	540,306.79	6,987,952.03	63.39
WESMEG	M12-1509	48.50	52.50	710	1.24	1.24	4.46	4.00	541,027.35	6,987,948.48	68.97
WESMEG	M12-1510	19.70	23.50	650	12.25	16.20	4.24	3.80	540,276.67	6,987,954.50	63.47
WESMEG	M12-1510	34.40	38.00	625	2.46	2.46	4.02	3.60	540,276.67	6,987,954.50	63.47
WESMEG	M12-1510	52.20	55.10	600	0.15	0.15	3.25	2.90	540,276.67	6,987,954.50	63.47
WESMEG	M12-1510	184.10	187.00	490	1.53	1.53	3.29	2.90	540,276.67	6,987,954.50	63.47
WESMEG	M12-1510	231.50	238.60	470	2.53	2.53	8.08	7.10	540,276.67	6,987,954.50	63.47
WESMEG	M12-1510	263.00	266.00	460	2.95	2.95	3.42	3.00	540,276.67	6,987,954.50	63.47
WESMEG	M12-1511	232.00	235.00	440	2.55	2.55	3.34	3.00	539,649.92	6,987,858.85	62.15
WESMEG	M12-1512	24.50	28.00	710	1.16	1.16	3.88	3.50	541,086.90	6,987,911.71	69.49
WESMEG	M12-1514	146.80	150.00	650	3.47	3.47	3.52	3.20	538,466.84	6,988,299.45	58.00
WESMEG	M12-1518	179.00	182.20	650	0.76	0.76	3.45	3.20	538,406.98	6,988,334.31	58.05
WESMEG	M12-1519	16.80	19.90	460	2.89	2.89	3.41	3.10	539,565.10	6,987,866.80	62.08
WESMEG	M12-1520	22.70	25.80	600	0.80	0.80	3.44	3.10	540,255.16	6,987,925.12	63.48
WESMEG	M12-1523	20.40	24.00	600	0.03	0.03	3.96	3.60	540,216.94	6,987,930.70	63.20
WESMEG	M12-1523	47.00	49.80	520	1.27	1.27	3.11	2.80	540,216.94	6,987,930.70	63.20
WESMEG	M12-1523	158.00	161.20	490	0.08	0.08	3.62	3.20	540,216.94	6,987,930.70	63.20
WESMEG	M12-1523	218.00	221.00	460	7.44	7.44	3.42	3.00	540,216.94	6,987,930.70	63.20
WESMEG	M12-1524	123.10	130.22	650	3.86	3.86	7.83	7.12	538,627.61	6,988,234.90	58.45
WESMEG	M12-1526	16.50	20.00	480	0.30	0.30	3.39	3.50	540,056.08	6,987,784.28	63.03
WESMEG	M12-1526	32.40	36.40	480	0.89	0.89	3.88	4.00	540,056.08	6,987,784.28	63.03
WESMEG	M12-1526	71.00	74.50	460	0.82	0.82	3.41	3.50	540,056.08	6,987,784.28	63.03
WESMEG	M12-1526	121.15	136.95	450	1.67	1.67	15.51	15.80	540,056.08	6,987,784.28	63.03
WESMEG	M12-1526	167.00	171.00	440	2.05	2.05	3.93	4.00	540,056.08	6,987,784.28	63.03
WESMEG	M12-1531	27.40	30.60	625	15.38	15.38	3.57	3.20	540,166.98	6,987,952.09	63.25
WESMEG	M12-1531	36.00	39.45	600	0.91	0.91	3.85	3.45	540,166.98	6,987,952.09	63.25
WESMEG	M12-1531	44.00	47.50	520	0.83	0.83	3.92	3.50	540,166.98	6,987,952.09	63.25
WESMEG	M12-1533	43.80	46.60	480	0.66	0.66	3.13	2.80	539,947.11	6,987,834.65	63.63
WESMEG	M12-1533	52.00	55.00	480	0.22	0.22	3.35	3.00	539,947.11	6,987,834.65	63.63
WESMEG	M12-1533	75.50	78.60	460	0.90	0.90	3.48	3.10	539,947.11	6,987,834.65	63.63
WESMEG	M12-1533	87.40	90.50	455	0.80	0.80	3.48	3.10	539,947.11	6,987,834.65	63.63
WESMEG	M12-1533	153.00	158.00	450	2.34	2.34	5.63	5.00	539,947.11	6,987,834.65	63.63
WESMEG	M12-1533	203.00	207.30	440	1.99	1.99	4.84	4.30	539,947.11	6,987,834.65	63.63
WESMEG	M12-1533	216.00	222.00	435	2.46	2.46	6.76	6.00	539,947.11	6,987,834.65	63.63
WESMEG	M12-1534	104.70	108.10	650	0.97	0.97	3.77	3.40	538,678.08	6,988,203.75	58.53
WESMEG	M12-1536	52.00	55.10	660	1.02	1.02	3.44	3.10	540,157.04	6,988,023.82	63.54
WESMEG	M12-1536	59.40	62.40	650	1.11	1.11	3.33	3.00	540,157.04	6,988,023.82	63.54
WESMEG	M12-1536	87.40	90.60	625	0.11	0.11	3.56	3.20	540,157.04	6,988,023.82	63.54
WESMEG	M12-1536	110.50	114.00	600	3.08	3.08	3.91	3.50	540,157.04	6,988,023.82	63.54
WESMEG	M12-1536	229.70	232.80	490	2.02	2.02	3.50	3.10	540,157.04	6,988,023.82	63.54
WESMEG	M12-1536	285.10	289.60	480	1.57	1.57	5.11	4.50	540,157.04	6,988,023.82	63.54
WESMEG	M12-1538	47.70	54.90	650	3.24	3.24	7.92	7.20	538,679.88	6,988,140.50	58.89
WESMEG	M12-1544	36.00	39.00	480	0.98	0.98	3.28	3.00	539,916.86	6,987,845.79	63.26
WESMEG	M12-1544	53.00	56.00	480	1.57	1.57	3.29	3.00	539,916.86	6,987,845.79	63.26
WESMEG	M12-1544	74.10	82.00	460	1.74	1.74	8.71	7.90	539,916.86	6,987,845.79	63.26
WESMEG	M12-1544	90.00	94.35	455	5.19	5.19	4.80	4.35	539,916.86	6,987,845.79	63.26
WESMEG	M12-1544	165.00	168.45	450	5.05	5.05	3.84	3.45	539,916.86	6,987,845.79	63.26
WESMEG	M12-1544	212.00	214.70	440	1.02	1.02	3.02	2.70	539,916.86	6,987,845.79	63.26
WESMEG	M12-1544	225.95	230.00	435	1.03	1.03	4.53	4.05	539,916.86	6,987,845.79	63.26
WESMEG	M12-1545	186.00	190.50	650	2.32	2.32	4.96	4.50	538,327.27	6,988,359.96	58.37
WESMEG	M12-1549	37.70	40.80	650	19.43	19.43	3.45	3.10	540,067.02	6,988,022.64	64.21
WESMEG	M12-1549	100.30	103.30	600	0.06	0.06	3.39	3.00	540,067.02	6,988,022.64	64.21
WESMEG	M12-1549	120.00	123.00	510	0.21	0.21	3.40	3.00	540,067.02	6,988,022.64	64.21
WESMEG	M12-1549	167.40	170.80	500	0.55	0.55	3.87	3.40	540,067.02	6,988,022.64	64.21
WESMEG	M12-1549	243.00	246.00	480	1.02	1.02	3.43	3.00	540,067.02	6,988,022.64	64.21
WESMEG	M12-1549	257.00	261.00	480	2.00	2.00	4.58	4.00	540,067.02	6,988,022.64	64.21
WESMEG	M12-1549	269.70	275.80	460	1.82	1.82	6.98	6.10	540,067.02	6,988,022.64	64.21
WESMEG	M12-1549	321.20	327.00	450	1.57	1.57	6.64	5.80	540,067.02	6,988,022.64	64.21
WESMEG	M12-1550	210.00	212.80	430	1.39	1.39	3.16	2.80	540,698.13	6,987,783.13	63.89
WESMEG	M12-1553	63.80	66.60	500	1.53	1.53	3.09	2.80	539,797.99	6,987,951.66	65.59
WESMEG	M12-1553	163.00	166.30	455	0.27	0.27	3.67	3.30	539,797.99	6,987,951.66	65.59
WESMEG	M12-1553	242.50	245.60	450	1.52	1.52	3.46	3.10	539,797.99	6,987,951.66	65.59
WESMEG	M12-1553	307.50	311.00	440	2.00	2.00	3.91	3.50	539,797.99	6,987,951.66	65.59
WESMEG	M12-1568	13.00	23.40	650	2.32	2.32	11.51	10.40	539,857.28	6,988,026.70	68.87
WESMEG	M12-1570	36.00	39.00	600	1.12	1.12	3.35	3.00	540,066.89	6,987,945.36	64.15
WESMEG	M12-1570	49.00	52.00	520	1.52	1.52	3.36	3.00	540,066.89	6,987,945.36	64.15
WESMEG	M12-1570	57.40	60.50	510	0.64	0.64	3.47	3.10	540,066.89	6,987,945.36	64.15
WESMEG	M12-1576	324.50	327.60	650	1.39	1.39	3.50	3.10	538,625.01	6,988,464.02	60.94
WESMEG	M12-1577	21.50	25.00	650	1.62	1.62	3.91	3.50	540,547.34	6,987,934.36	64.44
WESMEG	M12-1577	32.00	46.00	625	1.29	1.29	15.68	14.00	540,547.34	6,987,934.36	64.44
WESMEG	M12-1577	53.50	65.70	600	5.98	5.98	13.70	12.20	540,547.34	6,987,934.36	64.44
WESMEG	M12-1577	92.40	96.00	520	0.93	0.93	4.06	3.60	540,547.34	6,987,934.36	64.44
WESMEG	M12-1579	133.00	140.20	500	1.37	1.37	8.07	7.20	539,798.19	6,988,025.32	68.47
WESMEG	M12-1579	230.25	234.00	455	2.56	2.56	4.24	3.75	539,798.19	6,988,025.32	68.47

WESMEG	M12-1582	179.30	182.30	660	0.16	0.16	3.38	3.00	540,696.88	6,988,143.55	66.61
WESMEG	M12-1582	192.30	196.00	710	5.01	5.01	4.17	3.70	540,696.88	6,988,143.55	66.61
WESMEG	M12-1582	291.00	294.00	600	0.84	0.84	3.41	3.00	540,696.88	6,988,143.55	66.61
WESMEG	M12-1586	33.80	36.90	480	0.80	0.80	3.42	3.10	539,689.63	6,987,907.72	64.45
WESMEG	M12-1586	267.00	269.60	440	0.03	0.03	2.93	2.60	539,689.63	6,987,907.72	64.45
WESMEG	M12-1594	273.50	276.50	660	0.35	0.35	3.36	3.00	540,731.32	6,988,231.32	69.22
WESMEG	M12-1594	278.80	289.00	710	0.92	0.92	11.44	10.20	540,731.32	6,988,231.32	69.22
WESMEG	M12-1595	44.90	52.20	480	0.99	0.99	7.94	7.30	539,616.97	6,987,920.00	63.05
WESMEG	M12-1597	432.00	435.00	650	2.32	2.32	3.25	3.00	538,799.88	6,988,525.77	65.09
WESMEG	M12-1605	113.70	117.80	650	1.73	1.73	4.39	4.10	538,359.53	6,988,274.18	57.95
WESMEG	M12-1621	474.00	477.00	650	0.43	0.43	3.26	3.00	538,924.60	6,988,550.23	68.05
WESMEG	M12-1651	140.20	143.30	650	2.15	2.15	3.44	3.10	538,424.98	6,988,289.92	57.99
WESMEG	M12-1684	298.90	302.30	650	4.38	4.38	3.67	3.40	538,449.75	6,988,450.29	59.31
WESMEG	M12-1691	47.00	50.00	230	3.87	3.87	3.36	3.00	542,137.37	6,987,503.78	63.48
WESMEG	M12-1694	250.00	253.00	650	1.45	1.45	3.36	3.00	538,700.08	6,988,358.66	60.85
WESMEG	M12-1698	17.00	20.00	250	0.64	0.64	3.33	3.00	542,200.09	6,987,537.07	63.33
WESMEG	M12-1698	57.90	60.50	230	3.31	3.31	2.92	2.60	542,200.09	6,987,537.07	63.33
WESMEG	M12-1701	440.90	444.00	650	0.10	0.10	3.28	3.10	538,700.22	6,988,528.76	64.97
WESMEG	M12-1703	6.50	9.40	250	4.78	4.78	3.16	2.90	542,074.17	6,987,536.94	63.35
WESMEG	M12-1703	29.40	32.10	235	14.53	64.98	2.94	2.70	542,074.17	6,987,536.94	63.35
WESMEG	M12-1703	45.50	48.50	240	0.93	0.93	3.27	3.00	542,074.17	6,987,536.94	63.35
WESMEG	M12-1708	127.00	130.00	670	0.27	0.27	3.38	3.00	540,457.08	6,988,099.25	65.51
WESMEG	M12-1708	150.00	159.40	650	1.10	1.10	10.63	9.40	540,457.08	6,988,099.25	65.51
WESMEG	M12-1708	173.90	187.00	625	2.38	2.38	14.83	13.10	540,457.08	6,988,099.25	65.51
WESMEG	M12-1708	203.60	214.50	600	0.69	0.69	12.36	10.90	540,457.08	6,988,099.25	65.51
WESMEG	M12-1708	241.50	244.50	520	0.59	0.59	3.40	3.00	540,457.08	6,988,099.25	65.51
WESMEG	M12-1709A	286.40	289.90	650	3.83	3.83	3.84	3.50	538,774.96	6,988,385.23	67.87
WESMEG	M12-1713	216.00	218.60	225	1.00	1.00	2.92	2.60	542,317.38	6,987,649.63	67.87
WESMEG	M12-1716	74.40	77.80	500	-	-	3.82	3.40	540,126.99	6,987,902.02	62.84
WESMEG	M12-1721	459.00	462.20	660	3.00	3.00	3.46	3.20	540,250.06	6,988,439.18	66.03
WESMEG	M12-1725	551.60	554.90	650	0.59	0.59	3.48	3.30	539,025.02	6,988,614.65	73.98
WESMEG	M12-1730	525.00	528.00	670	6.63	6.63	3.30	3.00	540,095.39	6,988,546.07	67.69
WESMEG	M12-1730	563.80	578.00	625	1.75	1.75	15.71	14.20	540,095.39	6,988,546.07	67.69
WESMEG	M12-1730	599.10	603.00	600	1.19	1.19	4.32	3.90	540,095.39	6,988,546.07	67.69
WESMEG	M12-1756	506.10	508.80	660	0.72	0.72	3.07	2.70	540,175.19	6,988,512.32	66.34
WESMEG	M12-1759	666.00	669.00	650	3.58	3.58	3.36	3.00	539,180.06	6,988,740.08	68.15
WESMEG	M12-1765	544.40	547.60	650	0.09	0.09	3.42	3.20	538,925.04	6,988,608.39	70.68
WESMEG	M12-1767	670.90	675.10	650	11.34	11.63	4.48	4.20	539,075.06	6,988,724.65	65.47
WESMEG	M12-1772A	772.80	776.60	650	4.58	4.58	4.04	3.80	538,910.06	6,988,810.58	64.87
WESMEG	M12-1774	412.30	415.40	650	0.83	0.83	3.32	3.10	538,924.96	6,988,486.57	66.48
WESMEG	M12-1774	493.00	496.00	510	2.03	2.03	3.24	3.00	538,924.96	6,988,486.57	66.48
WESMEG	M12-1775	620.00	626.00	650	13.44	13.44	6.83	6.00	539,180.00	6,988,739.69	68.20
WESMEG	M12-1778	311.00	314.10	650	0.35	0.35	3.48	3.10	538,949.94	6,988,406.96	65.86
WESMEG	M12-1778	399.50	402.20	510	3.37	3.37	3.05	2.70	538,949.94	6,988,406.96	65.86
WESMEG	M12-1783	225.50	231.30	650	2.26	2.26	6.53	5.80	539,092.08	6,988,316.35	66.79
WESMEG	M12-1787	717.40	720.80	650	1.61	1.61	3.73	3.40	539,355.14	6,988,756.75	78.12
WESMEG	M12-1788	292.20	295.40	650	2.68	2.68	3.57	3.20	538,875.33	6,988,382.40	67.16
WESMEG	M12-1793	181.30	184.50	650	1.81	1.81	3.47	3.20	539,000.23	6,988,249.02	70.92
WESMEG	M12-1794	209.70	216.00	650	9.38	10.24	7.07	6.30	539,227.25	6,988,304.79	71.33
WESMEG	M12-1794	319.60	322.70	510	1.83	1.83	3.50	3.10	539,227.25	6,988,304.79	71.33
WESMEG	M12-1797	522.50	525.60	650	0.56	0.56	3.23	3.10	538,989.77	6,988,564.08	71.72
WESMEG	M12-1798	226.40	229.30	650	0.03	0.03	3.25	2.90	539,407.28	6,988,279.52	74.09
WESMEG	M12-1798	309.00	312.80	510	1.85	1.85	4.28	3.80	539,407.28	6,988,279.52	74.09
WESMEG	M12-1799	675.00	678.00	650	0.54	0.54	3.30	3.00	539,130.05	6,988,745.38	65.70
WESMEG	M12-1800	522.80	525.80	650	0.49	0.49	3.32	3.00	538,650.08	6,988,649.30	65.44
WESMEG	M12-1805	334.10	337.60	660	0.61	0.61	3.95	3.50	539,889.30	6,988,383.84	68.69
WESMEG	M12-1805	342.90	346.70	650	1.90	1.90	4.29	3.80	539,889.30	6,988,383.84	68.69
WESMEG	M12-1806	322.20	326.60	650	5.65	5.65	4.95	4.40	539,648.09	6,988,352.89	78.56
WESMEG	M12-1806	382.50	387.00	520	0.09	0.09	5.08	4.50	539,648.09	6,988,352.89	78.56
WESMEG	M12-1809	567.90	571.50	650	0.77	0.77	3.28	3.60	539,168.59	6,988,514.68	74.51
WESMEG	M12-1813	253.00	257.00	660	1.98	1.98	4.46	4.00	539,829.35	6,988,292.99	72.01
WESMEG	M12-1813	261.00	266.00	650	3.15	3.15	5.58	5.00	539,829.35	6,988,292.99	72.01
WESMEG	M12-1814	329.60	332.80	670	0.57	0.57	3.61	3.20	540,129.20	6,988,369.81	65.27
WESMEG	M12-1814	352.60	355.70	650	4.08	4.08	3.51	3.10	540,129.20	6,988,369.81	65.27
WESMEG	M12-1814	408.00	410.60	625	1.29	1.29	2.96	2.60	540,129.20	6,988,369.81	65.27
WESMEG	M12-1814	424.40	427.40	600	7.49	7.49	3.41	3.00	540,129.20	6,988,369.81	65.27
WESMEG	M12-1818	212.50	216.00	660	0.58	0.58	3.92	3.50	540,009.21	6,988,238.26	66.58
WESMEG	M12-1818	228.00	230.80	650	1.72	1.72	3.15	2.80	540,009.21	6,988,238.26	66.58
WESMEG	M12-1821	245.50	248.50	670	1.12	1.12	3.45	3.00	540,129.29	6,988,276.14	64.50
WESMEG	M12-1821	263.70	266.10	650	1.15	1.15	2.76	2.40	540,129.29	6,988,276.14	64.50
WESMEG	M12-1821	305.40	308.30	625	1.58	1.58	3.34	2.90	540,129.29	6,988,276.14	64.50
WESMEG	M12-1822	402.00	405.70	650	1.56	1.56	4.23	3.70	540,429.37	6,988,372.23	66.50
WESMEG	M12-1822	429.30	432.60	625	2.31	2.31	3.77	3.30	540,429.37	6,988,372.23	66.50
WESMEG	M12-1822	437.00	441.00	600	5.99	5.99	4.57	4.00	540,429.37	6,988,372.23	66.50
WESMEG	M12-1823	360.90	363.90	650	0.86	0.86	3.28	3.00	538,800.02	6,988,457.94	65.94
WESMEG	M12-1826	317.80	320.50	650	11.68	11.68	3.06	2.70	540,310.25	6,988,288.89	66.66
WESMEG	M12-1826	343.40	346.50	625	0.97	0.97	3.52	3.10	540,310.25	6,988,288.89	66.66
WESMEG	M12-1826	357.00	360.80	600	7.33	7.33	4.31	3.80	540,310.25	6,988,288.89	66.66
WESMEG	M12-1828	489.80	493.80	650	2.20	2.20	4.34	4.00	539,291.78	6,988,563.55	68.87
WESMEG	M12-1831	522.00	525.80	650	1.43	1.43	4.10	3.80	538,804.93	6,988,599.62	65.65
WESMEG	M12-1834	386.00	391.90	670	4.14	4.14	5.92	5.90	540,611.22	6,988,306.17	68.18
WESMEG	M12-1835	326.50	329.60	650	4.07	4.07	3.31	3.10	539,104.12	6,988,397.23	70.23
WESMEG	M12-1840	262.20	267.00	650	4.36	4.36	5.05	4.80	539,208.11	6,988,342.04	71.96
WESMEG	M12-1840	374.20	377.30	510	1.46	1.46	3.31	3.10	539,208.11	6,988,342.04	71.96
WESMEG	M12-1841	597.40	602.50	650	3.79	3.79	5.22	5.10	539,020.01	6,988,617.04	72.22
WESMEG	M12-1843	314.40	319.40	650	0.87	0.87	5.03	5.00	540,357.07	6,988,241.23	66.46
WESMEG	M12-1843	346.50	349.10	625	1.89	1.89	2.65	2.60	540,357.07	6,988,241.23	66.46
WESMEG	M12-1843	375.90	386.90	600	5.11	5.11	11.37	11.00	540,357.07	6,988,241.23	66.46
WESMEG	M12-1845	142.80	146.40	225	-	-	4.05	3.60	542,377.09	6,987,554.64	65.59
WESMEG	M12-1846	529.00	532.60	650	4.50	4.50	3.67	3.60	538,705.04	6,988,585.15	65.02

WESMEG	M12-1849	84.00	86.80	280	4.93	4.93	3.12	2.80	542,197.06	6,987,649.32	65.73
WESMEG	M12-1849	136.50	139.30	240	-	-	3.13	2.80	542,197.06	6,987,649.32	65.73
WESMEG	M12-1849	157.70	163.50	230	-	-	6.50	5.80	542,197.06	6,987,649.32	65.73
WESMEG	M12-1849	198.00	201.30	225	0.05	0.05	3.71	3.30	542,197.06	6,987,649.32	65.73
WESMEG	M12-1852	391.20	395.40	650	11.10	11.10	4.32	4.20	539,198.16	6,988,448.48	76.11
WESMEG	M12-1852	499.30	502.20	510	6.95	6.95	3.06	2.90	539,198.16	6,988,448.48	76.11
WESMEG	M12-1855	45.00	47.90	280	1.15	1.15	3.13	2.90	542,073.89	6,987,618.80	64.17
WESMEG	M12-1855	78.80	81.80	250	0.03	0.03	3.26	3.00	542,073.89	6,987,618.80	64.17
WESMEG	M12-1855	97.30	99.70	235	-	-	2.62	2.40	542,073.89	6,987,618.80	64.17
WESMEG	M12-1856	386.50	389.40	650	0.87	0.87	3.27	2.90	539,700.24	6,988,431.00	73.85
WESMEG	M12-1857	264.90	267.70	225	-	-	3.01	2.80	542,136.97	6,987,704.62	65.50
WESMEG	M12-1861	611.00	614.30	650	2.35	2.35	3.29	3.30	538,927.05	6,988,618.94	71.15
WESMEG	M12-1864	446.70	452.50	650	4.73	4.73	5.97	5.80	539,700.27	6,988,431.82	73.83
WESMEG	M12-1865	254.00	257.00	650	1.04	1.04	3.37	3.00	539,708.06	6,988,283.07	80.16
WESMEG	M12-1866	148.50	152.60	250	2.41	2.41	4.35	4.10	542,074.04	6,987,701.35	64.52
WESMEG	M12-1866	252.50	255.70	225	6.28	6.28	3.46	3.20	542,074.04	6,987,701.35	64.52
WESMEG	M12-1867	396.80	401.40	650	1.42	1.42	4.78	4.60	538,521.76	6,988,512.85	60.06
WESMEG	M12-1868	209.00	214.20	650	0.93	0.93	5.69	5.20	539,587.96	6,988,231.89	73.64
WESMEG	M12-1868	274.60	277.50	520	1.91	1.91	3.20	2.90	539,587.96	6,988,231.89	73.64
WESMEG	M12-1869	304.70	308.10	660	0.33	0.33	3.75	3.40	539,999.92	6,988,336.97	65.53
WESMEG	M12-1869	315.50	319.70	650	2.46	2.46	4.64	4.20	539,999.92	6,988,336.97	65.53
WESMEG	M12-1870	318.50	321.60	650	1.13	1.13	3.48	3.10	539,768.04	6,988,352.42	72.98
WESMEG	M12-1870	410.30	413.10	510	2.24	2.24	3.17	2.80	539,768.04	6,988,352.42	72.98
WESMEG	M12-1871	419.90	425.30	650	1.58	1.58	6.11	5.40	539,650.01	6,988,461.60	75.97
WESMEG	M12-1871	479.50	490.50	520	7.61	7.61	12.52	11.00	539,650.01	6,988,461.60	75.97
WESMEG	M12-1871	505.00	508.80	510	2.73	2.73	4.33	3.80	539,650.01	6,988,461.60	75.97
WESMEG	M12-1872	150.10	155.50	650	2.30	2.30	6.05	5.40	540,043.97	6,988,151.99	64.49
WESMEG	M12-1872	210.00	212.80	600	0.27	0.27	3.16	2.80	540,043.97	6,988,151.99	64.49
WESMEG	M12-1872	238.90	241.50	510	18.85	39.62	2.94	2.60	540,043.97	6,988,151.99	64.49
WESMEG	M12-1873	363.30	368.00	650	3.36	3.36	5.18	4.70	539,332.03	6,988,445.65	72.49
WESMEG	M12-1874	56.00	59.00	280	9.24	9.24	3.23	3.00	542,011.01	6,987,626.42	64.03
WESMEG	M12-1874	73.50	76.50	250	0.03	0.03	3.24	3.00	542,011.01	6,987,626.42	64.03
WESMEG	M12-1874	141.00	143.30	230	0.25	0.25	2.51	2.30	542,011.01	6,987,626.42	64.03
WESMEG	M12-1875	413.00	416.60	650	0.78	0.78	3.55	3.60	538,608.00	6,988,480.65	61.18
WESMEG	M12-1876	349.00	354.70	660	2.42	2.42	6.38	5.70	540,250.06	6,988,335.45	66.42
WESMEG	M12-1876	363.00	365.10	650	0.73	0.73	2.35	2.10	540,250.06	6,988,335.45	66.42
WESMEG	M12-1876	376.50	379.80	625	0.67	0.67	3.70	3.30	540,250.06	6,988,335.45	66.42
WESMEG	M12-1876	393.90	396.80	600	0.66	0.66	3.25	2.90	540,250.06	6,988,335.45	66.42
WESMEG	M12-1877	431.00	433.60	650	1.15	1.15	2.94	2.60	539,749.90	6,988,475.00	71.30
WESMEG	M12-1878	42.50	45.60	280	1.44	1.44	3.24	3.10	541,946.07	6,987,612.41	63.67
WESMEG	M12-1878	144.50	147.50	230	2.95	2.95	3.21	3.00	541,946.07	6,987,612.41	63.67
WESMEG	M12-1879	215.60	221.50	650	1.26	1.26	6.68	5.90	539,647.94	6,988,247.17	78.11
WESMEG	M12-1880	243.30	246.70	650	2.03	2.03	3.58	3.40	539,149.92	6,988,309.85	67.35
WESMEG	M12-1880	346.60	349.40	510	3.13	3.13	3.00	2.80	539,149.92	6,988,309.85	67.35
WESMEG	M12-1881	217.30	220.50	650	0.29	0.29	3.53	3.20	539,499.98	6,988,260.19	73.98
WESMEG	M12-1881	284.60	293.50	520	2.34	2.34	9.92	8.90	539,499.98	6,988,260.19	73.98
WESMEG	M12-1881	296.00	299.10	510	1.61	1.61	3.46	3.10	539,499.98	6,988,260.19	73.98
WESMEG	M12-1882	293.50	296.20	650	2.13	2.13	2.96	2.70	539,309.95	6,988,374.41	77.02
WESMEG	M12-1883	300.10	303.20	650	4.91	4.91	3.51	3.10	539,022.00	6,988,393.51	67.16
WESMEG	M12-1884	181.20	184.10	650	4.26	4.26	3.21	2.90	539,310.00	6,988,246.67	72.19
WESMEG	M12-1885	354.60	357.60	650	8.91	8.91	3.26	3.00	539,469.91	6,988,399.29	75.71
WESMEG	M12-1886	344.30	349.20	650	3.03	3.03	5.52	4.90	539,594.99	6,988,384.22	78.61
WESMEG	M13-1893	106.00	109.10	650	0.06	0.06	3.33	3.10	538,400.01	6,988,255.32	57.94
WESMEG	M13-1897	45.70	49.70	650	1.06	1.06	4.40	4.00	538,419.94	6,988,188.44	57.99
WESMEG	M13-1900	24.60	27.50	650	0.80	0.80	3.21	2.90	538,479.80	6,988,160.55	58.05
WESMEG	M13-1901	69.40	72.40	650	4.58	4.58	3.35	3.00	538,480.13	6,988,210.54	57.97
WESMEG	M13-1903	58.60	61.70	510	0.83	0.83	3.46	3.10	539,399.89	6,988,005.66	63.52
WESMEG	M13-1903	124.60	128.80	460	2.12	2.12	4.72	4.20	539,399.89	6,988,005.66	63.52
WESMEG	M13-1906	128.90	132.30	650	1.91	1.91	3.66	3.40	538,499.92	6,988,264.69	57.89
WESMEG	M13-1907	59.80	62.60	510	0.33	0.33	3.14	2.80	539,309.78	6,988,011.04	66.28
WESMEG	M13-1908	247.80	253.90	650	9.68	12.39	6.70	6.10	538,599.78	6,988,370.02	60.06
WESMEG	M13-1909	113.00	117.80	670	0.72	0.72	5.16	4.80	540,360.06	6,988,074.14	64.18
WESMEG	M13-1909	123.00	126.00	650	2.17	2.17	3.23	3.00	540,360.06	6,988,074.14	64.18
WESMEG	M13-1909	157.00	160.20	625	1.24	1.24	3.49	3.20	540,360.06	6,988,074.14	64.18
WESMEG	M13-1909	162.60	176.10	600	4.66	4.66	14.73	13.50	540,360.06	6,988,074.14	64.18
WESMEG	M13-1912	54.00	59.10	650	3.74	3.74	5.72	5.10	539,335.98	6,988,100.03	64.78
WESMEG	M13-1913	35.40	39.00	650	9.12	9.12	3.89	3.60	539,223.82	6,988,093.87	67.65
WESMEG	M13-1915	151.70	156.70	650	9.50	9.50	5.64	5.00	539,199.58	6,988,240.95	65.82
WESMEG	M13-1919	161.90	171.00	650	2.82	2.82	10.18	9.10	539,249.67	6,988,245.34	66.36
WESMEG	M13-1922	245.70	248.80	660	2.52	2.52	3.50	3.10	540,674.95	6,988,208.66	68.03
WESMEG	M13-1922	256.20	262.50	710	1.13	1.13	7.13	6.30	540,674.95	6,988,208.66	68.03
WESMEG	M13-1923	229.50	236.30	650	7.14	7.14	7.43	6.80	539,274.91	6,988,312.17	72.90
WESMEG	M13-1931	327.40	335.20	650	13.98	13.98	8.55	7.80	539,274.55	6,988,427.45	75.35
WESMEG	M13-1940	501.20	504.40	650	6.87	6.87	3.41	3.20	539,266.17	6,988,554.38	68.53
WESMEG	M13-1941	207.50	210.70	740	0.87	0.87	3.59	3.20	540,949.90	6,988,204.77	67.89
WESMEG	M13-1963	435.00	438.40	650	2.69	2.69	3.80	3.40	539,800.03	6,988,473.27	69.58
WESMEG	M13-1966	377.35	380.40	650	5.91	5.91	3.38	3.05	538,864.90	6,988,470.26	65.47
WESMEG	M13-1972	468.00	473.00	650	4.37	4.37	5.54	5.00	539,749.70	6,988,490.35	70.71
WESMEG	M13-1980	165.00	168.00	320	0.03	0.03	3.32	3.00	541,667.20	6,987,871.21	64.71
WESMEG	M13-1980	217.00	220.20	300	5.84	5.84	3.55	3.20	541,667.20	6,987,871.21	64.71
WESMEG	M13-1986	157.70	160.80	320	4.65	4.65	3.11	3.10	541,714.14	6,987,845.36	64.75
WESMEG	M13-1995	29.10	31.80	280	1.70	1.70	3.00	2.70	542,034.19	6,987,602.92	63.80
WESMEG	M13-1995	55.70	58.50	250	-	-	3.13	2.80	542,034.19	6,987,602.92	63.80
WESMEG	M13-1995	84.30	87.00	235	3.34	3.34	3.03	2.70	542,034.19	6,987,602.92	63.80
WESMEG	M13-1995	136.10	138.80	230	2.15	2.15	3.06	2.70	542,034.19	6,987,602.92	63.80
WESMEG	M13-1996	80.30	83.30	650	2.87	2.87	3.28	3.00	538,299.91	6,988,266.49	57.97
WESMEG	M13-1998	95.80	99.10	650	5.97	5.97	3.60	3.30	538,324.86	6,988,261.67	57.96
WESMEG	M13-2002	30.00	33.00	250	2.11	2.11	3.32	3.00	542,138.60	6,987,558.70	63.04
WESMEG	M13-2002	47.90	50.70	235	-	-	3.11	2.80	542,138.60	6,987,558.70	63.04
WESMEG	M13-2002	71.00	74.00	240	5.09	5.09	3.34	3.00	542,138.60	6,987,558.70	63.04

WESMEG	M13-2002	91.60	94.20	230	-	-	2.90	2.60	542,138.60	6,987,558.70	63.04
WESMEG	M13-2014	107.50	111.30	650	3.32	3.32	4.16	3.80	538,422.98	6,988,257.40	58.02
WESMEG	M13-2019	90.00	93.00	650	13.19	13.19	3.25	3.00	538,360.81	6,988,251.97	57.91
WESMEG	M13-2026	123.40	126.50	650	0.61	0.61	3.42	3.10	538,330.02	6,988,296.38	58.02
WESMEG	M13-2078	459.00	462.20	650	11.00	11.00	3.42	3.20	539,400.12	6,988,513.16	75.71
WESMEG	M13-2097A	419.60	426.50	650	3.36	3.36	7.56	6.90	539,500.06	6,988,465.06	76.96
WESMEG	M13-2097A	492.00	495.00	520	1.76	1.76	3.31	3.00	539,500.06	6,988,465.06	76.96
WESMEG	M13-2098	89.80	96.70	650	2.55	2.55	7.44	6.90	539,166.53	6,988,168.01	65.43
WESMEG	M13-2101	98.20	103.80	650	7.85	7.85	6.21	5.60	539,209.95	6,988,172.04	65.60
WESMEG	M13-2103	94.40	98.00	650	7.08	7.08	3.87	3.60	539,263.03	6,988,160.23	65.70
WESMEG	M13-2105	46.00	49.20	650	5.37	5.37	3.52	3.20	539,276.89	6,988,100.03	64.34
WESMEG	M13-2109	109.00	113.00	650	1.22	1.22	3.39	4.00	539,050.04	6,988,149.62	71.79
WESMEG	M13-2111	77.20	80.40	650	0.53	0.53	3.62	3.20	539,050.04	6,988,148.49	71.65
WESMEG	M13-2112	403.70	408.70	650	0.79	0.79	5.38	5.00	539,599.89	6,988,422.69	78.08
WESMEG	M13-2113	79.00	81.90	650	2.12	2.12	3.06	2.90	539,103.05	6,988,146.01	72.80
WESMEG	M13-2118	49.70	52.70	650	1.02	1.02	3.35	3.00	538,999.91	6,988,114.07	67.54
WESMEG	M13-2120	41.00	50.00	650	4.19	4.19	9.76	9.00	539,165.05	6,988,104.99	73.89
WESMEG	M13-2125	565.50	568.50	650	8.02	8.02	3.38	3.00	539,465.75	6,988,645.88	77.34
WESMEG	M13-2126	459.50	462.50	660	0.81	0.81	3.38	3.00	539,861.85	6,988,499.59	68.12
WESMEG	M13-2126	476.00	481.00	650	1.47	1.47	5.66	5.00	539,861.85	6,988,499.59	68.12
WESMEG	M14-2221	97.40	100.50	650	1.18	1.18	3.39	3.10	539,325.06	6,988,143.46	65.91
WESMEG	M14-2223	76.20	80.40	650	2.42	2.42	4.62	4.20	539,289.82	6,988,133.23	64.64
WESMEG	M14-2225	75.40	82.40	650	4.44	4.44	6.82	7.00	539,234.64	6,988,133.52	64.17
WESMEG	M14-2226	65.30	70.70	650	12.51	12.51	5.92	5.40	539,194.84	6,988,132.82	66.22
WESMEG	M14-2227A	122.00	128.30	650	6.21	6.21	6.87	6.30	539,245.76	6,988,195.00	65.60
WESMEG	M14-2231	124.00	128.00	650	4.07	4.07	4.33	4.00	539,213.71	6,988,200.21	65.49
WESMEG	M14-2233	160.00	162.90	650	10.97	10.97	3.15	2.90	539,162.78	6,988,242.05	65.78
WESMEG	M14-2235	116.70	119.80	650	2.89	2.89	3.39	3.10	539,163.75	6,988,197.33	65.76
WESMEG	M14-2237	202.20	204.50	650	1.62	1.62	2.58	2.30	539,164.10	6,988,293.22	66.94
WESMEG	M14-2245	175.00	178.60	650	7.86	7.86	3.96	3.60	539,203.18	6,988,264.04	66.63
WESMEG	M14-2249	201.00	204.80	650	10.86	10.86	4.16	3.80	539,284.24	6,988,279.81	72.09
WESMEG	M14-2250	14.50	17.70	440	2.51	2.51	2.58	3.20	539,803.89	6,987,606.51	61.89
WESMEG	M14-2250	25.70	29.20	435	1.56	1.56	2.84	3.50	539,803.89	6,987,606.51	61.89
WESMEG	M14-2252	168.80	171.30	650	7.83	7.83	2.78	2.50	539,324.12	6,988,225.95	71.41
WESMEG	M14-2253	154.70	159.40	650	6.84	6.84	5.09	4.70	539,284.19	6,988,223.07	67.70
WESMEG	M14-2254	68.50	71.90	650	13.39	13.39	3.73	3.40	538,340.23	6,988,229.54	57.79
WESMEG	M14-2255	132.90	136.00	650	9.70	9.70	3.39	3.10	539,290.67	6,988,201.84	67.13
WESMEG	M14-2256	74.00	76.80	650	0.25	0.25	3.09	2.80	538,380.23	6,988,223.16	57.62
WESMEG	M14-2257	602.40	605.80	660	2.52	2.52	3.70	3.40	539,910.18	6,988,580.93	66.71
WESMEG	M14-2258	76.50	79.50	650	0.80	0.80	3.28	3.00	538,419.80	6,988,226.08	57.86
WESMEG	M14-2259	67.00	73.80	650	4.28	4.28	5.25	6.80	539,125.80	6,988,118.86	72.80
WESMEG	M14-2260	109.40	116.70	650	1.61	1.61	8.03	7.30	538,580.16	6,988,229.31	58.18
WESMEG	M14-2262	140.60	143.50	650	0.65	0.65	3.19	2.90	539,095.13	6,988,222.60	66.05
WESMEG	M14-2263	165.90	168.70	650	8.18	8.18	3.11	2.80	538,619.92	6,988,279.48	58.45
WESMEG	M14-2265	218.40	221.50	650	2.08	2.08	3.39	3.10	538,575.62	6,988,337.20	59.28
WESMEG	M14-2266	247.50	253.00	650	2.20	2.20	6.09	5.50	538,536.31	6,988,384.88	60.14
WESMEG	M14-2269	236.20	242.40	650	9.43	11.13	6.95	6.20	538,496.81	6,988,386.02	59.58
WESMEG	M14-2272	327.00	329.90	650	0.28	0.28	3.20	2.90	538,640.00	6,988,443.80	61.02
WESMEG	M14-2309	579.50	582.20	650	1.48	1.48	2.95	2.70	539,545.19	6,988,580.72	77.01
WOLF	M11-1218	67.50	70.50	2130	0.43	0.43	3.05	3.00	535,540.42	6,988,971.76	62.35
WOLF	M11-1219	105.00	108.50	2130	0.04	0.04	3.54	3.50	535,555.84	6,989,008.23	59.28
WOLF	M11-1219	150.40	153.50	2115	1.59	1.59	3.15	3.10	535,555.84	6,989,008.23	59.28
WOLF	M11-1223A	53.40	56.30	2130	0.09	0.09	2.97	2.90	535,480.64	6,988,983.99	65.68
WOLF	M11-1226	67.20	71.00	2130	1.23	1.23	3.94	3.80	535,592.85	6,988,939.61	63.35
WOLF	M11-1229	111.90	115.50	2130	0.89	0.89	3.59	3.60	535,610.82	6,988,986.50	59.80
WOLF	M11-1229	153.50	157.00	2115	0.19	0.19	3.52	3.50	535,610.82	6,988,986.50	59.80
WOLF	M11-1231	68.80	72.00	2130	2.47	2.47	3.24	3.20	535,647.45	6,988,916.59	61.57
WOLF	M11-1231	111.85	122.00	2115	1.90	1.90	10.38	10.15	535,647.45	6,988,916.59	61.57
WOLF	M11-1231	127.00	129.80	2112	6.80	13.59	2.87	2.80	535,647.45	6,988,916.59	61.57
WOLF	M11-1233	118.00	122.00	2130	0.86	0.86	4.00	4.00	535,666.87	6,988,963.52	57.52
WOLF	M11-1233	161.10	166.70	2115	8.91	8.91	5.64	5.60	535,666.87	6,988,963.52	57.52
WOLF	M11-1233	176.10	179.30	2112	1.04	1.04	3.23	3.20	535,666.87	6,988,963.52	57.52
WOLF	M11-1235	64.10	66.80	2130	0.43	0.43	2.74	2.70	535,704.80	6,988,890.95	59.09
WOLF	M11-1235	106.80	110.00	2115	0.32	0.32	3.28	3.20	535,704.80	6,988,890.95	59.09
WOLF	M11-1235	116.30	120.70	2112	0.97	0.97	4.52	4.40	535,704.80	6,988,890.95	59.09
WOLF	M11-1238	81.80	84.50	2140	1.17	1.17	2.69	2.70	535,722.92	6,988,940.44	58.16
WOLF	M11-1238	115.50	118.30	2130	0.18	0.18	2.81	2.80	535,722.92	6,988,940.44	58.16
WOLF	M11-1238	155.90	158.90	2115	0.26	0.26	3.03	3.00	535,722.92	6,988,940.44	58.16
WOLF	M11-1238	163.90	167.00	2112	0.85	0.85	3.14	3.10	535,722.92	6,988,940.44	58.16
WOLF	M11-1243	38.00	41.15	2140	2.51	2.51	3.15	3.15	535,759.87	6,988,870.90	56.76
WOLF	M11-1243	52.00	55.00	2130	0.52	0.52	3.01	3.00	535,759.87	6,988,870.90	56.76
WOLF	M11-1243	105.00	108.00	2115	2.92	2.92	3.05	3.00	535,759.87	6,988,870.90	56.76
WOLF	M11-1243	109.85	113.00	2112	2.95	2.95	3.20	3.15	535,759.87	6,988,870.90	56.76
WOLF	M11-1244	81.00	84.40	2140	0.50	0.50	3.34	3.40	535,778.63	6,988,916.53	56.93
WOLF	M11-1244	99.90	104.40	2130	0.82	0.82	4.44	4.50	535,778.63	6,988,916.53	56.93
WOLF	M11-1244	149.50	153.70	2115	1.03	1.03	4.18	4.20	535,778.63	6,988,916.53	56.93
WOLF	M11-1244	168.80	173.90	2112	1.11	1.11	5.11	5.10	535,778.63	6,988,916.53	56.93
WOLF	M11-1247	262.50	265.50	2115	6.53	6.53	2.90	3.00	535,649.13	6,989,078.72	56.15
WOLF	M11-1249	267.80	271.90	2115	1.72	1.72	3.95	4.10	535,705.84	6,989,057.44	56.66
WOLF	M11-1249	285.90	293.00	2112	2.15	2.15	6.87	7.10	535,705.84	6,989,057.44	56.66
WOLF	M11-1254	192.50	195.50	2140	7.45	7.45	2.88	3.00	535,787.84	6,989,022.64	56.74
WOLF	M11-1254	229.00	232.50	2130	0.77	0.77	3.37	3.50	535,787.84	6,989,022.64	56.74
WOLF	M11-1254	271.00	274.30	2115	1.06	1.06	3.20	3.30	535,787.84	6,989,022.64	56.74
WOLF	M11-1254	281.70	285.40	2112	0.03	0.03	3.59	3.70	535,787.84	6,989,022.64	56.74
WOLF	M11-1258	234.00	238.60	2310	0.22	0.22	3.68	4.60	535,300.21	6,989,486.80	58.10
WOLF	M11-1258	540.00	545.50	2130	4.73	4.73	5.00	5.50	535,300.21	6,989,486.80	58.10
WOLF	M11-1258	557.70	578.20	2125	2.90	2.90	18.86	20.50	535,300.21	6,989,486.80	58.10
WOLF	M11-1261	74.00	78.80	2140	2.44	2.44	4.93	4.80	535,889.46	6,988,872.72	56.93
WOLF	M11-1261	120.00	123.00	2120	2.29	2.29	3.08	3.00	535,889.46	6,988,872.72	56.93
WOLF	M11-1264	220.00	223.90	2140	1.56	1.56	3.85	3.90	535,990.56	6,988,987.40	56.96

WOLF	M11-1264	255.00	262.10	2130	2.10	2.10	7.11	7.10	535,990.56	6,988,987.40	56.96
WOLF	M11-1264	275.00	279.00	2120	5.98	5.98	4.03	4.00	535,990.56	6,988,987.40	56.96
WOLF	M11-1275	261.00	264.30	2240	8.03	12.41	3.16	3.30	535,111.79	6,989,511.85	57.12
WOLF	M11-1275	408.80	412.45	2130	2.24	2.24	3.62	3.65	535,111.79	6,989,511.85	57.12
WOLF	M11-1275	430.40	433.65	2125	1.63	1.63	3.25	3.25	535,111.79	6,989,511.85	57.12
WOLF	M11-1276	45.40	49.00	2330	8.76	8.76	3.58	3.60	535,765.69	6,989,193.07	56.68
WOLF	M11-1276	69.30	72.90	2320	0.03	0.03	3.59	3.60	535,765.69	6,989,193.07	56.68
WOLF	M11-1276	362.50	365.40	2120	1.54	1.54	2.97	2.90	535,765.69	6,989,193.07	56.68
WOLF	M11-1283	146.50	149.50	2330	5.69	5.83	3.03	3.00	535,849.36	6,989,268.35	58.74
WOLF	M11-1283	171.00	174.00	2320	11.72	11.72	3.04	3.00	535,849.36	6,989,268.35	58.74
WOLF	M11-1283	185.50	189.00	2310	0.56	0.56	3.56	3.50	535,849.36	6,989,268.35	58.74
WOLF	M11-1283	209.00	213.00	2300	1.53	1.53	4.09	4.00	535,849.36	6,989,268.35	58.74
WOLF	M11-1284	154.90	158.00	2310	1.74	1.74	2.91	3.10	535,170.26	6,989,496.47	55.61
WOLF	M11-1284	258.00	261.00	2240	0.76	0.76	2.88	3.00	535,170.26	6,989,496.47	55.61
WOLF	M11-1284	404.00	409.00	2130	1.15	1.15	4.96	5.00	535,170.26	6,989,496.47	55.61
WOLF	M11-1284	431.40	434.80	2125	0.32	0.32	3.40	3.40	535,170.26	6,989,496.47	55.61
WOLF	M11-1292	185.30	189.00	2320	1.54	1.54	3.57	3.70	535,757.83	6,989,306.69	59.48
WOLF	M11-1292	203.30	207.80	2310	0.76	0.76	4.35	4.50	535,757.83	6,989,306.69	59.48
WOLF	M11-1292	223.50	228.00	2300	0.92	0.92	4.37	4.50	535,757.83	6,989,306.69	59.48
WOLF	M11-1292	488.80	492.00	2120	1.79	1.79	3.23	3.20	535,757.83	6,989,306.69	59.48
WOLF	M11-1295	248.30	259.00	2310	2.42	2.42	8.73	10.70	535,243.99	6,989,517.03	58.20
WOLF	M11-1295	536.60	543.00	2130	1.07	1.07	5.89	6.40	535,243.99	6,989,517.03	58.20
WOLF	M11-1295	556.50	560.30	2125	1.55	1.55	3.50	3.80	535,243.99	6,989,517.03	58.20
WOLF	M11-1303	76.80	80.00	2320	1.16	1.16	3.19	3.20	535,719.28	6,989,211.87	55.10
WOLF	M11-1303	367.50	370.50	2120	4.35	4.35	3.14	3.00	535,719.28	6,989,211.87	55.10
WOLF	M11-1309	156.80	160.50	2310	0.11	0.11	3.56	3.70	535,225.84	6,989,470.66	55.53
WOLF	M11-1309	412.10	415.50	2130	1.13	1.13	3.42	3.40	535,225.84	6,989,470.66	55.53
WOLF	M11-1309	429.00	432.00	2125	1.92	1.92	3.03	3.00	535,225.84	6,989,470.66	55.53
WOLF	M11-1309	434.30	442.50	2120	2.59	2.59	8.27	8.20	535,225.84	6,989,470.66	55.53
WOLF	M11-1313	162.40	166.30	2140	5.97	5.97	3.78	3.90	535,394.60	6,989,156.06	57.61
WOLF	M11-1313	170.00	174.00	2130	3.55	3.55	3.88	4.00	535,394.60	6,989,156.06	57.61
WOLF	M11-1313	229.00	232.60	2120	0.08	0.08	3.55	3.60	535,394.60	6,989,156.06	57.61
WOLF	M11-1313	249.80	253.60	2110	2.45	2.45	3.76	3.80	535,394.60	6,989,156.06	57.61
WOLF	M14-2261	286.20	290.00	2320	1.25	1.25	3.69	3.80	535,706.40	6,989,446.38	58.03
WOLF	M14-2268	342.70	347.10	2320	2.64	2.64	4.35	4.40	535,832.90	6,989,428.11	57.88
WOLF	M14-2268	351.00	355.60	2310	5.90	5.90	4.55	4.60	535,832.90	6,989,428.11	57.88
WOLF	M14-2268	383.30	387.00	2300	1.02	1.02	3.67	3.70	535,832.90	6,989,428.11	57.88
WOLF	M14-2287	215.50	220.40	2320	6.12	6.12	4.75	4.90	535,845.17	6,989,311.64	57.95
WOLF	M14-2287	240.80	244.50	2310	0.05	0.05	3.60	3.70	535,845.17	6,989,311.64	57.95
WOLF	M14-2287	264.00	267.80	2300	0.01	0.01	3.72	3.80	535,845.17	6,989,311.64	57.95
WOLF	M14-2292	278.60	285.30	2320	7.20	7.20	6.41	6.70	535,844.74	6,989,363.60	57.82
WOLF	M14-2292	289.60	298.30	2310	9.48	9.48	8.32	8.70	535,844.74	6,989,363.60	57.82
WOLF	M14-2292	321.00	324.80	2300	1.78	1.78	3.63	3.80	535,844.74	6,989,363.60	57.82
WOLF	M14-2314	63.20	66.90	2320	0.03	0.03	3.58	3.70	535,916.18	6,989,153.39	56.87
WOLF	M14-2324	326.60	330.60	2310	2.10	2.10	3.96	4.00	535,954.84	6,989,369.52	58.76
WOLF	M14-2326	285.00	288.50	2320	0.25	0.25	3.58	3.50	535,954.76	6,989,369.27	58.82
WOLF	M14-2326	296.00	300.80	2310	3.13	3.13	4.91	4.80	535,954.76	6,989,369.27	58.82
WOLF	M14-2329A	235.50	239.00	2320	2.29	2.29	3.61	3.50	535,972.93	6,989,308.25	58.83
WOLF	M14-2329A	245.00	248.40	2310	2.41	2.41	3.51	3.40	535,972.93	6,989,308.25	58.83
WOLF	M14-2332	256.90	260.40	2320	9.00	9.00	3.25	3.50	535,990.00	6,989,297.00	60.00
WOLF	M14-2332	272.90	276.50	2310	0.69	0.69	3.35	3.60	535,990.00	6,989,297.00	60.00
WOLF	M14-2334	232.90	236.30	2320	3.83	3.83	3.52	3.40	536,031.00	6,989,291.00	60.00
WOLF	M14-2335	270.90	274.70	2320	0.71	0.71	3.51	3.80	536,031.00	6,989,291.00	60.00
WOLF	M14-2335	291.80	295.60	2310	3.59	3.59	3.54	3.80	536,031.00	6,989,291.00	60.00

Appendix 13.1 - Summary of Mineral Processing and Metallurgical Testing

Lab. / Year / Project No.	Deposits	Metallurgical test work						
Lakefield Research 1997; LR5025	Tiriganiaq		√	√			√	√
Lakefield Research 1998; LR5195	Tiriganiaq; F zone	√	√	√	√			√
Lakefield Research 2001; LR10197-001	Pump; Wolf	√	√	√	√			√
SGS Lakefield Research 2006; 11166-001	Tiriganiaq		√	√				
SGS Lakefield Research 2007; 11166-002	Tiriganiaq	√	√	√			√	√
Resource Development inc. 2009;	Discovery	√	√	√				
Starkey & Associates inc. 2009;	Tiriganiaq; F zone	√						√
Outotec 2011; SE-1372-TR	Tiriganiaq; F zone				√			
SGS 2011; 12564-001	Tiriganiaq	√						
PMC 2011;	Tiriganiaq; F zone; Wesmeg							√
Knelson 2011;	Tiriganiaq; F zone; Wesmeg; Pump; Discovery		√					
Wardrop 2011; 1153470200	Grinding circuit simulation							√
Golder 2011; 11-1428-0011	Tiriganiaq				√			√
AEM Technical Services 2012;	Tiriganiaq; F zone; Wesmeg; Pump; Discovery; Wolf		√	√				
SGS Canada Inc. 2012; 12592-001	Tiriganiaq; F zone	√	√	√		√	√	
Eriez Magnetic 2012;	Tiriganiaq							√
FLSmidth 2012;	Tiriganiaq; F zone; Wesmeg; Pump; Discovery				√			
Starkey & Associates inc. 2012;	Tiriganiaq; F zone; Wesmeg; Pump; Discovery; Wolf	√						√
Contract Support Services 2012;	Grinding circuit simulation							√
AEM Technical Services 2013;	Tiriganiaq;			√				
EMSL Canada Inc. 2013a;	Tiriganiaq; Discovery							√
Orway Mineral Consultants 2013;	Grinding circuit simulation							√
SGS Canada Inc. 2013a; 12592-002	Tiriganiaq; F zone; Wesmeg; Pump; Discovery	√	√	√		√		√
FLSmidth Knelson 2013;	Gravity circuit simulation							√
Metso 2013;	Tiriganiaq	√						
Outotec 2013; 53835T1/T2	Tiriganiaq				√			
BBA 2013a;	Crushing circuit evaluation							√
SGS Canada Inc. 2013b; 12592-004	Tiriganiaq; F zone; Wesmeg	√						
SGS Canada Inc. 2013c; 12592-005	Tiriganiaq; Discovery		√	√				√
AMTEL 2013; 13/36	Tiriganiaq							√
BBA 2013b;	Grinding circuit evaluation							√
EMSL Canada Inc. 2013b;	Tiriganiaq							√
Air Liquide Canada 2013;	Tiriganiaq			√				√
AEM Technical Services 2014;	Tiriganiaq		√	√				
Pocock Industrial 2014;	Tiriganiaq				√			
SGS Canada Inc. 2014a; 12592-006	Tiriganiaq; Discovery				√			
SGS Canada Inc. 2014b; 12592-007	Tiriganiaq	√						
Starkey & Associates inc. 2014;	Tiriganiaq	√						
SGS Canada Inc. 2015; 12592-008	Tiriganiaq	√						

Lakefield Research, (1997, April 30).

An Investigation of the Recovery of Gold from Meliadine Project Samples.

This report summarizes the results of testwork conducted on Meliadine project Tiriganiaq samples as requested by WMC International Limited. The purpose of the testwork was to investigate the recovery of gold by gravity separation, flotation and cyanidation. Preliminary environmental test were also completed to evaluate the acid potential generation. Lakefield Research did not include details on the composite make-up and no sample selection information could be found in the historic WMC or Comaplex documents. There is therefore no indication of the sample source within the Tiriganiaq deposit and the results from this report can only be used as a high level reference.

- Head assay
- Mineralogical test
- Gravity recovery test
- Flotation test
- Direct cyanidation test
- Environmental test as Acid-Base Accounting

Lakefield Research, (1998, January 15).

An Investigation of the Recovery of Gold from Meliadine Project Samples.

This report summarizes the results of testwork conducted on Meliadine project Tiriganiaq and F zone samples as requested by WMC International Limited. The test program included gravity separation and cyanidation tests to investigate the recovery of gold as well as Bond work index and abrasion index determinations, thickening test and acid-base accounting. Lakefield Research did not include details on the composite make-up and no sample selection information could be found in the historic WMC or Comaplex documents. There is therefore no indication of the sample source within the Tiriganiaq and F zone deposits and the results from these two reports can only be used as a high level reference.

- Head assay
- Comminution test BWi, Ai
- Gravity + cyanidation recovery test
- Preg-robbing investigation
- Mineralogical test
- Thickening
- Environmental test as Acid-Base Accounting

Lakefield Research, (2001, April 24).

An Investigation of the Recovery of Gold from Meliadine Project Samples.

This report summarizes the results of testwork conducted on Meliadine project Pump and Wolf samples as requested by WMC International Limited. The test program included gravity separation and cyanidation tests to investigate the recovery of gold as well as Bond work index determination, thickening tests and acid-base accounting.

- Head assay
- Comminution test BWi
- Direct cyanidation test
- Gravity + cyanidation recovery test
- Preg-robbing investigation
- Mineralogical test
- Thickening
- Environmental test as Acid-Base Accounting

SGS Lakefield Research, (2006, February 08).

An Investigation into the Extraction of Gold from Meliadine Samples.

This report summarizes the results of testwork performed on Meliadine project Tiriganiaq samples for Cmaplex Minerals Corp. It included gravity separation and cyanidation tests to investigate the extraction of gold.

- Head assay
- Gravity recovery test
- Gravity + cyanidation recovery test
- Gravity + CIL recovery test

SGS Lakefield Research LTD. (2007, June 27).

The recovery of gold from Meliadine samples, Report 2(11166-002).

This report summarizes the results of testwork conducted on Meliadine project Tiriganiaq samples as requested by J.R. Goode and Associates of Comaplex Minerals Corp. The program included gravity separation, cyanidation and flotation testwork to investigate the recovery of gold, and a gold liberation study.

- Head assay
- Mineralogical test
- Comminution test BWi
- Gravity recovery test
- Gravity + CIL recovery test
- Flotation test

RDi. (2009, April 03).

Scoping metallurgical study for Meliadine project, Canada.

The test program was undertaken on four composites, from Discovery deposit, prepared from assay rejects of 2008 drill program and old core from 1995 drilling. The testwork included preparation of composite samples, head analyses, bottle roll direct and CIL cyanidation tests,

gravity tests and Bond's ball mill work index determinations. Samples localisation indicates that all four composites contain samples from either open pit or underground mining at Discovery.

- Head assay
- Mineralogical test
- Comminution test BWi
- Direct cyanidation test
- CIL cyanidation test
- Gravity + CIL recovery test

Starkey & Associates Inc., (2009, December 23).

Comaplex Project SAGDesign Testing Report.

The test program was requested by Comaplex Minerals Corp. and undertaken on eight samples, from Tiriganiaq and Discovery deposits.

- SAGDesign comminution testing and simulations

Outotec. (2011, March 04).

Thickener test data report, High Rate Thickening for Grinding and Cyanide Recovery Streams, Meliadine project(report SE-1372-TR).

A dynamic bench scale thickener test work campaign was conducted on one grinding thickener sample and one cyanide recovery thickener sample. Test work purpose was to investigate the settling characteristics and determine the high rate thickener sizing criteria. Samples come from Master composite made of Tiriganiaq and F zone deposits which was prepared during the SGS (2012) program.

- Static and dynamic sedimentation tests

SGS Canada Inc. (2011, July 21).

The grindability characteristics of a single composite from the Meliadine deposit(12564-001).

SGS perform an HPGR investigation on a sample from the Tiriganiaq deposit from the 2008 bulk sample. The report presents the grindability test results as well as the preliminary HPGR/BM grinding circuit design.

- Head assay
- Mineralogical test
- Comminution test BWi, Ai
- HPGR grindability test and simulations

PMC. (2011, September 20).

A mineralogical description of three head samples from Meliadine project for rapid ore characterization(AUG2011-05).

Select samples from Tiriganiaq, F zone and Wesmeg deposits were sent to Process Mineralogical Consulting (PMC) for x-ray diffraction and rapid ore characterization. Samples were prepared by SGS and can be compared to the mineralogical results from SGS (2013 a).

- Mineralogical test

Knelson. (2011, September 21).

Gravity test work report AEM Meliadine Project(KRTS 20627-1).

A sample of the master composite, prepared by SGS (2013 a), was sent to the Knelson Research and Technology Center for a standard Extended Gravity Recoverable Gold (E-GRG) test. It consists of a series of sequential liberation and gravity recovery steps to give an indication of the amenability of the sample to gravity recovery methods. The composite is a blend of representative Tiriganiaq, Discovery, F zone, Wesmeg and others deposits.

- Gravity E-GRG test

Wardrop (2011, December 12).

Meliadine gold project comminution circuit Trade-off study Final report(Document No. 1153470200-REP-R0001-01.

Agnico Eagle commissioned Wardrop to prepare an order-of-magnitude trade-off study for the comminution circuit of the Meliadine project. At a daily processing rate of 10,000 tonnes, the crushing and grinding stages will reduce the ore particles size to P80 of 105 µm. Three options were compared.

1. Conventional three-stage crushing followed by two-stage ball milling;
2. Primary crusher followed by semi-autogenous grinding and ball milling;
3. Two-stage crushing followed by high pressure grinding rolls and ball milling

- Comminution circuit simulations and design

Golder Associates. (2011, December 14).

Laboratory Report on AEM Meliadine Project Tailings(11-1428-0011).

Agnico Eagle has retained Golder Associates Ltd to carry out laboratory testing on the Tiriganiaq 2008 bulk samples which was ground to 80% passing 110 µm by SGS. Test work assess their material, flow and, strength properties for use as backfill. The test program also includes dewatering testing.

- Mineralogical test
- Rheological characterization
- Flow loop testing
- Static sedimentation tests
- Vacuum filtration test
- Unconfined compressive strength testing

AEM Technical Services 2012.

As part of the metallurgical programs, tests were conducted at Agnico Eagle Technical Services laboratory to confirm the metallurgical results from SGS (2013 a). The testwork included head analyses, gravity tests and combination of gravity plus cyanidation tests. Meliadine deposits were all tested excluding Normeg deposit.

- Head assay
- Gravity test
- Gravity + cyanidation test
- Gravity + CIL recovery test

SGS Canada Inc. (2012, February 05).

The recovery of gold from Meliadine project samples - Final report(Project 12592-001 (includes 11858-003)).

This metallurgical program was initiated by Comaplex Minerals Corp. in 2009 as the SGS project 11858-003 and pursuit, after Agnico Eagle acquisition, as the SGS project 12592-001. This metallurgical study is one of the largest ever performed on Meliadine project in terms of testwork wide but it was limited to samples from Tiriganiaq and F zone deposits only. The program included comminution testing, ore characterisation, flowsheet development and process optimisation testwork as well as a series of metallurgical variability tests.

- Head assay
- Comminution test SMC, RWi, BWi, Ai
- Gravity recovery test
- Gravity concentrate intensive leaching test
- Direct cyanidation test
- Gravity + cyanidation test
- Gravity + CIP recovery test
- Gravity + CIL recovery test
- Flotation test
- Cyanide destruction test
- CIP circuit simulations

Eriez Magnetics. (2012, February 10).

Gold ore from AEM, Sample Log # 17636(17636).

Two samples of the Tiriganiaq 2011 bulk sample were sent to Eriez Magnetics for magnetic susceptibility testing. The purpose of the testing was to confirm that the levels of magnetite and pyrrhotite were sufficient to interfere with tramp steel magnet operation.

- Magnetic susceptibility tests

FLSmidth. (2012, March 01).

Sedimentation and Rheology Testing on Meliadine Thickener Feasibility Project.

Agnico Eagle commissioned FLSmidth Salt Lake City Inc. to conduct sedimentation testing on eight samples for the Meliadine project. The testwork objectives were to determine sizing criteria and operating parameters for FLS high rate thickener and E-CAT thickener technology. A full testing campaign was conducted on Tiriganiaq 2011 bulk sample composite but only static settling tests and sample characterization was conducted on seven variability samples from Tiriganiaq, Discovery, F zone, Wesmeg and Pump deposits prepared during the SGS (2013a) program.

- Rheological characterization

- Static and dynamic sedimentation tests

Starkey & Associates Inc. (2012, March 16).

SAGDesign Comminution Analysis(S&A Project S99).

The test program was requested by Agnico Eagle and undertaken on eight samples, from Tiriganiaq, Discovery, F zone, Pump, Wesmeg and Wolf deposits which were prepared by SGS (2013a).

- SAGDesign comminution testing and simulations

CSS. (2012, December 27).

Meliadine grinding circuit Results of simulation study(Final report).

Agnico Eagle commissioned Contract Support Services (CSS) to perform simulations to determine required mill dimensions and motor capacities for a proposed grinding circuit for the Meliadine project. Base case scenario includes target throughput of 5,000 tonnes per day using an open circuit SAG mill feed by rocks having 80% passing 150 mm with a ball mill in closed circuit with cyclones producing 80% passing 105 µm. Three other options were evaluated as:

1. Pre-crushing at F80 = 75 mm;
2. Single-stage SAG milling;
3. Base case producing 80% passing 75 µm
- Comminution circuit simulations and design

AEM Technical Services 2013;

As complement of the metallurgical programs, preg-robbing tests were conducted at Agnico Eagle Technical Services laboratory to investigate the Tiriganiaq lode 1000 samples from the 2011 bulk sampling campaign. Six samples, located between the rounds 91E and 127E, were used to evaluate the preg-robbing potential by comparing direct cyanidation and CIL tests.

- Preg-robbing
- Gravity test
- Direct cyanidation recovery test
- CIL recovery test

EMSL. (2013a, February 28).

Meliadine composite samples(report 551300814 rev1).

Three samples from Tiriganiaq and Discovery deposits were sent to EMSL for asbestos characterization.

- Mineralogical test

OMC. (2013, March).

Meliadine gold project Comminution scoping study(report No. 7136.30 Rev1).

Agnico Eagle requested Orway Mineral Consultants Canada (OMC) to review earlier comminution equipment sizing reports and provide a comminution circuit selection and design study based on metallurgical data available for the Meliadine project. Base case scenario includes target throughput of 5,000 tonnes per day where grind size product varies to get 80% passing 75 µm and 105 µm. Four options were investigated:

1. SAB circuit;
2. Partial secondary crushed feed to SAG;
3. Single-stage SAG milling circuit;
4. Partial secondary crushed feed to single-stage SAG milling circuit

- Comminution circuit simulations and design

SGS Canada Inc. (2013a, March 21).

An investigation into Meliadine project samples Final report(report 12592-002).

This report contains results of ore characterisation and metallurgical testwork performed on samples from the Meliadine project. The purpose of the program was to evaluate eight variability composites and one master composite. This metallurgical study is the largest one performed on Meliadine project in terms of metallurgical testwork wide and it was realized on all deposits excepting Normeg. The testwork program included head analysis, comminution testing as well as a series of metallurgical variability as the gravity separation,

cyanidation, diagnostic leaching and cyanide destruction tests. The master composite consists of a mix of the variability composites made according to proportions provided by Agnico Eagle. This master composite was use in the program Knelson (2011), while the variability composites were use in the programs PMC (2011), AEM (2012), FLSmidth (2012) and Starkey (2012). Three samples of the comminution test were used to perform the testwork described in the SGS (2013c) report.

- Head assay
- Mineralogical test
- Comminution test DWT, SMC, CWi, RWi, BWi, Ai
- Gravity recovery test
- Gravity + cyanidation test
- Gravity + CIL recovery test
- CIP/CIL circuit simulations
- Preaeration test
- Flotation test
- Cyanide destruction test
- Diagnostic leach test (DLT)
- Rheological test

FLSmidth Knelson. (2013, May 08).

Gravity modeling report Agnico-Eagle Meliadine Project.

This report refers to the Knelson (2011) study and consists to perform gravity circuit simulations.

- Gravity circuit simulations

Metso. (2013, June 07).

Pilot Vertimill Test.

A pilot Vertimill test was conducted for Agnico Eagle on the Tiriganiaq deposit. The purpose of the this test was to assess the performance of a secondary Vertimill grinding circuit processing to determine the energy savings compare to a ball mill, and to size a Vertimill which is capacble of processing 271.7 t/hr.

- Vertimill piloting

Outotec. (2013, June 10).

Thickening and filtration individual test reports for AEM tailings samples(53835T1 & 53835T2).

This report combines four tests which were performed by Outotec on thickening and filtration processing. The purpose of the testing was to investigate the effect of bed height to determinate if a paste-like material was achievable with thickener and to determine the suitability of Outotec's vacuum filtration technology. Report T1 and T2 respectively refers to material having 80% passing 105 µm and 75 µm. The samples come from the bulk sample 2008. Thickening test consists to a dynamic bench scale thickener of 100 mm and a larger one supposed to represent a mini-pilot scale test having 190 mm diameter and 1,500 mm bed height. Filtration test consists to vacuum test.

- Rheological characterization
- Static and dynamic sedimentation tests
- Mini-pilot scale thickening test
- Vacuum filtration test

BBA. (2013a, June 11).

Technical note Underground crusher selection(AEM: 6505-REP-94_R80, BBA 5287055-000000-49-ERA-0004).

The design criteria for the Meliadine underground crusher selection were reviewed and adjusted by BBA and Agnico Eagle. This technical note summarizes the main parameters used for the selection as well as BBA's recommendation for the underground crusher.

- Crusher simulations and design

SGS Canada Inc. (2013b, June 28).

The grindability characteristics of composite samples from the Meliadine projects Final report(Project 12592-004).

Agnico Eagle requested that SGS perform grindability testwork on variability and waste composite samples from different zones of the Meliadine project which include Tiriganiaq, F zone and Wesmeg deposits.

- Comminution test SPI, SMC, CWi, RWi, BWi, Ai

SGS Canada Inc. (2013c, July 08).

Recovery of gold from Meliadine project samples Final report(Project 12592-005).

The report contains the results of the metallurgical program on samples from Agnico Eagle Meliadine project. The purpose of the program was to evaluate three samples by gravity and cyanidation which were originally submitted as variability composite for a comminution study under SGS (2013a). Those samples come from Tiriganiaq and Discovery deposits. The test program includes head analysis, gravity separation and cyanidation.

- Head assay
- Gravity recovery test
- Gravity + cyanidation test
- Gravity + CIL recovery test

AMTEL. (2013, July 12).

Mineralogical Analysis of meliadine Gold Project(13/36).

Six samples from Tiriganiaq deposit were sent to Amtel for mineralogical characterization. Purpose of the program was to establish the gold content, determine the general mineralogy and the sulphide mineralogy. A special attention was given to the characterization of the minerals potentially detrimental to cyanidation.

- Mineralogical test

BBA. (2013b, July 15).

Technical note Grinding circuit design(AEM: 6505-REP-08_R0, BBA 5287055-000500-49-ERA-0003).

The Meliadine grinding circuit was evaluated through simulation work, using testwork data. The objective of the circuit review is to allow Agnico Eagle to make a decision regarding the preferred circuit configuration to carry through the study, considering the updated project parameters such as a mill throughput at 6,000 tonnes per day and a final grind size of 75 µm.

- Grinding circuit simulations and design

EMSL. (2013b, August 06).

Asbestos grinding variability samples(report 551304611 rev1).

Twelve samples from the Tiriganiaq deposit were sent to EMSL for asbestos characterization.

- Mineralogical test

Air Liquide Canada. (2013, December 18).

Gold leaching Pre-oxydation and cyanide leaching of gold ore concentrate.

Agnico Eagle wanted to evaluate the impact of pre-oxidation on the cyanide leaching process for one ore sample from Tiriganiaq deposit which was originally submitted as variability composite for a comminution study under SGS (2013a). Purpose of test wants to quantify the degree of pre-oxidation vs cyanide consumption in leaching circuit and the oxygen requirement in the pre-oxidation and cyanide leaching circuit.

- Oxygen uptake rate test (OUR)
- Preaeration
- Cyanidation test

AEM Technical Services 2014.

Gravity testwork perform on Tiriganiaq samples indicates a good potential to gravity recovery. One of the metallurgical opportunities consists to verify the possibility to increase the gravity concentrate mass pull. As complement of the metallurgical programs, continuous gravity tests were conducted at Agnico Eagle Technical Services laboratory on the Tiriganiaq deposits. Testwork were extend on three phases to begin in 2012 and was pursuit until 2014.

- Continuous gravity test
- Gravity + cyanidation test
- Gravity concentrate regrind + cyanidation test

Pocock Industrial Inc. (2014, July).

Sample characterization flocculant screening gravity sedimentation pulp rheology and pressure filtration studies.

Pocock conduct solids liquid separation tests on one sample of the Tiriganiaq deposit. The sample was representative of the grinding thickener feed and one other sample was modified to simulate the filtration feed. The overall objective of the test program was to develop a

general set of data for the design of thickening and filtration equipment to dewater the grind material for further processing and dewater the tails material prior to final disposal.

- Rheological characterization
- Static and dynamic sedimentation tests
- Vacuum filtration test
- Pressure filtration test

SGS Canada Inc. (2014a, September 12).

Cyanidation study involving saline solution Final report(Project 12592-006).

The purpose of this program was to investigate the cyanide leaching circuit performance when exposed to saline

Appendix 14.1 - Absent value or deleted non-sampled intersections at Meliadine

DEPOSIT	BHID	SAMPLE	ZONE	FROM	TO	LENGTH	ACTION	COMMENT
Tiriganiaq	M04-529-05	-	1252	-	-	-	Delete	Suspicious position
	M11-1125	-	1100	96.2	100.1	3.9	Delete	Bulk Sample
	M11-1125	-	1102	88.3	92.2	3.9	Delete	Bulk Sample
	M11-1134	-	1050	125.1	131.7	6.7	Delete	Bulk Sample
	M11-1134	-	1075	111.7	118.4	6.7	Delete	Bulk Sample
	M11-1141	-	1075	110.6	114.2	3.6	Delete	Bulk Sample
	M11-1151	-	1050	113.8	116.7	2.9	Delete	Bulk Sample
	M11-1151	-	1075	108.1	111.0	2.9	Delete	Bulk Sample
	M11-1151	-	1087	102.4	105.3	2.9	Delete	Bulk Sample
	M11-1156	-	1050	124.8	127.9	3.1	Delete	Bulk Sample
	M11-1156	-	1100	84.8	88.8	4.0	Delete	Bulk Sample
	M11-1156	-	1102	74.6	78.0	3.4	Delete	Bulk Sample
	M11-1160	-	1025	123.5	125.0	1.5	Delete	Bulk Sample
	M11-1160	-	1075	107.5	111.5	4.0	Delete	Bulk Sample
	M11-1160	-	1087	103.5	107.5	4.0	Delete	Bulk Sample
	M14-2304	-	1000	447.1	455.3	8.2	Delete	Not sampled
	M14-2304	-	1050	425.8	428.9	3.1	Delete	Not sampled
	M14-2304	-	1075	411.5	425.8	14.3	Delete	Not sampled
	M14-2304	-	1150	385.4	392.1	6.7	Delete	Not sampled
	M14-2304	-	1153	372.1	378.8	6.7	Delete	Not sampled
	M14-2304	-	1153	378.8	385.4	6.7	Delete	Not sampled
	M14-2312	-	1000	219.1	224.9	5.8	Delete	Not sampled
	M14-2312	-	1050	204.8	219.1	14.3	Delete	Not sampled
	M14-2312	-	1100	180.6	193.3	12.7	Delete	Not sampled
Normeg	GT13-39	-	920	52.7	52.9	0.2	Delete	Not sampled
	M10-890	-	-	-	-	-	Delete	Abandoned
	M14-2223	-	904	18	18.2	0.2	Delete	Not sampled
	M14-2227	-	-	-	-	-	Delete	Abandoned
Wesmeg	M11-1003	-	-	-	-	-	Delete	Abandoned
	M11-1060	-	-	-	-	-	Delete	Abandoned
	M12-1463A	-	-	-	-	-	Delete	Abandoned
	M12-1484	-	-	-	-	-	Delete	Abandoned
	M13-2097	-	-	-	-	-	Delete	Abandoned
	M14-2227	-	-	-	-	-	Delete	Abandoned
Discovery	DS09GT-02	-	5230	90.73	91.6	0.87	Delete	Not sampled
	DS09GT-04	-	5240	106.6	110.3	3.8	Delete	Not sampled
	DS09GT-04	-	5220	117.8	120.7	2.9	Delete	Not sampled
	GT13-67	-	5240	30.7	43	12.3	Delete	Not sampled
	GT13-67		5230	43	57	14	Delete	Not sampled
Fzone	M12-1629	M12-1629_LC1	4120	91	91.2	0.2	Delete	Lost Core
	GT13-59	-	4140	68	75	7	Delete	Not sampled
	GT13-60	-	4120	43.5	48	4.5	Delete	Not sampled
	GT13-60	-	4130	39	43.5	4.5	Delete	Not sampled
Pump	M12-1515A	M12-1515A-LC1	3330	14.5	15	0.5	Absent	Lost Core
Wolf	M09-821	-	-	-	-	-	Delete	Abandoned
	M09-822	-	-	-	-	-	Delete	Abandoned
	M09-824	-	-	-	-	-	Delete	Abandoned
	M09-825	-	-	-	-	-	Delete	Abandoned
	M09-829	-	-	-	-	-	Delete	Abandoned
	M11-1223	-	-	-	-	-	Delete	Abandoned
	M11-1321	-	-	-	-	-	Delete	Abandoned
	M14-2329	-	-	-	-	-	Delete	Abandoned
	W92-13	-	-	-	-	-	Delete	Abandoned

Moved intersections at Tiriganiaq deposit

BHID	FROM	TO	Distance(m)	Direction	ZONE
M11-1066	144.8	148.1	1.5	N	1000
M11-1063	147.8	151.2	3.5	N	1000
M08-783	153.1	154.9	1.5	N	1000
M07-702	169	174.05	3	N	1000
M96-53	159.87	162.51	3.3	N	1000
M99-364	157.23	160.14	3.6	N	1000
M00-483	145.18	149.34	2.3	N	1000
M07-667A	159.6	161.55	1.5	N	1000
M99-443	200.45	202.66	5.3	N	1000
M10-882	56.3	59.1	3.6	S	1100
M11-1047	100.6	105.7	2.4	N	1100
M06-608	106.2	112.45	2.5	N	1100

Appendix 14.2 - Stats Zones

DEPOSIT	DOMAIN	ZONE	NBDDH	SAMPLES (uncapped)												COMPOSITES (capped)											
				NBSAMPLES	MEAN	MEDIAN	MINIMUM	10TH	25TH	75TH	90TH	MAXIMUM	STANDDEV	CV	IQR	NBCOMPOSITES	MEAN	MEDIAN	MINIMUM	10TH	25TH	75TH	90TH	MAXIMUM	STANDDEV	CV	IQR
TIRIGANIAQ	1000	1,000	797	3,011	6.78	0.86	0.00	0.03	0.10	4.49	15.25	511.20	21.68	3.20	4.39	2,447	6.41	1.34	0.00	0.03	0.23	5.78	16.44	212.25	14.79	2.31	5.55
	1000series	1,015	139	522	4.82	1.11	0.00	0.02	0.10	4.66	13.13	445.10	17.18	3.57	4.56	428	4.82	1.46	0.00	0.03	0.25	5.78	12.45	280.09	14.08	2.92	5.53
		1,025	655	2,410	3.58	0.66	0.00	0.02	0.03	3.17	8.86	196.00	10.31	2.88	3.14	2,015	3.56	1.02	0.00	0.03	0.16	3.70	8.52	182.16	8.67	2.44	3.54
		1,050	668	2,478	3.67	0.48	0.00	0.02	0.03	2.85	8.85	258.80	11.19	3.05	2.82	2,087	3.56	0.78	0.00	0.03	0.10	3.33	9.22	100.31	8.25	2.32	3.22
		1,075	499	1,731	2.60	0.21	0.00	0.02	0.03	1.73	6.45	148.70	8.56	3.30	1.71	1,490	2.55	0.38	0.00	0.02	0.03	2.17	6.40	99.36	7.05	2.76	2.14
		1,087	272	966	3.23	0.45	0.00	0.02	0.03	2.52	6.93	333.70	11.39	3.53	2.49	815	3.09	0.82	0.00	0.02	0.11	2.85	7.51	95.00	6.99	2.26	2.74
	1100	1,100	774	3,173	5.62	0.55	0.00	0.02	0.03	5.33	16.70	140.20	12.54	2.23	5.30	2,578	5.59	1.17	0.00	0.03	0.12	6.54	16.20	125.84	10.36	1.85	6.42
		1,102	156	558	4.88	0.38	0.01	0.02	0.03	3.52	14.41	98.10	11.18	2.29	3.49	441	4.87	1.34	0.01	0.03	0.15	5.20	14.49	72.83	8.66	1.78	5.06
	1150series	1,150	41	188	3.61	0.35	0.00	0.02	0.03	2.54	9.40	61.27	8.44	2.34	2.52	152	3.61	0.98	0.00	0.02	0.12	3.44	10.20	30.36	6.40	1.77	3.32
		1,151	43	170	5.01	0.21	0.00	0.01	0.03	2.90	10.90	254.40	20.39	4.07	2.88	151	5.01	0.82	0.00	0.02	0.05	3.55	10.90	205.45	17.91	3.57	3.50
		1,152	149	602	4.04	0.31	0.00	0.02	0.03	3.59	11.14	65.55	9.04	2.24	3.57	495	4.04	0.78	0.00	0.02	0.03	4.06	12.93	49.70	7.70	1.91	4.03
		1,153	242	1,167	6.25	0.36	0.00	0.02	0.03	5.23	17.90	338.00	17.77	2.85	5.21	966	5.96	1.05	0.00	0.02	0.04	6.03	17.46	100.00	12.56	2.11	5.99
		1,154	175	848	5.55	0.55	0.00	0.02	0.03	4.50	16.34	187.00	13.40	2.41	4.48	711	5.55	1.26	0.00	0.02	0.10	6.27	15.19	141.51	11.44	2.06	6.17
		1,155	166	773	3.90	0.30	0.00	0.02	0.03	2.49	9.21	375.70	16.65	4.26	2.47	678	3.90	0.59	0.00	0.02	0.03	3.07	9.50	362.94	15.82	4.05	3.03
		1,156	10	33	2.23	0.03	0.00	0.02	0.02	0.34	9.40	26.50	5.67	2.54	0.32	27	2.23	0.09	0.00	0.01	0.02	0.96	8.19	26.50	5.42	2.42	0.94
		1,157	13	49	4.04	0.10	0.01	0.02	0.03	1.42	7.99	150.50	18.42	4.56	1.40	40	3.29	0.23	0.01	0.02	0.03	1.07	7.64	65.37	10.15	3.09	1.04
		1,160	21	83	1.89	0.07	0.00	0.02	0.03	1.54	4.90	26.41	4.45	2.36	1.52	67	1.89	0.43	0.00	0.02	0.03	1.63	4.57	21.27	3.83	2.03	1.61
		1,170	27	113	6.78	0.54	0.00	0.02	0.03	4.94	24.70	123.00	16.09	2.37	4.92	98	6.78	0.95	0.00	0.02	0.08	7.42	24.49	62.10	11.52	1.70	7.34
	1250Series	1,251	119	562	3.31	0.37	0.00	0.02	0.03	2.66	7.79	119.00	9.75	2.94	2.64	465	3.28	0.88	0.00	0.02	0.10	3.02	7.92	96.16	7.86	2.39	2.92
		1,252	89	709	14.76	1.55	0.00	0.02	0.03	10.99	32.22	1,974.00	89.80	6.08	10.96	558	10.71	3.30	0.00	0.03	0.33	12.66	28.86	169.79	17.86	1.67	12.34
		1,253	29	132	4.00	0.28	0.00	0.02	0.02	2.62	9.77	83.09	11.52	2.88	2.60	110	4.00	0.71	0.00	0.02	0.06	3.38	7.57	55.26	8.88	2.22	3.32
		1,254	68	245	2.26	0.32	0.00	0.02	0.03	1.55	4.90	59.38	6.29	2.78	1.53	210	2.26	0.64	0.00	0.03	0.07	1.84	4.83	37.85	4.86	2.14	1.77
		1,255	65	359	6.79	0.77	0.00	0.02	0.03	5.71	20.06	115.70	14.86	2.19	5.69	284	6.79	1.45	0.00	0.02	0.14	7.11	19.46	89.39	12.63	1.86	6.97
		1,256	56	321	8.20	0.96	0.00	0.02	0.03	7.51	22.30	125.00	17.17	2.09	7.49	250	8.20	1.95	0.00	0.03	0.32	8.45	23.38	92.47	14.82	1.81	8.13
		1,257	45	193	1.74	0.24	0.00	0.02	0.03	1.82	5.45	32.76	3.67	2.11	1.80	164	1.74	0.72	0.00	0.02	0.08	1.78	5.22	18.98	2.77	1.59	1.70
		1,258	6	24	1.86	0.28	0.00	-	0.03	2.51	3.12	23.51	3.92	2.11	2.49	22	1.86	0.39	0.00	-	0.02	2.17	3.12	9.61	2.74	1.48	2.15
		1,260	44	191	3.47	0.50	0.00	0.02	0.02	3.19	11.08	47.84	7.32	2.11	3.17	141	3.47	1.18	0.00	0.02	0.13	4.45	9.83	45.00	6.03	1.74	4.32
		1,261	3	11	2.66	1.14	0.03	0.03	0.03	2.17	6.52	17.45	4.30	1.62	2.15	7	2.66	1.31	0.31	0.02	0.31	1.83	9.83	7.93	2.71	1.02	1.52
		1,262	9	49	5.90	0.75	0.02	0.02	0.03	8.44	20.04	54.70	10.61	1.80	8.42	41	5.90	1.19	0.02	0.02	0.17	6.73	13.71	52.35	9.90	1.68	6.56
		1,263	16	65	1.93	0.23	0.01	0.02	0.02	1.75	4.89	27.00	4.18	2.16	1.73	49	1.93	0.78	0.02	0.02	0.08	2.47	4.29	14.22	2.96	1.53	2.39
		1,264	10	31	0.69	0.02	0.00	-	0.02	0.33	2.31	10.68	1.72	2.49	0.31	31	0.69	0.11	0.00	-	0.02	0.82	1.54	5.68	1.19	1.72	0.80
	1350Series	1,265	3	10	2.62	1.11	0.03	0.03	0.12	2.05	4.98	20.00	4.68	1.79	1.93	8	2.62	1.82	0.10	-	0.13	3.08	1.54	8.98	2.91	1.11	2.95
		1,270	8	20	3.35	1.40	0.00	-	0.03	3.73	6.71	24.45	5.58	1.67	3.71	21	3.35	1.05	0.00	-	0.03	2.67	6.07	21.06	5.31	1.59	2.65
		1,350	3	17	6.16	0.65	0.02	0.02	0.02	5.63	22.50	27.60	9.20	1.49	5.61	14	6.16	0.66	0.02	0.02	0.02	5.63	15.21	27.16	8.57	1.39	5.61
		1,360	2	10	5.68	2.52	0.02	0.02	0.02	10.10	16.80	16.80	5.85	1.03	10.08	8	5.68	1.54	0.02	0.02	0.02	4.91	15.21	16.22	5.33	0.94	4.89
WESMEG	200-300	225	12	31	1.62	0.08	0.00	-	0.03	1.16	5.03	21.40	3.61	2.22	1.14	38	1.62	0.16	0.00	-	0.03	1.04	3.86	12.39	3.19	1.96	1.02
		230	13	58	6.55	1.10	0.00	-	0.06	5.19	9.54	188.00	24.65	3.76	5.13	61	4.41	1.15	0.00	-	0.13	3.90	9.51	60.00	9.36	2.12	3.77
		235	5	8	13.93	0.14	0.00	-	-	3.09	5.81	287.00	58.70	4.21	3.09	14	3.92	0.14	0.00	-	-	3.23	5.81	22.06	7.07	1.80	3.23
		240	10	26	1.55	0.36	0.00	-	0.03	1.45	2.93	21.50	3.63	2.34	1.43	29	1.55	0.53	0.00	-	0.04	1.51	4.93	8.57	2.39	1.54	1.47
		250	12	28	1.44	0.03	0.00	0.03	0.03	1.25	5.93	13.80	3.20	2.22	1.23	34	1.45	0.03	0.00	-	0.03	1.15	4.01	13.33	2.79	1.92	1.13
		270	6	43	3.57	0.22	0.02	0.03	0.03	2.69	5.84	52.27	9.32	2.61	2.66	32	3.24	0.91	0.03	0.03	0.09	2.67	5.03	26.78	5.60	1.73	2.59
		280	12	39	3.03	0.21	0.00	0.03	0.03	5.11	11.05	13.75	4.43	1.46	5.09	36	3.03	1.14	0.00	0.03	0.21	4.27	7.44	12.77	3.57	1.18	4.06
		290	5	17	3.71	0.45	0.00	-	0.03	1.59	19.00	19.75	6.36	1.71	1.56	15	3.71	1.07	0.00	-	0.03	2.31	7.52	19.75	5.65	1.52	2.28
		300	8	28	2.22	0.24	0.03	0.03	0.03	2.13	10.45	16.80	4.12	1.86	2.11	26	2.22	0.55	0.03	0.03	0.03	2.13	7.52	10.15	3.08	1.39	2.10
		310	5	15	1.15	0.03	0.00	0.03	0.03	2.00	4.11	6.56	1.79	1.55	1.98	15	1.15	0.13	0.02	0.02	0.03	2.07	2.61	4.11	1.32	1.14	2.04
		320	17	65	2.90	0.20	0.00	0.03	0.03	1.55	4.66	122.00	12.54	4.32	1.53	60	2.22	0.50	0.03	0.03	0.03	1.70	4.66	40.05	5.54	2.49	1.67
		330	2	6	3.13	0.45	0.24	0.24	0.30	1.03	18.65	18.65	6.34	2.03	0.73	7	3.13	0.38	0.24	0.03	0.24	0.83	4.66	18.65	6.34	2.03	0.59

		360	4	28	2.08	1.41	0.03	0.03	0.07	3.24	5.79	6.84	2.07	1.00	3.17	20	2.08	1.55	0.03	0.07	0.83	2.85	3.48	6.32	1.56	0.75	2.02
		420	6	21	1.58	0.54	0.03	0.03	0.03	1.24	5.91	11.35	2.63	1.67	1.22	20	1.58	0.41	0.03	0.03	0.03	1.20	2.70	10.54	2.31	1.47	1.18
		430	19	76	2.83	0.85	0.01	0.03	0.08	2.76	5.05	45.60	6.25	2.21	2.68	68	2.83	1.12	0.03	0.03	0.30	3.00	5.96	29.70	4.80	1.70	2.70
	400LOW	435	21	92	2.28	1.42	0.03	0.10	0.41	2.33	5.19	25.20	3.30	1.45	1.92	85	2.28	1.48	0.03	0.19	0.56	2.52	4.83	25.20	3.19	1.40	1.96
		440	45	175	1.53	0.61	0.00	0.03	0.08	2.09	3.96	19.47	2.31	1.51	2.01	163	1.50	0.88	0.00	0.03	0.17	2.02	3.77	11.35	1.88	1.26	1.85
		450	33	206	2.14	1.16	0.03	0.03	0.41	2.97	5.01	25.60	2.86	1.34	2.56	197	2.14	1.21	0.03	0.09	0.45	2.92	4.86	25.60	2.72	1.27	2.47
		455	7	26	2.18	1.20	0.03	0.03	0.34	2.78	5.81	10.50	2.70	1.24	2.44	25	2.18	1.20	0.03	0.03	0.34	3.12	4.77	9.40	2.30	1.05	2.78
		460	54	236	2.21	1.11	0.00	0.03	0.18	2.70	6.24	22.20	3.18	1.44	2.52	219	2.21	1.29	0.01	0.07	0.33	2.64	5.53	22.20	2.97	1.34	2.31
		470	27	118	3.39	1.31	0.00	0.03	0.20	3.76	9.61	22.00	4.87	1.44	3.56	103	3.39	1.51	0.03	0.03	0.47	4.01	8.40	22.00	4.41	1.30	3.54
	400HIGH	475	6	22	1.44	0.46	0.00	0.03	0.03	2.41	4.37	4.87	1.64	1.14	2.39	23	1.44	0.46	0.00	0.02	0.03	2.32	4.07	4.87	1.64	1.13	2.30
		480	22	181	2.10	0.92	0.03	0.03	0.21	2.42	5.67	23.70	3.31	1.57	2.21	170	2.10	0.95	0.03	0.03	0.29	2.41	5.30	23.70	3.14	1.49	2.12
		490	37	149	2.33	0.83	0.00	0.03	0.10	2.34	5.81	40.90	4.77	2.04	2.24	136	2.33	0.83	0.00	0.03	0.15	2.23	5.67	30.16	4.27	1.83	2.08
		500	18	65	1.46	0.55	0.00	0.03	0.03	2.06	3.60	9.90	1.96	1.34	2.04	62	1.46	0.72	0.00	0.03	0.18	1.74	3.42	9.90	1.86	1.28	1.56
		510	38	137	2.94	0.74	0.00	0.03	0.03	2.77	8.14	127.50	10.77	3.66	2.75	120	2.48	1.03	0.00	0.03	0.15	2.91	6.57	55.46	5.27	2.12	2.76
	650	650	213	1,072	3.50	1.54	0.00	0.03	0.35	3.69	7.89	59.70	6.59	1.88	3.34	957	3.45	1.70	0.01	0.15	0.61	3.84	7.60	44.43	5.50	1.59	3.23
		520	46	206	2.41	0.86	0.00	0.03	0.14	2.02	4.75	34.40	5.28	2.19	1.88	192	2.41	1.14	0.01	0.05	0.26	2.38	4.33	34.40	4.54	1.88	2.12
		600	71	530	4.19	1.47	0.01	0.03	0.38	3.06	5.68	1,145.00	38.22	9.11	2.68	493	2.65	1.55	0.03	0.12	0.55	3.10	5.53	60.00	4.38	1.65	2.55
		625	62	403	1.83	0.87	0.00	0.03	0.15	2.29	4.45	49.00	3.75	2.04	2.14	365	1.83	1.00	0.02	0.07	0.24	2.27	4.35	24.59	2.72	1.49	2.02
		660	26	84	1.63	0.37	0.00	0.03	0.03	1.78	4.26	56.90	4.90	3.01	1.76	86	1.63	0.57	0.00	0.03	0.10	1.83	3.65	34.34	3.84	2.35	1.73
	600-700	670	35	120	2.75	0.23	0.00	0.03	0.03	1.06	2.37	1,159.00	43.88	15.98	1.04	118	1.17	0.31	0.00	0.03	0.04	1.12	2.33	19.45	2.50	2.13	1.08
		710	39	196	2.72	1.23	0.01	0.03	0.19	2.88	6.66	41.70	4.85	1.78	2.69	170	2.72	1.41	0.03	0.12	0.32	3.26	6.45	22.15	3.88	1.43	2.95
		720	11	42	1.93	0.10	0.03	0.03	0.03	1.99	5.24	25.40	4.16	2.15	1.97	37	1.93	0.46	0.03	0.03	0.03	1.99	4.04	19.76	3.67	1.90	1.96
		730	6	24	1.30	0.31	0.03	0.03	0.08	1.82	4.46	4.84	1.63	1.25	1.74	22	1.30	0.53	0.03	0.06	0.12	1.47	2.73	4.47	1.41	1.08	1.35
		740	16	68	2.72	1.06	0.00	0.03	0.21	3.71	8.11	16.90	3.61	1.32	3.50	61	2.72	1.41	0.01	0.15	0.37	3.49	7.31	11.60	3.07	1.13	3.12
NORMEG	-	901	66	255	3.29	0.54	0.00	0.03	0.03	2.57	8.07	148.50	11.36	3.45	2.55	236	3.19	0.91	0.00	0.03	0.11	2.60	7.86	90.57	7.99	2.50	2.49
	-	902	61	213	2.33	0.31	0.00	0.03	0.03	2.00	4.54	50.90	6.66	2.86	1.98	220	2.33	0.65	0.00	0.03	0.10	1.85	4.59	50.90	6.32	2.72	1.75
	-	903	27	87	4.21	0.44	0.00	0.03	0.06	2.17	4.53	426.00	32.84	7.80	2.11	85	2.56	0.71	0.01	0.03	0.16	2.08	4.64	75.97	8.45	3.30	1.92
	-	904	29	98	2.34	0.21	0.00	0.02	0.03	1.03	2.93	69.70	9.43	4.03	1.01	97	2.34	0.34	0.01	0.03	0.05	1.01	2.93	69.70	8.91	3.80	0.96
	-	905	4	12	2.37	0.33	0.00	-	0.03	0.79	14.40	19.45	5.30	2.24	0.77	13	2.37	0.25	0.00	-	0.03	1.08	2.78	14.40	4.38	1.84	1.06
	-	906	32	105	2.94	0.17	0.00	0.03	0.03	0.89	8.92	56.10	8.72	2.96	0.86	102	2.94	0.23	0.00	0.03	0.06	1.55	8.92	56.10	7.83	2.66	1.49
	-	907	54	184	1.83	0.10	0.00	0.03	0.03	1.08	4.42	81.30	6.77	3.69	1.06	187	1.83	0.23	0.00	0.03	0.03	1.49	4.53	51.07	5.15	2.81	1.47
	-	909	15	49	2.14	0.45	0.01	0.03	0.03	1.94	3.24	48.80	6.85	3.20	1.92	50	2.14	0.57	0.03	0.03	0.14	1.72	2.76	48.80	6.82	3.19	1.58
	-	910	54	190	4.08	0.37	0.00	0.03	0.03	2.14	8.12	182.50	14.47	3.55	2.12	181	3.83	0.56	0.00	0.03	0.11	2.50	8.14	72.01	9.65	2.52	2.39
	-	911	101	367	3.65	0.32	0.00	0.03	0.03	2.20	6.94	169.00	14.99	4.11	2.18	371	3.48	0.51	0.00	0.03	0.06	2.38	6.60	150.00	11.79	3.38	2.32
	-	920	122	455	6.36	0.34	0.00	0.03	0.03	2.17	8.86	288.00	27.26	4.28	2.15	457	5.20	0.58	0.00	0.03	0.09	2.74	9.43	134.06	15.48	2.98	2.65
	-	921	21	86	4.81	1.14	0.00	0.03	0.10	3.46	11.65	78.00	11.38	2.37	3.36	77	4.81	1.34	0.01	0.03	0.32	3.45	10.57	78.00	10.84	2.25	3.14
	-	922	23	82	2.38	0.77	0.03	0.03	0.14	2.26	7.51	22.80	3.74	1.57	2.12	76	2.38	1.20	0.03	0.03	0.35	2.69	6.13	13.69	3.10	1.30	2.35
	-	923	39	144	3.92	0.77	0.00	0.03	0.03	2.77	9.46	59.90	9.52	2.43	2.74	147	3.92	0.88	0.00	0.03	0.10	2.54	9.15	57.51	9.02	2.30	2.45
	-	924	10	50	4.19	1.35	0.03	0.03	0.06	5.91	11.35	31.00	6.59	1.57	5.85	51	4.19	1.55	0.03	0.03	0.10	5.56	10.76	31.00	6.02	1.44	5.46
	-	925	23	74	2.63	0.22	0.00	0.03	0.03	2.07	5.09	105.00	11.00	4.18	2.05	74	2.63	0.49	0.00	0.03	0.03	1.75	4.65	49.45	7.71	2.93	1.72
	-	930	50	164	3.32	0.20	0.00	0.03	0.03	1.58	7.44	48.70	8.82	2.66	1.56	166	3.32	0.60	0.00	0.03	0.05	2.16	6.97	45.00	7.92	2.39	2.11
	-	987	97	316	2.65	0.14	0.00	0.02	0.03	1.07	3.20	354.90	18.81	7.10	1.05	322	1.99	0.28	0.00	0.02	0.03	1.21	3.11	120.00	8.36	4.20	1.18
	-	988	146	470	1.78	0.17	0.00	0.02	0.03	1.22	3.91	119.00	6.58	3.69	1.20	453	1.78	0.27	0.00	0.02	0.03	1.41	3.95	85.82	5.61	3.15	1.38
DISCOVERY		5,110	7	25	3.83	0.50	0.00	-	0.15	4.03	11.89	28.39	6.80	1.77	3.88	21	3.83	0.60	0.00	-	0.26	2.40	11.34	28.39	6.78	1.77	2.14
		5,120	11	40	2.37	0.07	0.00	0.01	0.02	0.20	1.47	92.33	11.83	5.00	0.18	35	1.76	0.08	0.00	-	0.02	0.20	4.28	17.41	4.17	2.37	0.18
	51	5,130	6	24	2.72	0.04	0.00	-	0.01	1.58	3.01	61.40	10.21	3.75	1.57	19	2.54	0.02	0.00	-	0.01	1.40	3.01	28.98	6.70	2.64	1.39
		5,140	11	46	2.09	0.15	0.00	0.02	0.03	2.24	7.82	14.39	3.71	1.77	2.22	35	2.09	0.19	0.01	0.01	0.05	2.43	6.69	13.10	3.18	1.52	2.39
		5,150	2	5	2.12	0.20	0.08	0.08	0.18	0.67	7.09	7.09	2.98	1.40	0.49	3	2.65	0.19	0.23	0.01	0.05	2.43	6.69	7.07	3.13	1.18	2.39
		5,210	110	559	5.76	1.07	0.00	0.03	0.12	6.40	17.10	132.38	10.79	1.87	6.28	412	5.53	1.94	0.00	0.03	0.25	7.71	15.59	54.86	8.17	1.48	7.46
	52LOW	5,220	39	171	4.81	0.48	0.00	0.04	0.10	3.70	11.30	99.61	11.89	2.47	3.60	122	4.81	1.04	0.00	0.05	0.22	4.68	12.18	91.59	10.35	2.15	4.46
		5,310	3	11	3.00	0.02	0.00	0.00	0.01	0.03	21.79	21.79	7.41	2.47	0.02	8	3.00	0.03	0.01	0.03	0.01	0.03	14.46	21.79	6.98	2.32	0.01
	52HIGH	5,230	116	515	3.77	0.20	0.00	0.02	0.03	1.58	9.96	105.19	10.65	2.83	1.56	398	3.62	0.39	0.00	0.02	0.07	2.32	10.50	56.52	8.27	2.28	2.25
		5,240	153	659	4.53	0.26	0.00	0.02	0.03	2.59	12.60	140.80	12.03	2.66	2.57	488	4.10	0.74	0.00	0.03	0.10	3.15	14.46	50.91	8.45	2.06	3.05
FZONE	-	4,100	45	111	1.05	0.03	0.00	-	0.01	0.40	2.02	63.60	4.80	4.57	0.39	83	0.91	0.15	0.00	-	0.00	0.77	1.59	14.57	2.27	2.51	0.76
	-	4,105	6	17	8.15	-	0.00	-	-	0.02	0.02	361.40	53.61	6.58	0.02	14	0.13	-	0.00	-	-	0.02	0.02	1.86	0.45	3.48	0.02
	-	4,110	195	638	1.12	0.03	0.00	-	0.02	0.69	3.61	38.45	3.02	2.70	0.67	364	1.10	0.13	0.00	0.01	0.03	1.04	3.05	19.66	2.31	2.10	1.02
	-	4,115	43	194	4.74	1.92	0.00	0.01	0.07	7.61	13.17	39.93	6.36	1.34	7.54	98	4.69	2.92	0.00	0.02	0.21	7.40	11.66	20.56	5.00	1.07	7.19
	-	4,120	298	1,178	2.89	0.55	0.00	0.02	0.03	3.74	8.06	43.43	5.10	1.77	3.72	618	2.86	1.08	0.00	0.03	0.10	4.11	7.99	26.00	4.05	1.42	4.01

	-	4,130	265	1,145	4.01	1.42	0.00	0.02	0.03	5.69	10.76	66.20	6.78	1.69	5.66	593	4.00	2.35	0.00	0.03	0.37	5.80	9.70	38.42	5.11	1.28	5.43
	-	4,135	107	450	5.18	1.58	0.00	0.01	0.03	6.51	14.30	78.44	8.77	1.69	6.49	245	5.15	3.17	0.00	0.01	0.20	7.46	13.08	49.92	6.58	1.28	7.26
	-	4,137	16	81	1.76	0.21	0.00	0.01	0.02	2.21	6.17	16.30	3.10	1.76	2.19	43	1.76	0.57	0.00	0.02	0.05	2.99	4.24	8.94	2.24	1.27	2.93
	-	4,140	20	51	0.39	0.02	0.00	-	0.01	0.03	0.54	5.97	1.26	3.21	0.02	40	0.39	0.03	0.00	-	0.01	0.18	1.58	5.77	1.00	2.54	0.17
	-	4,150	10	34	0.31	0.03	0.00	-	0.02	0.17	0.58	3.93	0.72	2.30	0.15	20	0.31	0.03	0.00	-	0.02	0.34	0.57	2.18	0.50	1.58	0.32
	-	4,160	15	53	2.21	0.03	0.00	0.01	0.03	0.89	4.10	41.40	6.89	3.12	0.87	32	1.96	0.23	0.00	0.01	0.03	1.19	5.66	19.65	3.96	2.02	1.16
	-	4,170	9	44	0.60	0.08	0.00	0.02	0.02	0.55	2.15	4.92	1.11	1.84	0.54	20	0.60	0.17	0.02	0.02	0.03	0.76	1.10	3.40	0.83	1.39	0.74
	-	4,180	9	40	2.04	0.56	0.02	0.02	0.03	2.90	5.57	18.59	3.45	1.69	2.87	17	2.04	0.41	0.02	0.02	0.11	2.51	3.27	9.59	2.67	1.31	2.39
PUMP	31-1	3,100	60	197	2.65	0.20	0.00	0.03	0.03	1.70	8.00	72.60	6.41	2.42	1.68	180	2.52	0.28	0.00	0.03	0.03	2.30	6.29	32.00	5.07	2.01	2.27
		3,101	78	298	5.46	1.55	0.00	0.03	0.16	6.01	16.76	91.30	10.54	1.93	5.85	267	4.99	1.80	0.01	0.07	0.45	7.08	14.13	65.91	7.34	1.47	6.62
	31-2	3,109	22	62	5.14	0.20	0.00	0.02	0.03	4.66	16.35	38.60	9.85	1.92	4.64	56	4.61	0.75	0.00	0.02	0.03	5.06	13.10	34.02	7.40	1.61	5.03
		3,110	19	59	4.45	0.43	0.00	0.02	0.03	2.90	10.95	84.51	11.73	2.64	2.88	57	3.73	1.08	0.00	0.03	0.03	4.32	10.94	27.10	5.97	1.60	4.29
		3,130	38	123	2.31	0.12	0.00	0.02	0.03	1.72	5.92	35.41	5.20	2.25	1.70	108	2.31	0.27	0.00	0.02	0.03	2.59	5.90	26.41	4.40	1.90	2.57
	31-3	3,165	9	25	3.61	0.54	0.00	-	0.03	2.39	10.60	29.00	6.97	1.93	2.37	27	3.61	0.54	0.00	-	0.03	3.14	7.34	28.10	6.60	1.83	3.11
		3,180	19	55	1.55	0.15	0.00	-	0.02	1.10	6.06	12.10	2.74	1.77	1.08	58	1.55	0.18	0.00	-	0.03	2.89	4.25	10.57	2.38	1.53	2.86
		3,190	18	87	3.54	1.76	0.01	0.03	0.16	4.59	7.78	40.79	5.61	1.58	4.43	75	3.50	1.76	0.03	0.06	0.70	4.23	7.78	24.92	4.61	1.32	3.53
		3,195	27	113	4.86	1.83	0.01	0.03	0.14	6.20	14.00	36.20	7.14	1.47	6.06	100	4.86	2.57	0.02	0.06	0.94	6.18	12.45	36.20	6.12	1.26	5.24
	34-2	3,299	13	49	3.96	1.54	0.01	0.05	0.31	4.33	13.70	20.40	5.13	1.30	4.02	41	3.96	2.12	0.03	0.11	0.49	4.68	11.26	15.50	4.41	1.12	4.19
	33-1	3,300	2	7	3.22	2.18	0.10	0.10	1.75	5.18	5.72	9.70	2.66	0.83	3.43	7	3.22	1.75	0.10	0.11	0.10	4.76	11.26	5.86	2.03	0.63	4.66
		3,301	25	112	5.17	2.09	0.00	0.03	0.55	6.03	15.10	50.00	8.12	1.57	5.48	108	5.02	2.48	0.00	0.03	1.01	6.03	13.07	39.47	6.97	1.39	5.03
		3,310	23	93	5.20	1.20	0.00	0.03	0.05	5.38	18.60	56.90	9.81	1.89	5.33	79	4.86	1.91	0.02	0.03	0.16	4.85	11.37	35.00	7.84	1.61	4.69
		3,320	42	145	3.75	1.16	0.00	0.01	0.03	4.27	10.35	82.59	7.64	2.04	4.25	137	3.58	1.49	0.00	0.01	0.12	4.31	9.48	38.40	5.58	1.56	4.18
		3,330	40	148	2.34	0.84	0.00	0.03	0.03	3.32	6.96	23.39	3.49	1.49	3.30	137	2.34	1.09	0.01	0.03	0.09	3.26	6.75	16.46	3.08	1.32	3.17
		3,340	38	140	4.05	2.63	0.01	0.03	0.52	6.48	9.77	25.20	4.52	1.12	5.96	128	4.05	2.69	0.01	0.08	1.04	5.88	9.33	20.75	4.04	1.00	4.84
	34-2	3,341	19	82	4.08	2.10	0.03	0.03	0.48	5.34	12.80	29.90	5.25	1.29	4.86	71	4.08	2.10	0.03	0.20	0.69	5.35	11.50	18.37	4.44	1.09	4.66
		3,400	13	47	3.35	1.98	0.03	0.03	0.52	4.33	9.32	20.10	4.11	1.23	3.81	46	3.35	1.98	0.03	0.03	0.58	4.32	9.32	17.24	3.63	1.08	3.74
		3,402	17	60	3.23	0.98	0.03	0.03	0.15	3.62	8.39	37.90	5.93	1.83	3.47	51	3.23	1.68	0.03	0.03	0.38	3.93	7.11	18.96	4.22	1.30	3.56
		3,405	3	14	6.45	5.44	0.03	2.12	3.95	6.55	17.90	20.80	5.26	0.81	2.60	13	6.45	5.44	0.11	0.11	2.90	6.22	7.31	20.80	4.89	0.76	3.32
	34-1	3,411	2	6	6.27	0.03	0.03	0.03	0.03	6.03	19.00	19.00	7.75	1.24	6.01	6	6.27	3.82	1.23	0.11	1.23	5.72	7.31	19.00	5.97	0.95	4.49
		3,412	12	55	3.70	1.45	0.03	0.03	0.08	4.90	9.31	48.50	7.62	2.06	4.82	54	3.70	1.53	0.03	0.03	0.28	3.96	6.59	40.50	6.76	1.82	3.69
		3,413	6	27	7.19	0.99	0.03	0.03	0.03	4.20	17.70	83.00	15.96	2.22	4.18	23	5.61	0.94	0.03	0.03	0.04	7.30	13.75	26.83	7.75	1.38	7.26
		3,440	8	28	1.80	0.99	0.00	0.00	0.03	2.51	5.20	9.58	2.34	1.30	2.49	24	1.80	1.20	0.00	0.03	0.25	2.27	3.47	7.33	1.70	0.94	2.02
		3,460	10	37	2.66	0.59	0.00	0.03	0.03	3.94	8.51	22.60	5.00	1.88	3.92	31	2.66	0.75	0.01	0.03	0.34	2.42	3.97	20.14	4.28	1.61	2.08
WOLF	21	2,107	2	9	2.23	0.66	0.01	0.01	0.02	1.27	1.45	18.40	5.17	2.32	1.25	8	2.23	0.18	0.08	0.02	0.08	1.27	11.40	13.44	4.29	1.93	1.19
		2,110	14	72	1.89	0.51	0.00	0.02	0.03	2.06	5.34	21.10	3.48	1.84	2.04	66	1.89	0.62	0.01	0.02	0.16	2.36	4.20	19.34	2.99	1.59	2.20
		2,112	9	39	2.41	0.37	0.00	0.03	0.03	1.65	4.26	73.00	8.77	3.64	1.63	35	1.87	0.81	0.00	0.03	0.03	1.79	5.14	14.31	2.95	1.58	1.77
		2,115	19	94	2.56	0.75	0.01	0.03	0.10	2.82	5.40	25.30	4.71	1.84	2.72	79	2.56	1.31	0.01	0.03	0.24	2.98	5.18	20.81	3.86	1.51	2.74
		2,120	32	148	2.92	0.70	0.01	0.02	0.03	3.28	5.96	61.95	6.95	2.38	3.26	139	2.66	1.08	0.01	0.02	0.16	3.60	5.68	30.00	4.59	1.73	3.44
		2,125	22	131	3.30	0.79	0.01	0.02	0.10	3.58	10.85	33.90	5.71	1.73	3.48	113	3.30	1.50	0.01	0.09	0.40	3.71	9.77	25.43	4.87	1.48	3.31
		2,130	44	188	1.53	0.23	0.00	0.02	0.03	1.69	4.07	33.30	3.63	2.38	1.67	170	1.53	0.46	0.00	0.02	0.05	1.67	3.91	19.90	2.93	1.91	1.62
		2,140	15	74	3.01	0.82	0.01	0.07	0.24	4.17	11.06	15.15	4.22	1.40	3.93	65	3.01	1.56	0.03	0.10	0.48	4.88	7.08	14.80	3.32	1.10	4.40
		2,240	4	15	4.32	0.23	0.01	0.02	0.03	1.64	8.57	63.90	12.36	2.86	1.62	13	3.21	0.34	0.02	0.02	0.03	3.89	7.76	9.79	3.72	1.16	3.87
		2,300	10	36	1.48	0.66	0.00	0.01	0.08	2.16	4.40	7.13	1.87	1.26	2.08	42	1.48	0.96	0.00	0.01	0.06	2.22	3.27	7.13	1.66	1.12	2.16
		2,305	12	39	1.51	0.47	0.00	0.02	0.06	1.47	5.23	12.68	2.65	1.76	1.41	37	1.52	0.49	0.00	0.02	0.08	1.30	3.26	12.13	2.52	1.66	1.22
	23	2,310	34	180	3.22	0.58	0.00	0.03	0.10	2.66	6.47	283.60	16.55	5.14	2.56	160	2.42	0.94	0.01	0.03	0.18	2.68	6.02	35.88	4.17	1.72	2.50
		2,320	39	253	5.02	0.88	0.00	0.03	0.03	3.93	11.40	224.80	17.51	3.49	3.91	202	3.92	1.26	0.01	0.03	0.10	4.78	11.14	43.39	6.47	1.65	4.68
		2,330	10	61	2.32	0.03	0.02	0.02	0.03	2.20	11.40	17.45	4.54	1.96	2.18	46	2.31	0.63	0.02	0.02	0.03	2.33	7.51	17.45	3.70	1.60	2.31

Appendix 14.3 - Density per rockcode

ROCK CODE	Rock description	Density is interpollated			Density is fixed by 3D lithological solids					
					F_Zone		Discovery		Normeg & Wesmeg	
		Tiriganiaq	Pump	Wolf	Density	3D Lithological solids	Density	3D Lithological solids	Density	3D Lithological solids
aUa	Lamprophyre	2.88	2.88	2.88	2.88	Lamprophyre	2.81	-	2.89	-
aUa-qv	Lamprophyre with Veining	2.88	2.88	2.88	2.88	Lamprophyre	2.81	-	2.89	-
Fi	Felsic intrusion	2.82	2.82	2.82	2.82	-	2.81	-	2.89	-
FJ	Fault	2.82	2.82	2.82	2.82	-	2.81	-	2.89	-
Ib	Intermediate volcanic flow	2.82	2.91	2.82	2.82	-	2.81	-	2.89	-
Ii	Intermediate intrusion	2.82	2.82	2.82	2.82	-	2.81	-	2.89	-
Iv	Intermediate volcaniclastics	2.82	2.91	2.82	2.82	-	2.81	-	2.89	-
K	Undifferentiated Clastics	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_K	Mineralized Undifferentiated Clastics	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Km	Mineralized Mudstone	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Kmg	Mineralized Graphitic Mudstone	2.81	2.81	2.81	2.81	-	2.81	-	2.6	Graphitic argillite
K_Kmg-qv	Mineralized Graphitic Mudstone with Veining	2.81	2.81	2.81	2.81	-	2.81	-	2.6	Graphitic argillite
K_Km-qv	Mineralized Mudstone with Veining	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Kms	Mineralized Laminated black-white tuff beds (MARKER)	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Kms-qv	Mineralized Laminated black-white tuff beds (MARKER) with Vn	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Ks	Mineralized Siltstone	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Ksc	Mineralized Chloritic Siltstone	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Ksc-lj	Mineralized Chloritic Siltstone with Cht-Mt Iron Formation	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Ksc-qv	Mineralized Chloritic Siltstone with Veining	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Ksc-wa	Mineralized Chloritic Siltstone with Greywacke	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Ks-m	Mineralized Siltstone with Mudstone	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Ks-qv	Mineralized Siltstone with Veining	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Kst	Mineralized Schistose Siltstone	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Kst-qv	Mineralized Schistose Siltstone with Veining	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Ks-wa	Mineralized Siltstone with Greywacke	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Kwa	Mineralized Greywacke	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Kwa-lj	Mineralized Greywacke with Chert-Magnetite Iron Formation	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Kwa-qv	Mineralized Greywacke with Veining	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
K_Kwa-sc	Mineralized Greywacke with Chloritic Siltstone	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Km	Mudstone	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Kmg	Graphitic Mudstone	2.6	2.6	2.6	2.6	-	2.81	-	2.6	Graphitic argillite
Kmg-qv	Graphitic Mudstone with Veining	2.6	2.6	2.6	2.6	-	2.81	-	2.6	Graphitic argillite
Km-qv	Mudstone with Veining	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
KMS	Laminated black-white tuff beds (MARKER)	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Kms-qv	Laminated black-white tuff beds (MARKER) with Veining	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Ks	Siltstone	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Ksc	Chloritic Siltstone	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Ksc-lj	Chloritic Siltstone with Chert-Magnetite Iron formation	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Ksc-qv	Chloritic Siltstone with Veining	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Ksc-wa	Chloritic Siltstone with Greywacke	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Ks-m	Siltstone with Mudstone	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Ks-qv	Siltstone with Veining	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Kst	Schistose Siltstone	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Kst-qv	Schistose Siltstone with Veining	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Ks-wa	Siltstone with Greywacke	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Kwa	Greywacke	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Kwa-Lj	Greywacke with Chert-Magnetite Iron formation	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Kwa-qv	Greywacke with Veining	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Kwa-s	Greywacke with Siltstone	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
Kwa-sc	Greywacke with Chloritic Siltstone	2.81	2.81	2.81	2.81	-	2.81	-	2.89	-
L	Lower Lean Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
L_L	Mineralized Lower Lean Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
L_Lj	Mineralized Magnetite Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
L_Ljm	Mineralized Magnetite-Chlorite Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
L_Lj-qv	Mineralized Magnetite Iron Formation with Veining	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
L_Ll	Mineralized Chert Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
L_Llj	Mineralized Chert-Magnetite Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
L_Llj-qv	Mineralized Chert-Magnetite Iron Formation with Veining	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
L_Llm	Mineralized Chert-Chlorite Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
L_Llm-qv	Mineralized Chert-Chlorite Iron Formation with Veining	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands

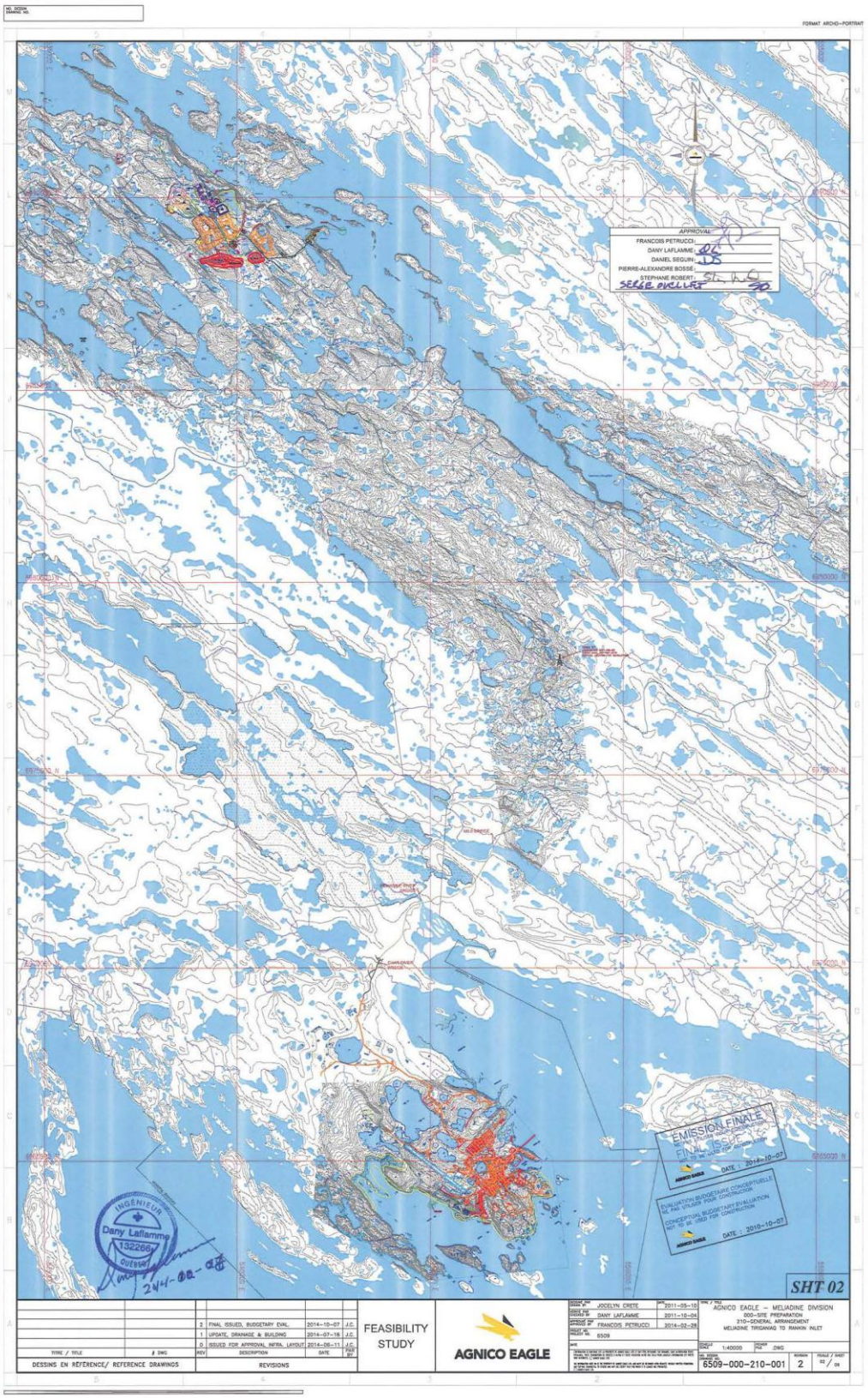
L_Ll-qv	Mineralized Chert Iron Formation with Veining	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
L_Lml	Mineralized Chlorite-Chert Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
L_Lm-qv	Mineralized Chlorite Iron Formation with Veining	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
L_L-qv	Mineralized Lower Lean Iron Formation with Veining	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
LC	Lost core	2.82	2.82	2.82	2.82	-	2.81	-	2.89	-
Lj	Magnetite Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Ljm	Magnetite-Chlorite Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Ljm-qv	Magnetite-Chlorite Iron Formation with Veining	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Lj-qv	Magnetite Iron Formation with Veining	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Ll	Chert Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Llj	Chert-Magnetite Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Llm	Chert-Chlorite Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Llm-qv	Chert-Chlorite Iron Formation with Veining	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Ll-qv	Chert Iron Formation with Veining	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Lm	Chlorite Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Lmj	Chlorite-Magnetite Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Lml	Chlorite-Chert Iron Formation	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Lml-qv	Chlorite-Chert Iron Formation with Veining	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Lm-qv	Chlorite Iron Formation with Veining	2.72	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
M	Mafic Volcanics	2.83	2.86	2.83	2.85	-	2.81	-	2.89	-
M_M	Mineralized Mafic Volcanics	2.83	2.86	2.83	2.85	-	2.81	-	2.92	-
M_MV	Mineralized Mafic Volcaniclastics	2.83	2.86	2.83	2.85	-	2.81	-	2.92	-
M_Mv-qv	Mineralized Mafic Volcaniclastics with Veining	2.83	2.86	2.83	2.85	-	2.81	-	2.92	-
Mb	Mafic Flow	2.83	2.87	2.83	2.85	-	2.81	-	2.89	-
Mb-qv	Mafic Flow with Veining	2.83	2.87	2.83	2.85	-	2.81	-	2.89	-
MD	"Dolerite(diabase)	2.88	2.88	2.88	2.88	Gabbro dykes	2.88	Gabbro dykes	2.88	-
Mg	Gabbro	2.88	2.96	2.88	2.88	Gabbro dykes	2.88	Gabbro dykes	2.93	-
Mg-qv	Gabbro with Veining	2.88	2.96	2.88	2.88	Gabbro dykes	2.88	Gabbro dykes	2.93	-
MV	Mafic Volcaniclastics	2.83	2.88	2.83	2.85	-	2.81	-	2.89	-
Mv-qv	Mafic Volcaniclastics with Veining	2.83	2.88	2.83	2.85	-	2.81	-	2.89	-
N	Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_N	Mineralized Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nj	Mineralized Magnetite Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Njm	Mineralized Magnetite-Chlorite Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Njm-qv	Mineralized Magnetite-Chlorite Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nj-qv	Mineralized Magnetite Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nl	Mineralized Chert Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nlj	Mineralized Chert-Magnetite Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nlj-qv	Mineralized Chert-Magnetite Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nlm	Mineralized Chert-Chlorite Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nlm-qv	Mineralized Chert-Chlorite Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nl-qv	Mineralized Chert Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nm	Mineralized Chlorite Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nmj	Mineralized Chlorite-Magnetite Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nmj-qv	Mineralized Chlorite-Magnetite Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nml	Mineralized Chlorite-Chert Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nml-qv	Mineralized Chlorite-Chert Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
N_Nm-qv	Mineralized Chlorite Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
NI	Not identified	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Nj	Magnetite Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Njm	Magnetite-Chlorite Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Njm-qv	Magnetite-Chlorite Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Nj-qv	Magnetite Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Nl	Chert Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Nlj	Chert-Magnetite Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Nlj-qv	Chert-Magnetite Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Nlm	Chert-Chlorite Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Nlm-qv	Chert-Chlorite Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Nl-qv	Chert Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Nm	Chlorite Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Nmj	Chlorite-Magnetite Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Nmj-qv	Chlorite-Magnetite Iron Formation with	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands

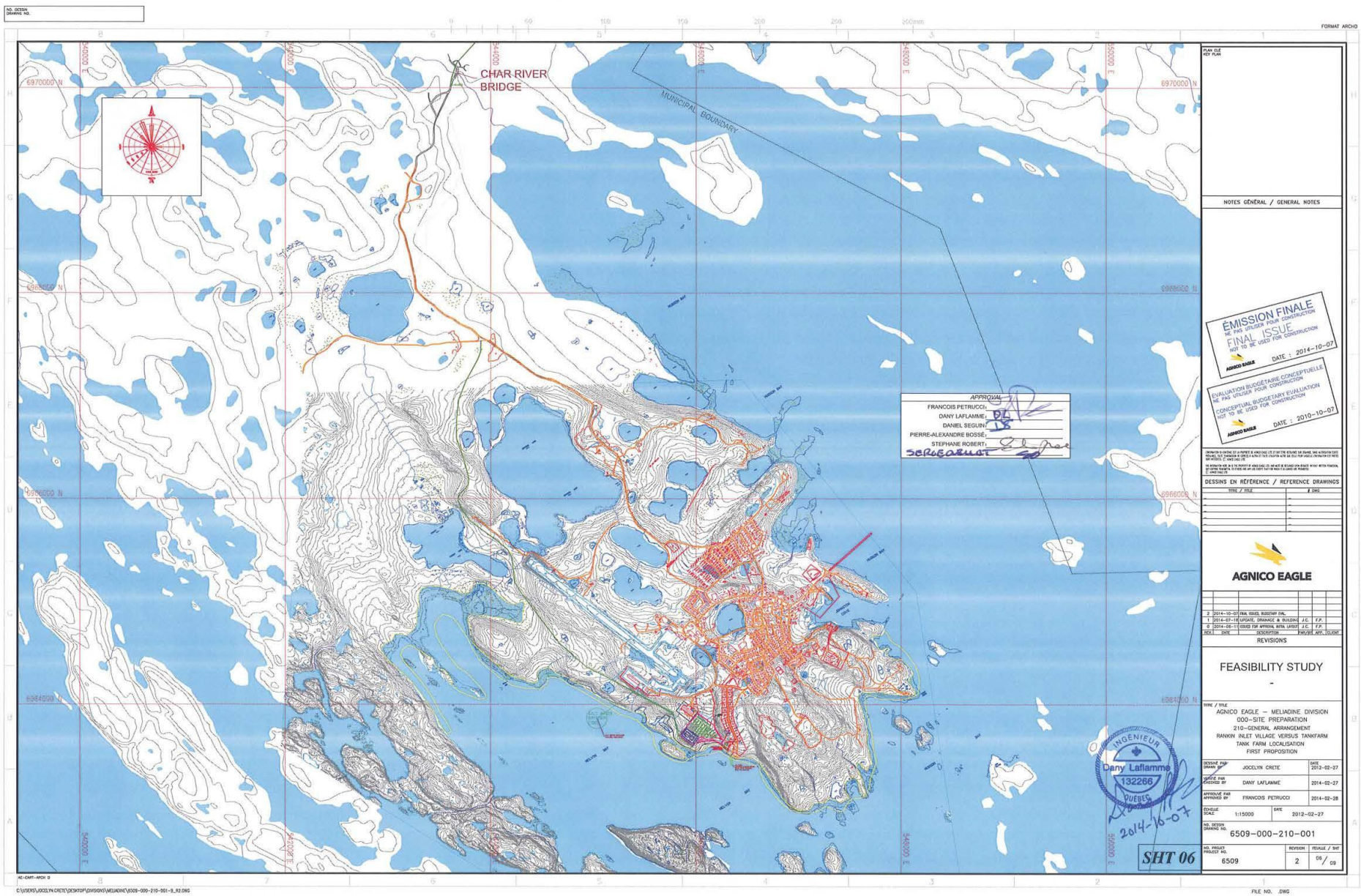
	Veining									
Nml	Chlorite-Chert Iron Formation	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Nml-qv	Chlorite-Chert Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
Nm-qv	Chlorite Iron Formation with Veining	3.06	3.06	2.92	2.96	Iron Formation Bands	3.17	Iron Formation Bands	3.02	Iron Formation Bands
OVB	Overburden	1.9	1.9	1.9	1.9	-	1.9	-	1.9	
pMg	Porphyritic Gabbro	2.88	2.88	2.88	2.88	Gabbro dykes	2.88	Gabbro dykes	2.89	2.93
pMg-qv	Porphyritic Gabbro with Veining	2.88	2.88	2.88	2.88	Gabbro dykes	2.88	Gabbro dykes	2.89	2.93
Q	Quartz Veining	2.85	3.03	2.85	2.83	-	2.81	-	2.89	-
Q_Q	Mineralized Quartz Veining	2.85	3.03	2.85	2.98	-	2.81	-	2.89	-
Q_Qak	Mineralized Quartz-Ankerite veining	2.85	3.03	2.85	2.98	-	2.81	-	2.89	-
Q_Qcc	Mineralized Quartz-Calcite Veining	2.85	3.03	2.85	2.98	-	2.81	-	2.89	-
Q_Qcl	Mineralized Quartz-Chlorite Veining	2.85	3.03	2.85	2.98	-	2.81	-	2.89	-
Qak	Quartz-Ankerite Veining	2.85	2.83	2.85	2.83	-	2.81	-	2.89	-
Qcc	Quartz-Calcite Veining	2.85	2.83	2.85	2.83	-	2.81	-	2.89	-
Qcl	Quartz-Chlorite Veining	2.85	2.83	2.85	2.83	-	2.81	-	2.89	-
Qtl	Quartz-Tourmaline Veining	2.85	2.83	2.85	2.83	-	2.81	-	2.89	-
U	Ultramafic Volcanics	2.9	2.92	2.9	2.9	-	2.81	-	2.92	Ultramafic volcanic rock
Ub	Ultramafic Flow	2.9	2.92	2.9	2.9	-	2.81	-	2.92	Ultramafic volcanic rock
Ub-qv	Ultramafic Flow with Veining	2.9	2.92	2.9	2.9	-	2.81	-	2.92	Ultramafic volcanic rock
UK	Unkown	2.82	2.92	2.9	2.9		2.81		2.89	
Uv	Ultramafic Volcaniclastics	2.9	2.92	2.9	2.9	-	2.81	-	2.92	Ultramafic volcanic rock
						2.85 out of 3D solids		**2.81 out of 3D solids**		**2.89 out of 3D solids**

Appendix 14.4 - Block model attributes

Field value	Description	Field Origin
IJK	Code generated and used by Datamine to identify each parent cell position uniquely within the model. Subcells that lie within the same parent cell will have the same IJK value.	Datamine specific Block model field
XC	The X, Y and Z coordinates of the cell centre	Datamine specific Block model field
ZC		
YC		
XINC	The dimensions of the cell in the X, Y and Z directions. If the model will not contain any subcells, then these three fields can be implicit (not stored in every record). This will reduce the storage space required by the model.	Datamine specific Block model field
ZINC		
YINC		
COOKICAT	Cell specific class (IND, INF or INV)	User defined
ZONE	Zone field	User defined
ROCKTYPE	Cell rock type number	User defined
DENSITY	Cell density	Estimation Output
AUIPD	Gold value estimated with a gold composite using the Inverse Power of Distance method	Estimation Output
AUOK	Gold value estimated with a gold composite using the Ordinary Kriging method	Estimation Output
UNCAUOK	Gold value estimated with an uncapped gold composite using the Ordinary Kriging method	Estimation Output
SGNN	Density value estimated using the Nearest Neighbour method	Estimation Output
SRCHIPD	Ellipsoid use for the cell estimation using Inverse Power of Distance method	Estimation Output
NSOK	Number of samples found within the search volume using the Ordinary Kriging method	Estimation Output
SRCHOK	Ellipsoid used for the cell estimation using the Ordinary Kriging method	Estimation Output
MDOK	Minimal distance from cell centre and the nearest sample within the search volume using the Ordinary Kriging Method	Estimation Output
VAROK	Variance between samples within the search volume using the Ordinary Kriging Method	Estimation Output
ELLSG	Ellipsoid used for the density estimation using Nearest Neighbour method	Estimation Output
OLD_AU	Gold & density estimation output using DEC 2013 parameters	Estimation Output
OLD_SRCH		Estimation Output
OLD_NS		Estimation Output
OLD_VAR		Estimation Output
OLD_MD		Estimation Output
OLD_DENS		Estimation Output
XMORIG	The X, Y and Z coordinates of the model origin. Datamine sets the origin at the corner, not the centroid, of the first parent cell.	Datamine specific Block model field
YMORIG		
ZMORIG		
NX	Number of parent cells in the X, Y and Z directions of the model. Studio allows a value of 1 for modelling seams. The number of cells, in combination with the cell dimensions, defines the extent of the model.	Datamine specific Block model field
NY		
NZ		

Appendix 18.1 - Infrastructure drawings

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MUNICIPAL BOUNDARY
6970000 N
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6958000 E
6962000 E
6966000 E
6970000 E
APPROVAL
FRANCOIS PETRUCCI
DANY LAFLAMME
DANIEL SEGUIN
PIERRE-ALEXANDRE BOSSÉ
STEPHANE ROBERT
NOTES GÉNÉRAL / GENERAL NOTES
ÉMISSION FINALE
NE PAS UTILISER POUR CONSTRUCTION
FINAL ISSUE
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CONCEPTUAL BUDGETARY EVALUATION
NOT TO BE USED FOR CONSTRUCTION
DATE : 2010-10-07
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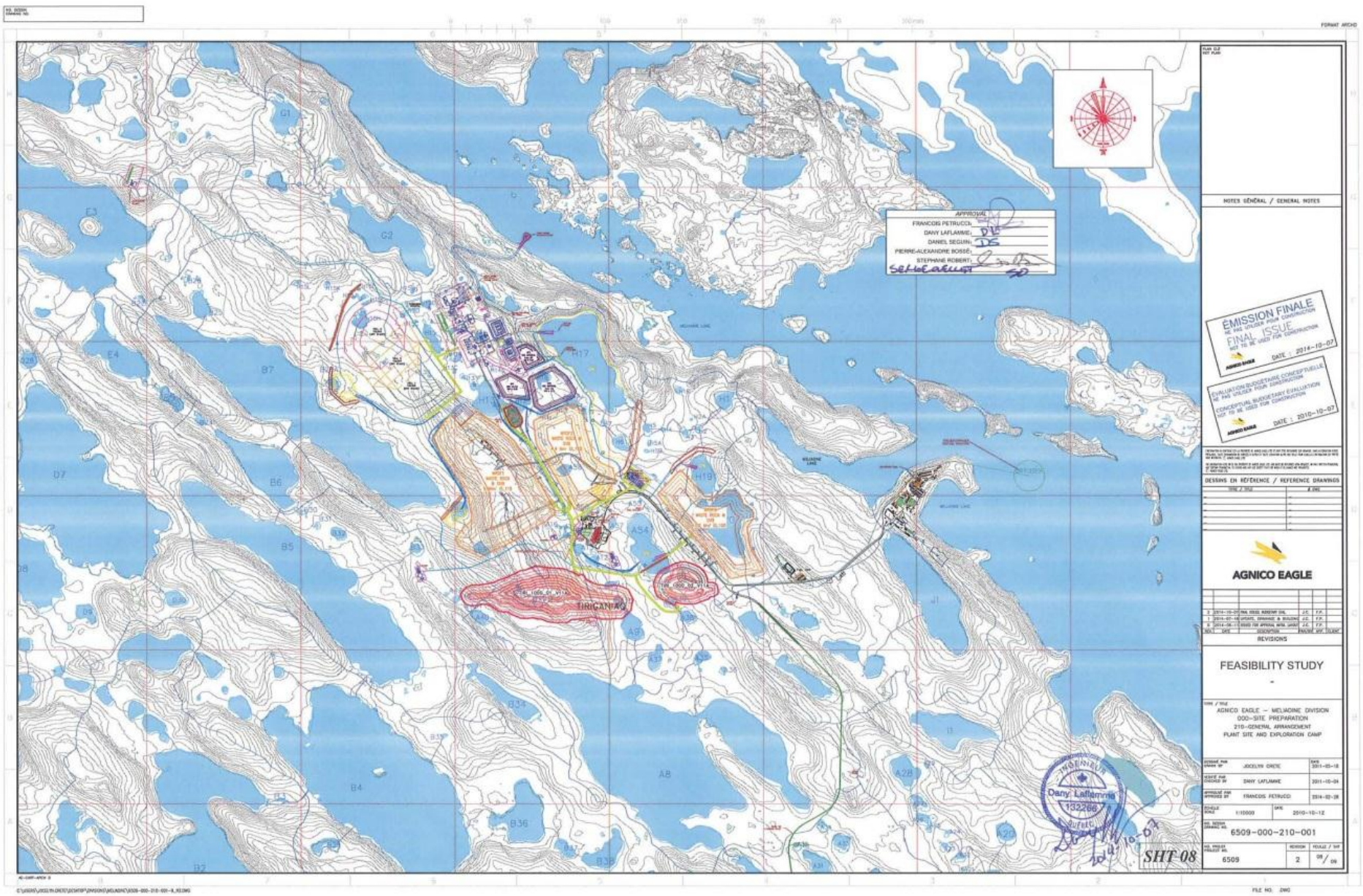
REVISIONS
FEASIBILITY STUDY
AGNICO EAGLE – MELIADINE DIVISION
000-SITE PREPARATION
210-GENERAL ARRANGEMENT
RANKIN INLET VILLAGE VERSUS TANKFARM
TANK FARM LOCALISATION
FIRST PROPOSITION
JOCELYN CRETE
DANY LAFLAMME
FRANCOIS PETRUCCI
1:15000
2012-02-27
6509-000-210-001
6509
2
SHT 06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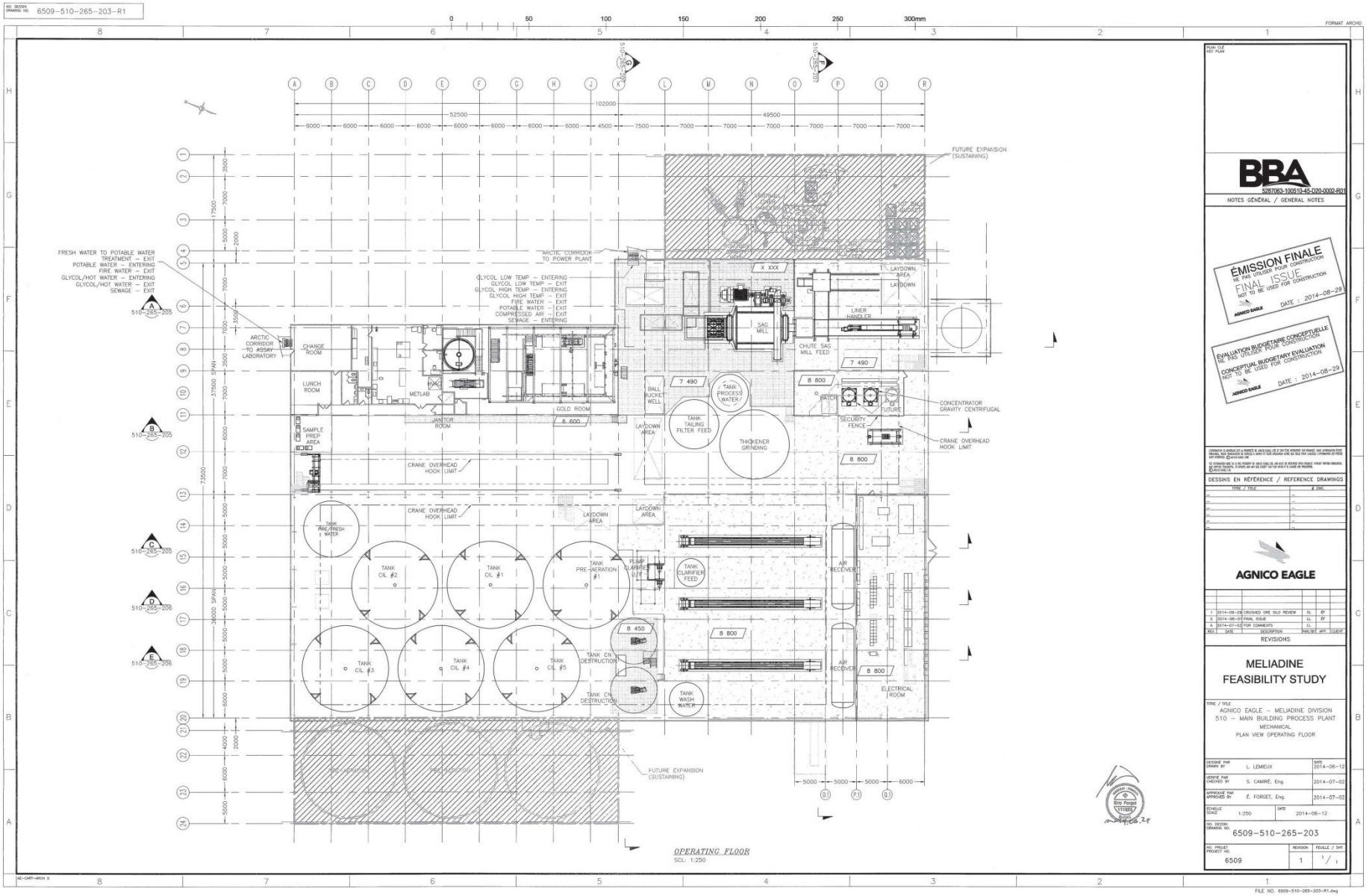
FEASIBILITY STUDY
AGNICO EAGLE – MEL/ADINE DIVISION
000–SITE PREPARATION
210–GENERAL ARRANGEMENT
PLANT SITE AND EXPLORATION CAMP
6509–000–210–001
SHT-08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FRESH WATER TO POTABLE WATER TREATMENT – EXIT
POTABLE WATER – ENTERING
FIRE WATER – EXIT
GLYCOL/HOT WATER – ENTERING
GLYCOL/HOT WATER – EXIT
SEWAGE – EXIT
ARCTIC CORRIDOR TO ASSAY LABORATORY
GLYCOL LOW TEMP – ENTERING
GLYCOL LOW TEMP – EXIT
GLYCOL HIGH TEMP – ENTERING
GLYCOL HIGH TEMP – EXIT
FIRE WATER – EXIT
POTABLE WATER – EXIT
COMPRESSED AIR – EXIT
SEWAGE – ENTERING
CHANGE ROOM
LUNCH ROOM
METLAB
HVAC
JANITOR ROOM
GOLD ROOM
SAMPLE PREP AREA
CRANE OVERHEAD HOOK LIMIT
LAYDOWN AREA
SAG MILL
CHUTE SAG MILL FEED
LINER HANDLER
BALL BLOCK WELL
TANK PROCESS WATER
TANK TAILING FILTER FEED
THICKENER GRINDING
CONCENTRATOR GRAVITY CENTRIFUGAL
SECURITY FENCE
CRANE OVERHEAD HOOK LIMIT
TANK FIRE/FRESH WATER
TANK CIL #2
TANK CIL #1
TANK PRE-AERATION #1
PUMP CLARIFIER U/F
TANK CLARIFIER FEED
AIR RECEIVER
TANK CIL #3
TANK CIL #4
TANK CIL #5
TANK CN DESTRUCTION
TANK WASH WATER
ELECTRICAL ROOM
FUTURE EXPANSION (SUSTAINING)
OPERATING FLOOR
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NOT TO BE USED FOR CONSTRUCTION
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MELIADINE
FEASIBILITY STUDY
AGNICO EAGLE – MELIADINE DIVISION
510 – MAIN BUILDING PROCESS PLANT
MECHANICAL
PLAN VIEW OPERATING FLOOR
DESSINÉ PAR DRAWN BY L. LEMIEUX 2014-06-12
VÉRIFIÉ PAR CHECKED BY S. CAMIRÉ, Eng. 2014-07-02
APPROUVÉ PAR APPROVED BY É. FORGET, Eng. 2014-07-02
ÉCHELLE SCALE 1:250 DATE 2014-06-12
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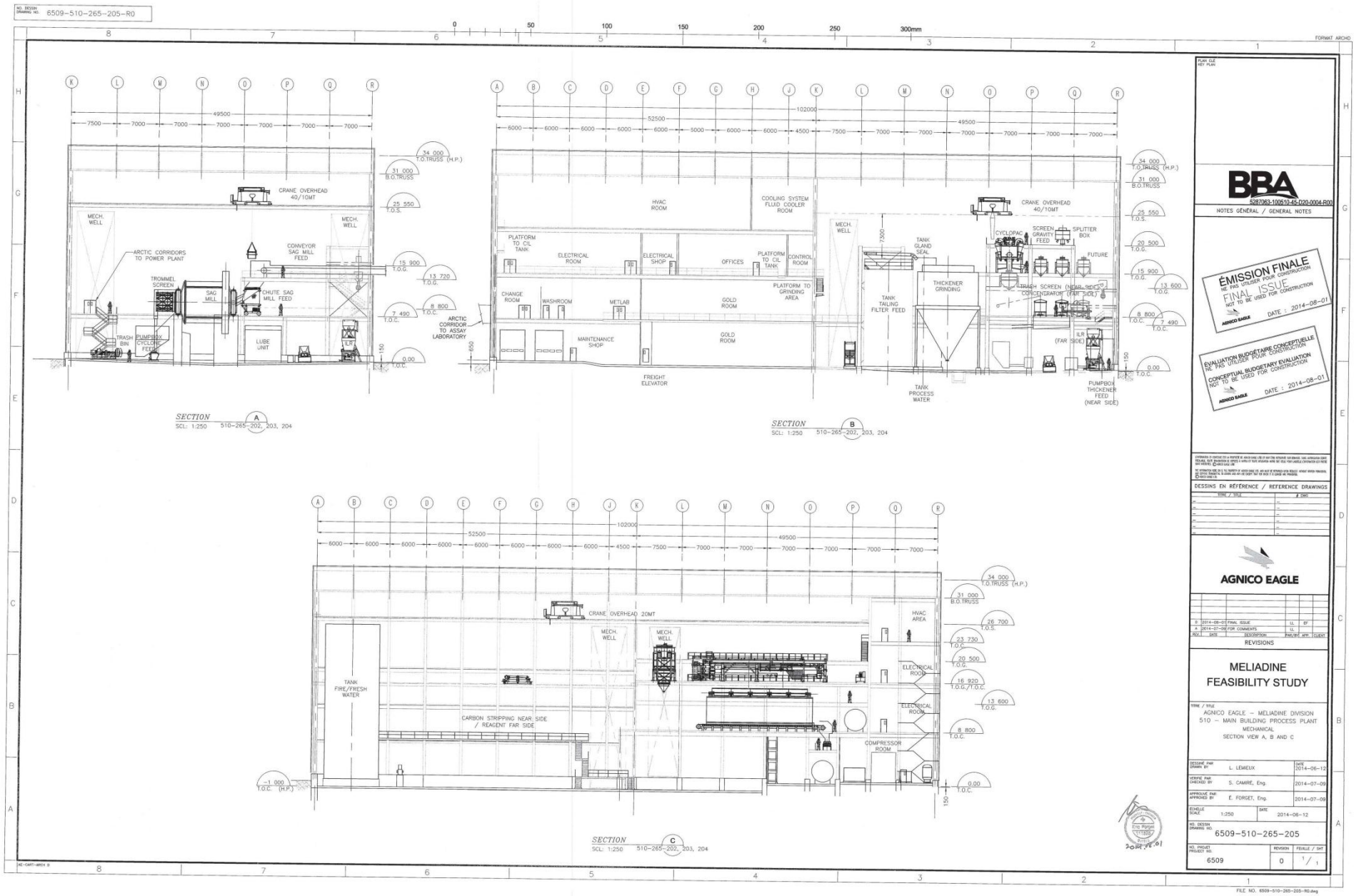
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SECTION C
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CRANE OVERHEAD 40/10MT
CRANE OVERHEAD 20MT
ARCTIC CORRIDORS TO POWER PLANT
ARCTIC CORRIDOR TO ASSAY LABORATORY
TROMMEL SCREEN
SAG MILL
CHUTE SAG MILL FEED
CONVEYOR SAG MILL FEED
TRASH BIN
PUMPBOX CYCLONE FEED
LUBE UNIT
ILR
MECH. WELL
HVAC ROOM
COOLING SYSTEM FLUID COOLER ROOM
PLATFORM TO OIL TANK
ELECTRICAL ROOM
ELECTRICAL SHOP
OFFICES
CONTROL ROOM
CHANGE ROOM
WASHROOM
METLAB
MAINTENANCE SHOP
GOLD ROOM
FREIGHT ELEVATOR
PLATFORM TO GRINDING AREA
TANK GLAND SEAL
TANK TAILING FILTER FEED
THICKENER GRINDING
TANK PROCESS WATER
CYCLOPAC
SCREEN GRAVITY FEED
SPLITTER BOX
FUTURE
TRASH SCREEN (NEAR SIDE)
CONCENTRATOR (FAR SIDE)
PUMPBOX THICKENER FEED (NEAR SIDE)
TANK FIRE/FRESH WATER
CARBON STRIPPING NEAR SIDE / REAGENT FAR SIDE
HVAC AREA
COMPRESSOR ROOM
34 000 T.O.TRUSS (H.P.)
31 000 B.O.TRUSS
25 550 T.O.S.
20 500 T.O.C.
15 900 T.O.G.
13 720 T.O.G.
13 600 T.O.G.
8 800 T.O.C.
7 490 T.O.C.
0.00 T.O.C.
-1 000 T.O.C. (H.P.)
26 700 T.O.S.
23 730 T.O.C.
16 920 T.O.C./T.O.C.
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A 2014-07-09 FOR COMMENTS LL
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MELIADINE
FEASIBILITY STUDY
AGNICO EAGLE – MELIADINE DIVISION
510 – MAIN BUILDING PROCESS PLANT
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L. LEMIEUX 2014-06-12
S. CAMIRÉ, Eng. 2014-07-09
E. FORGET, Eng. 2014-07-09
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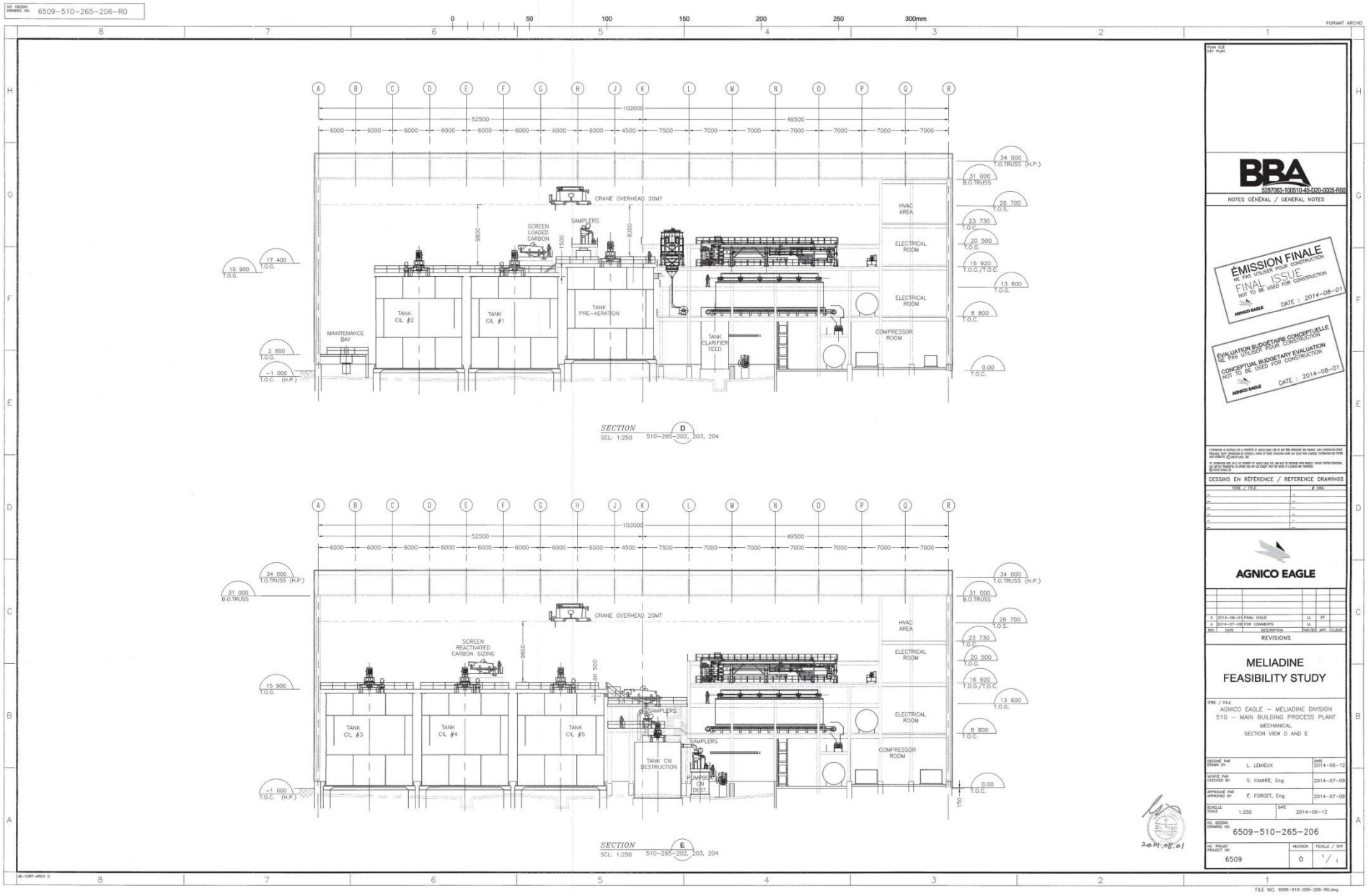
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ELECTRICAL ROOM
COMPRESSOR ROOM
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TANK CIL #1
TANK PRE-AERATION
TANK CLARIFIER FEED
MAINTENANCE BAY
34 000 T.O.TRUSS (H.P.)
31 000 B.O.TRUSS
26 700 T.O.S.
23 730 T.O.C.
20 500 T.O.G.
16 920 T.O.G./T.O.C.
13 600 T.O.G.
8 800 T.O.C.
17 400 T.O.G.
15 900 T.O.G.
2 500 T.O.G.
-1 000 T.O.C. (H.P.)
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TANK CIL #5
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SECTION E
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MELIADINE
FEASIBILITY STUDY
AGNICO EAGLE – MELIADINE DIVISION
510 – MAIN BUILDING PROCESS PLANT
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SECTION VIEW D AND E
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APPROUVÉ PAR APPROVED BY É. FORGET, Eng. 2014-07-09
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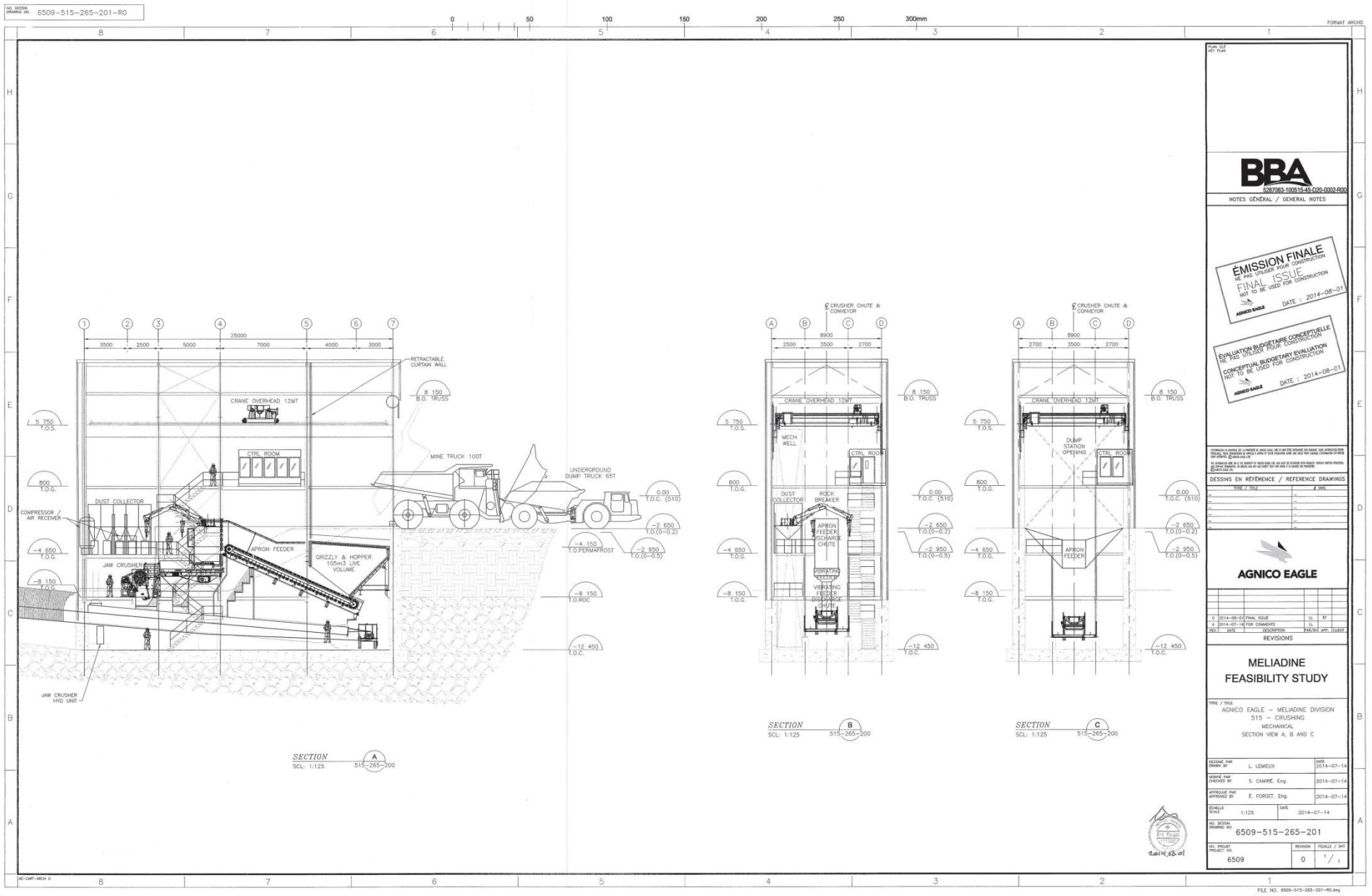
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CRANE OVERHEAD 12MT
CTRL ROOM
MINE TRUCK 100T
UNDERGROUND DUMP TRUCK 65T
DUST COLLECTOR
COMPRESSOR / AIR RECEIVER
APRON FEEDER
GRIZZLY & HOPPER 105m3 LIVE VOLUME
JAW CRUSHER
JAW CRUSHER HYD UNIT
SECTION A SCL: 1:125 515-265-200
℄ CRUSHER CHUTE & CONVEYOR
MECH WELL
ROCK BREAKER
APRON FEEDER DISCHARGE CHUTE
VIBRATING FEEDER
VIBRATING FEEDER DISCHARGE CHUTE
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DUMP STATION OPENING
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FINAL ISSUE
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NE PAS UTILISER POUR CONSTRUCTION
CONCEPTUAL BUDGETARY EVALUATION
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AGNICO EAGLE DATE : 2014-08-01
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REVISIONS
MELIADINE
FEASIBILITY STUDY
TITRE / TITLE
AGNICO EAGLE – MELIADINE DIVISION
515 – CRUSHING
MECHANICAL
SECTION VIEW A, B AND C
DESSINÉ PAR DRAWN BY L. LEMIEUX DATE 2014-07-14
VÉRIFIÉ PAR CHECKED BY S. CAMIRÉ, Eng. 2014-07-14
APPROUVÉ PAR APPROVED BY É. FORGET, Eng. 2014-07-14
ÉCHELLE SCALE 1:125 DATE 2014-07-14
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FEUILLE / SHT 1/1
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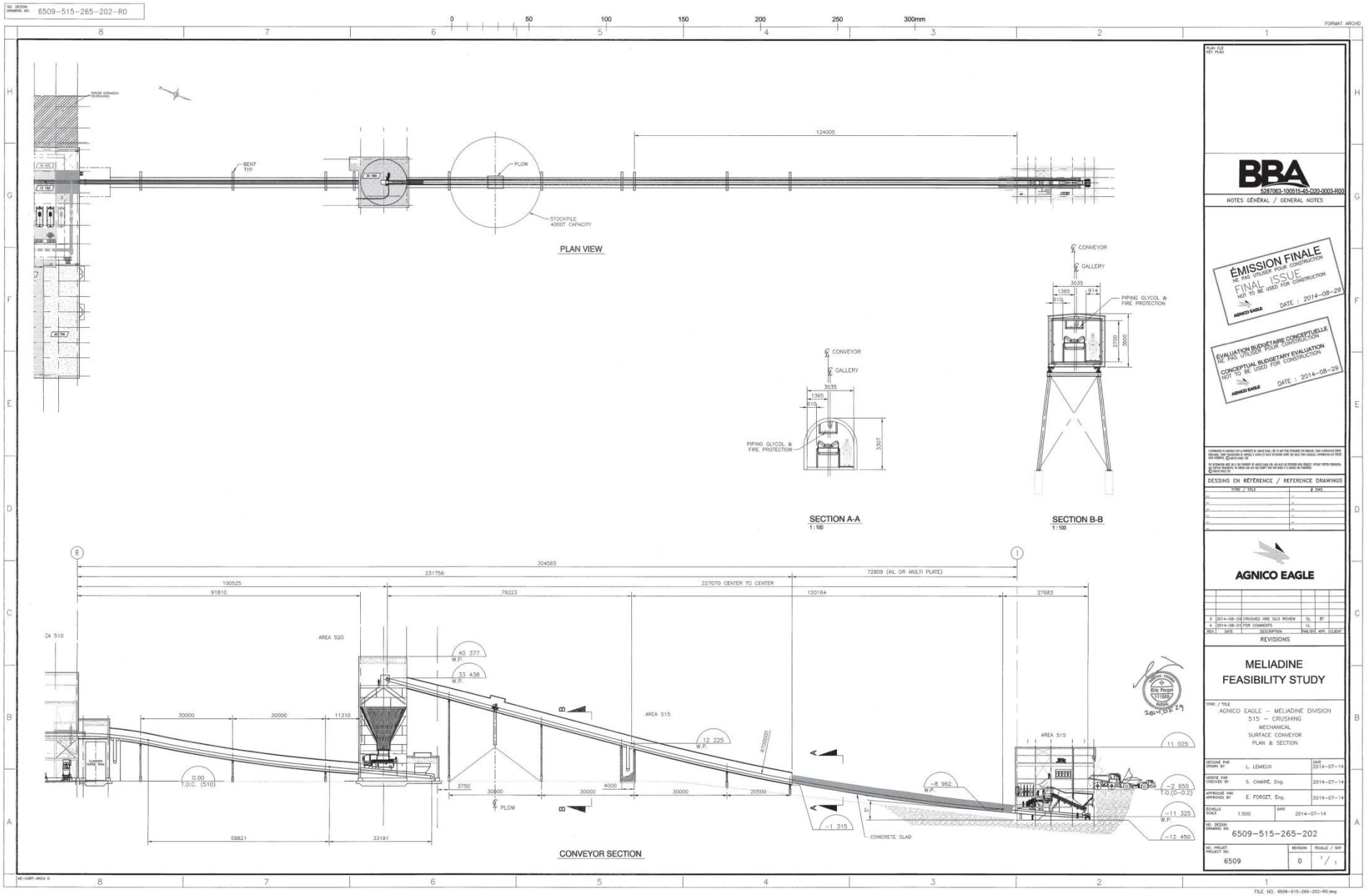
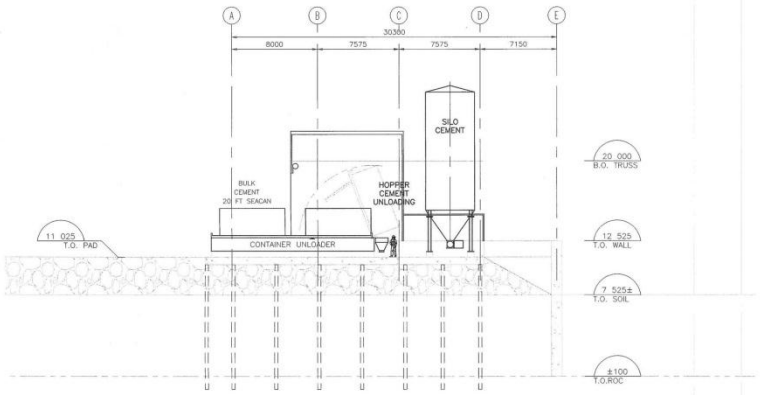
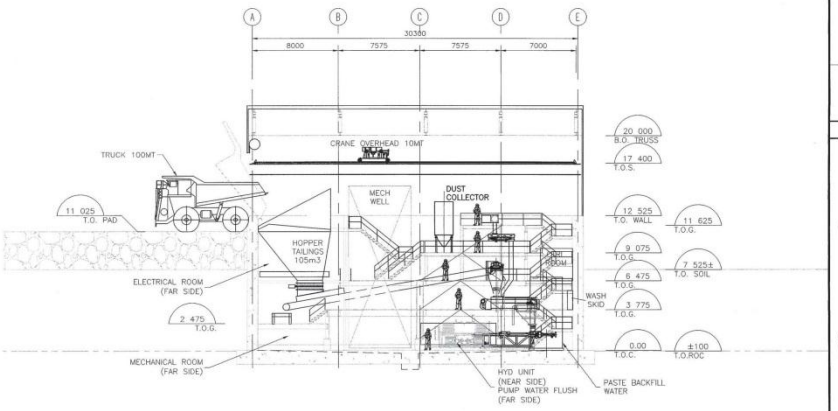

6509-515-265-202-R0
PLAN VIEW
BENT TYP.
PLOW
STOCKPILE 40000T CAPACITY
124005
SECTION A-A
1:100
CONVEYOR
GALLERY
PIPING GLYCOL & FIRE PROTECTION
SECTION B-B
1:100
CONVEYOR SECTION
AREA 520
AREA 515
CONCRETE SLAB
304565
231756
72809 (AIL OR MULTI PLATE)
227070 CENTER TO CENTER
100525
91810
79223
120164
27683
58821
33181
BBA
5287063-100515-45-D20-0003-R00
NOTES GÉNÉRAL / GENERAL NOTES
ÉMISSION FINALE
NE PAS UTILISER POUR CONSTRUCTION
FINAL ISSUE
NOT TO BE USED FOR CONSTRUCTION
DATE : 2014-08-29
ÉVALUATION BUDGÉTAIRE CONCEPTUELLE
NE PAS UTILISER POUR CONSTRUCTION
CONCEPTUAL BUDGETARY EVALUATION
NOT TO BE USED FOR CONSTRUCTION
DATE : 2014-08-29
DESSINS EN RÉFÉRENCE / REFERENCE DRAWINGS
AGNICO EAGLE
REVISIONS
MELIADINE
FEASIBILITY STUDY
AGNICO EAGLE – MELIADINE DIVISION
515 – CRUSHING
MECHANICAL
SURFACE CONVEYOR
PLAN & SECTION
DESSINÉ PAR / DRAWN BY L. LEMIEUX 2014-07-14
VERIFIÉ PAR / CHECKED BY S. CAMIRÉ, Eng. 2014-07-14
APPROUVÉ PAR / APPROVED BY É. FORGET, Eng. 2014-07-14
ÉCHELLE / SCALE 1:500
DATE 2014-07-14
NO. DESSIN / DRAWING NO. 6509-515-265-202
NO. PROJET / PROJECT NO. 6509
RÉVISION 0
FEUILLE / SHT 1/1

NO. DESSIN / DRAWING NO. 6509-575-265-201-R0

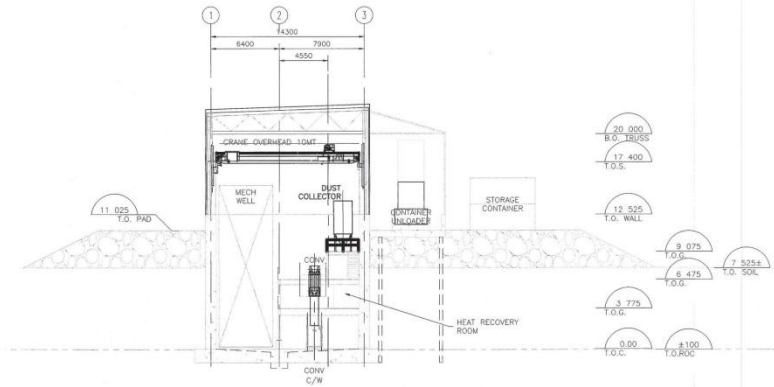
FORMAT ARCH D



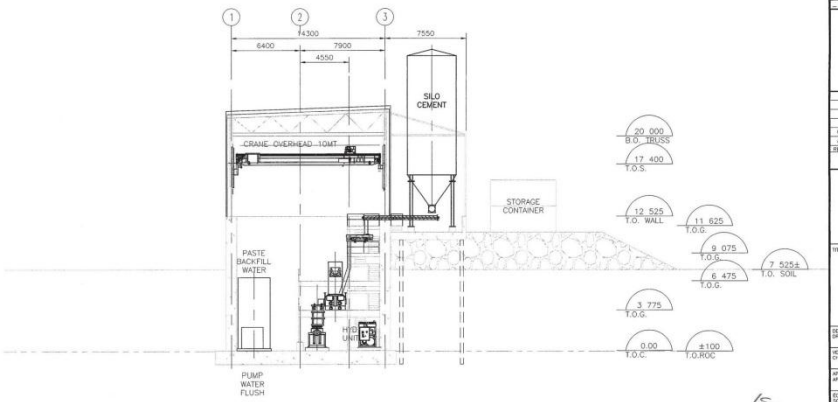
SECTION A
SCL: 1:200 575-265-200



SECTION B
SCL: 1:200 575-265-200



SECTION C
SCL: 1:200 575-265-200



SECTION D
SCL: 1:200 575-265-200

PLAN CLÉ
KEY PLAN

BBA

5287063-100575-45-D20-0002-R00

NOTES GÉNÉRAL / GENERAL NOTES

ÉMISSION FINALE
NE PAS UTILISER POUR CONSTRUCTION
FINAL ISSUE
NOT TO BE USED FOR CONSTRUCTION
AGNICO EAGLE DATE : 2014-08-01

ÉVALUATION BUDGÉTAIRE CONCEPTUELLE
NE PAS UTILISER POUR CONSTRUCTION
CONCEPTUAL BUDGETARY EVALUATION
NOT TO BE USED FOR CONSTRUCTION
AGNICO EAGLE DATE : 2014-08-01

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DESSINS EN RÉFÉRENCE / REFERENCE DRAWINGS

TITRE / TITLE	# DWG

AGNICO EAGLE

REV.	DATE	DESCRIPTION	DESS./DRT.	APP.	CLIENT
0	2014-08-01	FINAL ISSUE	LL	EF	
A	2014-07-21	FOR COMMENTS	LL		

REVISIONS

MELIADINE FEASIBILITY STUDY

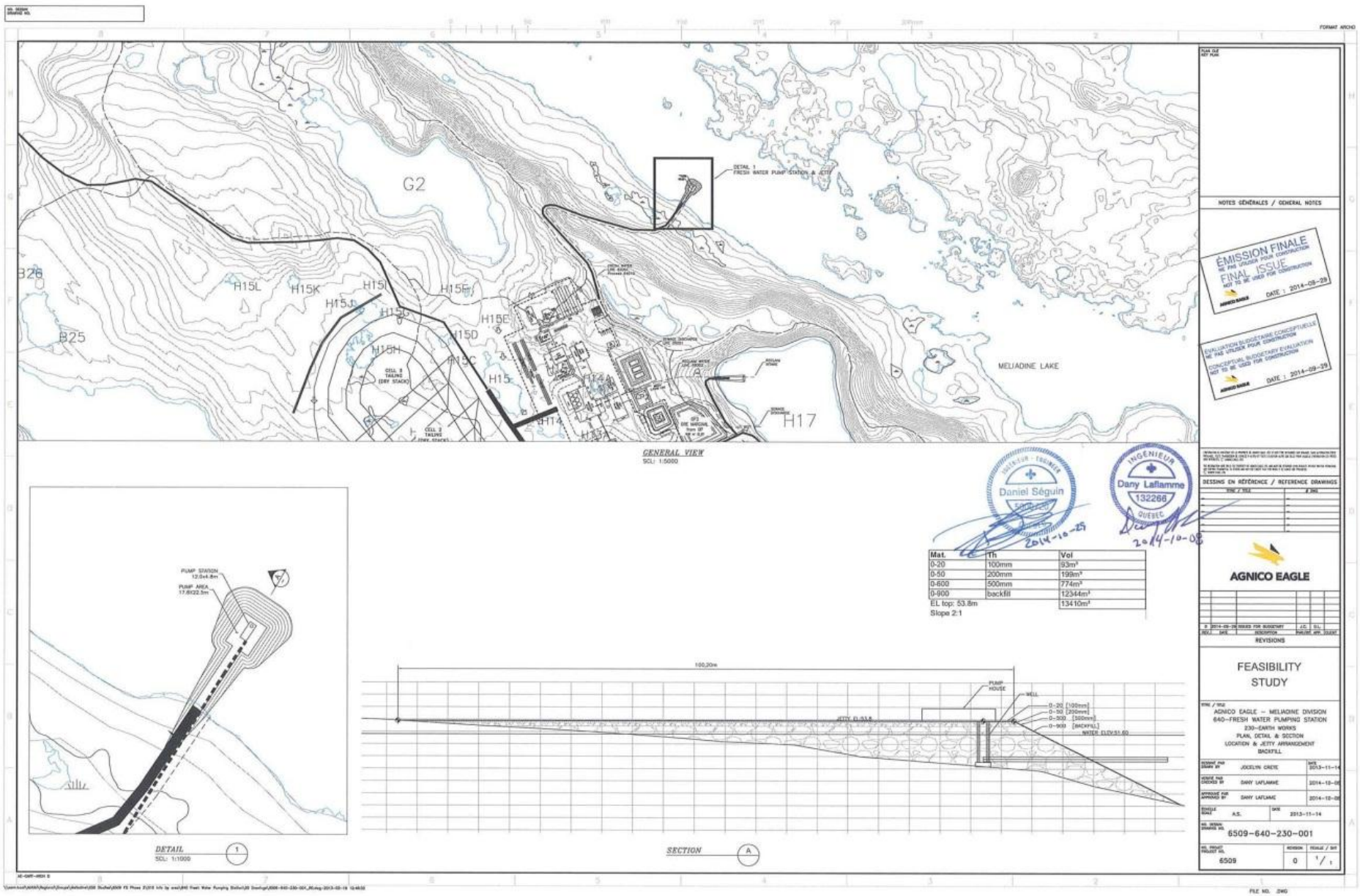
TITRE / TITLE
AGNICO EAGLE – MELIADINE DIVISION
575 – PASTE PLANT
MECHANICAL
SECTION VIEW A, B AND C

DESSINÉ PAR / DRAWN BY	L. LEMIEUX	DATE 2014-07-21
VÉRIFIÉ PAR / CHECKED BY	S. CAMIRÉ, Eng.	2014-07-21
APPROUVÉ PAR / APPROVED BY	É. FORGET, Eng.	2014-07-21
ÉCHELLE / SCALE	1:200	DATE 2014-07-21

NO. DESSIN / DRAWING NO. 6509-575-265-201

NO. PROJET / PROJECT NO.	REVISION	FEUILLE / SHT
6509	0	1 / 1

FILE NO. 6509-575-265-201-R0.dwg



Mat.	Th	Vol
0-20	100mm	93m³
0-50	200mm	199m³
0-600	500mm	774m³
0-900	backfill	12344m³
EL top: 53.8m		13410m³
Slope 2:1		